

March 13, 2025

Final Stormwater Management & Drainage Report

Client

Intrinsic Development 3622 Endeavor Ave, Ste. 101 Columbia, MO 65201

Project

Alura Apartments at Discovery Park SW Corner of NE Douglas St and Lee's Summit Rd Lee's Summit, MO

P.N. 24KC10030

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Project Description and General Information

The proposed project is a 22 acre apartment development located southwest of the intersection of NE Douglas Street and Lee's Summit Road in Lee's Summit, Missouri. Alura Apartments is the second phase of the Village at Discovery Park project located on the northwest corner of NW Colbern Road and NE Douglas Street.

The purpose of this report is to analyze the stormwater impacts of the proposed residential development and show that the post-development conditions meet the regulations established by the City of Lee's Summit. This phase of the development is located on the northwest corner of Douglas Street and Colbern Road in Lee's Summit, Missouri. The full site is bounded by undeveloped ground to the north, Douglas Street to the east, Phase 1 of Discovery Park with mixed use to the south, and an existing detention basin to the west. This phase is the northern most portion encompassing approximately 22 acres of the overall site. The existing site is undeveloped, consisting mostly of grass and farmland.

The existing soil characteristics as published in the Soil Survey for Jackson County, Missouri are summarized in the table below. Additional information on the existing soil is provided in the Web Soil Survey located in the Appendix.

Map Unit Symbol	Map Unit Name	Slopes	Hydrologic Soil Group
10120	Sharpsburg Silty Loam	2 to 5%	С
30080	Greenton Silty Clay Loam	5 to 9%	C/D
40107	Snead-Rock Outcrop Complex	5 to 14%	D
40108	Snead-Rock Outcrop Complex	14 to 30%	D

Table 1: Soil Classifications

According to FEMA flood maps (FIRM Panel 29095C0409G), the site is located in zone X, an area of minimal flood hazard. No amendments or revisions to the map are being proposed.

Methodology

The Alura site was analyzed in both the pre-development and post-development conditions. The analysis was conducted utilizing HydroCAD which uses an SCS Type-II 24 hr. rainfall distribution data in computing unit hydrographs for varying conditions. Precipitation depths used in the analysis have been interpolated from the "Technical Paper No. 40 Rainfall Frequency Atlas of the United States" (TP-40).

Table 2: Rainfall Precipitation



Annual Exceedance Probability (AEP)	Rainfall Depth (inches)
90% (Water Quality Event)	1.37
50% (2 year)	3.50
10% (10 year)	5.34
1% (100 year)	7.71

The post-development rates were determined utilizing the APWA 5600 Comprehensive Protection Strategy in accordance with the City of Lee's Summit regulations. Under this strategy, peak runoff control is provided for the 1%, 10%, and 50% chance storms and volumetric and/or extended detention control (\geq 40 hr.) of the 90% mean annual event storm. The maximum allowable release rates for the design storm events are established for the 2-year (0.50 cfs/acre), 10-year (2.0 cfs/acre), 100-year (3.0 cfs/acre).

Existing Conditions Analysis

The site generally drains to the north and west. The west watershed drains to the existing storm sewer network constructed with the first phase of Discovery Park, and ultimately into the regional detention basin. The north watershed drains into the stream located north of the site that ultimately drains to Unity Lake Number Two located northwest of the project site. Refer to the Pre-Development Plan in the Appendix. A summary of the existing conditions design parameters is in the table below.

Subarea	Total Area (ac)	NRCS Weighted CN	Time of Concentration (min)
North	11.62	80	7.7
West	10.87	81	10.2

Table 3: Existing Conditions Parameters

The portion draining to the west has been included in the previous drainage study titled "Discovery Park Macro Stormwater Report" prepared by Olsson dated October 24, 2023 and the drainage study titled "Stormwater Management and Drainage Report" prepared by OWN, Inc. dated July 9, 2024. The previous studies determined the allowable release rates and calculated the required detention for The Village at Discovery Park, Alura (Previously called Aria) Apartments, and a portion of Discovery Crossing. A portion of Alura Apartments will drain into the existing basin constructed as part of the Village at Discovery Park. The existing peak runoff rates were calculated for the design storms and summarized below.



Table 4: Existing Peak Flow Summary

Watershed	Peak Flow 2-yr Event (cfs)	Peak Flow 10-yr Event (cfs)	Peak Flow 100-yr Event (cfs)
North	31.49	60.58	99.32
West	27.92	53.19	86.71

Proposed Conditions Analysis

The proposed development for this phase consists of 12 apartment buildings and associated surface parking. The proposed site has 2 watersheds; north and west. Refer to the Post-Development Plan in the Appendix. The allowable release rates were determined using the Comprehensive Control Strategy as defined in APWA 5608.4. A summary of the allowable release rates is provided in the table below:

Table 5: Allowable Release Rates

Design Storm	Allowable Release Rate (cfs/acre)	North (11.29 ac.) (cfs)	West (11.21 ac.) (cfs)
50% (2 year)	0.5	5.65	N/A
10% (10 year)	2.0	22.58	N/A
1% (100 year)	3.0	33.87	N/A

*Note: The west watershed is not included in the allowable release rate calculations as detention has been previously provided.

A summary of the proposed design parameters is in the table below.

Table 6: Proposed Conditions Parameters

Subarea	Total Area (ac)	NRCS Weighted CN	Time of Concentration (min)
North	11.29	87	6
West	11.21	87	6

To mitigate the impact of the proposed increase in impervious area associated with the development and to satisfy the requirement for detention, an above ground detention basin is proposed to capture stormwater and release at rates at or below the allowable release rates as established above. The proposed basin will receive stormwater from enclosed pipe systems that collect water from the streets and parking lots.

Outlet control structures with multiple stage release controls are proposed to provide controlled release over the design storms. Specific detail of each outlet control structure is provided in the associated watershed review below.



West Watershed

The proposed improvements in the west watershed are consistent with the previously approved drainage studies. Below is a comparison summary of the previously assumed parameters for the sizing of the regional detention basin and the proposed improvements.

Table 7: Existing Basin	Design	Comparison	Summary
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	Previous Studies	Proposed
Total Area (ac.)	11.29	11.21
NRCS CN	92	87

The proposed condition onsite area shows a reduction in the area originally proposed and reduced CN value and therefore no additional detention is required.

North Watershed

The north watershed is approximately 11.29 acres located generally on the eastern side of the project site. The calculated CN for this area is 87, which is consistent with dense residential development.

An above ground extended dry detention basin is proposed to provide the volume needed to meet the allowable release rate for this development. The basin will have a 5'x5' outlet control structure to control the release rates for the 2-yr, 10-yr, and 100-yr design storms and to provide a controlled release of the water quality storm. A 2.25-inch diameter orifice is proposed to drain the water quality storm over the required 40 hour period. The associated water quality volume and sizing calculations are provided in the Appendix. A 48-inch by 8-inch rectangular opening and 60-inch by 60-inch open top will provide the controlled release of the 2-yr, 10-yr, and 100-yr design storms. The peak release rates are summarized in the table below:

Table 8: North Watershee	Release Rate Summary
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Storm Event	Allowable Release Rate (cfs)	Proposed Peak Release Rates (cfs)
2 year	5.65	3.56
10 year	22.58	20.02
100 year	33.87	31.82

The peak flows were also compared to the existing flows and summarized in the table below. The proposed west and south watershed peak flows were combined to compare to the existing west watershed.



Proposed Existing Proposed Existing Proposed Existing **Peak Flow** Peak Flow **Peak Flow Peak Flow Peak Flow Peak Flow** Watershed 2-yr Event 10-yr 10-yr 100-yr 100-yr 2-yr Event Event **Event** (cfs) Event Event (cfs) (cfs) (cfs) (cfs) (cfs) North 31.49 3.56 20.02 31.82 60.58 99.32 27.92 41.38 71.64 110.44 West 53.19 86.71

Table 9: Peak Flow Comparison

The west watershed shows an increase in the peak flow rates as a result of the development. This increase has already been mitigated with the detention basin previously provided in the first phase of the project.

Summary and Recommendations

The existing site is undeveloped, consisting mostly of grass and farmland. The proposed development for this phase consists of 12 apartment buildings and associated surface parking. To mitigate the increase in runoff release rates due to the increase in impervious area, an enclosed pipe network in conjunction with above ground detention basins with an outlet control structure was designed. As stated previously, approximately 11 acres of the west watershed was included in the design of the first phase of Discovery Park and the proposed changes in this phase still meet the assumed parameters set for its design. Peak runoff control is provided for the 1%, 10%, and 50% chance storms and volumetric and/or extended detention control (≥40 hr.) of the 90% mean annual event storm. Post-development site conditions and detention basins were modeled and analyzed using HydroCAD. Detailed calculations are presented in the Appendix to support the presented release rate summaries, detention volumes, and maximum water surface elevations.





Pre-Development Plan





Post-Development Plan





Soil Report





United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Jackson County, Missouri

Alura Apartments



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND)	MAP INFORMATION	
Area of In	Area of Interest (AOI)		Spoil Area	The soil surveys that comprise your AOI were mapped at	
	Area of Interest (AOI)	٥	Stony Spot	1:24,000.	
Soils	Coll Mars Link Dalaman	۵	Very Stony Spot	Warning: Soil Map may not be valid at this scale.	
		\$2	Wet Spot		
\sim	Soil Map Unit Lines	Δ	Other	Enlargement of maps beyond the scale of mapping can cause	
	Soil Map Unit Points		Special Line Features	line placement. The maps do not show the small areas of	
Special	Special Point Features		atures	contrasting soils that could have been shown at a more detailed scale.	
	Borrow Pit	\sim	Streams and Canals		
	Clay Spot	Transport	tation	Please rely on the bar scale on each map sheet for map	
衆	Classed Depression	+++	Rails	measurements.	
<u></u>	Closed Depression	~	Interstate Highways	Source of Map: Natural Resources Conservation Service	
÷	Gravel Plt	~	US Routes	Web Soil Survey URL:	
000	Gravelly Spot	~	Major Roads	Coordinate System. Web Mercator (EPSG.3657)	
ø	Landfill	\sim	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator	
Λ.	Lava Flow	Backgrou	nd Aerial Photography	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the	
علله	Marsh or swamp	No.		Albers equal-area conic projection, should be used if more	
Ŕ	Mine or Quarry			accurate calculations of distance or area are required.	
0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as	
0	Perennial Water			of the version date(s) listed below.	
\sim	Rock Outcrop			Soil Survey Area: Jackson County, Missouri	
+	Saline Spot			Survey Area Data: Version 25, Aug 22, 2023	
000	Sandy Spot			Soil map units are labeled (as space allows) for map scales	
-	Severely Eroded Spot			1:50,000 or larger.	
0	Sinkhole			Date(s) aerial images were photographed: Aug 30, 2022—Sep	
à	Slide or Slip			8, 2022	
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.	

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI			
10120	Sharpsburg silt loam, 2 to 5 percent slopes	2.0	7.3%			
30080	Greenton silty clay loam, 5 to 9 percent slopes	18.5	66.7%			
40107	Snead-Rock outcrop complex, warm, 5 to 14 percent slopes	3.1	11.0%			
40108	Snead-Rock outcrop complex, warm, 14 to 30 percent slopes	4.2	15.1%			
Totals for Area of Interest	•	27.7	100.0%			

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Jackson County, Missouri

10120—Sharpsburg silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2yy7v Elevation: 1,000 to 1,300 feet Mean annual precipitation: 33 to 41 inches Mean annual air temperature: 50 to 55 degrees F Frost-free period: 177 to 220 days Farmland classification: All areas are prime farmland

Map Unit Composition

Sharpsburg and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Sharpsburg

Setting

Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam A - 6 to 16 inches: silty clay loam Bt1 - 16 to 22 inches: silty clay loam Bt2 - 22 to 46 inches: silty clay loam BC - 46 to 58 inches: silty clay loam C - 58 to 79 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 45 to 50 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 7.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: C Ecological site: R109XY002MO - Loess Upland Prairie Hydric soil rating: No

Minor Components

Sibley

Percent of map unit: 5 percent Landform: Hillslopes Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Ecological site: R109XY002MO - Loess Upland Prairie Hydric soil rating: No

Higginsville, eroded

Percent of map unit: 5 percent Landform: Hillslopes Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope Down-slope shape: Concave Across-slope shape: Concave Ecological site: R109XY002MO - Loess Upland Prairie Hydric soil rating: No

30080—Greenton silty clay loam, 5 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2xjd9 Elevation: 640 to 1,120 feet Mean annual precipitation: 35 to 41 inches Mean annual air temperature: 50 to 57 degrees F Frost-free period: 177 to 209 days Farmland classification: Not prime farmland

Map Unit Composition

Greenton and similar soils: 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Greenton

Setting

Landform: Hillslopes Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Parent material: Loess over residuum weathered from limestone and shale

Typical profile

Ap - 0 to 12 inches: silty clay loam *Bt - 12 to 28 inches:* silty clay

2Bt - 28 to 30 inches: silty clay 2C - 30 to 79 inches: silty clay

Properties and qualities

Slope: 5 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 12 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 10 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 9.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C/D Ecological site: R109XY002MO - Loess Upland Prairie Hydric soil rating: No

Minor Components

Sampsel

Percent of map unit: 10 percent Landform: Hillslopes Landform position (two-dimensional): Footslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Ecological site: R109XY002MO - Loess Upland Prairie Hydric soil rating: Yes

40107—Snead-Rock outcrop complex, warm, 5 to 14 percent slopes

Map Unit Setting

National map unit symbol: 2zccr Elevation: 660 to 1,130 feet Mean annual precipitation: 39 to 43 inches Mean annual air temperature: 54 to 57 degrees F Frost-free period: 185 to 220 days Farmland classification: Not prime farmland

Map Unit Composition

Snead, warm, and similar soils: 70 percent Rock outcrop: 20 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Snead, Warm

Setting

Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Residuum weathered from limestone and shale

Typical profile

A - 0 to 10 inches: silty clay loam Bw - 10 to 20 inches: silty clay BC - 20 to 24 inches: silty clay C - 24 to 35 inches: silty clay Cr - 35 to 45 inches: bedrock

Properties and qualities

Slope: 5 to 14 percent
Depth to restrictive feature: 20 to 40 inches to paralithic bedrock
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 24 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 10 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: D Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna Hydric soil rating: No

Description of Rock Outcrop

Typical profile

R - 0 to 79 inches: bedrock

Properties and qualities

Slope: 5 to 14 percent Depth to restrictive feature: 0 inches to lithic bedrock Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: No

Minor Components

Oska

Percent of map unit: 4 percent Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Linear Ecological site: R106XY015KS - Loamy Upland (PE 30-37) Hydric soil rating: No

Sampsel

Percent of map unit: 3 percent Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Concave Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna Hydric soil rating: Yes

Kennebec, occasionally flooded

Percent of map unit: 3 percent Landform: Drainageways Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Ecological site: R109XY028MO - Loamy Upland Drainageway Savanna Hydric soil rating: No

40108—Snead-Rock outcrop complex, warm, 14 to 30 percent slopes

Map Unit Setting

National map unit symbol: 2zccp Elevation: 670 to 1,130 feet Mean annual precipitation: 39 to 43 inches Mean annual air temperature: 54 to 57 degrees F Frost-free period: 185 to 220 days Farmland classification: Not prime farmland

Map Unit Composition

Snead, warm, and similar soils: 65 percent Rock outcrop: 20 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Snead, Warm

Setting

Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Residuum weathered from limestone and shale

Typical profile

A - 0 to 10 inches: silty clay loam Bw - 10 to 20 inches: silty clay BC - 20 to 24 inches: silty clay C - 24 to 35 inches: silty clay Cr - 35 to 45 inches: bedrock

Properties and qualities

Slope: 14 to 30 percent
Depth to restrictive feature: 20 to 40 inches to paralithic bedrock
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 24 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 10 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: D Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna Hydric soil rating: No

Description of Rock Outcrop

Typical profile

R - 0 to 79 inches: bedrock

Properties and qualities

Slope: 14 to 30 percent Depth to restrictive feature: 0 inches to lithic bedrock Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: No

Minor Components

Norris

Percent of map unit: 5 percent

Landform: Hillslopes Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope Down-slope shape: Concave, convex Across-slope shape: Convex Ecological site: F109XY025MO - Interbedded Sedimentary Exposed Backslope Woodland Hydric soil rating: No

Sampsel

Percent of map unit: 5 percent Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Concave Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna Hydric soil rating: Yes

Oska

Percent of map unit: 3 percent Landform: Hillslopes Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Linear Ecological site: R106XY015KS - Loamy Upland (PE 30-37) Hydric soil rating: No

Kennebec, occasionally flooded

Percent of map unit: 2 percent Landform: Drainageways Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Ecological site: R109XY028MO - Loamy Upland Drainageway Savanna Hydric soil rating: No

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.




Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
10120	Sharpsburg silt loam, 2 to 5 percent slopes	С	2.0	7.3%
30080	Greenton silty clay loam, 5 to 9 percent slopes	C/D	18.5	66.7%
40107	Snead-Rock outcrop complex, warm, 5 to 14 percent slopes	D	3.1	11.0%
40108	Snead-Rock outcrop complex, warm, 14 to 30 percent slopes	D	4.2	15.1%
Totals for Area of Inter	est	27.7	100.0%	

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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FEMA Floodplain Map



Engineering beyond.^m

National Flood Hazard Layer FIRMette



Legend



Basemap Imagery Source: USGS National Map 2023

HydroCAD Report



Engineering beyond.^m



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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type II 24-hr		Default	24.00	1	3.50	2
2	10-Year	Type II 24-hr		Default	24.00	1	5.34	2
3	100-Year	Type II 24-hr		Default	24.00	1	7.71	2

Discovery Park Alura Existing	Discovery Park Alura Apartments Type II 24-hr 2-Year Rainfall=3.50"
Prepared by OWN Inc	Printed 1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 HydroCAD Software Solution	ns LLC Page 3
Time span=0.00-48.00 hrs, dt=0.05 hr	rs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment A1: North Existing	Runoff Area=11.620 ac 0.00% Impervious Runoff Depth=1.64" Tc=7.7 min CN=80 Runoff=31.49 cfs 1.585 af
Subcatchment A2: West Existing	Runoff Area=10.870 ac 0.00% Impervious Runoff Depth=1.71" Tc=10.2 min CN=81 Runoff=27.92 cfs 1.548 af

Total Runoff Area = 22.490 acRunoff Volume = 3.132 af
100.00% Pervious = 22.490 acAverage Runoff Depth = 1.67"
0.00% Impervious = 0.000 ac

Summary for Subcatchment A1: North Existing

Runoff = 31.49 cfs @ 11.99 hrs, Volume= 1.585 af, Depth= 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 2-Year Rainfall=3.50"



Summary for Subcatchment A2: West Existing

Runoff = 27.92 cfs @ 12.02 hrs, Volume= 1.548 af, Depth= 1.71"

0

2 4

6

8 10 12 14 16 18 20

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 2-Year Rainfall=3.50"

	Area	(ac)	CN	Desc	cription				
*	4.	880	80						
*	5.	990	81						
	10.	870	81	Wei	ghted Aver	rage			
	10.	870		100.	00% Pervi	ous Area			
	Тс	Leng	th	Slope	Velocity	Capacity	Description		
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)			
	10.2						Direct Entry,		
					Su	bcatchme	ent A2: West Existing		
						Hydro	ograph		
	1								Due off
	30-			2	7.92 cfs				
	28						Type II	24-hr	
	26- 24-						2-Year Rainfall=	:3.50"	
	22						Runoff Area=10.8	70 ac	
	20]					Runoff Volume=1.	548 af	
	(sj)						Runoff Depth=	:1 71"	
	° 16- ≥							0	
	음 14 1						IC=10.	2 min	
	12-							SN=81	
	10-								

Time (hours)

22 24 26 28 30 32 34 36 38 40 42 44 46 48

Discovery Park Alura Existing	Discove Type II 24-hr	ry Park Alura A <i>10-Year Rair</i>	Apartments afall=5.34"
Prepared by OWN Inc		Printed	1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 HydroCAD Software Solution	s LLC		Page 6
Time span=0.00-48.00 brs. dt=0.05 brs	s 961 points		

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment A1: North Existing	Runoff Area=11.620 ac 0.00% Impervious Runoff Depth=3.19" Tc=7.7 min CN=80 Runoff=60.58 cfs 3.090 af
Subcatchment A2: West Existing	Runoff Area=10.870 ac 0.00% Impervious Runoff Depth=3.29" Tc=10.2 min CN=81 Runoff=53.19 cfs 2.978 af

Total Runoff Area = 22.490 acRunoff Volume = 6.068 afAverage Runoff Depth = 3.24"100.00% Pervious = 22.490 ac0.00% Impervious = 0.000 ac

Summary for Subcatchment A1: North Existing

Runoff = 60.58 cfs @ 11.99 hrs, Volume= 3.090 af, Depth= 3.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=5.34"



Summary for Subcatchment A2: West Existing

Runoff = 53.19 cfs @ 12.02 hrs, Volume= 2.978 af, Depth= 3.29"

Ó

2 4

6

8 10 12 14 16 18 20

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=5.34"

	Area (a	ac) CN	Descriptio	n					
*	4.8	80 80)						
*	5.9	90 81							
	10.8	70 81	Weighted	Average					
	10.8	70	100.00%	Pervious Area					
	Тс	Length	Slope Velo	ocity Capacity	Description				
	(min)	(feet)	(ft/ft) (ft/s	sec) (cfs)	1				
	10.2				Direct Entry,				
				• • • •					
				Subcatchm	ent A2: West Ex	isting			
				Hydro	ograph				
	1								Runoff
	55		53.19 cfs						
	50-						l ype II	24-hr	l
	45				10-Ye	ar Ra	ainfall=	=5.34"	1
	40				Runof	f Are	a=10.8	870 ac	1
	40								1
	35 ∃				Runom	voiu	me=z.:	978 ar	1
	(cts)				Rui	noff [Depth=	=3.29"	1
	Flow						Гс=10.	2 min	1
	25-							N=81	1
	20-								l
	- /								

Time (hours)

22 24 26 28 30 32 34 36 38 40 42 44 46 48

	Discov	ery Park Alura A	Apartments
Discovery Park Alura Existing	Type II 24-hr	100-Year Rair	n fall=7.71"
Prepared by OWN Inc		Printed	1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 HydroCAD Software Solutic	ons LLC		Page 9

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment A1: North Existing	Runoff Area=11.620 ac 0.00% Impervious Runoff Depth=5.35" Tc=7.7 min CN=80 Runoff=99.32 cfs 5.184 af
Subcatchment A2: West Existing	Runoff Area=10.870 ac 0.00% Impervious Runoff Depth=5.47" Tc=10.2 min CN=81 Runoff=86.71 cfs 4.954 af

Total Runoff Area = 22.490 acRunoff Volume = 10.138 af
100.00% Pervious = 22.490 acAverage Runoff Depth = 5.41"
0.00% Impervious = 0.000 ac

Summary for Subcatchment A1: North Existing

Runoff = 99.32 cfs @ 11.99 hrs, Volume= 5.184 af, Depth= 5.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=7.71"



Summary for Subcatchment A2: West Existing

Runoff = 86.71 cfs @ 12.01 hrs, Volume= 4.954 af, Depth= 5.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=7.71"

	Area (ac)	CN	Description						
*	4.880	80							
*	5.990	81							
	10.870	81	Weighted Ave	rage					
	10.870		100.00% Perv	ious Area					
	Tc Leng (min) (fe	gth et)	Slope Velocity (ft/ft) (ft/sec)	Capacity (cfs)	Description				
	10.2				Direct Entry,				
Subcatchment A2: West Existing									
	95								
	90- 85-		86.71 cfs		Type II 24-hr				
	80				100-Year Rainfall=7.71"				
	70				Runoff Area=10.870 ac				





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Rainfall Events Listing (selected events)

I	Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
		Name				(hours)		(inches)	
	1	2-Year	Type II 24-hr		Default	24.00	1	3.50	2
	2	10-Year	Type II 24-hr		Default	24.00	1	5.34	2
	3	100-Year	Type II 24-hr		Default	24.00	1	7.71	2

	Discovery Park Alura Apartments
Discovery Park Alura Proposed	Type II 24-hr 2-Year Rainfall=3.50"
Prepared by OWN Inc	Printed 1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 Hydro	oCAD Software Solutions LLC Page 3
	-
Time span=0.00	0-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR	R-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Tr	rans method - Pond routing by Stor-Ind method
Subcatchment A1: Onsite	Runoff Area=10.300 ac 0.00% Impervious Runoff Depth=2.18"
	Tc=6.0 min CN=87 Runoff=38.02 cfs 1.873 af
Subcatchment A1 BYP: Undetained	Runoff Area=0.990 ac 0.00% Impervious Runoff Depth=1.64"
	Tc=6.0 min CN=80 Runoff=2.79 cfs 0.135 af
Subcatchment A2: West Proposed	Runoff Area=11.210 ac 0.00% Impervious Runoff Depth=2.18"
	Tc=6.0 min CN=87 Runoff=41.38 cfs 2.039 af
Pond P1: Detention Basin	Peak Elev=926.22' Storage=44,815 cf Inflow=38.02 cfs 1.873 af
	Outflow=3.29 cfs 1.528 af
Link PT1: Point #1	above 5.000.00 cfs Inflow=3.56 cfs 1.663 af
	Primary=0.00 cfs 0.000 af Secondary=3.56 cfs 1.663 af

Total Runoff Area = 22.500 acRunoff Volume = 4.047 afAverage Runoff Depth = 2.16"100.00% Pervious = 22.500 ac0.00% Impervious = 0.000 ac

Summary for Subcatchment A1: Onsite

Runoff = 38.02 cfs @ 11.97 hrs, Volume= Routed to Pond P1 : Detention Basin 1.873 af, Depth= 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 2-Year Rainfall=3.50"



Summary for Subcatchment A1 BYP: Undetained

Runoff = 2.79 cfs @ 11.97 hrs, Volume= 0.135 af, Depth= 1.64" Routed to Link PT1 : Point #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 2-Year Rainfall=3.50"



Summary for Subcatchment A2: West Proposed

Runoff = 41.38 cfs @ 11.97 hrs, Volume= 2.039 af, Depth= 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 2-Year Rainfall=3.50"



Summary for Pond P1: Detention Basin

Inflow Are	ea =	10.300 ac,	0.00% Impervious,	Inflow Depth = 2.7	18" for 2-Year event
Inflow	=	38.02 cfs @	11.97 hrs, Volume	= 1.873 af	
Outflow	=	3.29 cfs @	12.50 hrs, Volume	= 1.528 af,	Atten= 91%, Lag= 32.1 min
Primary	=	3.29 cfs @	12.50 hrs, Volume	= 1.528 af	-
Route	d to Lir	nk PT1 : Point #	1		

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 926.22' @ 12.50 hrs Surf.Area= 12,335 sf Storage= 44,815 cf

Plug-Flow detention time= 661.1 min calculated for 1.526 af (81% of inflow) Center-of-Mass det. time= 584.1 min (1,396.2 - 812.1)

Volume	Inve	rt Avail.Sto	rage Storage [Description					
#1	919.00	D' 176,84	45 cf Custom	5 cf Custom Stage Data (Conic) Listed below (Recalc)					
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	Wet.Area				
	20	(34-11)			(30-11)				
919.0	00	1,307	0	0	1,307				
920.0	00	2,240	1,753	1,753	2,252				
921.0	00	3,138	2,676	4,429	3,168				
922.0	00	5,147	4,101	8,530	5,190				
923.0	00	6,695	5,904	14,434	6,762				
924.0	00	8,340	7,502	21,937	8,435				
925.0	00	10,081	9,197	31,134	10,209				
926.0	00	11,918	10,987	42,120	12,083				
927.0	00	13,851	12,872	54,993	14,057				
928.0	00	15,880	14,854	69,847	16,132				
929.0	00	18,005	16,931	86,778	18,306				
930.0	00	20,218	19,101	105,879	20,573				
931.0	00	22,485	21,341	127,220	22,898				
932.0	00	24,806	23,636	150,856	25,282				
933.0	00	27,189	25,988	176,845	27,733				
Device	Routing	Invert	Outlet Devices	5					
#1	Primary	919 00'	24.0" Round	Culvert					
	1 milery	010.00	I = 200.0' RC	P sa cut end proje	ecting Ke= 0.500				
			Inlet / Outlet In	vert= 919 00' / 91	0.00' S = 0.0450 '/'	$C_{C} = 0.900$			
			n=0.013 Con	crete nine bends /	& connections Flov	w Area= 3 14 sf			
#2	Device 1	919 00'	2 2" Vert Orifi	ice/Grate C=06	00 Limited to weir	flow at low heads			
#2 #3	Device 1	925.85	48 0" W x 8 0"	H Vert Orifice/G	rate $C = 0.600$	now at low neuros			
<i>#</i> 0	Device I	020.00	Limited to weir	flow at low heads	ute 0= 0.000				
#4	Device 1	930 10'	60.0" x 60.0" H	Horiz. Orifice/Grat	e C = 0.600				
	2011001	000.10	Limited to weir	flow at low heads					

Primary OutFlow Max=3.25 cfs @ 12.50 hrs HW=926.22' (Free Discharge) 1=Culvert (Passes 3.25 cfs of 37.73 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.34 cfs @ 12.86 fps) 3=Orifice/Grate (Orifice Controls 2.91 cfs @ 1.96 fps) 4=Orifice/Grate (Controls 0.00 cfs)



Pond P1: Detention Basin

Prepared by OWN Inc HydroCAD® 10.20-5c s/n 09171 © 2023 HydroCAD Software Solutions LLC

Stage-Area-Storage for Pond P1: Detention Basin

$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Elevation	Surface	Storage	Elevation	Surface	Storage
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	919.00	1,307	0	929.20	18,437	90,422
919.40 1,650 590 929.60 19,317 97,973 919.60 2,033 1,326 930.00 20,218 105,879 920.00 2,240 1,753 930.20 20,662 109,967 920.20 2,408 2,217 930.20 20,662 109,967 920.20 2,408 2,217 930.60 21,564 118,411 920.40 2,581 2,716 930.80 22,202 122,770 920.80 2,946 3,821 931.00 22,485 127,720 921.20 3,500 5,093 931.40 23,400 136,6397 921.40 3,882 5,831 931.60 23,864 141,123 921.60 4,706 7,545 932.00 24,806 150,856 922.20 5,147 8,530 932.20 25,746 160,966 922.40 5,742 10,707 932.60 26,723 166,163 922.80 6,655 11,866 932.80 26,704 171,456 923.80 7,997 20,303	919.20	1,474	278	929.40	18,875	94,153
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	919.40	1,650	590	929.60	19,317	97,973
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	919.60	1,837	939	929.80	19,765	101,881
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	919.80	2,033	1,326	930.00	20,218	105,879
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	920.00	2,240	1,753	930.20	20,662	109,967
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	920.20	2,408	2,217	930.40	21,110	114,144
920.80 2,046 3,821 931.80 22,485 127,220 921.00 3,138 4,429 931.20 22,485 127,220 921.40 3,600 5,093 931.40 23,400 136,397 921.40 3,882 5,831 931.60 23,864 141,123 921.60 4,284 6,647 931.80 24,306 150,864 922.00 5,147 8,530 932.20 25,274 155,864 922.00 5,147 8,530 932.20 25,274 166,163 922.80 6,051 11,886 932.80 26,704 171,456 922.80 6,369 13,128 933.00 27,189 176,845 923.80 7,997 20,303 93.00 27,189 176,845 924.00 8,340 21,937 93.300 27,189 176,845 925.40 10,797 35,309 925.60 11,165 37,505 924.40 9,017 25,407 92,407 38,51 93.165 925.40 10,797 35,309 925.60 11,165 37,505 925.60 11,165 37,505 926,60 13,613 54,993 927.20	920.40	2,581	2,710	930.60	21,304	110,411
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	920.00	2,701	3,200	930.00	22,022	122,770
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	920.00	2,940	3,021	931.00 031.20	22,405	127,220
321.20 3.300 3.003 3.1.00 23,864 141,123 921.60 4.284 6.647 931.80 24,333 145,943 921.80 4.706 7,545 932.00 24,806 150,856 922.00 5,147 8,530 932.20 25,274 155,864 922.20 5,440 9,589 932.40 25,746 160,966 922.40 5,742 10,707 932.60 26,704 171,456 922.80 6,369 13,128 933.00 27,189 176,845 923.00 6,695 14,434 933.00 27,189 176,845 923.60 7,660 18,738 933.00 27,189 176,845 923.60 7,660 13,738 933.00 27,189 176,845 924.00 8,340 21,937 924.60 9,365 27,245 924.40 9,017 25,607 10,686 33,185 925.20 10,436 33,185 925.20 10,436 33,185 925.40 10,797 35,309 925.80	921.00	3,130	5,003	031.20	22,940	136 307
221.10 3.021 3.021 3.031 24.333 145.943 921.80 4.706 7.545 932.00 24.806 150.856 922.00 5.147 8.530 932.20 25.274 155.864 922.20 5.440 9.589 932.40 25.746 160.966 922.40 5.742 10.707 932.60 26.223 166.163 922.60 6.051 11.886 932.80 26.704 171.456 923.00 6.695 14.434 933.00 27.189 176.845 923.20 7.010 15.805 933.40 27.189 176.845 923.40 7.331 17.239 923.60 7.660 18.738 923.80 7.997 20.303 22.400 8.340 21.937 924.40 9.017 25.407 92.400 8.340 21.937 924.40 9.017 25.407 92.500 10.081 31.134 925.00 10.081 31.134 925.20 10.436 33.185 925.40 10.797 35.309 925.60 11.918 42.120 926.20 12.293 44.541 926.80 13.453 52.262 927.00 13.851 54.993 927.20 14.246 57.802 927.40 14.646 60.691 927.40 14.646 60.691 927.80 15.463 66.712 928.80 17.569 83.221 928.80 17.569 83.221 <	921.20	3,882	5,035	931.40	23,400	141 123
921.80 4.706 7.545 932.00 24.806 150.856 922.00 5.147 8.530 932.20 25.274 155.864 922.20 5.440 9.589 932.40 25.746 160.966 922.40 5.742 10.707 932.60 26.223 166.163 922.80 6.051 11.886 932.80 26.704 171.456 923.00 6.695 14.434 933.00 27.189 176.845 923.40 7.331 17.239 933.00 27.189 176.845 923.40 7.331 17.239 923.60 7.660 18.738 923.80 7.997 20.303 924.00 8.340 21.937 924.20 8.675 23.638 924.40 9.017 25.407 924.60 9.365 27.245 92.500 10.081 31.134 925.00 10.081 31.134 925.20 10.436 33.185 924.40 9.017 25.407 92.500 11.918 42.120 925.60 11.918 42.120 92.600 11.918 42.120 926.20 12.293 44.541 92.620 12.674 47.038 927.40 14.646 67.802 92.740 14.646 67.802 927.40 14.646 67.802 92.740 14.646 67.802 927.40 15.463 66.712 92.800 15.880 69.847 928.40 16.714 76.365	921.40	4 284	6 647	931.80	24,333	145 943
922.005,1478,530 932.20 $25,274$ $155,864$ 922.20 5,4409,589 932.40 $25,746$ $160,966$ 922.40 5,74210,707 932.60 $26,223$ $166,163$ 922.80 6,36913,128 933.00 $27,189$ $176,845$ 923.00 6,69514,434 933.00 $27,189$ $176,845$ 923.20 7,60018,738 933.00 $27,189$ $176,845$ 923.40 7,33117,239 924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.20 10,436 $33,185$ 925.40 $10,797$ $35,309$ 925.60 11,165 $37,505$ 925.80 $11,538$ $39,775$ 926.00 12,293 $44,541$ 926.60 $13,060$ $49,611$ 926.60 13,060 $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.40 $16,714$ $76,365$ 928.60 $17,569$ $83,221$ 929.00 $18,005$ $86,778$ 929.00 $18,005$ $86,778$ $86,778$	921.80	4 706	7 545	932.00	24 806	150 856
922.20 $5,440$ $9,589$ 932.40 $25,746$ $160,966$ 922.40 $5,742$ $10,707$ 932.60 $26,223$ $166,163$ 922.60 $6,051$ $11,886$ 932.80 $26,704$ $171,456$ 923.00 $6,695$ $14,434$ 933.00 $27,189$ $176,845$ 923.00 $6,695$ $14,434$ 933.00 $27,189$ $176,845$ 923.40 $7,331$ $17,239$ 932.60 $27,189$ $176,845$ 923.60 $7,660$ $18,738$ 923.80 $7,997$ $20,303$ 924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 928.00 $15,880$ $69,847$ 928.00 $15,880$ $69,847$ 928.00 $15,880$ $69,847$ 928.00 $15,880$ $69,778$ 928.00 $15,800$ $83,221$ 929.00 $18,005$ $86,778$	922.00	5,147	8,530	932.20	25.274	155,864
922.40 $5,742$ $10,707$ 932.60 $26,223$ $166,163$ 922.60 $6,051$ $11,886$ 932.80 $26,704$ $171,456$ 922.80 $6,695$ $14,434$ 933.00 $27,189$ $176,845$ 923.00 $6,695$ $14,434$ 933.00 $27,189$ $176,845$ 923.40 $7,331$ $17,239$ 923.60 $7,660$ $18,738$ 923.80 $7,997$ $20,303$ 924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.20 $10,081$ $31,134$ 925.20 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 926.60 $11,153$ $39,775$ 926.00 $11,918$ $42,120$ 926.60 $13,660$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.00 $15,880$ $69,847$ 928.00 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	922.20	5,440	9,589	932.40	25,746	160,966
922.60 6,051 11,886 932.80 26,704 171,456 922.80 6,369 13,128 933.00 27,189 176,845 923.00 6,695 14,434 933.00 27,189 176,845 923.40 7,331 17,239 923.60 7,660 18,738 923.80 7,997 20,303 924.40 9,017 25,407 924.40 9,017 25,407 924.60 9,365 27,245 925.00 10,436 33,185 925.40 10,797 35,309 925.60 11,165 37,505 925.40 10,797 35,309 925.20 10,436 33,185 926.60 13,060 49,611 926.60 13,060 49,611 926.80 13,453 52,262 927.00 13,851 54,993 927.20 14,246 57,802 927.20 14,246 57,802 927.40 14,646 60,691 927.80 15,463 66,712 928.00 15,880 69,847 928.40 16,714 76,365	922.40	5,742	10,707	932.60	26,223	166,163
922.80 6,369 13,128 933.00 27,189 176,845 923.00 6,695 14,434 933.00 27,189 176,845 923.20 7,010 15,805 923.40 7,331 17,239 923.60 7,660 18,738 923.80 7,997 20,303 924.00 8,340 21,937 924.20 8,675 23,638 924.40 9,017 25,407 924.60 9,365 27,245 924.80 9,720 29,154 925.00 10,436 33,185 925.20 10,436 33,185 925.60 11,165 37,505 925.80 11,538 39,775 926.00 11,918 42,120 926.20 12,293 44,541 926.60 13,060 49,611 926.80 13,453 52,262 927.00 13,851 54,993 927.20 14,246 57,802 927.40 14,646 60,691 927.80 15,463 66,712 928.00 15,880 69,847 928.40 16,714 76,6365	922.60	6,051	11,886	932.80	26,704	171,456
923.00 $6,695$ $14,434$ 923.207,010 $15,805$ 923.407,331 $17,239$ 923.607,660 $18,738$ 923.807,997 $20,303$ 924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	922.80	6,369	13,128	933.00	27,189	176,845
923.207,01015,805923.407,33117,239923.607,66018,738923.807,99720,303924.00 $8,340$ 21,937924.20 $8,675$ 23,638924.409,01725,407924.609,36527,245924.809,72029,154925.0010,08131,134925.2010,43633,185925.4010,79735,309925.6011,6537,505925.8011,53839,775926.0012,29344,541926.4012,67447,038926.6013,06049,611926.8013,45352,262927.0013,85154,993927.2014,24657,802927.4014,64660,691927.6015,05263,661927.8015,46366,712928.0015,88069,847928.2016,29473,064928.4016,71476,365928.6017,13979,750928.8017,56983,221929.0018,00586,778	923.00	6,695	14,434			
923.407,33117,239 923.60 7,66018,738 923.80 7,99720,303 924.00 8,34021,937 924.20 8,67523,638 924.40 9,01725,407 924.60 9,36527,245 924.80 9,72029,154 925.00 10,08131,134 925.20 10,43633,185 925.40 10,79735,309 925.60 11,16537,505 926.00 11,91842,120 926.20 12,67447,038 926.60 13,06049,611 926.80 13,45352,262 927.00 13,85154,993 927.20 14,24657,802 927.40 14,64660,691 927.80 15,46366,712 928.00 15,88069,847 928.40 16,71476,365 928.60 17,13979,750 928.80 17,56983,221 929.00 18,00586,778	923.20	7,010	15,805			
923.607,66018,738 923.80 7,99720,303 924.00 8,34021,937 924.20 8,67523,638 924.40 9,01725,407 924.60 9,36527,245 924.80 9,72029,154 925.00 10,08131,134 925.20 10,43633,185 925.40 10,79735,309 925.60 11,16537,505 926.00 11,91842,120 926.20 12,29344,541 926.40 12,67447,038 926.60 13,06049,611 926.80 13,45352,262 927.00 13,85154,993 927.20 14,24657,802 927.40 14,64660,691 927.80 15,46366,712 928.00 15,88069,847 928.40 16,71476,365 928.60 17,13979,750 928.80 17,56983,221 929.00 18,00586,778	923.40	7,331	17,239			
923.807,99720,303 924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $12,674$ $47,038$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	923.60	7,660	18,738			
924.00 $8,340$ $21,937$ 924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	923.80	7,997	20,303			
924.20 $8,675$ $23,638$ 924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $12,293$ $44,541$ 926.20 $12,293$ $44,541$ 926.60 $13,060$ $49,611$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.40 $16,714$ $76,365$ 928.60 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	924.00	8,340	21,937			
924.40 $9,017$ $25,407$ 924.60 $9,365$ $27,245$ 924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	924.20	8,675	23,638			
924.80 $9,720$ $29,154$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	924.40	9,017	25,407			
924.80 $9,720$ $29,134$ 925.00 $10,081$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	924.60	9,305	27,243			
925.00 $10,031$ $31,134$ 925.20 $10,436$ $33,185$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	924.00	9,720	29,104			
925.20 $10,430$ $35,103$ 925.40 $10,797$ $35,309$ 925.60 $11,165$ $37,505$ 925.80 $11,538$ $39,775$ 926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	925.00	10,001	33 185			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	925.20	10,430	35 309			
925.8011,538 $39,775$ 926.0011,918 $42,120$ 926.2012,293 $44,541$ 926.4012,674 $47,038$ 926.6013,060 $49,611$ 926.8013,453 $52,262$ 927.0013,851 $54,993$ 927.2014,246 $57,802$ 927.6015,052 $63,661$ 927.8015,463 $66,712$ 928.0015,880 $69,847$ 928.2016,294 $73,064$ 928.4016,714 $76,365$ 928.6017,139 $79,750$ 928.8017,569 $83,221$ 929.0018,005 $86,778$	925.60	11 165	37 505			
926.00 $11,918$ $42,120$ 926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	925.80	11,538	39,775			
926.20 $12,293$ $44,541$ 926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	926.00	11,918	42,120			
926.40 $12,674$ $47,038$ 926.60 $13,060$ $49,611$ 926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	926.20	12,293	44,541			
926.6013,06049,611926.8013,45352,262927.0013,85154,993927.2014,24657,802927.4014,64660,691927.6015,05263,661927.8015,46366,712928.0015,88069,847928.2016,29473,064928.4016,71476,365928.6017,13979,750928.8017,56983,221929.0018,00586,778	926.40	12,674	47,038			
926.80 $13,453$ $52,262$ 927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	926.60	13,060	49,611			
927.00 $13,851$ $54,993$ 927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	926.80	13,453	52,262			
927.20 $14,246$ $57,802$ 927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	927.00	13,851	54,993			
927.40 $14,646$ $60,691$ 927.60 $15,052$ $63,661$ 927.80 $15,463$ $66,712$ 928.00 $15,880$ $69,847$ 928.20 $16,294$ $73,064$ 928.40 $16,714$ $76,365$ 928.60 $17,139$ $79,750$ 928.80 $17,569$ $83,221$ 929.00 $18,005$ $86,778$	927.20	14,246	57,802			
927.60 15,052 63,661 927.80 15,463 66,712 928.00 15,880 69,847 928.20 16,294 73,064 928.40 16,714 76,365 928.60 17,139 79,750 928.80 17,569 83,221 929.00 18,005 86,778	927.40	14,646	60,691			
927.80 15,463 66,712 928.00 15,880 69,847 928.20 16,294 73,064 928.40 16,714 76,365 928.60 17,139 79,750 928.80 17,569 83,221 929.00 18,005 86,778	927.60	15,052	63,661			
928.00 15,880 69,847 928.20 16,294 73,064 928.40 16,714 76,365 928.60 17,139 79,750 928.80 17,569 83,221 929.00 18,005 86,778	927.80	15,463	66,/12			
928.20 16,294 73,064 928.40 16,714 76,365 928.60 17,139 79,750 928.80 17,569 83,221 929.00 18,005 86,778	928.00	15,880	69,847			
928.60 17,139 79,750 928.80 17,569 83,221 929.00 18,005 86,778	920.20	10,294	73,064			
928.80 17,569 83,221 929.00 18,005 86,778	920.40 028 60	10,/14	10,305			
929.00 18,005 86,778	920.00 028 80	17 560	13,100			
	929.00	18 005	86 778			
	020.00	10,000	00,770			

Summary for Link PT1: Point #1

Inflow Area =	11.290 ac,	0.00% Impervious, Inflow	/ Depth > 1.77"	for 2-Year event
Inflow =	3.56 cfs @	12.48 hrs, Volume=	1.663 af	
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 100%, Lag= 0.0 min
Secondary =	3.56 cfs @	12.48 hrs, Volume=	1.663 af	-

Primary outflow = Inflow above 5,000.00 cfs, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs



Link PT1: Point #1

		Discovery Park Alura Apartments
Discovery Park Alura Proposed		Type II 24-hr 10-Year Rainfall=5.34"
Prepared by OWN Inc		Printed 1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 Hyd	roCAD Software Solutions	LLC Page 11
Time span=0.0	0-48.00 hrs, dt=0.05 hrs,	961 points
Runoff by SCS T	R-20 method, UH=SCS,	Weighted-CN
Reach routing by Stor-Ind+T	rans method - Pond rou	iting by Stor-Ind method
Subactobrant A4: Onaita	Dupoff Area-10 200 oc	0.00% Imponious Bunoff Dopth-2.90"
Subcalchment AT: Onsite		min $CN=87$ Pupoff=65.83 efc. 3.338 af
	10-0.0	
Subcatchment A1 BYP: Undetained	Runoff Area=0.990 ac	0.00% Impervious Runoff Depth=3.19"
	Tc=6.	0 min CN=80 Runoff=5.37 cfs 0.263 af
Subcatchment A2: West Proposed	Runoff Area=11.210 ac	0.00% Impervious Runoff Depth=3.89"
	Tc=6.0	min CN=87 Runoff=71.64 cfs 3.633 af
Pond P1: Detention Basin	Peak Elev=927.97 Stor	age=69,329 cf Inflow=65.83 cfs 3.338 af
		Outflow=17.50 cfs 2.986 af
l ink PT1. Point #1	abov	e 5 000 00 cfs Inflow=20 02 cfs 3 250 af
	Primary=0.00 cfs	0.000 af Secondary=20.02 cfs 3.250 af
	1 mildiy=0.00 013	
Tatal Dumoff Amage - 00 500	$\mathbf{D}_{\mathbf{r}} = \mathbf{D}_{\mathbf{r}} + \mathbf{c} \mathbf{f} \mathbf{f} \mathbf{h} \mathbf{r} + \mathbf{c} \mathbf{h} \mathbf{r} \mathbf{h} \mathbf{r} \mathbf{h} \mathbf{r} \mathbf{h} \mathbf{h} \mathbf{h} \mathbf{h} \mathbf{h} \mathbf{h} \mathbf{h} h$	004 of Assessed Dura off Double - 0.001

Total Runoff Area = 22.500 acRunoff Volume = 7.234 afAverage Runoff Depth = 3.86"100.00% Pervious = 22.500 ac0.00% Impervious = 0.000 ac

Summary for Subcatchment A1: Onsite

Runoff = 65.83 cfs @ 11.97 hrs, Volume= Routed to Pond P1 : Detention Basin 3.338 af, Depth= 3.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=5.34"



Summary for Subcatchment A1 BYP: Undetained

Runoff = 5.37 cfs @ 11.97 hrs, Volume= 0.263 af, Depth= 3.19" Routed to Link PT1 : Point #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=5.34"



Summary for Subcatchment A2: West Proposed

Runoff = 71.64 cfs @ 11.97 hrs, Volume= 3.633 af, Depth= 3.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=5.34"



Summary for Pond P1: Detention Basin

Inflow Are	a =	10.300 ac,	0.00% Impervious,	Inflow Depth =	3.89" fo	r 10-Year event
Inflow	=	65.83 cfs @	11.97 hrs, Volume	= 3.338	af	
Outflow	=	17.50 cfs @	12.12 hrs, Volume	= 2.986 a	af, Atten=	73%, Lag= 9.2 min
Primary	=	17.50 cfs @	12.12 hrs, Volume	= 2.986 a	af	
Routed	l to Link	PT1 : Point #	1			

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 927.97' @ 12.12 hrs Surf.Area= 15,812 sf Storage= 69,329 cf

Plug-Flow detention time= 370.3 min calculated for 2.983 af (89% of inflow) Center-of-Mass det. time= 318.7 min (1,114.4 - 795.7)

Volume	Inve	rt Avail.Sto	rage Storage	Description		
#1	919.00	0' 176,84	45 cf Custom	n Stage Data (Conic	c) Listed below (Re	calc)
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	Wet.Area	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)	
919.0	00	1,307	0	0	1,307	
920.0	00	2,240	1,753	1,753	2,252	
921.0	00	3,138	2,676	4,429	3,168	
922.0	00	5,147	4,101	8,530	5,190	
923.0	00	6,695	5,904	14,434	6,762	
924.0	00	8,340	7,502	21,937	8,435	
925.0	00	10,081	9,197	31,134	10,209	
926.0	00	11,918	10,987	42,120	12,083	
927.0	00	13,851	12,872	54,993	14,057	
928.0	00	15,880	14,854	69,847	16,132	
929.0	00	18,005	16,931	86,778	18,306	
930.0	00	20,218	19,101	105,879	20,573	
931.0	00	22,485	21,341	127,220	22,898	
932.0	00	24,806	23,636	150,856	25,282	
933.0	00	27,189	25,988	176,845	27,733	
Device	Routing	Invert	Outlet Device	es		
#1	Primary	919.00'	24.0" Round	l Culvert		
	-		L= 200.0' R	CP, sq.cut end proje	ecting, Ke= 0.500	
			Inlet / Outlet	Invert= 919.00' / 91	0.00' S= 0.0450 '/	' Cc= 0.900
			n= 0.013 Co	ncrete pipe, bends	& connections, Flo	w Area= 3.14 sf
#2	Device 1	919.00'	2.2" Vert. Or	ifice/Grate C= 0.6	600 Limited to wei	r flow at low heads
#3	Device 1	925.85'	48.0" W x 8.0	" H Vert. Orifice/G	rate C= 0.600	
			Limited to we	ir flow at low heads		
#4	Device 1	930.10'	60.0" x 60.0"	Horiz. Orifice/Grat	te C= 0.600	
			Limited to we	ir flow at low heads	5	

Primary OutFlow Max=17.41 cfs @ 12.12 hrs HW=927.95' (Free Discharge) 1=Culvert (Passes 17.41 cfs of 42.65 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.38 cfs @ 14.33 fps) -3=Orifice/Grate (Orifice Controls 17.04 cfs @ 6.39 fps)

4=Orifice/Grate (Controls 0.00 cfs)



Pond P1: Detention Basin

Stage-Area-Storage for Pond P1: Detention Basin

Elevation	Surface	Storage	Elevation	Surface	Storage
	(sq-ft)	(cubic-feet)		(sq-tt)	(cubic-reet)
919.00	1,307	0	929.20	18,437	90,422
919.20	1,474	278	929.40	18,875	94,153
919.40	1,650	590	929.60	19,317	97,973
919.60	1,837	939	929.80	19,765	101,881
919.80	2,033	1,326	930.00	20,218	105,879
920.00	2,240	1,753	930.20	20,662	109,967
920.20	2,408	2,217	930.40	21,110	114,144
920.40	2,581	2,716	930.60	21,564	118,411
920.60	2,761	3,250	930.80	22,022	122,770
920.80	2,946	3,821	931.00	22,485	127,220
921.00	3,138	4,429	931.20	22,940	131,763
921.20	3,500	5,093	931.40	23,400	136,397
921.40	3,882	5,831	931.60	23,864	141,123
921.60	4,284	6,647	931.80	24,333	145,943
921.80	4,706	7,545	932.00	24,806	150,856
922.00	5,147	8,530	932.20	25,274	155,864
922.20	5,440	9,589	932.40	25,746	160,966
922.40	0,74Z	10,707	932.00	20,223	100,103
922.00	0,001	11,000	932.00	20,704	17 1,430
922.00	0,309	13,120	933.00	27,109	170,045
923.00	7 010	14,434			
923.20	7,010	17 230			
923.40	7,001	18 738			
923.80	7,000	20,303			
924.00	8 340	21,937			
924.20	8,675	23,638			
924.40	9.017	25,407			
924.60	9,365	27,245			
924.80	9,720	29,154			
925.00	10,081	31,134			
925.20	10,436	33,185			
925.40	10,797	35,309			
925.60	11,165	37,505			
925.80	11,538	39,775			
926.00	11,918	42,120			
926.20	12,293	44,541			
926.40	12,674	47,038			
926.60	13,060	49,611			
926.80	13,453	52,262			
927.00	13,851	54,993			
927.20	14,246	57,802			
927.40	14,646	60,691			
927.60	15,052	63,661			
927.80	15,403	00,71Z			
928.00	15,880	09,847			
920.20 028 10	10,294	13,004 76 265			
920.40 928 RN	10,714	70,303			
928 80	17 569	83 221			
929.00	18,005	86,778			
0_0.00	. 5,000				

Summary for Link PT1: Point #1

Inflow Area =	11.290 ac,	0.00% Impervious, Ir	nflow Depth > 3.45"	for 10-Year event
Inflow =	20.02 cfs @	12.04 hrs, Volume=	3.250 af	
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Att	en= 100%, Lag= 0.0 min
Secondary =	20.02 cfs @	12.04 hrs, Volume=	3.250 af	

Primary outflow = Inflow above 5,000.00 cfs, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs



Link PT1: Point #1

		Discovery Park Alura Apartments
Discovery Park Alura Proposed	Туре	II 24-hr 100-Year Rainfall=7.71"
Prepared by OWN Inc		Printed 1/27/2025
HydroCAD® 10.20-5c s/n 09171 © 2023 Hy	vdroCAD Software Solutions LLC	2 Page 19
Time span=0 Runoff by SCS Reach routing by Stor-Ind-	.00-48.00 hrs, dt=0.05 hrs, 96′ TR-20 method, UH=SCS, Wei +Trans method - Pond routing	1 points ghted-CN g by Stor-Ind method
Subcatchment A1: Onsite	Runoff Area=10.300 ac 0. Tc=6.0 min	00% Impervious Runoff Depth=6.17" CN=87 Runoff=101.48 cfs 5.294 af
Subcatchment A1 BYP: Undetained	Runoff Area=0.990 ac 0. Tc=6.0 m	00% Impervious Runoff Depth=5.35" in CN=80 Runoff=8.81 cfs 0.442 af
Subcatchment A2: West Proposed	Runoff Area=11.210 ac 0. Tc=6.0 min	00% Impervious Runoff Depth=6.17" CN=87 Runoff=110.44 cfs 5.762 af
Pond P1: Detention Basin	Peak Elev=930.09' Storage=10	07,737 cf Inflow=101.48 cfs 5.294 af Outflow=25.80 cfs 4.937 af
Link PT1: Point #1	above 5, Primary=0.00 cfs 0.0	000.00 cfs Inflow=31.82 cfs 5.379 af 000 af Secondary=31.82 cfs 5.379 af
Total Runoff Area = 22.500) ac Runoff Volume = 11.497	af Average Runoff Depth = 6.13"

il Runoff Area = 22.500 ac Runoff Volume = 11.497 at Average אטחסד שפעה = ס.ז.ס 100.00% Pervious = 22.500 ac 0.00% Impervious = 0.000 ac
Summary for Subcatchment A1: Onsite

Runoff = 101.48 cfs @ 11.96 hrs, Volume= Routed to Pond P1 : Detention Basin 5.294 af, Depth= 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=7.71"

	Area	(ac) (CN E	Descr	riptic	on																		
*	10.	300	87																					
	10.	300	1	00.0	0%	Pervi	ious /	Are	а															
	Tc (min)	Length (feet)	Slo (ft.	pe /ft)	Velo (ft/:	ocity sec)	Ca	oac (cl	ity fs)	Des	scri	ptio	n											
	6.0									Dire	ect	Ent	t ry ,											
							Sul	oca	atch	nme	nt	A1	: 0	ns	ite									
								Ну	/drog	graph														
	110			10	1 49 of o	1																	Runoff	
	105	\square			1.46 CIS												Ту	ре	- 11	24	ŀ-h	r		
	95 90											10)0-	Ye	ar	R	air	nfa	=	:7 .	71	••		
	80 80											R	lur	10	ff /	Are	a	=1(0.3	00) a	С		
	75- 70-							-				Ru	nc	off	Vo	blu	Im	e=	5.2	294	4 a	f		
	(cts) 65													Ru	nc	ff	De	ept	:h=	:6 .	17	••		
	55 6 1 1																Ī	C=	=6.	0 r	ni	n		
	45- 40-																		C	:N:	=8	7		
	35- 30-																							
	25 20																							
	15 10-																							
	5					<u>M</u>																		
	Ŭ	2 4	68	10	12	14 16	6 18	20	22 Time	24 (hou	26 rs)	28	30	32	34	36	38	40	42	44	46	48		

Summary for Subcatchment A1 BYP: Undetained

Runoff = 8.81 cfs @ 11.97 hrs, Volume= 0.442 af, Depth= 5.35" Routed to Link PT1 : Point #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=7.71"

Area (ac) CN Description							
0.990	80	>75%	% Grass co	over, Good,	HSG D		
0.990 100.00% Pervious Area							
Tc Leng (min) (fe	gth et)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0 Direct Entry,							
Subcatchment A1 BYP: Undetained							



Summary for Subcatchment A2: West Proposed

Runoff = 110.44 cfs @ 11.96 hrs, Volume= 5.762 af, Depth= 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=7.71"



Summary for Pond P1: Detention Basin

Inflow Ar	rea =	10.300 ac,	0.00% Impervious,	Inflow Depth = $6.^{\circ}$	17" for 100-Year event
Inflow	=	101.48 cfs @	11.96 hrs, Volume	= 5.294 af	
Outflow	=	25.80 cfs @	12.12 hrs, Volume	= 4.937 af,	Atten= 75%, Lag= 9.4 min
Primary	=	25.80 cfs @	12.12 hrs, Volume	= 4.937 af	-
Route	ed to Lin	k PT1 : Point #	[!] 1		

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 930.09' @ 12.12 hrs Surf.Area= 20,420 sf Storage= 107,737 cf

Plug-Flow detention time= 252.9 min calculated for 4.932 af (93% of inflow) Center-of-Mass det. time= 216.8 min (999.7 - 782.9)

Volume	Inve	rt Avail.Sto	rage Storage [Description		
#1	919.00	D' 176,84	45 cf Custom	Stage Data (Conic	c) Listed below (Re	ecalc)
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	Wet.Area	
010 (20	1 207	0	0	1 207	
919.0		2 240	1 753	1 753	1,307	
920.0		2,240	1,755	1,755	2,252	
921.0		5,130	2,070	4,429	5,100	
922.0		5,147	4,101	0,000	5,190	
923.0		0,095	5,904 7,502	14,404	0,702	
924.0		10 091	0,107	21,937	10 200	
920.0		11,001	9,197	31,13 4 42,120	10,209	
920.0		13 851	10,907	42,120	12,003	
927.0		15,001	12,072	54,995 60 847	14,007	
920.0		19,000	14,004	09,047 96 779	19 206	
929.0		20.219	10,931	105 970	20 572	
930.0		20,210	21 241	100,079	20,073	
022 (22,400	21,341	127,220	22,090	
932.0		24,000	25,030	176 945	20,202	
933.0	50	27,109	25,900	170,045	21,133	
Device	Routing	Invert	Outlet Devices	i		
#1	Primary	919.00'	24.0" Round	Culvert		
			L= 200.0' RC	P. sa.cut end proje	ectina. Ke= 0.500	
			Inlet / Outlet In	vert= 919.00' / 91	0.00' S= $0.0450'/$	" Cc= 0.900
			n= 0.013 Con	crete pipe, bends	& connections. Flo	ow Area= 3.14 sf
#2	Device 1	919.00'	2.2" Vert. Orifi	ce/Grate C= 0.6	600 Limited to we	r flow at low heads
#3	Device 1	925.85'	48.0" W x 8.0"	H Vert. Orifice/G	rate C= 0.600	
			Limited to weir	flow at low heads		
#4	Device 1	930,10'	60.0" x 60.0" H	loriz. Orifice/Grat	e C= 0.600	
			Limited to weir	flow at low heads		

Primary OutFlow Max=25.72 cfs @ 12.12 hrs HW=930.07' (Free Discharge) 1=Culvert (Passes 25.72 cfs of 48.00 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.42 cfs @ 15.95 fps) 3=Orifice/Grate (Orifice Controls 25.30 cfs @ 9.49 fps) 4=Orifice/Grate (Controls 0.00 cfs)



Pond P1: Detention Basin

Stage-Area-Storage for Pond P1: Detention Basin

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
919.00	1,307	0	929.20	18,437	90,422
919.20	1,474	278	929.40	18,875	94,153
919.40	1,650	590	929.60	19,317	97,973
919.60	1,837	939	929.80	19,765	101,881
919.80	2,033	1,326	930.00	20,218	105,879
920.00	2,240	1,700	930.20	20,002	109,907
920.20	2,400	2,217	930.40	21,110	114,144
920.40	2,001	3 250	930.80	22,004	122 770
920.80	2,946	3.821	931.00	22,485	127.220
921.00	3,138	4,429	931.20	22,940	131,763
921.20	3,500	5,093	931.40	23,400	136,397
921.40	3,882	5,831	931.60	23,864	141,123
921.60	4,284	6,647	931.80	24,333	145,943
921.80	4,706	7,545	932.00	24,806	150,856
922.00	5,147	8,530	932.20	25,274	155,864
922.20	5,440	9,589	932.40	25,746	160,966
922.40	5,742	10,707	932.60	20,223	166,163
922.00	6 360	11,000	932.00	20,704 27 189	17 1,430 176 845
923.00	6 695	14 434	333.00	27,105	170,045
923.20	7.010	15,805			
923.40	7.331	17.239			
923.60	7,660	18,738			
923.80	7,997	20,303			
924.00	8,340	21,937			
924.20	8,675	23,638			
924.40	9,017	25,407			
924.60	9,365	27,245			
924.80	9,720	29,154			
925.00	10,001	31,134			
925.20	10,430	35,100			
925.60	11,165	37,505			
925.80	11.538	39,775			
926.00	11,918	42,120			
926.20	12,293	44,541			
926.40	12,674	47,038			
926.60	13,060	49,611			
926.80	13,453	52,262			
927.00	13,851	54,993			
927.20	14,240	57,802 60,601			
927.40	14,040	63 661			
927.80	15 463	66 712			
928.00	15.880	69.847			
928.20	16,294	73,064			
928.40	16,714	76,365			
928.60	17,139	79,750			
928.80	17,569	83,221			
929.00	18,005	86,778			

Summary for Link PT1: Point #1

Inflow Area =	11.290 ac,	0.00% Impervious,	Inflow Depth > 5.7	2" for 100-Year event
Inflow =	31.82 cfs @	12.01 hrs, Volume=	= 5.379 af	
Primary =	0.00 cfs @	0.00 hrs, Volume=	= 0.000 af,	Atten= 100%, Lag= 0.0 min
Secondary =	31.82 cfs @	12.01 hrs, Volume=	= 5.379 af	-

Primary outflow = Inflow above 5,000.00 cfs, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs



Link PT1: Point #1

Water Quality Computations



Engineering beyond.^m

WORKSHEET: EXTENDED DRY DETENTION BASIN (EDD) DESIGN

Project: Alura Apartments		By:	JWB 1/27/2
Location: Lee's Summit, MO		Checked:	
Basin ID: P1			
Required Volume Calculation			
$WQ_V = F - RV - A / 12 (ac-1i)$ R = W(ator Quality Storm rainfall donth = 1.27 in			
A = Local Treatment Drainage Area (acres)			
Rv = Volumetric Runoff Coefficient = 0.05 + 0.009 * I			
I = Percent Site Imperviousness (%)			
Drainage Area: 11.29 acres	WQ_V (required):	0.93	ac-ft
% Impervious: 75.0 %		40,706	cu ft
Water Quality Outlet Type			
Step 1) Set water quality outlet type	Outlet Type	1	
Type 1 = single orifice		-	-
Type 2 = perforated riser or plate			
Type 3 = v-notch weir			
Water Quality Outlet, Single Orifice			
Step 1) Depth of water quality volume at outlet, Z_{WQ} (ft)	Z _{WQ} :	5.8	ft
Step 2) Average head of water quality volume over invert of orifice, H_{WQ} (ft)			4
$H_{WQ} = 0.5 * Z_{WQ}$	H _{WQ} :	2.92	ft
Step 3) Average water quality outflow rate, Q_{WQ} (cfs)	Q _{WQ} :	0.28	cfs
$Q_{WQ} = (WQ_V * 43,560) / (40 * 3,600)$			4
Step 4) Set value of orifice discharge coefficient, C $_{ m O}$	Co	0.66	1
C_0 = 0.66 when thickness of riser/weir plate is \leq orifice diameter			
C_{O} = 0.80 when thickness of riser/weir plate is > orifice diameter			-
Step 5) Water quality outlet orifice diameter (minimum of 4 inches), D $_{ m O}$ (in)	D _o :	2.39	in
$D_{O} = 12 * 2 * (Q_{WQ} / (C_{O} * \pi * (2 * g * H)^{0.5}))^{0.5}$			-

WQv (proposed): 0.92 ac-ft

40-Hour WQv Outlet

Outlet Elevation:	919.00
Outlet Type:	Orifice
Outlet Size:	2.25" Diameter
Outlet Protection:	Submerged Well-screen

2025