

Mid-Continent Public Library East Lee's Summit Branch Final Stormwater Study

BATTERY DRIVE AND SOUTHEAST BLUE PARKWAY LEE'S SUMMIT, MISSOURI

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Prepared for: Mid-Continent Public Libraries (MCPL)

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Olsson Project No. B18-0330

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GENERAL INFORMATION

This Stormwater Management Study is being submitted on behalf of the Mid-Continent Public Library (MCPL) for the proposed library facility located at the northeast corner of SE Blue Parkway and Battery Drive.

Project Location and Description

The proposed site is located on Lot 2 of the Magnolia Place at Charleston Park, 1st Plat in the Northeast ¼ of Section 10, Township 47 North, Range 31 West, in Jackson County, Lee's Summit, Missouri and includes approximately 3.8 acres. The site is located at the northeast corner of the SE Blue Parkway and Battery Drive intersection and is generally bounded by Village Cooperative of Lee's Summit to the north, SE Battery Dr to the west, SE Blue Parkway to the south, and an undeveloped lot to the east (See Figure 2). The Church of Jesus Christ of Latter-Day Saints lies east of the undeveloped lot. The proposed development includes a 18,500 S.F. library facility with associated parking lots, landscaping, grading, and utilities. The entirety of the site is located outside of the 100-Year FEMA Floodplain.

Study Purpose

The purpose of this study is to provide a Stormwater Management Plan for the proposed development in accordance with the American Public Works Association (APWA) *Standard Specifications and Design Criteria* Section 5600 "Storm Drainage Systems and Facilities", APWA Manual of Best Management Practices (BMP) for Stormwater Quality, and applicable City of Lee's Summit, Missouri guidelines.

Soils Descriptions

Soil classifications were obtained from the Natural Resource Conservation Service's website by utilizing the Web Soil Survey feature. The site soil composition and classification are listed below:

10082 – Arisburg-Urban Land Complex, 1 to 5 percent slopes – HSG Type C.
10180 – Udarents-Urban Land-Sampsel Complex, 2 to 5 percent slopes - HSG Type C.

*HSG – Hydrologic Soils Group

See Soils Map in Appendix B.

METHODOLOGY

General Criteria and References

Analytical and design criteria conform to those of Division V - Section 5600 – "Storm Drainage Systems and Facilities" of the Kansas City Metropolitan Chapter of the American Public Works Association's "Standard Specifications and Design Criteria". Based on these criteria, Post-development discharge rates for 2, 10, and 100-year storm events will be limited to provisions in section 5608.4-C1 Performance Criteria – "Comprehensive Control". Post-development discharge rates are limited to 0.5 cfs per acre for the 2-Year event, 2.0 cfs per acre for the 10-year event, and 3.0 cfs per acre for 100-year storm event. Pre and post-development flows from the site are shown below and were calculated using HEC-HMS for the 2, 10 and 100-year storm events. Existing and proposed hydrographs were calculated using the 24-hour SCS Type II rainfall distribution. Given the size of the site, all times of concentration were set a minimum of 5 minutes, the defined minimum per Section 5600.

HYDROLOGIC/HYDRAULIC ANALYSES

Existing Conditions Analysis

The existing site is an undeveloped parcel of land that consist of native vegetation. The site is bounded by SE Battery Drive to the west, The Village Cooperative Apartments to the north, undeveloped property to the east, and SE Blue Parkway to the South. Currently, Blue Parkway lies within MoDOT's US-50 right of way.

The existing drainage for the site is split by a ridge into two outfalls, "A" and "B". The east section drains to outfall "A" and the west section drains to outfall "B". Outfall "A" drains northwest over the curb into the gutter. The gutter drains to an existing public curb inlet on Battery Drive. Outfall "B" drains overland to the northeast. This area drains over the back of the curb to an existing storm structure in the parking lot of the Village Cooperative Apartments.

South of the property there is an existing ditch that lies within US-50 right of way. The ditch drains run-off from Blue Parkway. There is no curb and gutter on Blue Parkway, just a graveled shoulder that allows run-off to drain into the existing ditch. There is an existing 18x24 arch culvert that drains to the ditch from under Battery Drive flows east along the north side of Blue Parkway.

As stated previously, there is an undeveloped lot to the east of the property that is owned by Richard D. Link. Mr. Link is also the person who sold Lot 2, Magnolia place to MCPL. The proposed development did not require all of the property for Lot 2. The east 81' of the property was excluded from the sale and remains the property of Richard D. Link. The proposed drive from the south will be a common access drive that will serve both the MCPL property and the future developed lot to the east. The east half of this drive will be constructed on the undeveloped lot under a mutual understanding with Mr. Link.

This property generally drains to the east to an existing swale away from the library property. None of this area drains to the proposed collection system for the library.

For the purposes of the drainage calculations moving forward this area will be included, therefore the studied area will increase from 3.8 acres to 4.5 acres.

A composite curve number was generated for the site by referencing the Web Soil Survey available in Appendix C, APWA Section 5600 and considered the following factors:

- Existing impervious area
- Existing pervious area
- Hydrologic soil group

The following tables summarize the pre-development composite curve number generation.

Sub-Area	Area (AC)	Soil Group	Curve Number
Pasture (Good)	3.0	С	74
Pasture (Good)	1.5	С	74

 Table 1: Pre-Development Curve Number Analysis

The existing peak discharge rates for the 2-year, 10-year, and 100-year storm events from the site are shown in Table 2 below:

Table	2:	Existing	Peak	Flows
1 4 8 10		Exioting		

Sub-Area / Outfall	Area (acres)	Q (2-Year Storm) (cfs)	Q (10-Year Storm) (cfs)	Q (100-Year Storm) (cfs)
А	3	4.8	7.4	12.8
В	1.5	2.4	3.6	6.4

Proposed Conditions Analysis

The proposed Public Library will include a 18,500 SF library with associated parking lots, landscaping, grading, and utilities. A site plan has been included in Appendix A. The site will generally continue to drain in the same pattern as existing. Drainage from the site will

enter into an enclosed storm sewer system that will be constructed with the development. The proposed system will collect drainage from the parking area and building. The increase in impervious area will increase runoff from the site. To mitigate the increase in runoff, the following strategy will be implemented.

The site will be graded so that Drainage Areas A & B, noted in the Existing Conditions, will drain north and directed into a detention basin. A proposed drainage map is included in Appendix A.

A post-development composite curve number was generated using the same methodology implemented during the pre-development curve number analysis. Table 3 below summarizes the post-development composite curve number generation.

Sub-Area	Area (AC)	Soil Group	Curve Number
Pavement, Buildings, Impervious	2.0	С	98
Turf (Good)	2.5	С	85

 Table 3: Post-Development Curve Number Analysis

A peak flow analysis of the post-development site was conducted using HEC-HMS, the composite curve number, and rainfall and distribution information acquired from APWA section 5600. Post-development peak to the outfall are summarized in the Table 4. Detailed reports from HEC-HMS are available in Appendix D

Table 4: Proposed Peak Flows

Sub-Area / Outfall	Tributary Area	Q (2-Year Storm)	Q (10-Year Storm)	Q (100-Year Storm)
	(acres)	(cfs)	(cfs)	(cfs)
Detention Basin	4.5	13.7	21.1	33.4

The existing ditch to the south will remain essentially unchanged. The drainage area, for the ditch, lies within the existing right of way. An embankment will need to be constructed across the ditch for the southern entrance. A culvert will be installed under the entrance to

maintain flow in the ditch. The 30" culvert will receive the flow from the existing 18x24 (24" equivalent) local drainage from Blue Parkway.

Stormwater Detention Requirements

One proposed detention pond will be utilized to mitigate the increase in flow due to an increase in impervious area. The Detention Basin will be located on the northern part of the property. It will collect runoff from the 4.5-acre property. The pond has an outlet pipe that connects to an orifice plate within a junction box structure that will be within the dam.

The outlet for the detention basin will be a flared end section with a trash rack connected by a 15" pipe to a control structure. The control structure will have an internal control plate. The control plate will have a series of 6 - 1" holes arranged in a single vertical row beginning at Elevation 1006.5. There will be a 2 stage cuts into the control plate.

The series of 1" vertical holes are designed for the water treatment requirements. the water quality volume (WQv) will be controlled by the vertical holes at the bottom of the plate. The 1" holes will release the water quality volume over a 40-hour period to allow pollutants to settle out of this precipitation event.

The weir will be located above the WQv surface elevation and will control the release of the 2, 10 and 100-year storm events. A 1'-0 wide weir (ie 1008.4) weir located at control plate will control the 2-year flow. A 2'-2" weir (I.E. 1009.00) will control the 10-year flow. There will be a 24" inlet pipe into the control structure that will ultimately control the 100-year flow. Finally, an 18" outlet pipe will be connect to an existing city storm structure that will route the flow into the public storm system These storms have been analyzed through the control structure and will release below the pre-existing storm events and below the Comprehensive Control release rates defined in APWA section 5600. A Storage-Discharge Table has been provided in Appendix D that details the flows through the outlet structure. The dam will have an emergency spillway to control the 100-year overflow should the outlet become blocked.

Table 5 provides the water surface elevations (WSE's) and peak flows for the proposed detention basin.

Table 5: Detention Ba	sin, WSE's and Peak Flows
Description	Statistics
Bottom of Basin	1006.70
Total Storage Volume	1.2 ac-ft
Emergency Spillway	
(IE, 100-Yr WSE)	1011.12, 1011.75
Top of Dam Elevation	1012.20
WQv Perf. Plate	1003.30, 1" Vertical Holes 4" C to C
(IE Elevation, Perf and Spacing)	(15 – Holes)
Water Quality Volume	
WSE, Storage, Peak Outflow	1008.40, 0.3 ac-ft, 0.6 cfs
2 nd Stage Weirs	1008.4, 1.00 ft
(IE, Width)	1009, 2.17 ft
10–Year Storm	
WSE, Storage, Peak Outflow	1009.43, 0.41 ac-ft, 5.5 cfs
100–Year Storm	
WSE, Storage, Peak Outflow	1010.32, 0.63 ac-ft, 13.4 cfs

Table 6 shows the overall peak flows for the site for both pre and post-construction. In addition, it also shows the allowable Comprehensive control release rate. Note that peak flow for post-construction has been lowered in all storm events.

Site	Q (2-Year Storm) (cfs)	Q (10-Year Storm) (cfs)	Q (100-Year Storm) (cfs)
Pre-Construction	7.2	11	19.2
Section 5600 Allowable Comprehensive Release Rate	2.3 (0.5 cfs per acre)	9 (2.0 cfs per acre)	13.5 (3.0 cfs per acre)
Post Construction	2.2	5.5	13.4
Post Const Less Than Allowable	Yes	Yes	Yes

 Table 6: Peak Flow Change Analysis

STORMWATER TREATMENT REQUIREMENTS

As stated previously, the proposed detention is designed to act an extended dry bottom detention facility will be used to treat stormwater per MARC water quality standards. The orifice plate for the basin will be sized to release the water quality volume (1.37") over a 40-hour period to allow pollutants to settle from runoff before entering the public stormwater system. The maximum storage for the water quality event in the basin will be 0.3 acre-ft reaching a peak water surface of elevation 1008.40 feet.

CLEAN WATER ACT SECTION 404 PERMITTING REQUIREMENTS

No jurisdictional Waters of the United States have been identified on the study site. Therefore, a Section 404 permit is not required.

FEMA/DWR PERMIT REQUIREMENTS

No FEMA permitting or submittals will be required on this site because there are no FEMA delineated floodplains on the site. A copy of the FIRM map for this area has been included in Appendix B.

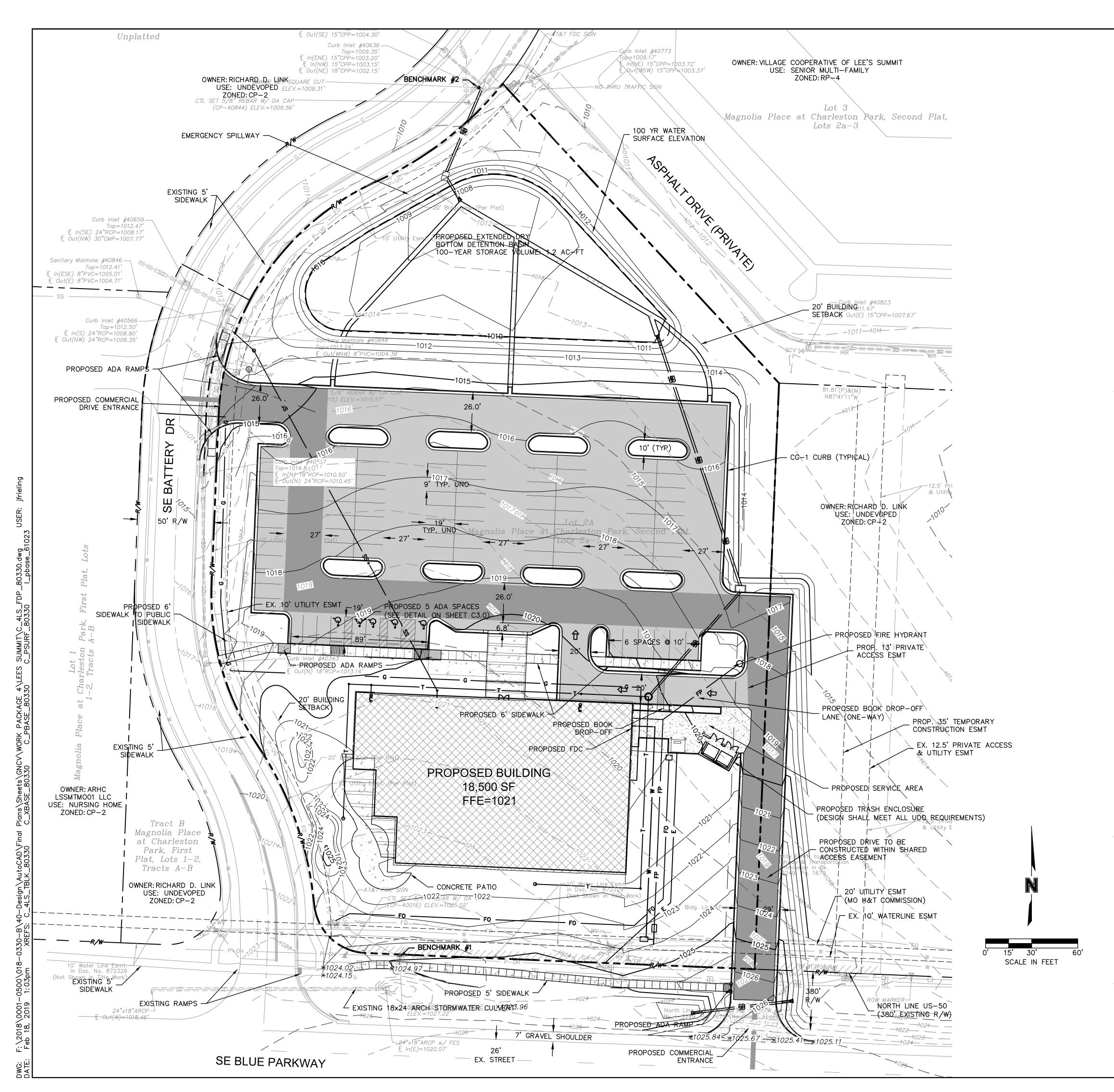
CONCLUSIONS AND RECOMMENDATIONS

As outlined in the preceding report, increased runoff rates in the post-development conditions are mitigated by the detention basins. Drainage patterns on the site remain relatively unchanged. An extended dry detention basin has been designed to maintain or improve storm water quality. Based on these facts and other information provided herein, we request that this stormwater study be approved.

Appendix A Map Exhibits



30' 60' SCALE IN FEET



SITE DATA			
	ZONING & SITE AREA		
PROPOSED USE:	PUBLIC LIBRARY		
	SITE AREA		ZONING
LOT 2 (AS DECRIBED):	3.80 ACRES (165,528 SF	·)	CP-2
IMPERVIOUS:	1.71 ACRES (74,488 SF)	(45%)	
PERVIOUS:	2.09 ACRES (91,040 SF)	(55%)	
FAR (0.55 MAX):	0.15		
	BUILDING AREA		
BUILDING TYPE	# STORIES SQ	UARE F	OOTAGE
BUILDING	1	18,50	0 SF
	PARKING		
USE	REQUIRED	F	ROVIDED
LIBRARY	4 PER 1000 SF = 74	83	
ADA	3 (PER CITY TABLE)	5	
TOTAL	74	88 (IN	CLUDING ADA)

<u>NOTE:</u>

ACCORDING TO MDNR STATE OIL & GAS COUNSEL THERE ARE NO OIL AND GAS WELLS LOCATED WITHIN OR ADJACENT TO THE PROPERTY.

EXISTING CONDITIONS LEGEND

· ·
P-0H
P-UG
TEL
FO
G
W
<u>=</u>
SS

PROPERTY LINES RIGHT-OF-WAY LINES EASEMENT LINES BUILDING SETBACK LINES OVERHEAD ELECTRIC UNDERGROUND ELECTRIC UNDERGROUND TELEPHONE UNDERGROUND FIBER OPTIC GAS LINE WATER LINE STORM SEWER LINE SANITARY SEWER LINE GRADE CONTOURS

PROPOSED CONDITIONS LEGEND

Ε	PROPOSED	UNDERGROUND ELECTRIC
FO	PROPOSED	FIBER OPTIC
— w —	PROPOSED	WATER LINE
FP	PROPOSED	FIRE PROTECTION LINE
SD	PROPOSED	STORM SEWER LINE
T	PROPOSED	TURF DRAIN LINE
SS	PROPOSED	SANITARY SEWER SERVICE
	CONCRETE	CURB & GUTTER
	PROPOSED	BUILDING
	PROPOSED	CONCRETE SIDEWALK
	PROPOSED	LIGHT DUTY ASPHALT
851	PROPOSED	GRADE CONTOURS
	PROPOSED	FIRE ACCESS ROAD

BENCHMARKS:

<u>BENCHMARK #1:</u> ELEVATION=1027.22'

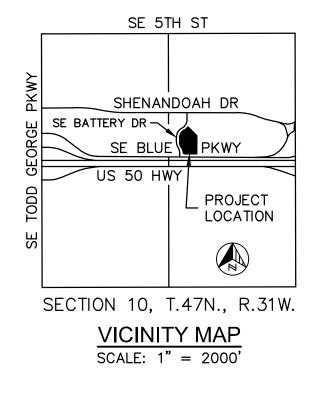
SET RAILROAD SPIKE IN THE NORTH SIDE OF A POWER POLE, $66' \pm$ NORTH OF THE Q OF SE BLUE PARKWAY, 86' EAST OF THE Q OF SE BATTERY DRIVE.

BENCHMARK #2: ELEVATION=1009.31'

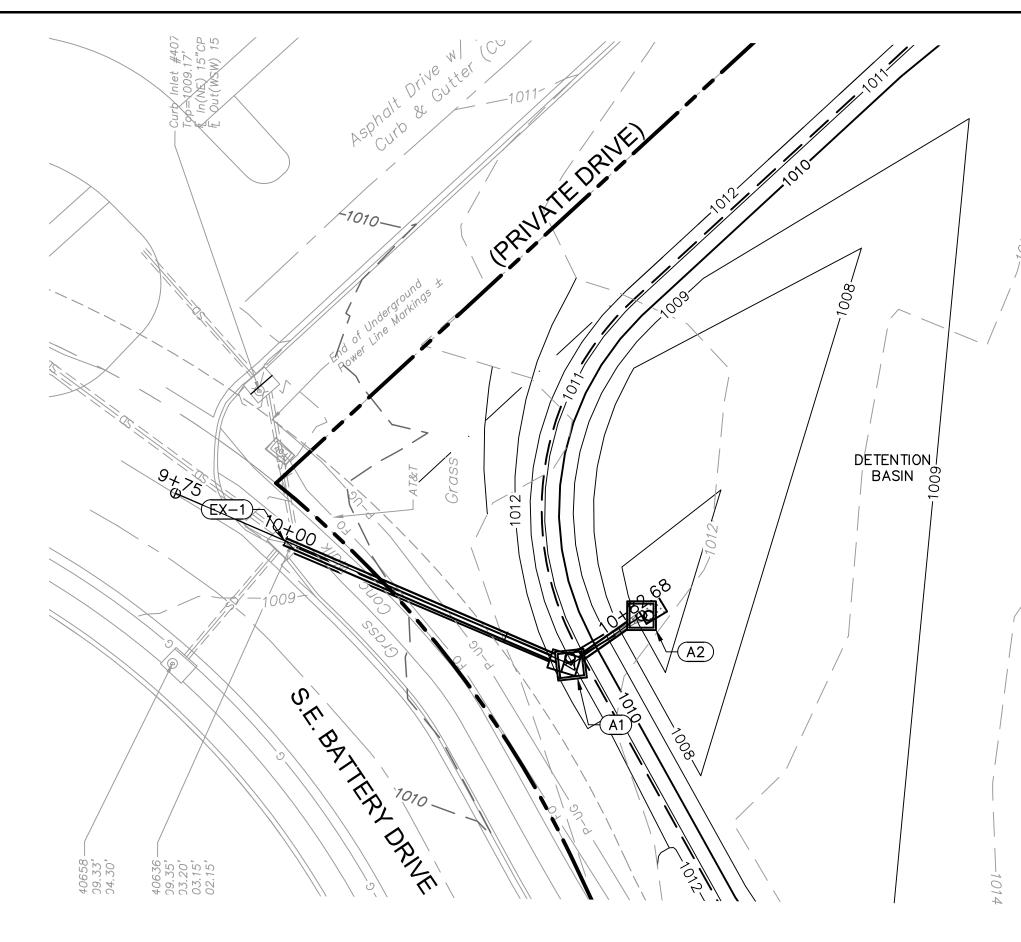
SET CHISELED "□" CUT ON THE SOUTHWESTERLY CORNER OF A CONCRETE CURB INLET #40636, 630'± NORTH OF THE € OF SE BLUE PARKWAY, 15' EAST OF THE € OF SE BATTERY DRIVE.

LEGAL DESCRIPTION:

LOT 2A, MAGNOLIA PLACE AT CHARLESTON PARK, SECOND PLAT, LOTS 2A-3, A SUBDIVISION IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, EXCEPT THE EAST 81.81 FEET THEREOF, CONTAINING 165,561 SQUARE FEET OR 3.8008 ACRES, MORE OR LESS.

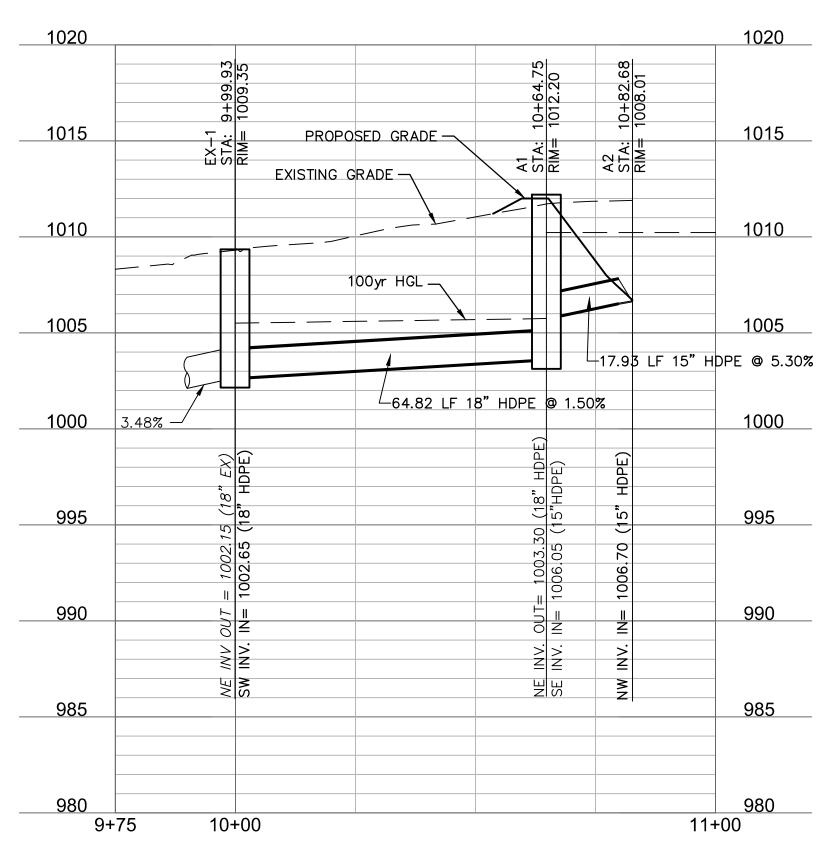


Sapp Des Missouri S		ciates Arch tificate of A	itects, P.C uthority #0	000607
In the event the changes to any documents, ar design profess results thereof Therefore, the any lability ari- changes. In ac by law, to inde any damage, ii costs of defens The personal s legal equivaler owner of the s sections pertai for all other pla	e client cons y plans, spec id these char ional, the cli are not the r client agrees sing from the client agrees sing from the client agrees sing from the client agrees sing from the client agrees sel arising from seal of the re to f his signa eal shall auth ning to this s ins, specifica instruments	EIAL NO ents to, allows, ifications or oth nges are not appert exponsibility of s to release the e construction, u lient agrees to the e construction, u lient agrees to the attree whenever neuticate this shi sheet. Respons ations, estimates relating to or intr tural project.	authorizes or a er construction proved in writiin hat such chan the design profess se or result of ne fullest exter foressional har sonable attornuss. ct or Engineer & wherever us eet and the sp s, reports or ot	approves of ng by the ges and the fessional. sional from such tt permitted miless from ey's fees ar shall be th sed, and the ecification disclaimed her
Mid-Continent Public Library	CONSTRUCTION DOCUMENT PLANS FOR	T LEE'S SUMMIT BRANCH	2240 SE BLUE PARKWAY	LEE'S SUMMI I, MU 64063 JACKSON COUNTY
	CO	EAST	PACKAGE	4



20 SCALE IN FEET

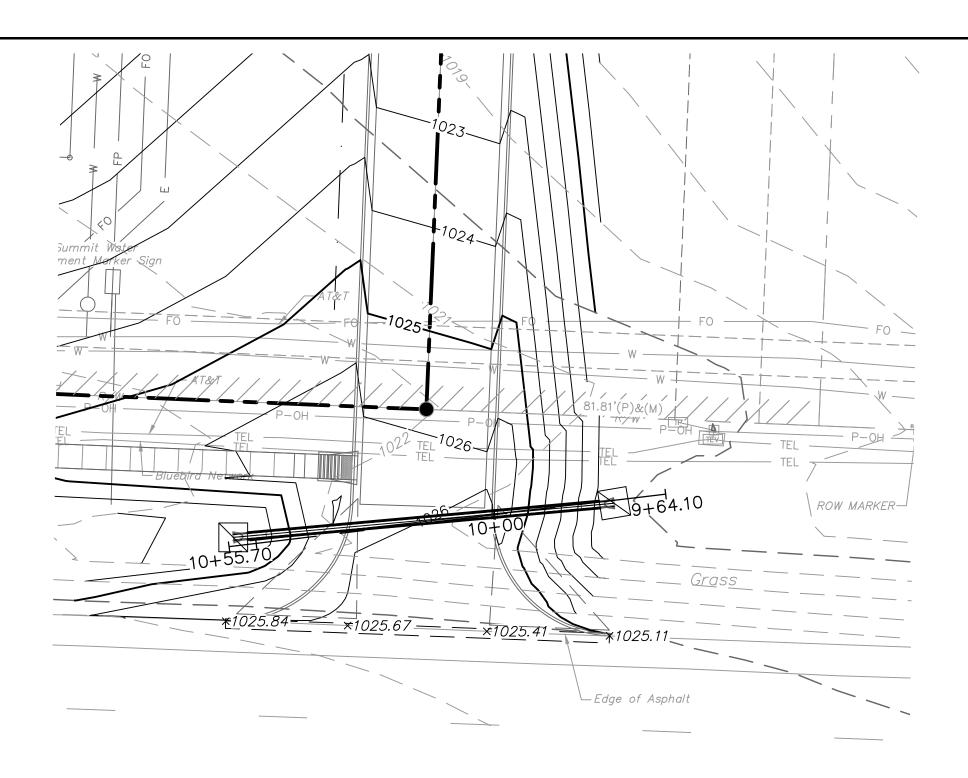
STORM 1 (1) (9+75 - 11+00)

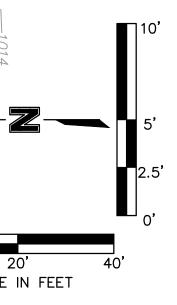


OUTLET CONDITION 10 YEAR FLOW 10_YR OUTLET FLOW = 4.6 CFS PROPOSED CAPACITY FOR 15" HDPE @ 5.30% = 15.0 CFS (31% FULL)CAPACITY FOR 18" HDPE @ 1.50% = 12.9 CFS (35% FULL) EXISTING CAPACITY FOR 18" HDPE @ 3.48% = 19.2 CFS (24% FULL) *OUTLET CONDITION 100 YEAR FLOW 100_YR OUTLET FLOW = 11.9 CFS PROPOSED* CAPACITY FOR 15" HDPE @ 5.30% = 15.0 CFS (79% FULL) CAPACITY FOR 18" HDPE @ 1.50% = 12.9 CFS (92% FULL) EXISTING CAPACITY FOR 18" HDPE @ 3.48% = 19.2 CFS (61% FULL)

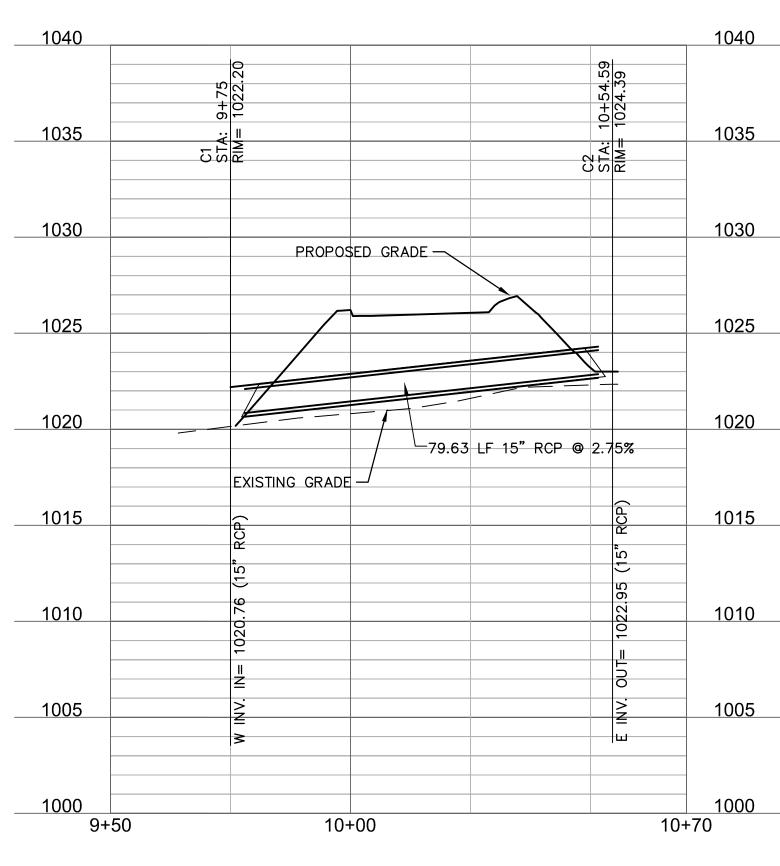
	STRUCTURES
ID	DESCRIPTION
A1	5' X 5' JUNCTION BOX RE: CONTROL STRUCTURE DETAIL, SHEET C10.6 10+64.75, 0.00' STORM 1 (1) RIM= 1012.20 INV IN = 1005.75 (15" HDPE) INV IN = 1003.62 (18" HDPE) N: 996661.070; E: 2837287.498
A2	INSTALL 15" HDPE END SECTION W/TOEWALL 10+82.68, 0.00' STORM 1 (1) INV IN = 1006.70 (15" HDPE) N: 996646.340; E: 2837297.721
EX-1	EXISTING INLET 9+99.93, 0.19' RT STORM 1 (1) RIM= 1009.35 INV IN = 1002.65 (18" HDPE) N: 996720.622; E: 2837313.108

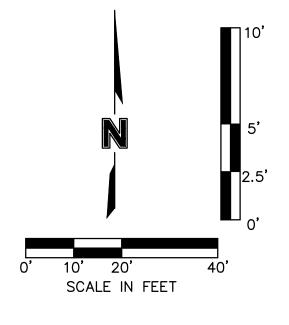
OUTLET CONDITION 10 YEAR FLOW



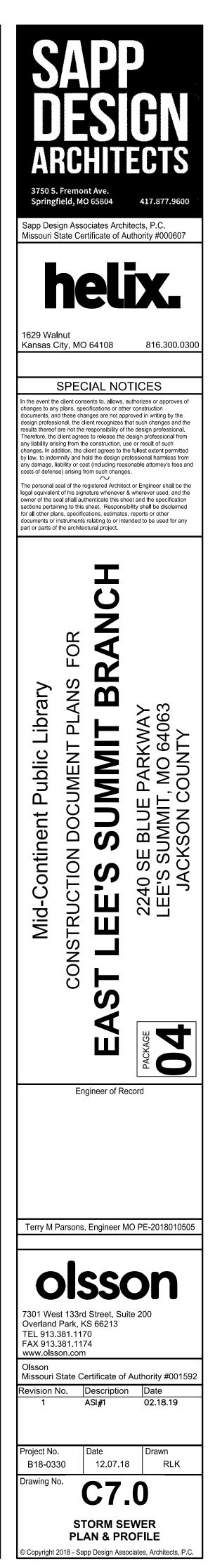


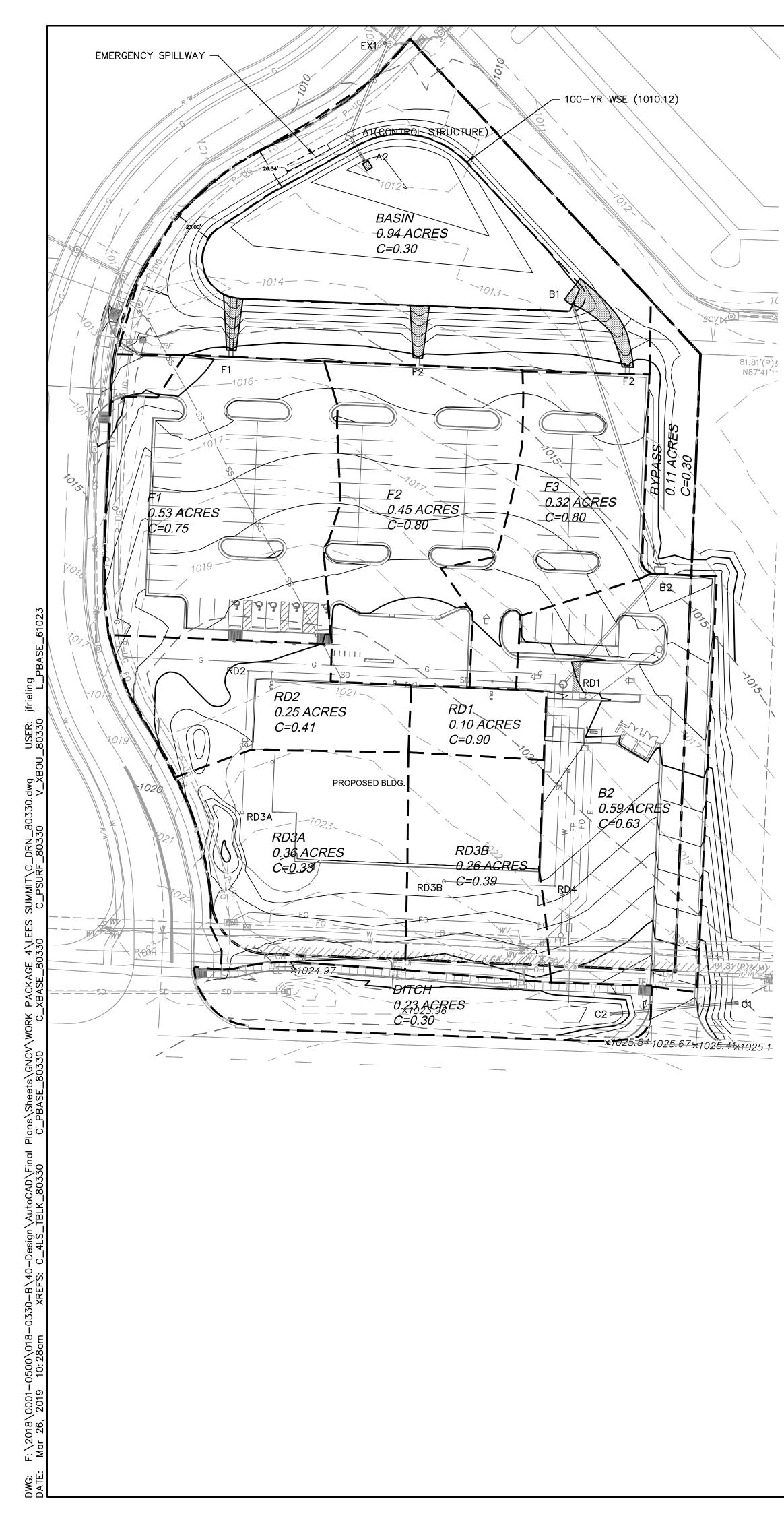
STORM 4 (9+50 - 10+70)



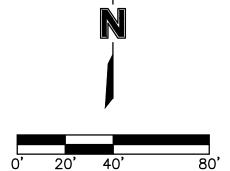


	STRUCTURES
ID	DESCRIPTION
C1	INSTALL 15" RCP END SECTION WITH CONCRETE TOEWALL AND 1.9 CUBIC YARDS CLASS 2 RIPRAP 9+75, -0.61 ' LT STORM 4 RIM= 1022.20 INV IN = 1020.76 (15" RCP) N: 996126.759; E: 2837528.253
C2	INSTALL 15" RCP END SECTION WITH CONCRETE TOEWALL AND 1.9 CUBIC YARDS CLASS 2 RIPRAP 10+54.59, 1.82' RT STORM 4 RIM= 1024.39 INV OUT = 1022.95 (15" RCP) N: 996119.661; E: 2837448.943

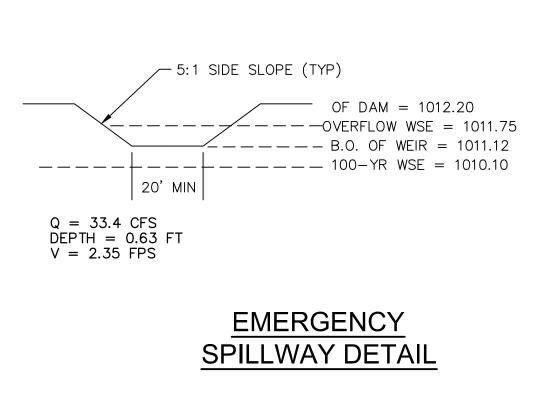




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		ER PIPE AN																TORMS	EWER	PIPE AND S	SIROCIOR	ETABLE											
	E #: 017-14	.EES SUMM	IT LIBRARY	r																													
	DESIGN CONDITIONS: 10 YEAR STORM EVENT STRUCTURES RUNOFF CALCULATIONS PIPE DESIGN																																
	FROM	то	AREA (ACRES)		с	KC (K=1.00)	Tc (MIN)	FLOW TIME (MIN)	INTENSITY (IN/HR)	DESIGN Q (CFS)	DESCRIPTION	LENGTH (L.F.)	PIPE SLOPE (%)	DIA (N)	Q FULL (CFS)	PIPE AREA (SQ.FT.)	10100	DESIGN V (F/S)		MH TOP ELEVATION		DOWINSTREAM FLOWLINE	DOWNSTREAM WATER ELEVATION	FRICTION HEAD (h f)	ENTRY LOSS COEFFICIENT (k)	ENTRY	ENTRY LOSS (h m)		HW, INLET CONTROL	HW, OUTLET CONTROL	HYDRAUUC GRADE ELEV.	GRADE (MAX)	Comments
	RD3A		0.36		0.33			-	7.35	0.87	ADS BASINS/ROOF DRAINS									1020.20											1017.54	1019.20	
	RD2	RD2	0.05	-	0.33	0.33			7.36	0.87	8 in HDPE ADS BASINS/ROOF DRAINS	88.00	1.00	8	1.21	0.35	3.47	3.80	1.04	1020.20	1016.70	1015.82	1016.85	0.47	1.00	1.00	0.22	0.69	1017.40	1017.54	1016.85	1019.20	
-	NDE	RD1	0.25		0.42	0.42			7.35	0.75	10 in. HDPE	193.00	1.00	10	2.20	0.55	4.03	4.53	1.24	1020.20	1015.82	1013.89	1013.48	1.45	0.40	0.40	0.13	1.57	1016.85	1015.82	1010.00	1010.20	
	RD1		0.10		0.90				7.36	0.66	JUNCTION BOX									1020.20											1018.25	1019.20	
_	82	82	0.59	0.97	0.63	0.53			7.35	3.78	15 in. HDPE CURB INLET	92.14	4.00	15	12.95	1.23	10.56	9.15	0.97	1017.86	1015.72	1012.02	1017.54	0.32	0.30	0.30	0.39	0.71	1016.94	1018.25	1013.48	1016.88	
_	02	B1	0.00	1.56	0.67				7.35	7.68	18 in. HDPE	173.65	1.00	18	10.53	1.77	5.96	6.50	1.17	1017.00	1011.72	1009.98	1009.52	0.94	0.50	0.50	0.33	1.27	1013.48	1011.72	1013.40	1010.00	END SECTION TO BASIN
	RD3B		0.26		0.30	0.39	5.0	-	7.35	0.75	ADS BASINS/ROOF DRAINS									1020.20											1017.33	1019.20	
	0.04	RD4		0.26					2.35	0.75	8 in. HDPE	67.00	1.00	8	1.21	0.35	3.47	3.64	0.94	1000.00	1016.70	1016.01	1016.59	0.26	1.00	1.00	0.21	0.46	1017.33	1017.06			
	RD4	RD1	0.00	0.26	0.39				7.35	0.00	ADS BASINS/ROOF DRAINS 8 in. HDPE	125.00	1.00	8	1.21	0.35	3.47	3.64	0.94	1020.20	1016.01	1014.76	1017.54	0.48	0.40	1.00	0.21	0.69	1016.64	1018.23			
	F1	BAS	0.53	0.53	0.75	0.75	5.0		7.35	2.92	FLUME																						
	F2	BAS	0.45	0.45	0.80	0.80	5.0		7.35	2.65	FLUME																						
_	F3	BAS	0.32	0.32	0.80	0.80	5.0		2.35	1.88	FLUME		-	-			-		-					-									
_																-																	
10						_	-						-				s	TORMS	EWER	PIPE AND S	STRUCTUR	E TABLE		-									
		ER PIPE AN																															
<u> 7</u>	TITLE: EAST LEES SUMMIT LIBRARY JOB #: 017-1488																																
	STRUC	ONDITION					ALCUL	ATIONS	5										_			IPE DESIGN		_									
	FROM	то	AREA	AREA (ACRES)	c	KC K=1.25)	Tc (MIN)	FLOW TIME (MIN)	INTENSITY (IN/HR)	DESIGN Q (CFS)	DESCRIPTION	LENGTH (L.F.)	SLOPE (%)	DIA (N)	Q FULL (CFS)	AREA (SQ.FT.)	V FULL	DESIGN V (F/S)		MH TOP ELEVATION	UPSTREAM FLOWUNE	DOWINSTREAM FLOWLINE	WATER ELEVATION	FRICTION HEAD (h f)	COEFFICIENT (k)		ENTRY LOSS (h m)		HW, INLET CONTROL	HW, OUTLET CONTROL	GRADE ELEV.	GRADE (MAX)	Comments
10	RD3A	000	0.36	0.00	0.33				7.35	1.09	ADS BASINS/ROOF DRAINS		1.00		1.71	0.25	0.17		1.77	1020.20	1010.00	4045.53	4040.05	0.70		4.00	0.04	0.03	4047.54	4047.45	1017.82	1019.20	
	RD2	RD2	0.25	0.36	0.33				7.35	1.09	8 in: HDPE ADS BASINS/ROOF DRAINS	88.00	1.00	8	1.21	0.35	3.47	3.94	1.25	1020.20	1016.70	1015.82	1016.85	0.73	1.00	1.00	0.24	0.97	1017.54	1017.82	1016.85	1019.20	
		RD1		0.61	0.42				7.35	2.35	12 in. HDPE	193.00	1.00	12	3.57	0.79	4.55	4.88	1.03		1015.82	1013.89	1013.90	0.85	0.40	0.40	0.15	1.00	1018.85	1015.82			
_	RD1	0.0	0.10		a second s		5.0		7.35	0.83	JUNCTION BOX 15 in: HDPE	00.44	1.00		10.05	1.00	10.62	0.30		1020.20	1016 20	1012.02	1017.82	0.50	0.90	0.50	0.44	0.94	4047.46	50.59 79	1018.76	1019.20	
-	B2	82	0.59	0.87	0.53	0.68	5.0		7.35	4.72	CURB INLET	82.14	4.00	10	12.95	1.20	10.30	8.72	1,19	1017.88	1015.72	1012.02	1017.02	0.50	0.30	0.30	0.44	0.54	1017.15	1018.78	1013.90	1016.88	
_		81		1.56	0.67				7.35	9.60	18 in. HDPE	173.65	1.00	18	10.53	1.77	5.96	6.74	1.45		1011.72	1009.98	1010.12	1.47	0.50	0.50	0.35	1.82	1013.90	1011.94			END SECTION TO BASIN
	RD3B	22.1	0.26				5.0		7.35	0.93	ADS BASINS/ROOF DRAINS						0.17			1020.20		1010.01							1017.00	1017.01	1017.43	1019.20	
-	RD4	RD4	0.00	0.26	0.39				7.35	0.93	8 in. HDPE ADS BASINS/ROOF DRAINS	67.00	1.00	8	1.21	0.35	3.47	3.84	1.10	1020.20	1016.70	1016.01	1016.68	0.40	1.00	1.00	0.23	0.63	1017.43	1017.31	1018.80	1019.20	
	1.001	RD1		0.26					2.35	0.93	8 in. HDPE	125.00	1.00	8	1.21	0.35	3.47	3.84	1.10	1 0 40 0 1 40 0	1016.01	1014.76	1017.82	0.76	0.40	1.00	0.23	0.98	1016.74	1018.80			
	E1	RAG	0.52	0.52	0.75	0.04	5.0	-	7.54	3.65	C IIMC		-	-			-		1														
	F1	BAS	0.53	0.53	0.75	0.94	5.0		7.35	3.65	FLUME																						
_	F1 F2	BAS		0.53					7.35 7.35	3.65 3.31	FLUME																						



0' 20' 40' SCALE IN FEET



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any damage, liability or cost (including reasonable attorney's fees and costs of defense) arising from such changes. The personal seal of the registered Architect or Engineer shall be the legal equivalent of his signature whenever & wherever used, and the owner of the seal shall authenticate this sheet and the specification sections pertaining to this sheet. Responsibility shall be disdaimed for all other plans, specifications, estimates, reports or other documents or instruments relating to or intended to be used for any part or parts of the architectural project.
And Continent Public Library CONSTRUCTION DOCUMENT PLANS FOR EAST LEE'S SUMMIT BRANCH 2240 SE BLUE PARKWAY 2240 SE BLUE PARKWAY LEE'S SUMMIT, MO 64063 JACKSON COUNTY
Terry M Parsons, Engineer MO PE-2018010505
7301 West 133rd Street, Suite 200 Overland Park, KS 66213 TEL 913.381.1170 FAX 913.381.1174 www.olsson.com
Olsson Missouri State Certificate of Authority #001592 Revision No. Description Date 1 ASI#1 02.18.19
Project No. Date Drawn B18-0330 12.07.18 RLK Drawing No. C8.0
DRAINAGE PLAN

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Appendix B FEMA Flood Classification Firm

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local dwinage source of themail iso. The commanity map repeatings should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in arreas where Base Flood Elevations (IPES), and/or floodways have been determined, using an encouraged to consult the Flood Profiles and Floodway Data and/or Survivary of Stillwaiter Elevations tables contained whith the Flood Insurance Staty (FIS) Report that accompanies this FIMU. Users should be aware that (BYEs shown on the FIMU represent munded while that diversitions. These BYEs are intended fits flood insurstone anting purposes rolly and should not be used as the sole source of flood elevation information. Accordingly, flood devated on that presented in the TIS Breyn should be usiliated in conjunction with the FIBM for purposes of construction and/or floodplain management.

Boundaries of the **Soudways** were computed at cross sectors and interpolated between cross sectors. The Soudways were based on hydraulic considerations with regard to repowersents of the National Fiscol treasmone Program. Floodway widths and other pertinent floodway data are provided in the Fiscol treasmone Budy Report for the prediction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 'Thood Protection Measures' of the Flood Insurance Study Report for Information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Massuri State Plane West Zove (FIP) zove 2420. The bardsontal datam was NAD-33, GIS 1980 softwards. Differences in datam, sphereld, projection or UPM cores used in the production of FIPIs for adjacent predictione may result in slight positional differences in may feature actions jurisdiction boundaries. These differences do not affect the accuracy of this FIFM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to shouture and gloods elevations enterenced to the same evential datum. For information regarding conversion between the National Geosteic Vertical Calum of 1929 and the North American Vertical Calum of 1988, will the National Geosteic Survey at the following address:

VGG Information Services VGA, Intr0312 National Geodetic Survey SSIRC-3, Alligot 1315 East Illegt Highway Sever Spring, Maryland 20910-3282 (201) 713-3242

To obtain current elevation, description, and/or location information for banch marks shown on this map, please contact the information Services Branch of the National Geodetic Survey at (381) 713-3342, or visit its website at <u>this inner non-non-non-</u>

Base map information shown on this FIRM was derived from the U.S.D.A.Farm Service National Agriculture ImageryProgram (NKP) dated 2014. Produced at scale of 1:24.000.

The profile baselines depicted on this mag represent the hydraulic modeling baselines that match the food purples in the FG report. As a neutral trimproved topographic data, the profile baseline, in some cases, may deviate significantly from the channel certainfield are appear outlob the SFHA.

Based on updated topographic information, this map reflects more detailed and up-to-date stream channel configurations and floodplain deliverations than those shown on the previous FIRM for this juraticitors. As a result the Flood Profiles and Floodpary Date tobins for multiple streams in the Flood Profiles and Floodpary Date tobins for multiple streams in the Flood insurance Study Report Interio contains autoritative ruphatele date) may inflood stream channel distances that other from what is shown on the map. Also, the road to floodplain instantionships for unrevised streams may differ from what is shown on previous maps.

Corporate levels shown on this map are based on the best data available at the time of publication. Because changes due to annexatives or de-annexatives may have occurred after this map was published, map users should contact appropriate community officials to unity current corporate limit locations.

Please refer to the separately printed Map index for an overview map of the county shouring the layout of map panels; community may expectely addresses, and a Listing of Communities table containing National Flood meurance Program dates for each community as well as a listing of the panels on which each community as incided.

For information on available products associated with this FPME voil the Map Service Center (MSC) vehicles al <u>Nuclimations</u> Available products may include providely abundi Limits of Mac Cange, a Ficial Invention Candin additional devices of this map. Many of these products can be ordered or obtained devices from the MSC website.



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Conservation Service

National Cooperative Soil Survey

Appendix C Soil Map

	MAP L	EGEND		MAP INFORMATION
Area of Intere A	est (AOI) area of Interest (AOI)	₩ ¢	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils Special Poi Special Poi Special Poi S Special Poi B S S S S S S S S S S S S S	Soil Map Unit Polygons Soil Map Unit Lines Soil Map Unit Points Soil Map Unit Points Soil Map Unit Points Soir Features Blowout Sorrow Pit Clay Spot Closed Depression Gravel Pit Scavel Pi	Water Fea Vater Fea Cransport	Very Stony Spot Wet Spot Other Special Line Features tures Streams and Canals ation Rails Interstate Highways US Routes Major Roads Local Roads	 Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detaile scale. Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data of the version date(s) listed below. Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 18, Sep 16, 2017 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jun 11, 2017—Se 22, 2017 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor
 Severely Eroded Spot Sinkhole Slide or Slip Sodic Spot 				

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	3.3	79.5%
10180	Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes	0.9	20.5%
Totals for Area of Interest		4.2	100.0%



Jackson County, Missouri

10082—Arisburg-Urban land complex, 1 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w7ld Elevation: 750 to 1,130 feet Mean annual precipitation: 39 to 45 inches Mean annual air temperature: 50 to 55 degrees F Frost-free period: 177 to 220 days Farmland classification: All areas are prime farmland

Map Unit Composition

Arisburg and similar soils: 61 percent
Urban land: 30 percent
Minor components: 9 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Arisburg

Setting

Landform: Interfluves Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam A - 6 to 13 inches: silt loam Bt - 13 to 19 inches: silty clay loam Btg - 19 to 56 inches: silty clay loam BCg - 56 to 79 inches: silty clay loam

Properties and qualities

Slope: 1 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.60 in/hr)
Depth to water table: About 18 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: High (about 11.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e

USDA

Hydrologic Soil Group: C *Ecological site:* Loess Upland Prairie (R107BY007MO) *Hydric soil rating:* No

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8 Hydric soil rating: No

Minor Components

Sharpsburg

Percent of map unit: 3 percent Landform: Ridges Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve Down-slope shape: Linear Across-slope shape: Linear Ecological site: Loess Upland Prairie (R109XY002MO) Hydric soil rating: No

Sampsel

Percent of map unit: 3 percent Landform: Hills Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Concave Ecological site: Interbedded Sedimentary Upland Savanna (R109XY010MO) Hydric soil rating: Yes

Greenton

Percent of map unit: 3 percent Landform: Hillslopes Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope Down-slope shape: Convex Across-slope shape: Convex Ecological site: Loess Upland Prairie (R109XY002MO) Hydric soil rating: No

Data Source Information

Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 18, Sep 16, 2017

Jackson County, Missouri

10180—Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1n85h Elevation: 600 to 900 feet Mean annual precipitation: 33 to 43 inches Mean annual air temperature: 50 to 57 degrees F Frost-free period: 175 to 220 days Farmland classification: All areas are prime farmland

Map Unit Composition

Udarents and similar soils: 41 percent Urban land: 39 percent Sampsel and similar soils: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udarents

Setting

Landform position (two-dimensional): Summit Landform position (three-dimensional): Crest Down-slope shape: Convex Across-slope shape: Convex Parent material: Mine spoil or earthy fill

Typical profile

C1 - 0 to 5 inches: silt loam C2 - 5 to 80 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.14 to 0.57 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Moderate (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: C Ecological site: Deep Loess Upland Prairie (R107BY002MO)

JSDA

Other vegetative classification: Mixed/Transitional (Mixed Native Vegetation) *Hydric soil rating:* No

Description of Urban Land

Setting

Landform: Interfluves Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve Across-slope shape: Convex

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8 Hydric soil rating: No

Description of Sampsel

Setting

Landform: Hillslopes Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Concave Across-slope shape: Convex Parent material: Residuum weathered from shale

Typical profile

Ap - 0 to 13 inches: silty clay loam *Bt - 13 to 80 inches:* silty clay

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C/D Ecological site: Wet Footslope Prairie (R112XY041MO) Other vegetative classification: Grass/Prairie (Herbaceous Vegetation)

USDA

Appendix D Drainage and Detention Calculations

MCPL EAST LEE'S SUMMIT - DRAINAGE CALCULATIONS

	STORM SEWER PIPE AND STRUCTURE TABLE																												
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		DIRECT	TOTAL	кс	TC FLOW		DESIGN Q		PIPE	PIPE F		PIPE	V FULL	DESIGN		MH TOP	UPSTREAM	DOWNSTREAM	DOWNSTREAM	1 FRICTION	ENTRY LOSS	ACTUAL	ENTRY	hf+hm	HW. INLET	. HW,		HYDRAULIC	1
FROM	TO	AREA	AREA	C (K=1.00)	(MIN) TIME	(IN/HP)	(CFS)	DESCRIPTION	LENGTH		DIA (CE	AREA	(E(C))		Hw/D	ELEVATION	FLOWLINE	FLOWLINE	WATER	HEAD (h f)	COEFFICIENT	ENTRY	LOSS (h m)	(FT)	CONTROL	OUTLET	GRADE	GRADE	Comments
		(ACRES)	(ACRES)		(MIN)) ` '			(L.F.)	(%)	IN) (Cr	(SQ.FT	.) (.,)	• (LOWENTE		ELEVATION		(k)	LOSS (k)	2000 ()	()	00111102	CONTROL	ELEV.	(MAX)	
RD3A		0.36		0.33 0.33	5.0 -	7.35	0.87	ADS BASINS/ROOF DRAINS								1020.20											1017.54	1019.20	↓
DDO	RD2	0.05	0.36	0.33 0.33	5.0 -	7.35	0.87	8 in. HDPE ADS BASINS/ROOF DRAINS	88.00	1.00	8 1.2	1 0.35	3.47	3.80	1.04	4000.00	1016.70	1015.82	1016.85	0.47	1.00	1.00	0.22	0.69	1017.40	1017.54	4040.05	4040.00	↓
RD2	RD1	0.25	0.04	0.41 0.41	5.0 -	7.35	0.75	ADS BASINS/ROOF DRAINS 10 in. HDPE	193.00	1.00	10 2.2	0.55	4.00	4.53	1.24	1020.20	1015.82	1013.89	1013.48	1.45	0.40	0.40	0.13	1.57	1010.05	1015.82	1016.85	1019.20	↓
DD1	RD1	0.10	0.61	0.42 0.42	0.0	7.35	0.66	JUNCTION BOX	193.00	1.00	10 2.2	0 0.55	4.03	4.53	1.24	1020.20	1015.82	1013.89	1013.48	1.45	0.40	0.40	0.13	1.57	1016.85	1015.82	1018.25	1010.00	łł
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B2	ΒZ	0.59	0.97	0.63 0.63	5.0 -	7.35	2.73	CURB INLET	92.14	4.00	10 12.	1.23	10.50	9.10	0.97	1017.86	1015.72	1012.02	1017.34	0.32	0.30	0.30	0.39	0.71	1010.94	1016.25	1013.48	1016.86	h
DZ	B1	0.55	1.56	0.67 0.67	50 -	7.35	7.68	18 in. HDPE	173.65	1.00	18 10	53 1.77	5.96	6.50	1 17	1017.00	1011.72	1009.98	1009.52	0.94	0.50	0.50	0.33	1.27	1013 48	1011.72	1013.40	1010.00	END SECTION TO BASIN
			1.00	0.01	0.0	1.55	1.00	IO III. HEI E					0.00	0.00			1011112	1000.00	1000.02	0.01	0.00	0.00	0.00		1010.10	1011112			
RD3B		0.26		0.39 0.39	5.0 -	7.35	0.75	ADS BASINS/ROOF DRAINS								1020.20							1 1				1017.33	1019.20	
	RD4			0.39 0.39		7.35	0.75	8 in. HDPE	67.00	1.00	8 1.2	1 0.35	3.47	3.64	0.94		1016.70	1016.01	1016.59	0.26	1.00	1.00	0.21	0.46	1017.33	1017.06			
RD4		0.00		0.39 0.39	5.0 -	7.35	0.00	ADS BASINS/ROOF DRAINS						1		1020.20													1
	RD1		0.26	0.39 0.39	5.0 -	7.35	0.75	8 in. HDPE	125.00	1.00	8 1.2	1 0.35	3.47	3.64	0.94		1016.01	1014.76	1017.54	0.48	0.40	1.00	0.21	0.69	1016.64	1018.23			
F1	BAS	0.53	0.53	0.75 0.75	5.0 -	7.35	2.92	FLUME																					
																													ļ
F2	BAS	0.45	0.45	0.80 0.80	5.0 -	7.35	2.65	FLUME																					l
=-																													l
F3	BAS	0.32	0.32	0.80 0.80	5.0 -	7.35	1.88	FLUME																					↓
																													<u> </u>
		1					1							07004			TRUCTURE	TABLE											<u></u>
0705140514	STORM SEWER PIPE AND STRUCTURE TABLE																												
TITLE: EAST																													
JOB #: 017-14		II LIDRAR I																											
DESIGN CO		> 100 VE					1 1		<u>г т</u>	1			1		1								r r		1	1			
STRUC	TIRES	5. 100 TE	ARSION			20	1		1 1								P	IPE DESIGN					1						<u> </u>
011100	UNEO	DIRECT	TOTAL		- FLOW	V			PIPE	PIPE F	IPF	PIPE		1					DOWNSTREAM	1	ENTRY LOSS	ACTUAL	<u>г г</u>		1	HW	HYDRAULIC	HYDRAULIC	l
FROM	то	AREA	AREA	C KC		INTENSITY		DESCRIPTION	LENGTH				V FULL	DESIGN	Hw/D	MH TOP	UPSTREAM	DOWNSTREAM	WATER	FRICTION	COEFFICIENT	ENTRY			HW, INLET		GRADE	GRADE	Comments
		(ACRES)	(ACRES)	(K=1.25)	(MIN) (MIN)		(CFS)		(L.F.)		IN) (CF	S) (SQ.FT	(F/S)	V (F/S)		ELEVATION	FLOWLINE	FLOWLINE	ELEVATION	HEAD (h f)	(k)	LOSS (k)	LOSS (h m)	(FT)	CONTROL	CONTROL	ELEV.	(MAX)	Commonia
RD3A		0.36	,	0.33 0.41	5.0 -	7.35	1.09	ADS BASINS/ROOF DRAINS						1		1020.20							1				1017.82	1019.20	
	RD2		0.36	0.33 0.41	5.0 -	7.35	1.09	8 in. HDPE	88.00	1.00	8 1.2	1 0.35	3.47	3.94	1.25		1016.70	1015.82	1016.85	0.73	1.00	1.00	0.24	0.97	1017.54	1017.82	_		
RD2		0.25		0.41 0.51	5.0 -	7.35	0.94	ADS BASINS/ROOF DRAINS								1020.20											1016.85	1019.20	
	RD1		0.61	0.42 0.53		7.35	2.35	12 in. HDPE	193.00	1.00	12 3.5	7 0.79	4.55	4.86	1.03		1015.82	1013.89	1013.90	0.85	0.40	0.40	0.15	1.00	1016.85	1015.82			
RD1		0.10		0.90 1.13	5.0 -	7.35	0.83	JUNCTION BOX								1020.20											1018.76	1019.20	
	B2		0.97	0.53 0.66	5.0 -	7.35	4.72	15 in. HDPE	92.14	4.00	15 12.	95 1.23	10.56	9.72	1.14		1015.72	1012.02	1017.82	0.50	0.30	0.30	0.44	0.94	1017.15	1018.76			
B2		0.59		0.63 0.79		7.35	3.41	CURB INLET								1017.86											1013.90	1016.86	l
	B1		1.56	0.67 0.84	5.0 -	7.35	9.60	18 in. HDPE	173.65	1.00	18 10.	53 1.77	5.96	6.74	1.45		1011.72	1009.98	1010.12	1.47	0.50	0.50	0.35	1.82	1013.90	1011.94			END SECTION TO BASIN
DDaD		0.00		0.00	5.0	2.35			└──┤				-			1000.00							├ ───┤			+	4047.40	4040.00	łł
RD3B	RD4	0.26		0.39 0.49 0.39 0.49	5.0 -	7.35	0.93	ADS BASINS/ROOF DRAINS 8 in. HDPE	67.00	1.00	0 4 7	1 0.35	2 47	3.84	1.10	1020.20	1016.70	1016.01	1016.68	0.40	1.00	1.00	0.23	0.63	1017 / 2	1017.31	1017.43	1019.20	łł
RD4	KD4	0.00	0.20	0.39 0.49		7.35	0.93	ADS BASINS/ROOF DRAINS	67.00	1.00	0 1.2	0.35	3.47	3.04	1.10	1020.20	1016.70	1016.01	1010.00	0.40	1.00	1.00	0.23	0.63	1017.43	1017.31	1018.80	1019.20	łł .
ND4	RD1	0.00	0.26	0.39 0.49	5.0 -	7.35	0.00	8 in. HDPE	125.00	1.00	8 12	1 0.35	3.47	3.84	1 10	1020.20	1016.01	1014.76	1017.82	0.76	0.40	1.00	0.23	0.98	1016 74	1018.80	1010.00	1019.20	<u> </u>
	NUT		0.20	0.39 0.49	5.0 -	1.55	0.85		120.00	1.00	0 1.2	0.35	3.47	3.04	1.10		1010.01	1014.70	1017.02	0.70	0.40	1.00	0.23	0.90	1010.74	1010.00		1	<u> </u>
F1	BAS	0.53	0.53	0.75 0.94	5.0 -	7.35	3.65	FLUME	1 1				-	1						1									l
	0/10	0.00	0.00	0.04	0.0	1.55	0.00	1 LOWE						1						1					1				ł
F2	BAS	0.45	0.45	0.80 1.00	5.0 -	7.35	3.31	FLUME					1	1						1	1		1 1			1	1	1	1
							1 1	-	1 1					1									1						1
F3	BAS	0.32	0.32	0.80 1.00	5.0 -	7.35	2.35	FLUME						1									1						1

MID CONTINENT PUBLIC LIBRARY - EAST LEE'S SUMMIT BRANCH DETENTION BASIN STAGE DISCHARGE 11-Apr-19

STAGE	ELEV	TOTAL DISCHARGE		ROM STRUCTURE WSE FOR	-	AND ELEVAT			ET PIPE FROM POND TO E WSE FOR DESIGN RELEASE	REMARK
			DESIG	N RELEASE RATE	FLOW THOUGH 1" PERF HOLES	THOUGH 1" THROUGH WSE			RATE	
		cfs	cfs	elev ft	cfs	cfs	elev ft	cfs	elev ft	
0	1003.30	0.00	0	1003.38	0	0	1003.30	0.00	1006.70	INVERT OF OUTLE T STRUCTURE
+0.70	1004.00	0.03	0.03	1003.46	0.03	0	1004.00	0.03	1006.78	
+1.70	1005.00	0.11	0.11	1003.91	0.11	0	1005.00	0.11	1006.86	
+2.70	1006.00	0.22	0.22	1003.90	0.22	0	1006.00	0.22	1006.88	
+3.70	1007.00	0.34	0.34	1003.91	0.34	0	1007.00	0.34	1007.23	
+4.70	1008.00	0.49	0.49	1003.91	0.49	0	1008.00	0.49	1007.54	
+5.10	1008.40	0.56	0.56	1003.93	0.56	0	1008.40	0.56	1008.35	BOTTOM OF WEIR
+5.69	1008.99	2.20	2.2	1004.06	0.92	1.28	1008.98	2.20	1008.99	2-Yr WSE
+5.70	1009.00	2.32	2.32	1004.48	0.65	1.67	1008.99	2.32	1009.00	
+6.13	1009.43	5.50	5.5	1004.62	0.98	4.52	1009.36	5.50	1009.43	10-Yr WSE
+6.70	1010.00	12.20	12.2	1006.56	1.02	11.18	1009.69	12.20	1010.00	
+7.02	1010.32	13.40	13.4	1006.26	1.08	12.32	1009.92	13.40	1010.32	100-Yr WSE
+7.70	1011.00	19.90	19.9	1008.35	1.11	18.79	1010.13	19.90	1011.00	

- INDICATES WSE CONTROL

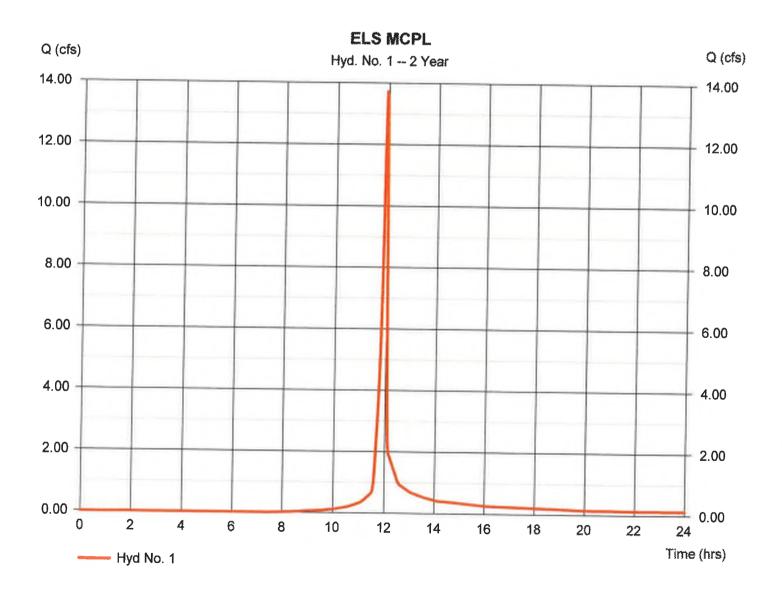
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No. 1

E	LS	Μ	C	P	L
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Hydrograph type= SCS RunoffStorm frequency= 2 yrsTime interval= 2 minDrainage area= 4.500 acBasin Slope= 0.0 %Tc method= UserTotal precip.= 3.27 inStorm duration= 24 hrs	Peak discharge Time to peak Hyd. volume Curve number Hydraulic length Time of conc. (Tc) Distribution Shape factor	 = 13.72 cfs = 11.93 hrs = 27,834 cuft = 90 = 0 ft = 5.00 min = Type II = 484 	
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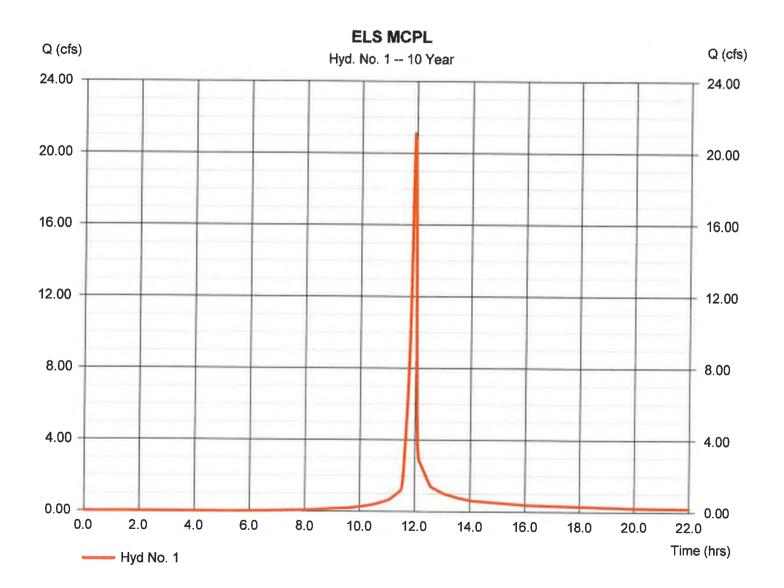
Wednesday, 02 / 13 / 2019



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No. 1

ELS MCPL			
Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration	 SCS Runoff 10 yrs 2 min 4.500 ac 0.0 % User 4.42 in 24 hrs 	Peak discharge Time to peak Hyd. volume Curve number Hydraulic length Time of conc. (Tc) Distribution Shape factor	 = 21.11 cfs = 11.93 hrs = 43,436 cuft = 90 = 0 ft = 5.00 min = Type II = 484



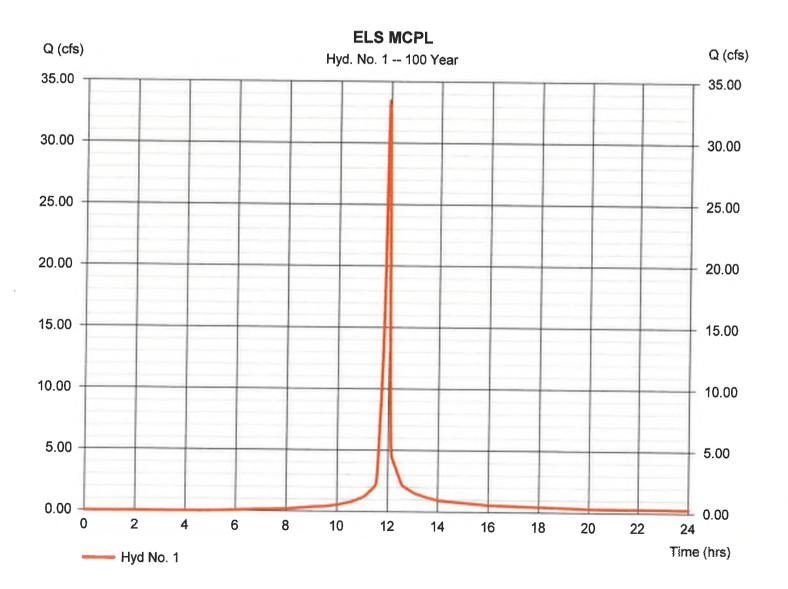
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No. 1

ELS	MCPL
-----	------

Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method	= SCS Runoff = 100 yrs = 2 min = 4.500 ac = 0.0 % = User	Peak discharge Time to peak Hyd. volume Curve number Hydraulic length Time of conc. (Tc)	= 33.45 cfs = 11.93 hrs = 70,523 cuft = 90 = 0 ft = 5.00 min
Tc method Total precip.	= User = 6.32 in		= 5.00 min
Storm duration	= 24 hrs	Shape factor	= Type II = 484

Wednesday, 02 / 13 / 2019



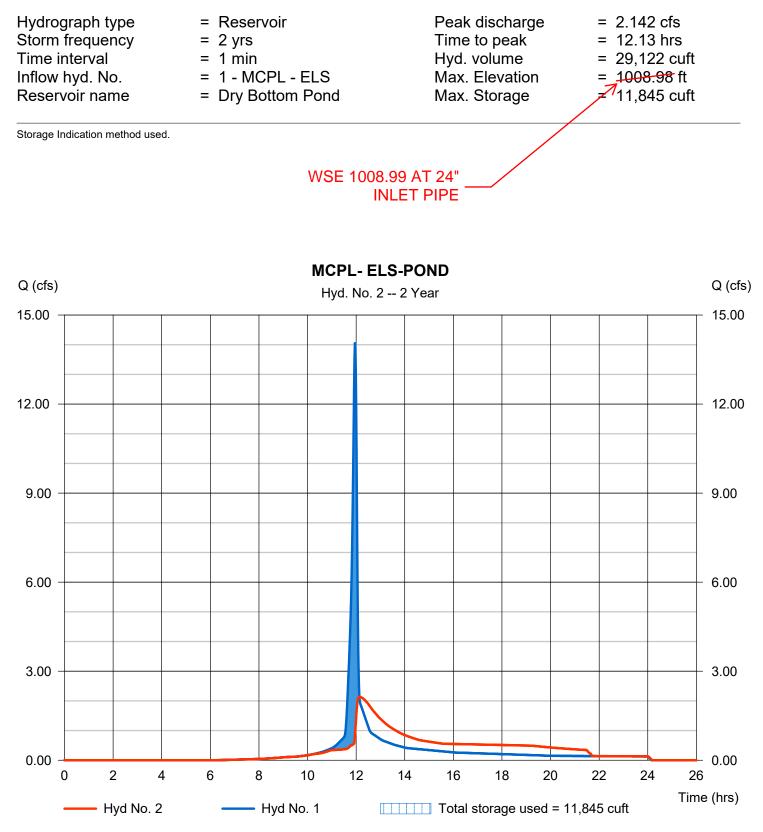
Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 04 / 16 / 2019

Hyd. No. 2

MCPL- ELS-POND



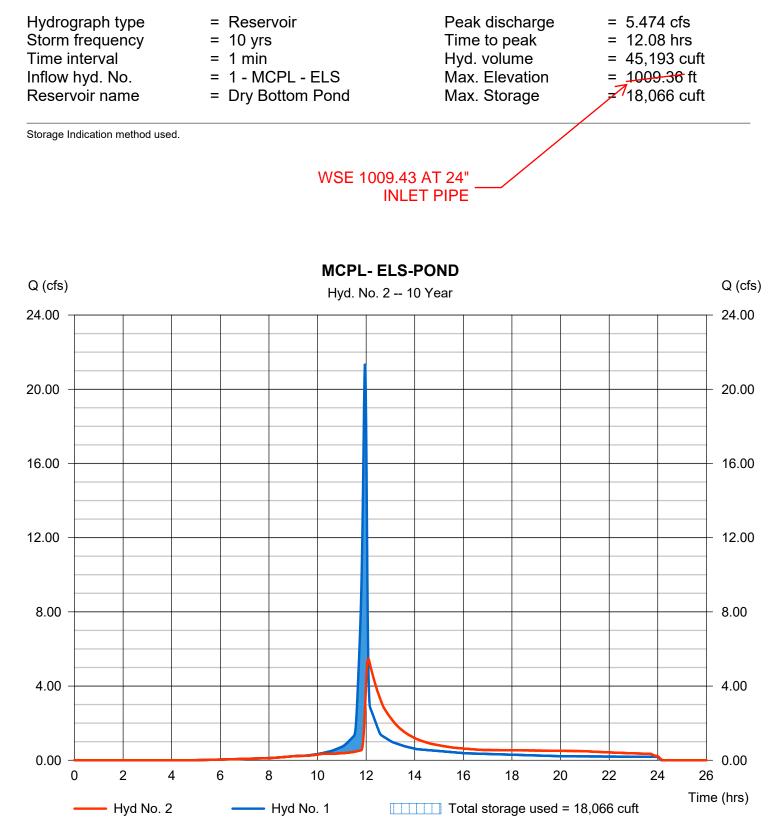
Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 04 / 16 / 2019

Hyd. No. 2

MCPL- ELS-POND



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 04 / 16 / 2019

0.00

26

Time (hrs)

24

Hyd. No. 2

0.00

0

2

Hyd No. 2

4

6

8

10

Hyd No. 1

12

16

14

18

Total storage used = 27,267 cuft

20

22

MCPL- ELS-POND

Hydrograph type Storm frequency Time interval Inflow hyd. No. Reservoir name	 Reservoir 100 yrs 1 min 1 - MCPL - ELS Dry Bottom Pond 	Peak discharge Time to peak Hyd. volume Max. Elevation Max. Storage	= 13.39 cfs = 12.07 hrs = 72,628 cuft = 1009.92 ft 27,267 cuft
Storage Indication method used.	WSE 1010.32	2 AT 24" ET PIPE	<u> </u>
Q (cfs)	MCPL- ELS	-POND	Q (cfs)
35.00	Hyd. No. 2 1	00 Year	35.00
30.00			30.00
25.00			25.00
20.00			20.00
15.00			15.00
10.00			10.00
5.00			5.00

MCPL EAST LEE'S SUMMIT STAGE/STORAGE CURVE

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Pond No. 1 - Dry Bottom Pond

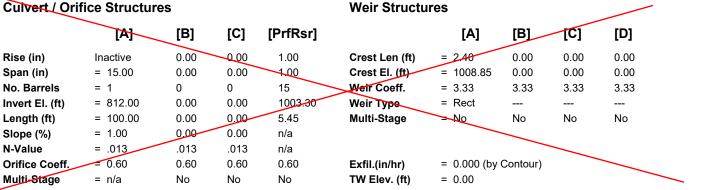
Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1003.30 ft

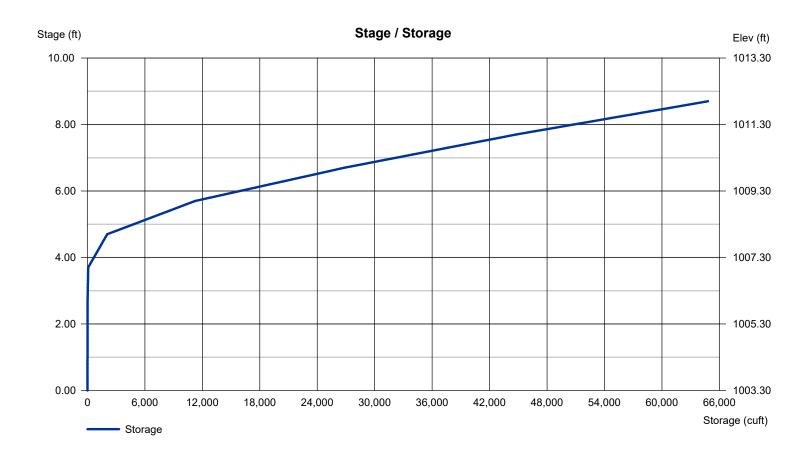
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	1003.30	00	0	0
0.70	1004.00	04	1	1
1.70	1005.00	04	4	5
2.70	1006.00	04	4	9
3.70	1007.00	160	63	72
4.70	1008.00	4,920	1,989	2,061
5.70	1009.00	14,260	9,184	11,245
6.70	1010.00	16,950	15,584	26,829
7.70	1011.00	18,940	17,934	44,763
8.70	1012.00	21,190	20,052	64,816

Culvert / Orifice Structures



Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

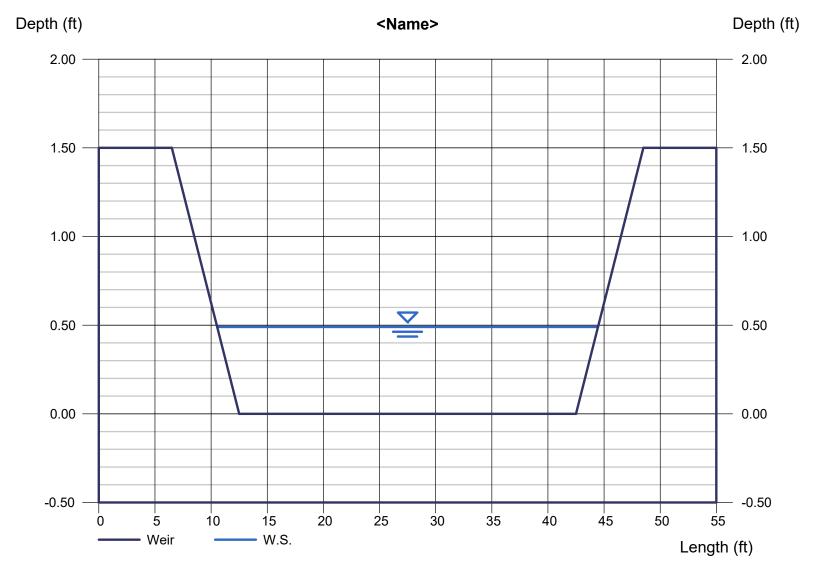


Weir Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

<Name>

Trapezoidal Weir		Highlighted	
Crest	= Broad	Depth (ft)	= 0.49
Bottom Length (ft)	= 30.00	Q (cfs)	= 33.40
Total Depth (ft)	= 1.50	Area (sqft)	= 15.66
Side Slope (z:1)	= 5.00	Velocity (ft/s)	= 2.13
		Top Width (ft)	= 33.92
Calculations			
Weir Coeff. Cw	= 3.10		
Compute by:	Known Q		
Known Q (cfs)	= 33.40		



Appendix E Water Treatment Calculations

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet - EDD-1

Project:	MCPL East Lee's Summit	Date:	01/18/2019		
Location:	Lee's Summit	Company:	Olsson		
Designer:	ТМР	Checked:	LWM		
I. Basin V	Vater Quality Volume				
Step 1:	Tributary area to EDDB, A _T (ac.)			A _T (ac) =	4.50
Step 2:	Calculate WQ_V using methodology in Section 6			WQ _V (ac-ft) =	0.29
Step 3:	Add 20 percent to account for silt and sediment basin	depositatior	in the $\$	/ _{DESIGN} (ac-ft) =	0.34
					14911.83
IIa. Wate	r Quality Outlet Type				
Stop 1:	Set water quality outlet type:				2
Step 1:	Set water quality outlet type: Type 1 = Single Orifice Type 2 = Perforated Riser or Plate Type 3 = V-Notch Weir			Outlet Type =	2
Step 2:	Proceed to part IIb, IIc, or IId based on water qu	uality outlet t	ype selected		
llb. Wate	r Quality Pool Outlet, Single Orifice				
Step 1:	Depth of water quality volume at outlet, $Z_{WQ}\ensuremath{\left(ft \right)}$			Z_{WQ} (ft) =	2.40
Step 2:	Average head of water quality volume over inve $H_{WQ} = 0.5 * Z_{WQ}$	ert of orifice,	H _{WQ} (ft)	H_{WQ} (ft) =	1.20
Step 3:	Average water quality outflow rate, Q_{WQ} (cfs) Q_{WQ} = (WQ _V * 43,560) / (40*3,600)			Q _{WQ} (cfs) =	0.09
Step 4:	Set value of orifice discharge coefficient, C_0 $C_0 = 0.66$ when thickness of riser/weir p $C_0 = 0.80$ when thickness of riser/weir p			C _O =	0.66
Step 5:	Water quality outlet orifice diameter (minimum o $D_0 = 12 * 2 (Q_{WQ} / (C_0 * p * (2 * g * H_{WC})))$ (if orifice diameter < 4 inches use outlet	$(2)^{0.5})^{0.5}$		D _o (in) =	1.65 Does not work
Step 6:	To size outlet orifice for EDDB with an irregular Worksheet	stage-volum	e relationship	use the Single	Orifice

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet

Project:	MCPL East Lee's Summit	Date:	01/18/2019		
Location:	Lee's Summit	Company:	Olsson		
Designer		Checked:	LWM		
5					
IIc. Wate	r Quality Outlet, Peforated Riser (Continued)				
Step 1:	Depth of water quality volume at outlet, $Z_{\rm WQ}$ (ft)			Z_{WQ} (ft) =	2.40
Step 2:	Recommended maximum outlet area per row, A $A_{O} = WQ_{V} / (0.013 * Z_{WQ}^{2} + 0.22 * Z_{WQ} - 0.02)$,		$A_{0}(in^{2}) =$	0.57
Step 3:	Circular perforation diameter per row assuming	a single col	umn, D _I (in)	D ₁ (in) =	1.00
Step 4:	Numbers of columns, n_c			n _c =	Use 1" 1.00
Step 5:	Design circular perforation diameter (from 1 to 2	2 inches), D _r	_{Perf} (in)	D _{Perf} (in) =	1.00
Step 6:	Horizontal peforation column spacing when n_c > If D_{Perf} is not > or = 1, S_c = 4	· 1, center to	o center, S _c	S _c =	NA
Step 7:	Number of rows, 4" vertical spacing between pe	rforations, c	enter to center,	n _r =	7
IIc. Wate	r Quality Outlet, V-Notch Weir				
Step 1:	Depth of water quality volume above permanent	t pool, Z _{WQ} (ft)	Z_{WQ} (ft) =	NA
Step 2:	Average head of water quality pool volume over H_{WQ} = 0.5 * Z_{WQ}	invert of v-r	notch H _{WQ} (ft)	H _{WQ} (ft) =	NA
Step 3:	Average water quality pool outflow rate, Q_{WQ} (cf Q_{WQ} = (WQ _V * 43,560) / (40*3,600)	s)		Q_{WQ} (cfs) =	NA
Step 4	V-notch weir coefficient, C_v			C _v =	NA
Step 5:	V-notch weir angle, q (deg) $\theta = 2 * (180/ \pi) * \arctan(Q_{WQ} / (C_v * H_{WQ}^5))$ V-notch angle should be at least 20 deg 20 degrees if calculated angle is smalle	rees. Set to		q (deg) = _	NA
Step 6:	V-notch weir top width, W_v (ft) $W_v = 2^* Z_{WQ} * TAN(\theta/2)$			W_v (ft) =	NA

Step 7: To calculate v-notch angle for EDW with an irregular stage-volume relationship, use th V-notch Weir Worksheet

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet

Project:	MCPL East Lee's Summit	Date:	01/18/2019
Location:	Lee's Summit	Company:	Olsson
Designer:	ТМР	Checked:	LWM

III. Flood Control

Refer to APWA Specifications Section 5608

IV. Trash Racks

Step 1:	Total outlet area, A _{ot} (in ²)	A_{ot} (in ²) =	5.46
Step 2:	Required trash rack open area, A_t (in ²) $A_t = A_{ot} * 77 * e^{(-0.124 *D)}$ for single orifice outlet	A_t (in ²) =	60.83
	$A_t = (A_{ot} / 2) * 77 * e^{(-0.124*D)}$ for orifice plate or perforated riser outlet		
	At = 4 * A_{ot} for v-notch weir outlet		

V. Basin Shape

Step 1:	Length to width ratio should be at least 3:1 (L:W) wherever practica	ble (L:W) =	10:1 Plus
Step 2:	Low flow channel side lining	Concrete: Soil/Riprap: No low flow channel:	Yes NA NA
Step 3:	Top stage floor drainage slope (toward low flow channel), $S_{TS}~(\%)$ Top stage depth, $D_{TS}~(ft)$	S _{TS} (%) = D _{TS} (ft) =	2.00 5.00
Step 4:	Bottom stage volume, V _{BS} (ac-ft)	V _{BS} (% of WQ _V) = V _{BS} (ac-ft) =	0.33

VI. Forebay (Optional)

Step 1:	Volume should be greater than 10% of WQ $_{\rm V}$	Min Vol _{FB} (ac-ft) =	NA
Step 2:	Forebay depth, Z _{FB} (ft)	Z_{FB} (ft) =	NA
Step 3:	Forebay surface area, A _{FB} (ac)	A _{FB} (ac) =	NA
Step 2:	Paved/hard bottom and sides?		NA