# LEE'S SUMMIT DOWNTOWN MARKET DRAINAGE STUDY

Lee's Summit, Missouri

#### Prepared for:

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# 1. GENERAL INFORMATION

The Lee's Summit Downtown Market is a proposed commercial development on approximately 6 acres. The project is located in the downtown area of Lee's Summit, MO located east of City Hall. The project lies in the southwest 1/4 of Section 5, Township 47N, Range 31W, in Jackson County, Lee's Summit, Missouri.

#### 1.1. Project Location

The Lee's Summit Downtown Market development is located entirely in the city of Lee's Summit, Missouri. The area to be developed is bounded by City Hall and Douglas Street to the West, SE 2<sup>nd</sup> St to the North, SE Johnson Street to the East, SE 3<sup>rd</sup> Street to the South. The site ultimately discharges to the northeast, through public storm sewer, into a drainage ditch, ultimately discharging into Lake Jacomo.



Figure 1. Lee's Summit Downtown Market Location Map.

# 1.2. Federal Emergency Management Agency Floodplain Classification

FEMA Flood Boundary and Floodway Map Community Panel Number 29095C0436G classifies the Lee's Summit Downtown Market property as a "Zone X Unshaded" Area. This is the FEMA flood insurance rate zone that corresponds to areas outside the 0.2% annual chance floodplain. No Base Flood Elevations or depths are shown within this zone. Refer to Appendix F for the FIRM Map.

#### 1.3. Soil Classifications

Soil maps published on the Natural Resources Conservation Service (NRCS) Web Soil Survey categorize soils on the Lee's Summit Downtown Market as shown in Table 1. Refer to Appendix E for a map of soils on the property.

**Table 1. Soil Classifications** 

HSG	Symbol	Name	Slope
С	10082	Arisburg-Urban land complex	1-5%
D	10128	Sharpsburg-Urban land complex	2-5%
С	10180	Udarents-Urban land-Sampsel complex	2-5%
С	10181	Udarents-Urban land-Sampsel complex	5-9%
D	99012	Urban land	5-9%

## 2. METHODOLOGY

The storm drainage study will be analyzed in accordance with the February 15, 2006 edition of the Kansas City Metropolitan Chapter, American Public Works Association, (KCAPWA) Construction and Material Specifications, Section 5601.5.A.4.

The Existing Conditions hydrology will be evaluated in Section 3, and Proposed Conditions hydrology will be computed in Section 4. The Proposed Conditions discharge data for each stage of development will be compared to the Existing Conditions results; variations in quantity and rate of stormwater discharge between these models will represent the hydrologic impact generated by the proposed development. The overall stormwater management plan will be designed utilizing this information. Section 3 assumes current land use within the tributary subwatersheds, and pre-development conditions within the project boundary. Section 4 assumes completion of the entire development. The program used is Autodesk Storm & Sanitary Analysis 2018 (SSA).

The following methods were used in this study to model Existing, Proposed (Micro) and Future (Macro) Conditions in for stormwater runoff:

- NRCS TR-55 Unit Hydrograph Method
- 1-,10-, and 100-year Return Frequency, 24-hr. Storm Precip. Depths (TP-40)
- ARC Type II Soil Moisture Conditions
- 24-Hour NRCS Type II Rainfall Distribution
- Runoff Curve Numbers per NRCS TR-55 (Tables 2-2a 2-2c) and KCAPWA Section 5602.3
- NRCS TR-55 Methods for determination of Time of Concentration and Travel Time.

  NOTE: SSA models use "Time of Concentration" rather than "Lag Time" for computing subarea hydrology.

City code follows the February 16, 2011 version of APWA 5600, requiring comprehensive control to reduce flows to maximum allowable release rates. However, after conversations with the city, reaching maximum allowable release rates will cause an undue burden on the project, and a goal has been set of reducing post-development flows to pre-development rates.

Stormwater runoff models were created for the 1%, 10%, and 100% design storm events. The precipitation depths used in the analyses have been interpolated from the NOAA Atlas 14, Volume 8, Ver. The following Table 2 summarizes the rainfall depths used in this analysis:

**Table 2. Precipitation Depths.** 

Return Period	24-Hour Precipitation Depth (in.)
Water Quality Volume	1.37
1-Year (100% Storm)	3.10
2-Year (50% Storm)	3.71
10-Year (10% Storm)	5.67
100-Year (1% Storm)	9.25

## 3. EXISTING CONDITIONS

To quantify the effects of development of this project, the following area and point of interest has been used for Existing and Proposed Conditions analyses. See Exhibit 301 in Appendix A, Existing Macro Conditions Drainage Area Map.

**Watershed A** discharges to the northeast through public storm sewer systems. The drainage boundaries begin around SW Market Street, collecting into the public storm sewer, and traveling east. The flows collected are routed through our proposed site, ultimately discharging into a concrete drainage ditch to the northeast of the site. Total area modeled within this watershed is 133.48 acres, 5% of which is within the Lee's Summit Market site and considered "onsite". **Area A** is the entirety of the watershed, excepting the undeveloped, grassed area on the SE corner of SE 2<sup>nd</sup> St and SE Johnson St. **Undeveloped Area** is the grassed area that will be developed in the proposed conditions. **Outfall A** is the location where Watershed A discharges into a concrete lined channel that contributes to Tributary P4 to Prairie Lee Lake.

The following table summarizes the results of the Existing Conditions analysis. The Proposed Conditions data will be compared to these results in Section 4 of this report. Refer to Appendix D for output from and a schematic of the Existing Conditions model.

Curve Numbers were assumed as follows:

Table 3-1. Lee's Summit Downtown Market – Existing Conditions Subarea

Cover Type	Soil Type	CN Value
Single-Family Residential	С	83
	D	87
Urban Commercial	С	94
	D	95
Multi-Family Residential	С	90
Impervious Pavement	Any	98
Turf	D	84

The following tables summarize the results of the Existing Conditions analysis. The Proposed Conditions data will be compared to these results in Sections 4 of this report. Refer to Appendix D for output from and a schematic of the Existing Conditions model.

Table 3-2. Lee's Summit Downtown Market – Existing Conditions Subarea

Subarea	Area (acres)	T <sub>c</sub> (hours)	Weighted Curve Number
A-1	132.96	0.431	91.58
Undeveloped	0.52	0.083	84

Table 3-3 Lee's Summit Downtown Market – Existing Conditions Subarea Results

Subarea	WQv (cfs)	V <sub>wQv</sub> (ac-ft)	Q <sub>1</sub> (cfs)	V <sub>R-1</sub> (ac-ft)	Q <sub>2</sub> (cfs)	V <sub>R-2</sub> (ac-ft)	Q <sub>10</sub> (cfs)	V <sub>R-10</sub> (ac-ft)	Q <sub>100</sub> (cfs)	V <sub>R-100</sub> (ac-ft)
A-1	85.12	7.41	279.69	24.56	349.78	31.00	574.93	52.07	977.27	91.20
Undeveloped	0.25	0.02	1.32	0.07	1.74	0.09	3.14	0.17	5.72	0.32

<sup>\*</sup> cfs - cubic feet per second

Table 3-4 Lee's Summit Downtown Market – Existing Conditions Outfall Results

Outfall		V <sub>wqv</sub> (ac-ft)			Q <sub>2</sub> (cfs)			V <sub>R-10</sub> (ac-ft)		V <sub>R-100</sub> (ac-ft)
Α	85.16	7.43	279.96	24.63	350.13	31.09	575.48	52.24	978.28	91.52

#### 4. PROPOSED CONDITIONS

The Future Conditions section of analysis assumes completion of the Lee's Summit Downtown Market site. The mixed-use site includes construction of a multi-story apartment complex, openair market area, commercial buildings, and associated parking and utilities.

#### 4.1. PROPOSED CONDITIONS

The proposed developments will result in no changes in tributary areas on the site. The impervious area onsite will increase due to the construction of the Market. Area A is unchanged, as the offsite area is unchanged. The onsite area in Area A is already developed, and redevelopment of that area will not alter the land use, as it will remain Urban Commercial.

The following tables summarize the results of the Future Conditions analysis for the revised subareas within Watershed A. Tables 4-2 and 4-3 assume no detention is provided, to demonstrate the effects of development in this watershed. Refer to Appendix A for outputs from the Proposed Conditions SSA model.

Table 4-1. Lee's Summit Downtown Market - Proposed Conditions Subarea Data

Subarea	Area (acres)	T <sub>c</sub> (hours)	Weighted Curve Number
A-1	132.96	0.431	91.58
Undeveloped	0.52	0.083	95

**Table 4-2** Lee's Summit Downtown Market –Proposed (No Detention) Conditions Subarea Results

Subarea	WQv (cfs)	V <sub>wQv</sub> (ac-ft)	Q <sub>1</sub> (cfs)	V <sub>R-1</sub> (ac-ft)	Q <sub>2</sub> (cfs)	V <sub>R-2</sub> (ac-ft)	Q <sub>10</sub> (cfs)	V <sub>R-10</sub> (ac-ft)	Q <sub>100</sub> (cfs)	V <sub>R-100</sub> (ac-ft)
A-1	85.12	7.41	279.69	24.56	349.78	31.00	574.93	52.07	977.27	91.20
Undeveloped	0.73	0.06	1.97	0.11	2.40	0.14	3.78	0.22	6.25	0.38

Table 4-3 Lee's Summit Downtown Market –Proposed (No Detention) Conditions Outfall Results

Outfall		V <sub>WQv</sub> (ac-ft)	Q <sub>1</sub> (cfs)		Q <sub>2</sub> (cfs)			V <sub>R-10</sub> (ac-ft)		V <sub>R-100</sub> (ac-ft)
Α	85.25	7.47	280.06	24.67	350.22	31.14	575.55	52.29	978.38	91.58

The following table compares the results of the Proposed Conditions analysis to the Existing Conditions from Section 3 at Outfall A. Positive values indicate an increase from Existing to Proposed conditions, while negative values indicate a decrease.

Table 4-4. Lee's Summit Downtown Market -Proposed (No Detention) vs. Existing Conditions Point of Interest Comparison

Point of Interest	WQv (cfs)	V <sub>WQv</sub> (ac-ft)		V <sub>R-1</sub> (ac-ft)			Q <sub>10</sub> (cfs)		Q <sub>100</sub> (cfs)	V <sub>R-100</sub> (ac-ft)
Undeveloped	+0.48	+0.04	+0.65	+0.04	+0.66	+0.05	+0.64	+0.05	+0.53	+0.06
Outfall A	+0.09	+0.04	+0.10	+0.04	+0.09	+0.05	+0.07	+0.05	+0.10	+0.06

As can be seen in the previous table, the flows from the undeveloped area increases noticeably, while the final Outfall A has negligible increases in peak flow. This occurs due to the peak from the undeveloped area having a significantly lower time of concentration, traveling through the system before the peak arrives from the upstream areas. To mitigate for the increases shown in the previous table, detention will be provided within the previously undeveloped area, to be constructed as part of the private development. Detention is intended to be constructed via underground isolator rows that will treat flows from the proposed developed site. The majority of Watershed I flows into the proposed basin, with a portion bypassing it.

The below table shows results for the proposed isolator rows.

Table 4-5. Lee's Summit Downtown Market – Future Conditions Detention Basin Flow and Volume Results

Storm Event	Peak Q In (cfs)	TP In (hr)	Peak Q Out (cfs)	TP Out (hr)	Peak W.S.E. (ft)	Stored Volume (ac-ft)
WQv	0.73	11.93	0.02	14.73	101.10	0.039
1-Year	1.97	11.93	0.21	12.26	101.89	0.064
2-Year	2.40	11.93	0.25	12.38	102.22	0.079
10-Year	3.78	11.93	0.35	12.44	103.27	0.125
100-Year	6.25	11.93	1.05	12.14	105.53	0.191

The following table shows the results of the points of interest that are impacted by the constructed basin.

Table 4-6. Lee's Summit Downtown Market -Proposed (With Detention) Conditions Point of Interest Results

Outfall							Q <sub>10</sub> (cfs)	V <sub>R-10</sub> (ac-ft)	Q <sub>100</sub> (cfs)	
Α	85.10	7.47	279.90	24.67	350.02	31.14	575.24	52.29	978.22	91.58

The following table compares the results of the Proposed Conditions analysis with the detention described above to the Existing Conditions from Section 3.

Table 4-7. Lee's Summit Downtown Market –Proposed (With Detention) vs. Existing Conditions Point Data

Subarea	WQv (cfs)	V <sub>wqv</sub> (ac- ft)	Q₁ (cfs)	V <sub>R-1</sub> (ac-ft)	Q <sub>2</sub> (cfs)	V <sub>R-10</sub> (ac-ft)	Q <sub>10</sub> (cfs)	V <sub>R-10</sub> (ac- ft)	Q <sub>100</sub> (cfs)	V <sub>R-100</sub> (ac-ft)
Undeveloped	-0.23	+0.04	-1.11	+0.04	-1.49	+0.05	-2.79	+0.05	-4.67	+0.06
Outfall A	-0.06	+0.04	-0.06	+0.04	-0.11	+0.05	-0.24	+0.05	-0.06	+0.06

As shown in the table above, the proposed underground isolator system reduces flows in the WQv, 1-, 2-, 10- and 100-year storms to below pre-development conditions at Outfall A.

# 5. RESULTS

As shown in the discussion and tables in the previous sections, the proposed detention basin adequately reduces the peak stormwater rates and do not negatively impact downstream areas. Table 6-1 below, summarizes the Proposed and Future Conditions results and compares them with Existing conditions.

Table 6-1 Lee's Summit Downtown Market -Points of Interest Discharge Comparison

Outfall	Condition	Q <sub>wqv</sub> (cfs)	Q₁ (cfs)	Q <sub>2</sub> (cfs)	Q <sub>10</sub> (cfs)	Q <sub>100</sub> (cfs)
	Existing	85.16	279.96	350.13	575.48	978.28
Outfall A	Proposed	85.10	279.90	350.02	575.24	978.22
, ,	Difference	-0.06	-0.06	-0.11	-0.24	-0.06

# 6. CONCLUSION

This Stormwater Drainage Study has been prepared for the proposed project to establish a comprehensive stormwater management plan for the site. The results of this analysis demonstrate that the proposed stormwater management plan for the project achieves compliance the stated goal of reducing peak flows for the WQv, 1-year, 2-year, 10-year and 100 year storm events to below the existing peak flow rates. As mentioned in Section 2, a waiver is requested to achieve pre-vs-post reduction, without achieving allowable rates, per APWA 2011.Based on information received, Olsson requests that this stormwater drainage report be approved.

# **APPENDIX A**

Exhibits

USER: 

PROJECT BOUNDARIES	

LAND COVER LEGEND							
	TREATMENT						
	UNDEVELOPED						
	SINGLE FAMILY RESIDENTIAL						
	COMMERCIAL						
	MULTI FAMILY RESIDENTIAL						
	PAVEMENT	0.40					



OLSSON - CIVIL ENGINEERING MISSOURI CERTIFICATE OF AUTHORITY #

PROJECT NO: 022-03930 DRAWN BY: DFG DATE: 05/05/2023

**EXISTING CONDITIONS** 

1301 Burlington Street North Kansas City, MO 64116 TEL 816.361.1177

**EXHIBIT** 

EX-301

F:\2022\00001-00500\022-00393\40-Design\Reports\GNCV\Appendix A - Exhibit\Micro Proposed Drainage Areas.dwg May 10, 2023 10:46am XREFS: V\_XTOPO\_02200393 STORM\_LINES\_ExportCAD C\_PSTRM\_02200393

DWG: DATE:

PROJECT BOUNDARIES

LAND COVER LEGEND							
	TREATMENT						
	SINGLE FAMILY RESIDENTIAL	35.72					
	COMMERCIAL						
	MULTI FAMILY RESIDENTIAL	3.11					
	PAVEMENT	0.40					



OLSSON - CIVIL ENGINEERING MISSOURI CERTIFICATE OF AUTHORITY #

PROJECT NO: 022-03930 DRAWN BY: DFG DATE: 05/05/2023

PROPOSED CONDITIONS

olsson

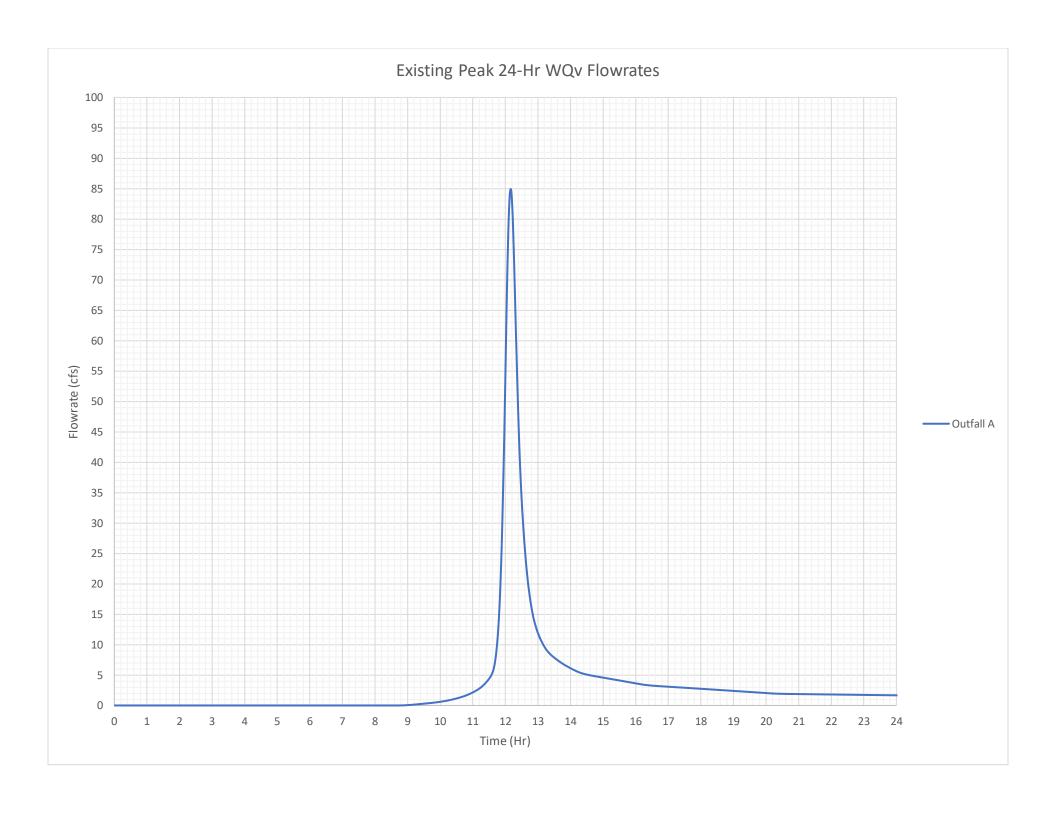
1301 Burlington Street North Kansas City, MO 64116 TEL 816.361.1177

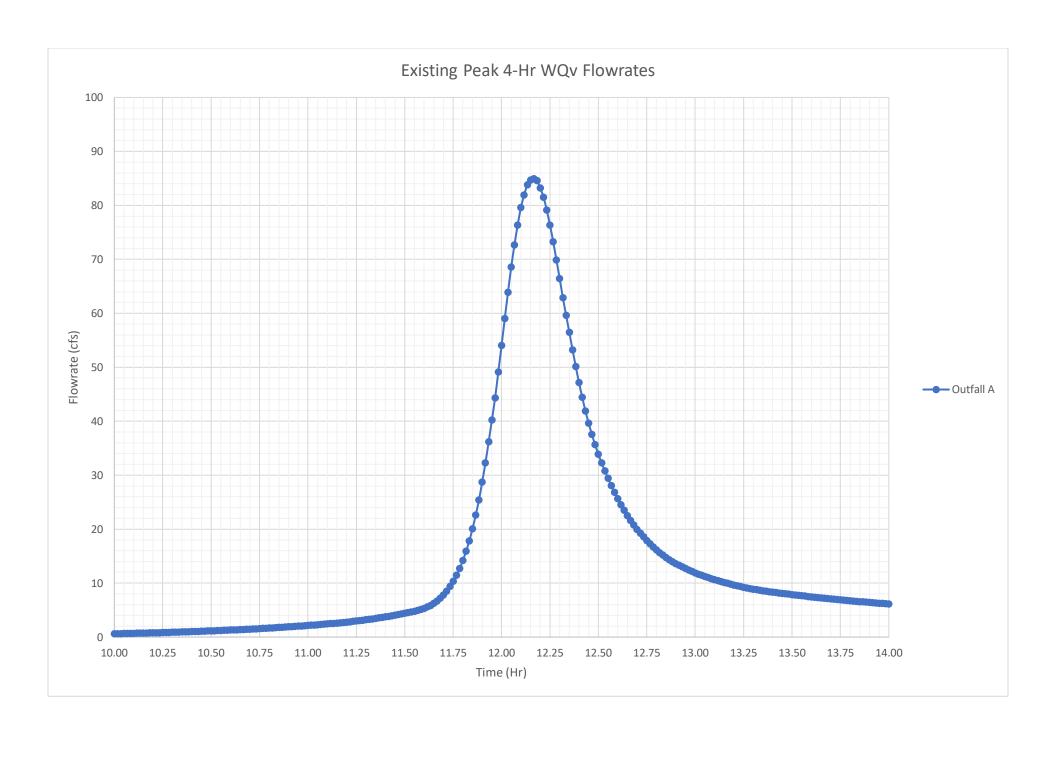
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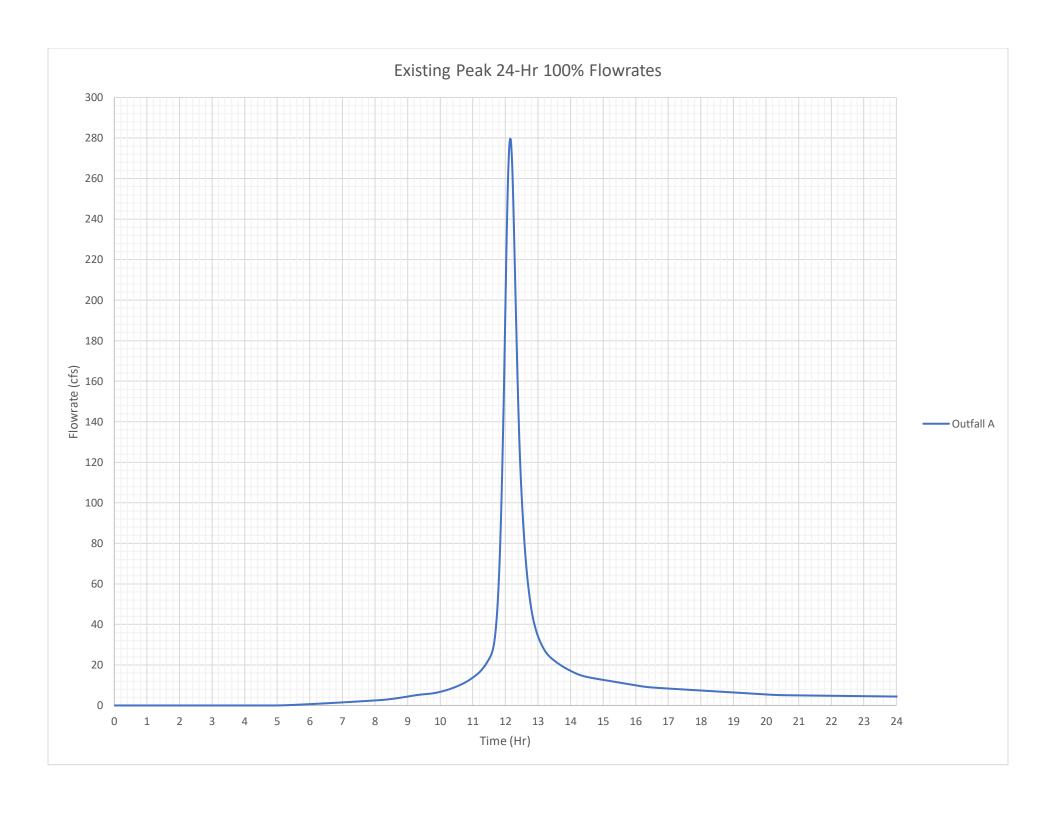
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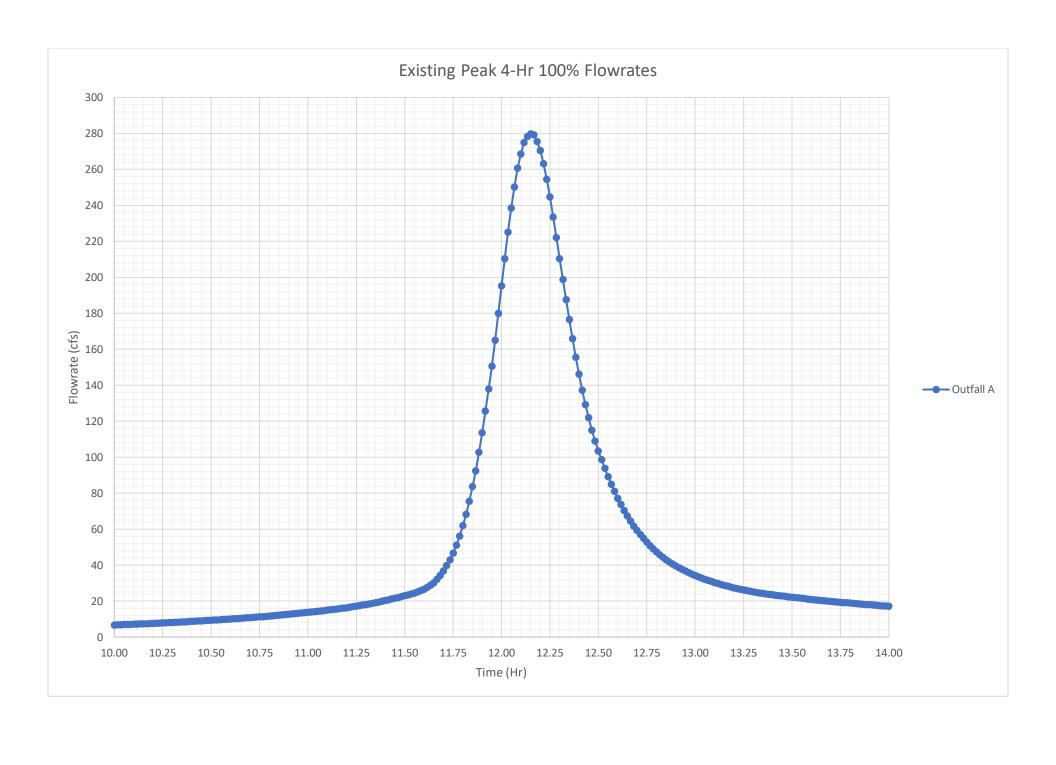
# **APPENDIX B**

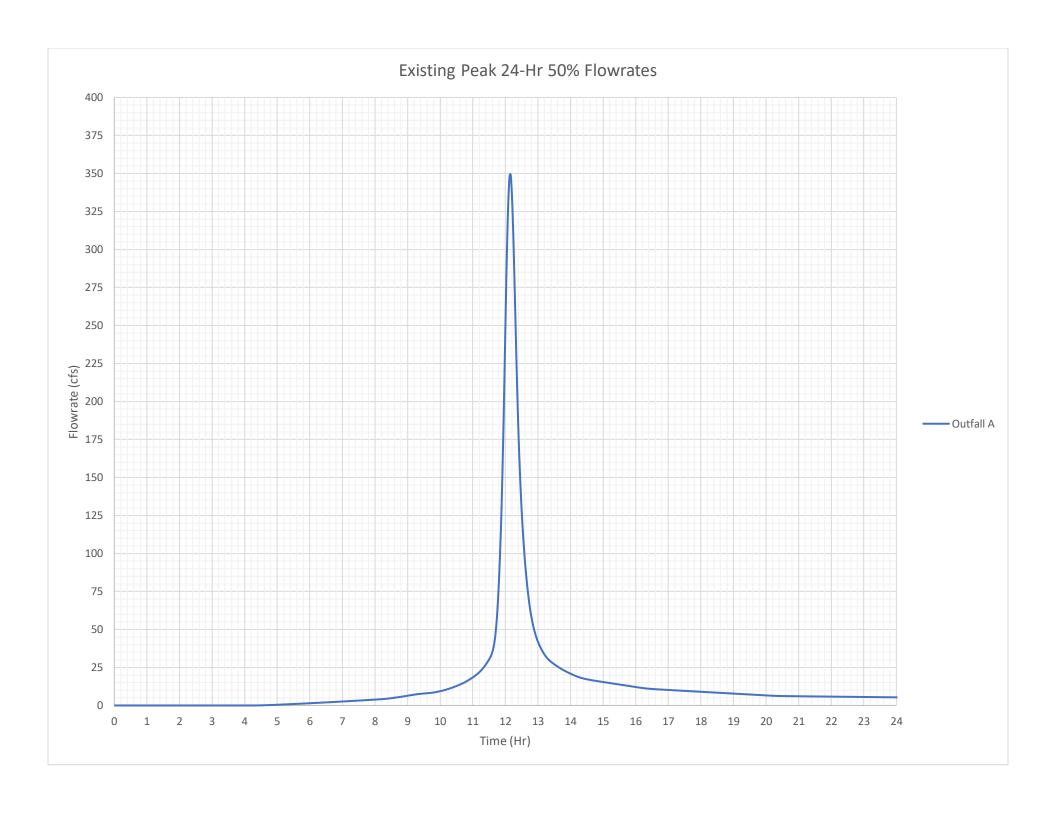
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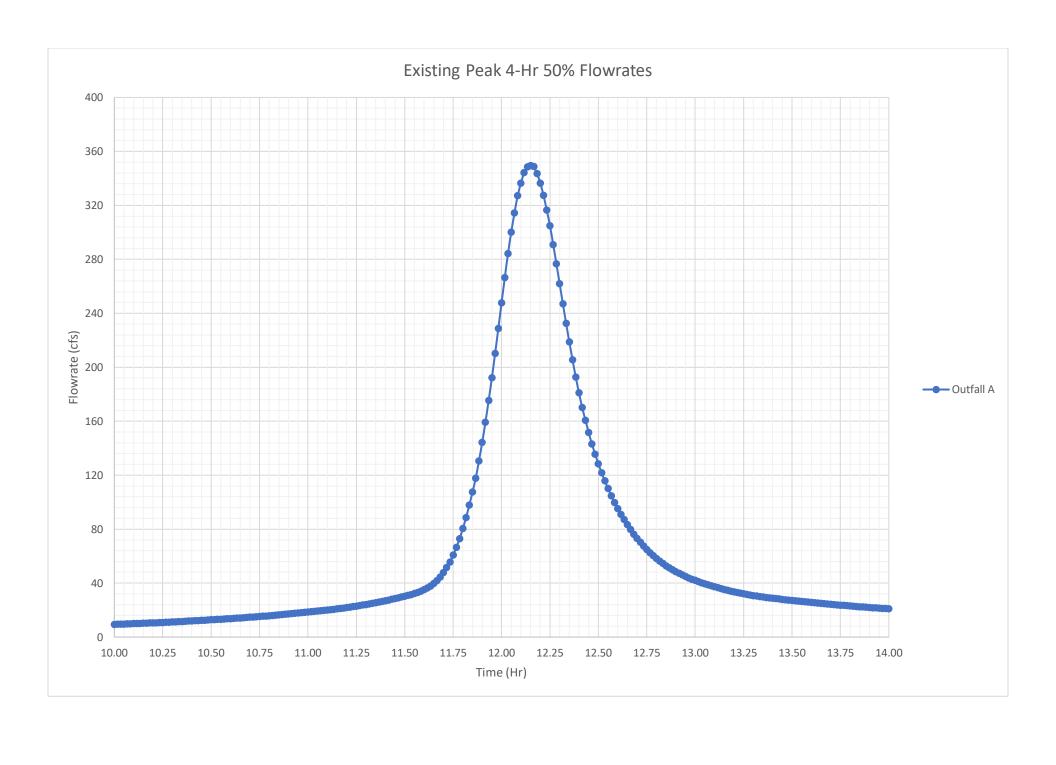


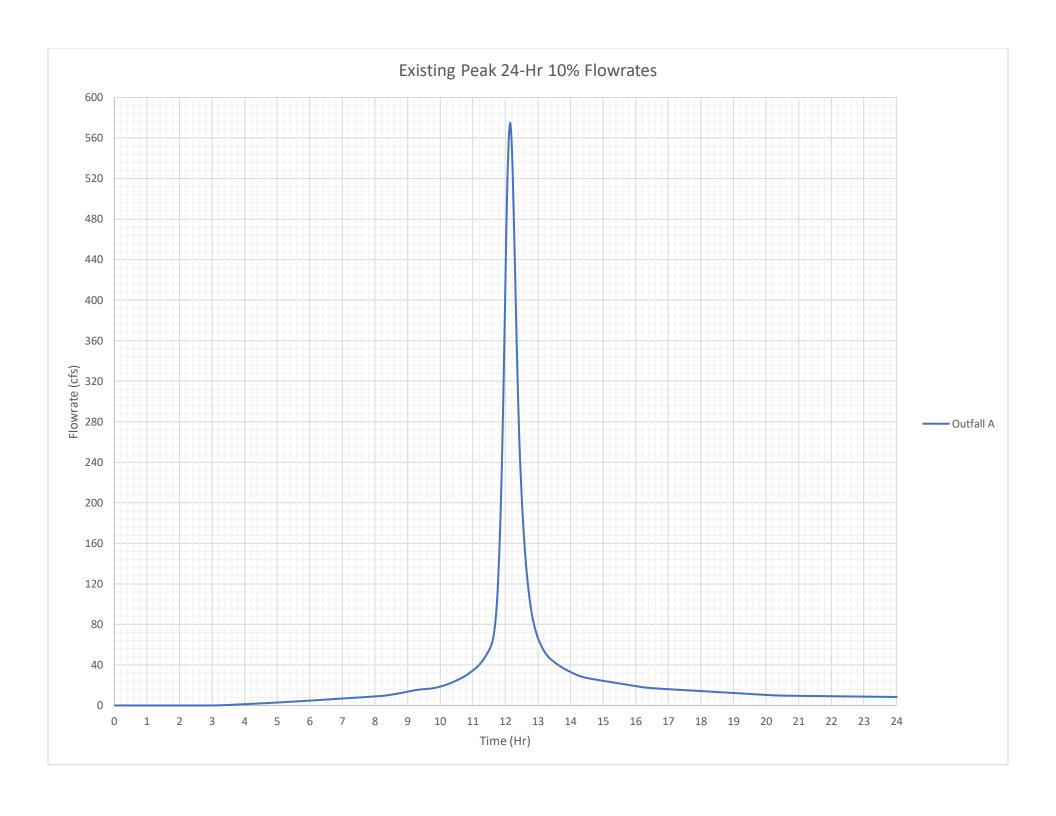


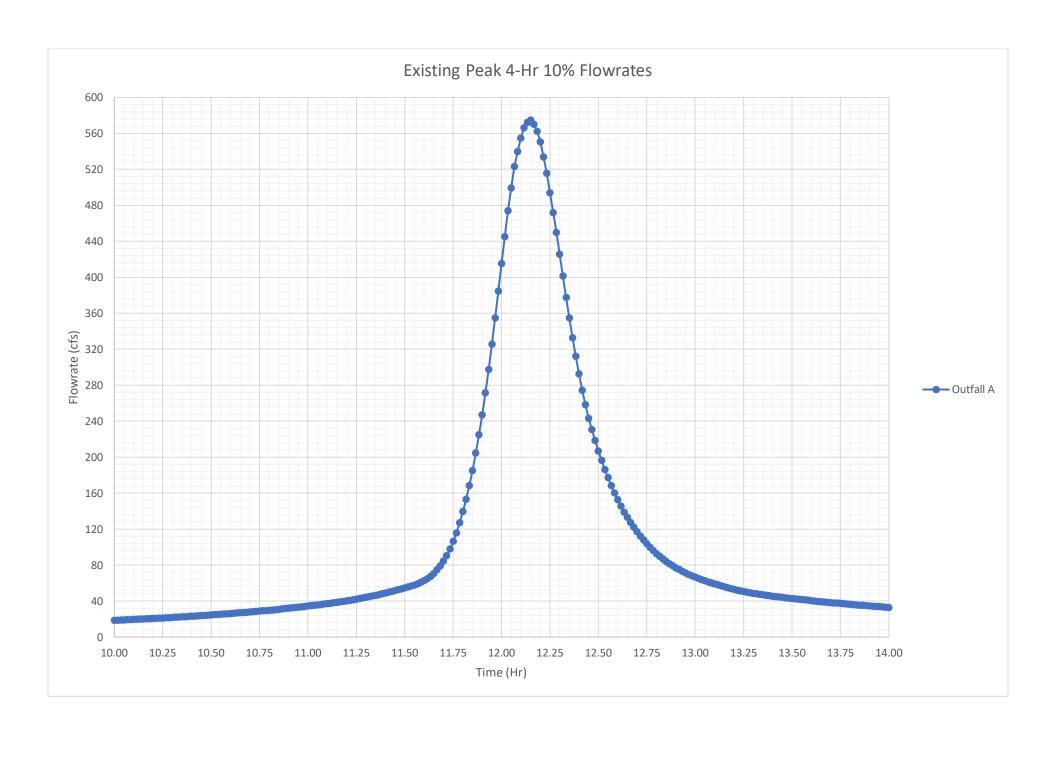


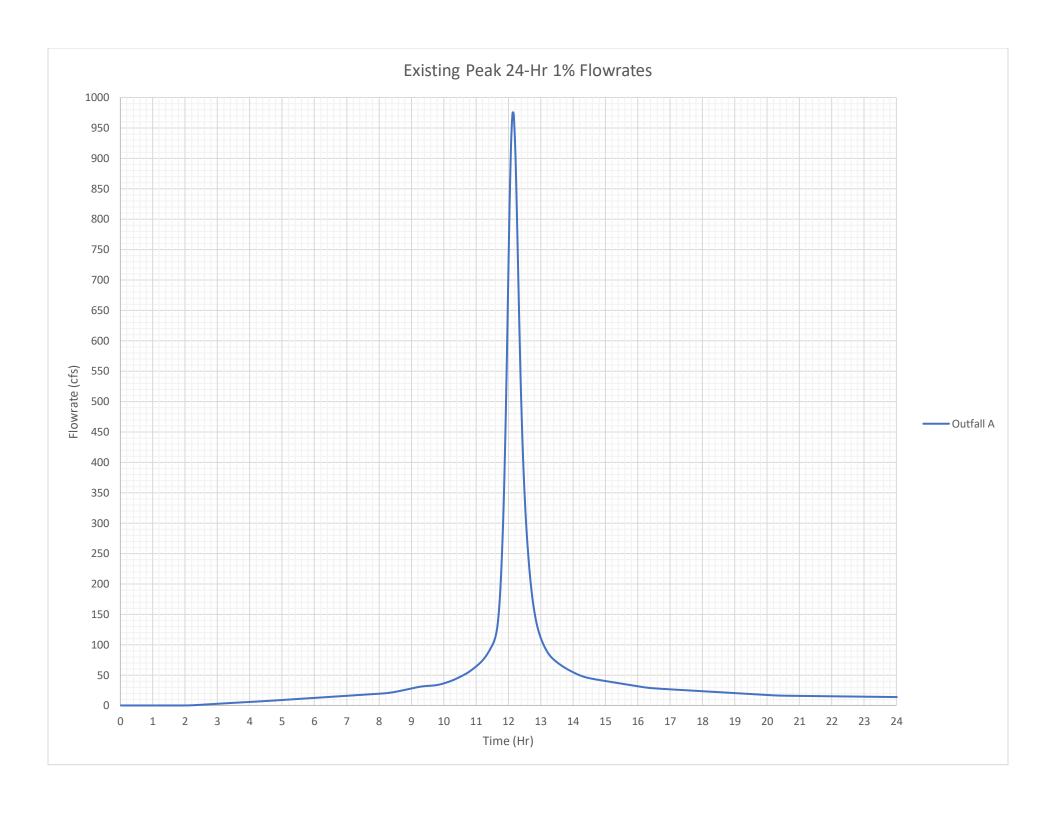


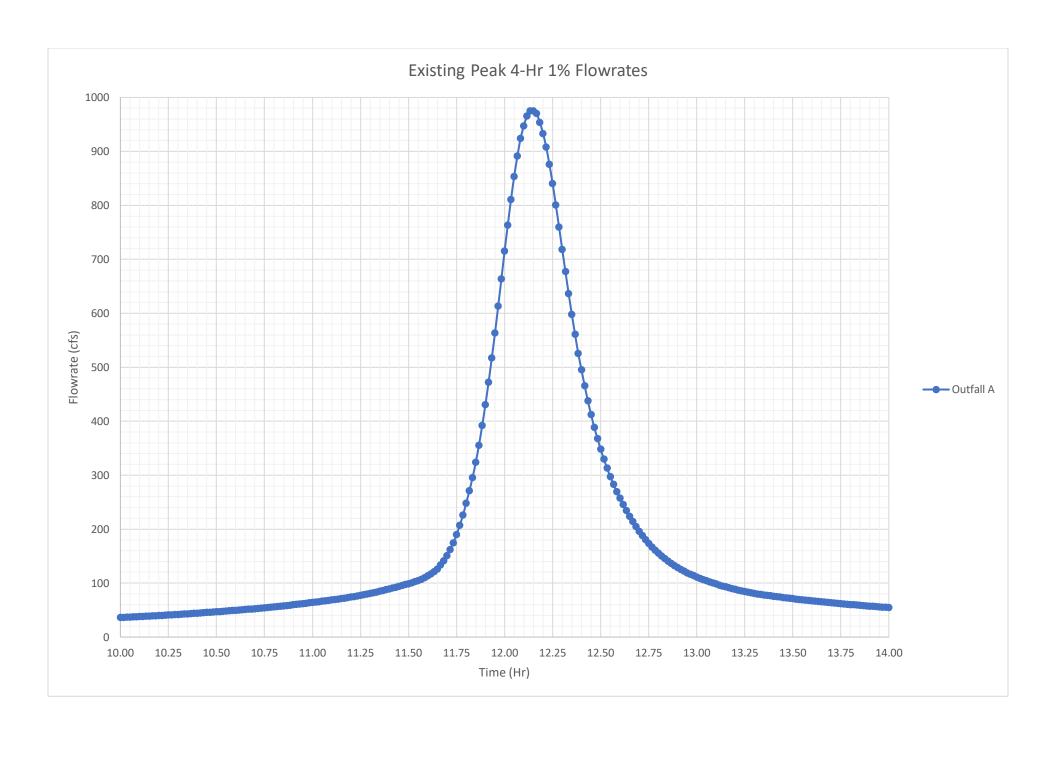


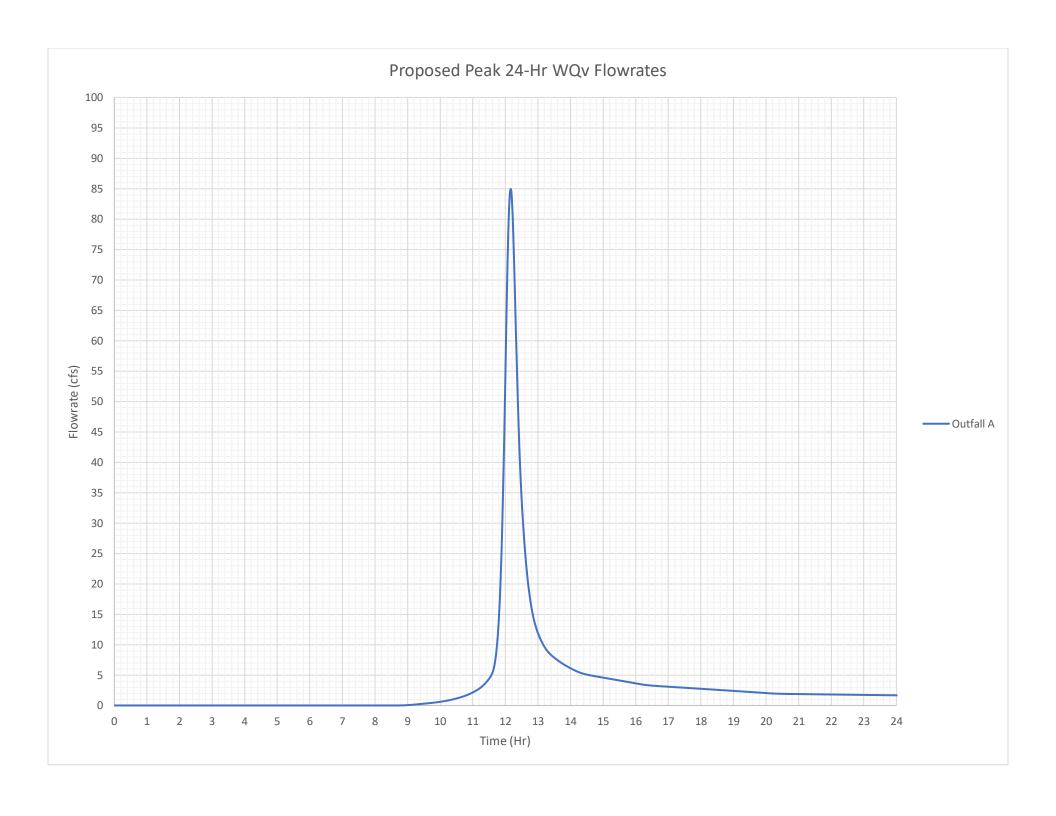


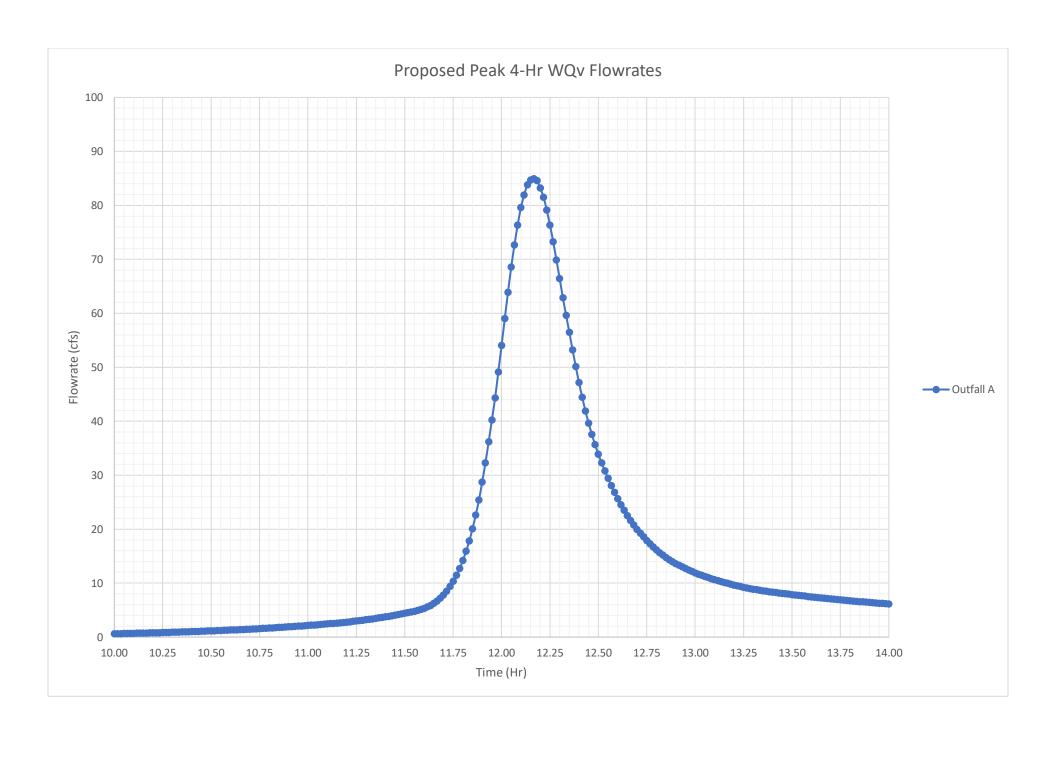


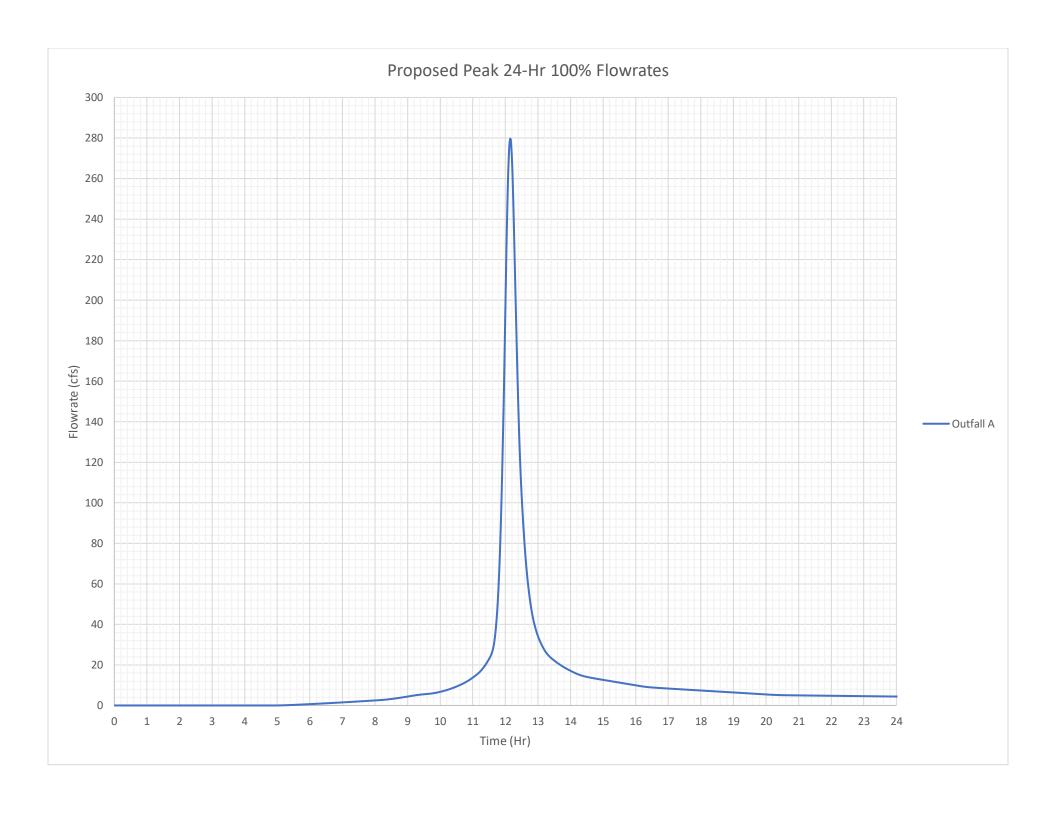


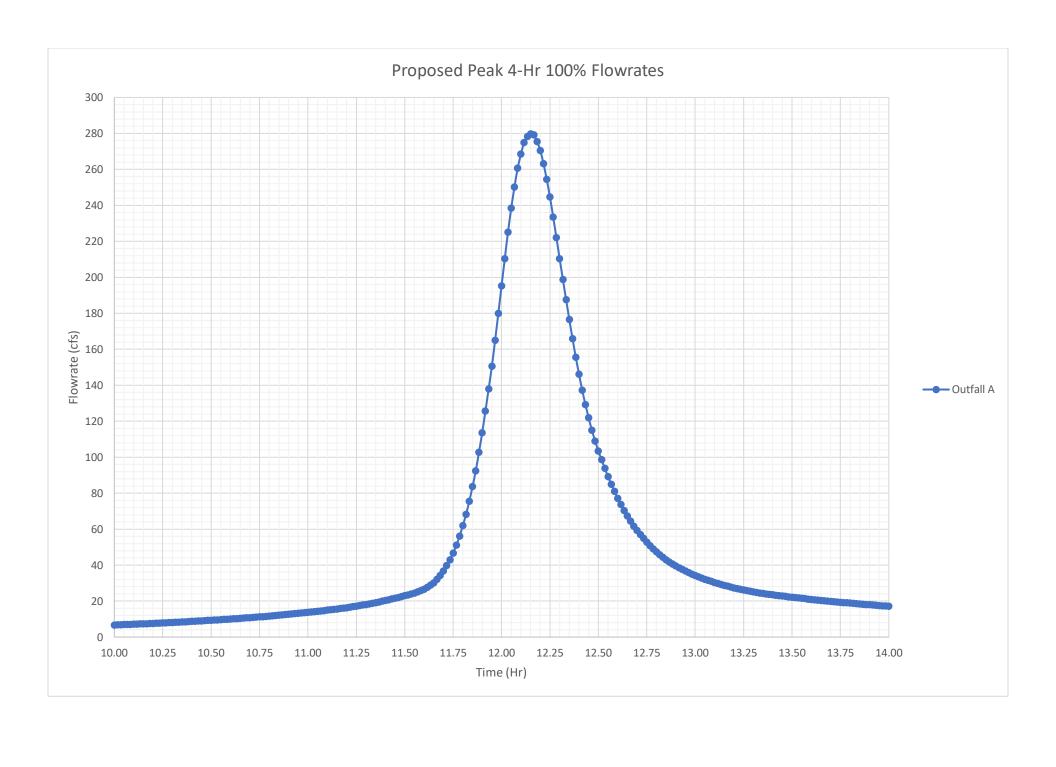


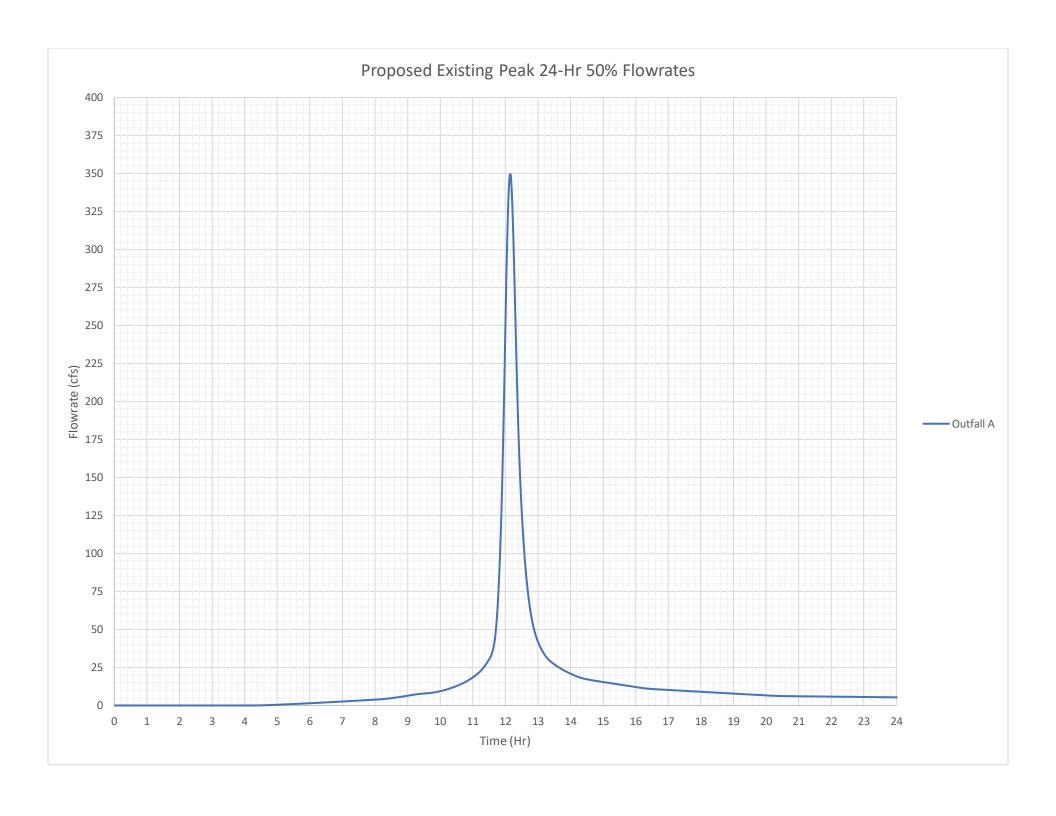


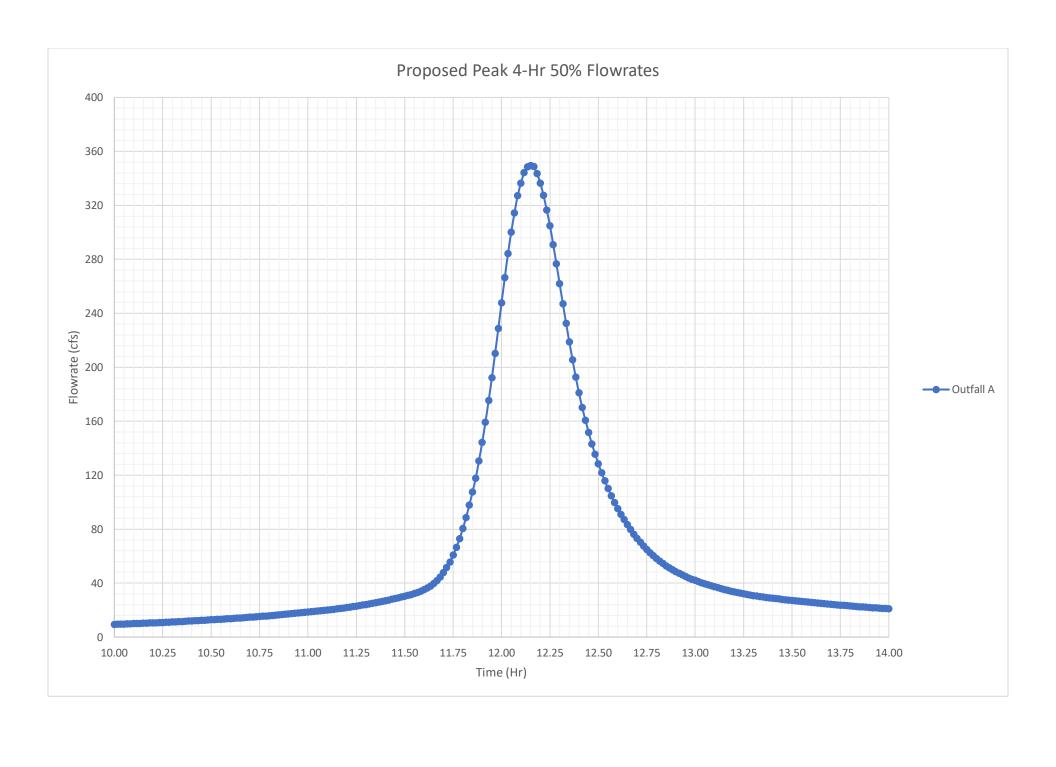


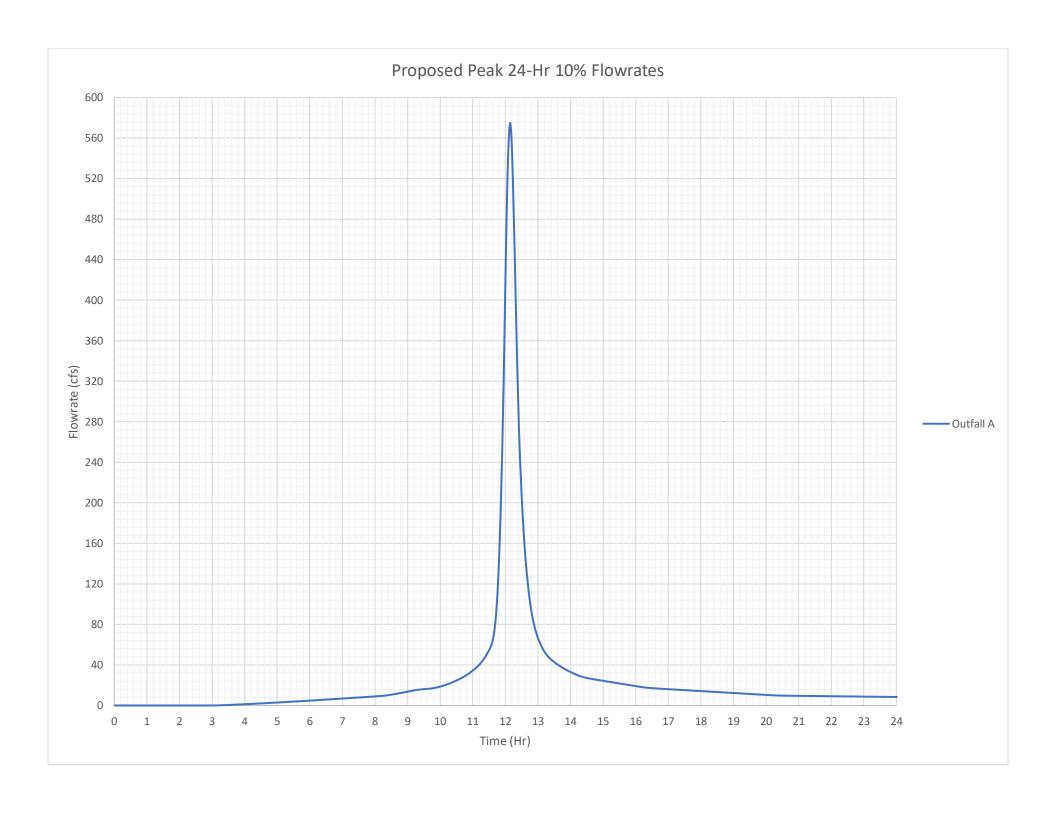


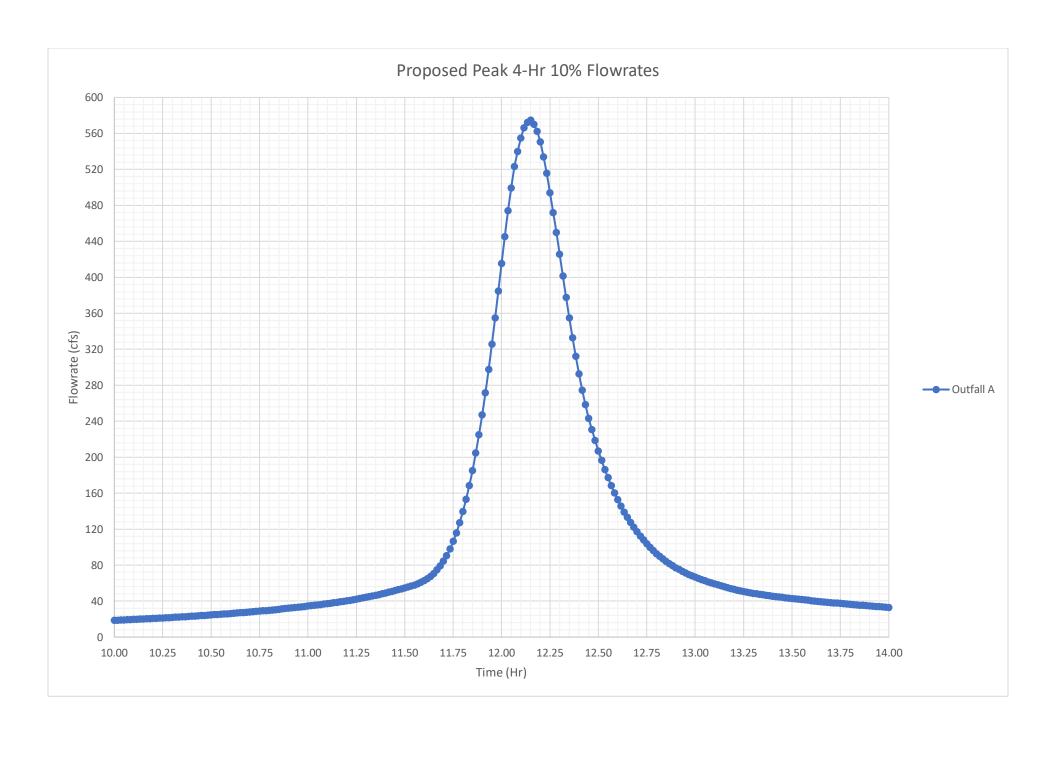


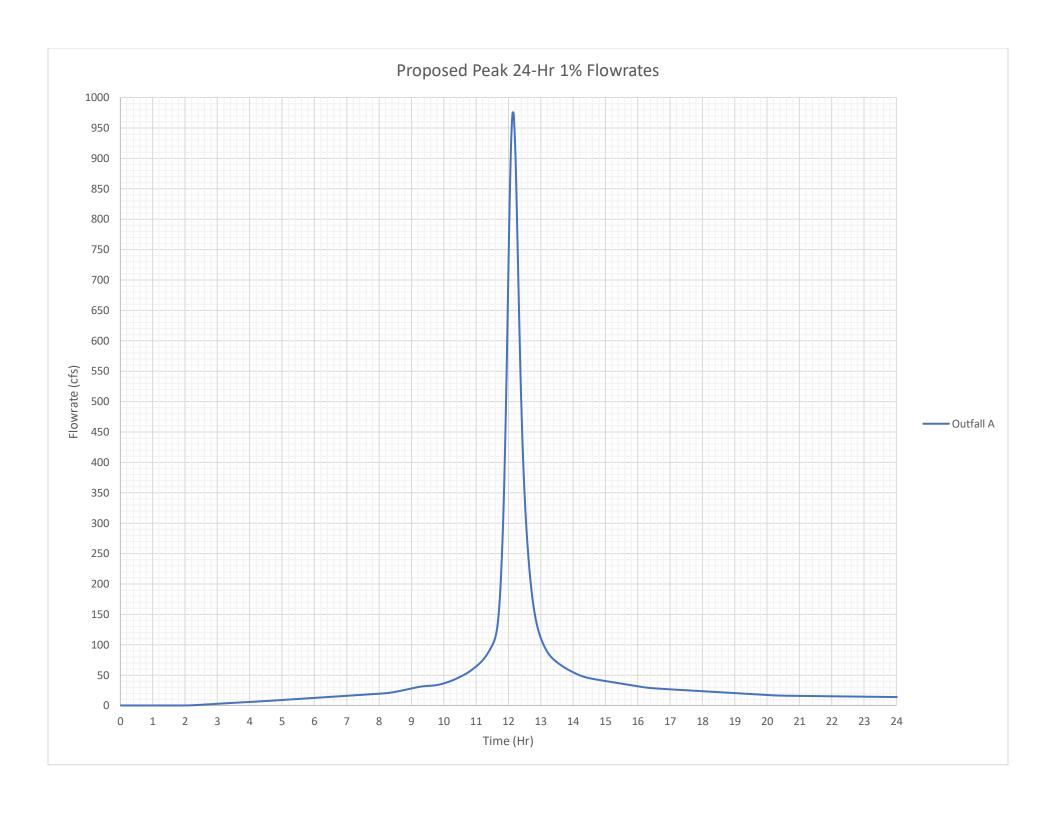


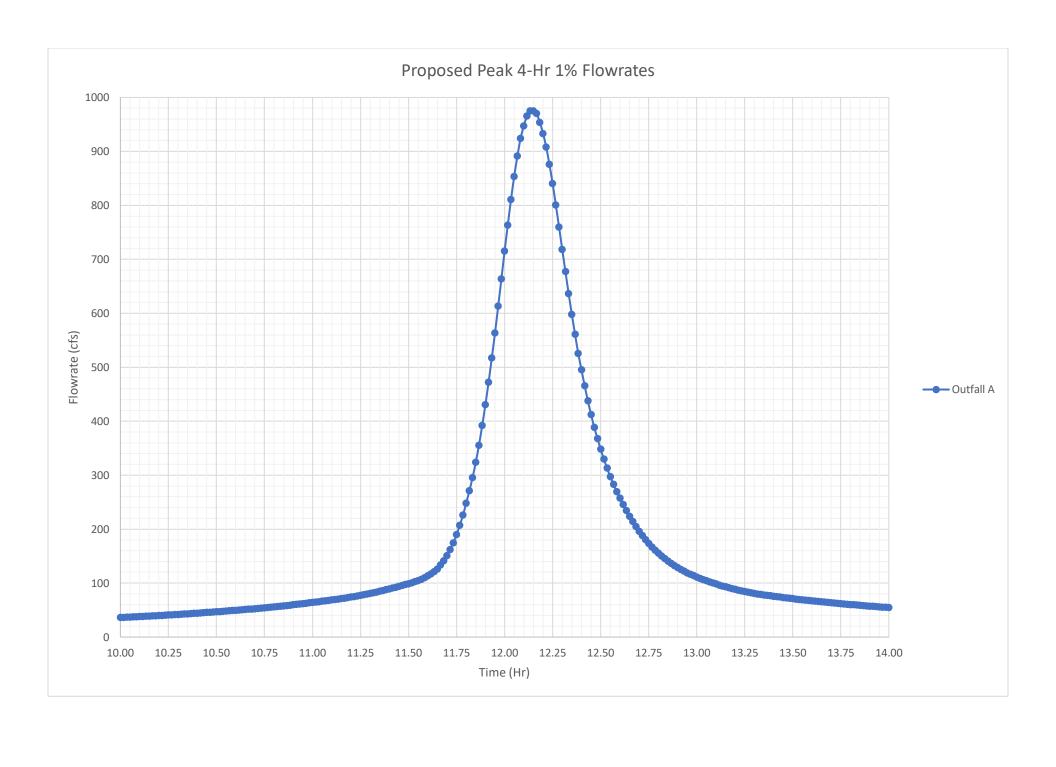








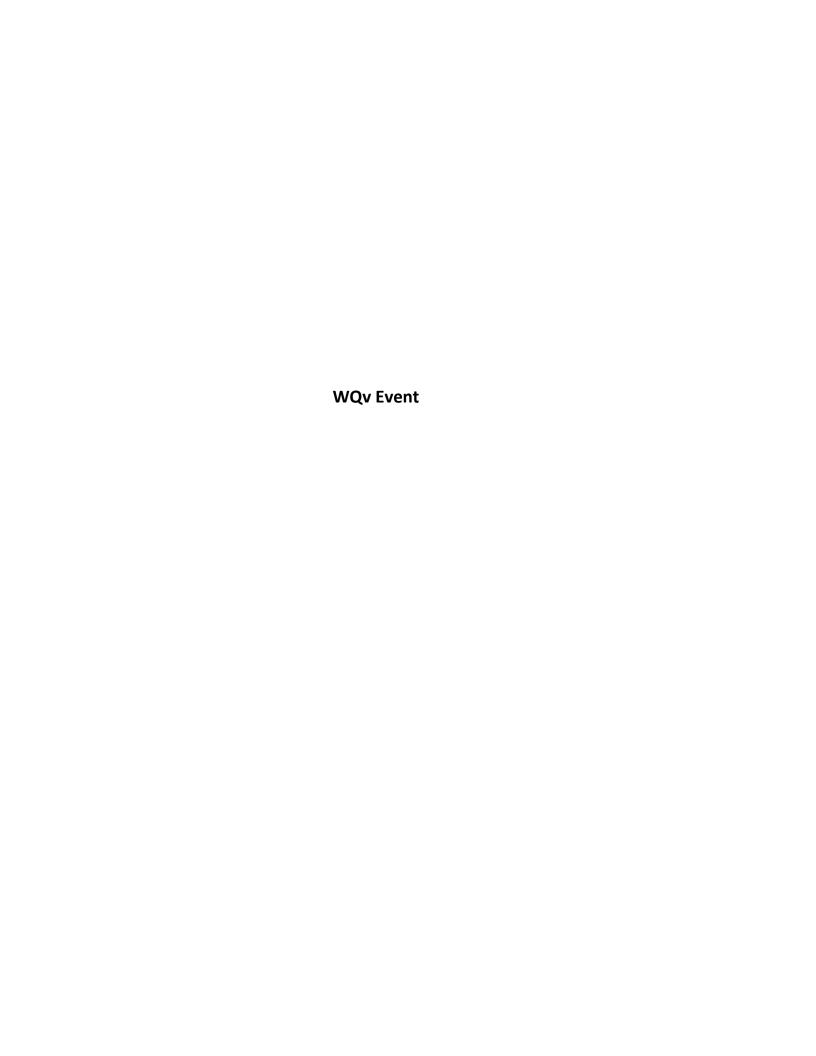




# **APPENDIX C**

Model Results





## **Project Description**

File Name ...... Existing Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

## **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	Feb 18, 2023	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	. 1	seconds

## **Number of Elements**

	Qty
Rain Gages	2
Subbasins	2
Nodes	2
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	1
Channels	0
Pipes	1
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
	ID	Source	ID	Туре	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	90% Event (WQv)	Cumulative	inches	Missouri	Jackson	1	1.37	SCS Type II 24-hr

## **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 A-1	132.96	484.00	91.58	1.37	0.67	88.82	85.12	0 00:25:53
2 Undeveloped	0.52	484.00	84.00	1.37	0.34	0.18	0.25	0 00:05:00

## **Node Summary**

SN Elen	nent Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
			Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
									Attained		Occurrence		
		(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1 Jun-	01 Junction	0.00	6.00	0.00	6.00	0.00	85.16	0.00	0.00	6.00	0 00:00	0.00	0.00
2 Out-	01 Outfall	0.00					85.16	0.00					

## Link Summary

SN Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-01	Pipe	Jun-01	Out-01	426.71	0.00	0.00	0.0000	0.000	0.0150	85.16	0.00	0.00	0.00	0.00	0.00	0.00

## **Subbasin Hydrology**

### Subbasin: A-1

### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
50 - 75% grass cover, Fair	0.00	D	84.00
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$ 

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)
P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation:

V = 16.1345 \* (Sf^0.5) (unpaved surface)
V = 20.3282 \* (Sf^0.5) (paved surface)
V = 15.0 \* (Sf^0.5) (grassed waterway surface)
V = 10.0 \* (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 \* (Sf^0.5) (cultivated straight rows surface)
V = 7.0 \* (Sf^0.5) (short grass pasture surface)
V = 5.0 \* (Sf^0.5) (woodland surface)
V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / WpTc = (Lf / V) / (3600 sec/hr)

### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

n = Manning's roughness

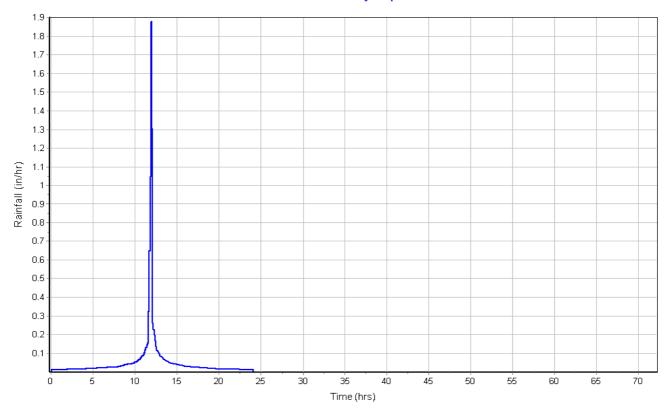
	Subarea		Subarea
Sheet Flow Computations	A	В	С
Manning's Roughness :	.3	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.50	0.00	0.00
Velocity (ft/sec):	0.10	0.00	0.00
Computed Flow Time (min):	16.31	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0.00	0.00
Computed Flow Time (min) :	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness:	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) : Total TOC (min)25.89	7.01	0.00	0.00

## Subbasin Runoff Results

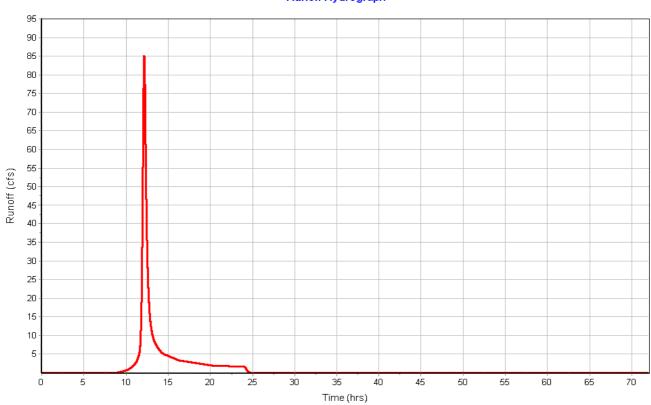
Total Rainfall (in)	1.37
Total Runoff (in)	0.67
Peak Runoff (cfs)	85.12
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0.00:25:53

Subbasin : A-1

## Rainfall Intensity Graph



## Runoff Hydrograph



## Subbasin : Undeveloped

### Input Data

Area (ac)	0.52
Peak Rate Factor	
Weighted Curve Number	84.00
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

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	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	84.00
Composite Area & Weighted CN	0.52		84.00

## Time of Concentration

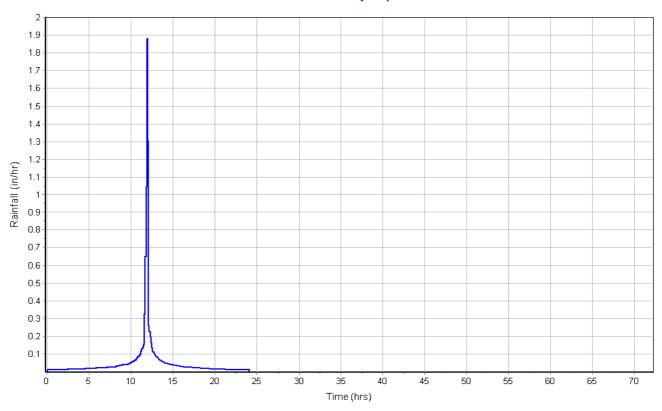
User-Defined TOC override (minutes): 5

### **Subbasin Runoff Results**

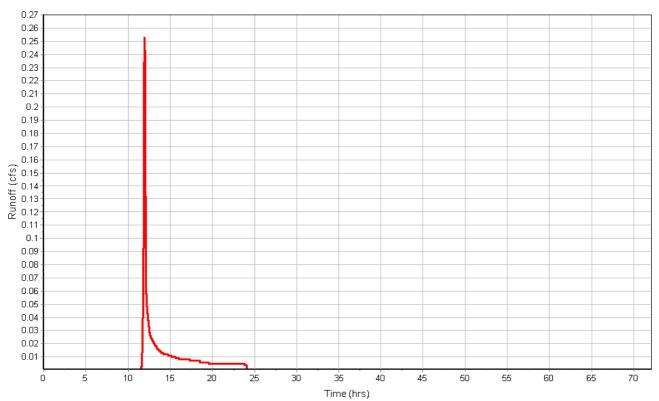
Total Rainfall (in)	1.37
Total Runoff (in)	0.34
Peak Runoff (cfs)	0.25
Weighted Curve Number	84.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Subbasin: Undeveloped

## Rainfall Intensity Graph



## Runoff Hydrograph



## **Junction Input**

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(in)
1 Jun-01	0.00	6.00	6.00	0.00	0.00	6.00	0.00	0.00	0.00

## **Junction Results**

	SN Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
	ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
			Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
						Attained					Occurrence		
_		(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
_	1 Jun-01	85.16	85.16	0.00	0.00	0.00	6.00	0.00	0.00	0 00:00	0 00:00	0.00	0.00

## **Pipe Input**

	SN Element	Length	Inlet	Inlet	Outlet	Outlet 7	Γotal	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional	Initial Flap	No. of
	ID		Invert	Invert	Invert	Invert [	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses	Flow Gate	Barrels
			Elevation	Offset	Elevation	Offset			Height							
_		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)					(cfs)	
_	1 Link-01	426.71	0.00	0.00	0.00	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	0.5000	0.5000	0.0000	0.00 No	1

## **Pipe Results**

SN Element	Peak	Time of	Design Flow	Peak Flow/	Peak Flow	Travel	Peak Flow	Peak Flow	Total Time	Froude Reported
ID	Flow	Peak Flow	Capacity	Design Flow	Velocity	Time	Depth	Depth/	Surcharged	Number Condition
		Occurrence		Ratio	•			Total Depth	-	
								Ratio		
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)	
1 Link-01	85.16	0 12:08	0.00	0.00	0.00		0.00	0.00	0.00	



## **Project Description**

File Name ...... Existing Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

## **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	Feb 18, 2023	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	2
Subbasins	2
Nodes	2
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	1
Channels	0
Pipes	1
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
	ID	Source	ID	Туре	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	1 Year	Cumulative	inches	Missouri	Jackson	1	3.10	SCS Type II 24-hr

## **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 A-1	132.96	484.00	91.58	3.10	2.22	294.77	279.69	0 00:25:53
2 Undeveloped	0.52	484.00	84.00	3.10	1.60	0.83	1.32	0 00:05:00

## **Node Summary**

S	N Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	Junction	0.00	6.00	0.00	6.00	0.00	279.96	0.00	0.00	6.00	0 00:00	0.00	0.00
	2 Out-01	Outfall	0.00					279.96	0.00					

## Link Summary

S	N Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
	ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
			Node			Elevation	Elevation						Ratio			Total Depth	
																Ratio	
					(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
	1 Link-01	Pipe	Jun-01	Out-01	426.71	0.00	0.00	0.0000	0.000	0.0150	279.96	0.00	0.00	0.00	0.00	0.00	0.00

## **Subbasin Hydrology**

### Subbasin: A-1

### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
50 - 75% grass cover, Fair	0.00	D	84.00
Composite Area & Weighted CN	132.96		91.58

### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$ 

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation:

V = 16.1345 \* (Sf^0.5) (unpaved surface)
V = 20.3282 \* (Sf^0.5) (paved surface)
V = 15.0 \* (Sf^0.5) (grassed waterway surface)
V = 10.0 \* (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 \* (Sf^0.5) (cultivated straight rows surface)
V = 7.0 \* (Sf^0.5) (short grass pasture surface)
V = 5.0 \* (Sf^0.5) (woodland surface)
V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / WpTc = (Lf / V) / (3600 sec/hr)

### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

n = Manning's roughness

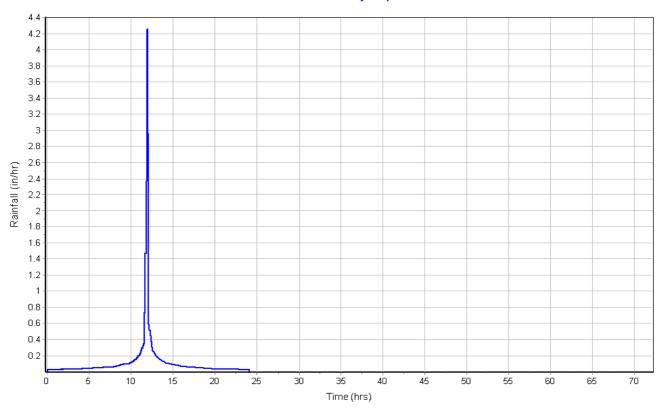
	Subarea		Subarea
Sheet Flow Computations	A	В	С
Manning's Roughness :	.3	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.50	0.00	0.00
Velocity (ft/sec):	0.10	0.00	0.00
Computed Flow Time (min):	16.31	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0.00	0.00
Computed Flow Time (min) :	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness:	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) : Total TOC (min)25.89	7.01	0.00	0.00

## Subbasin Runoff Results

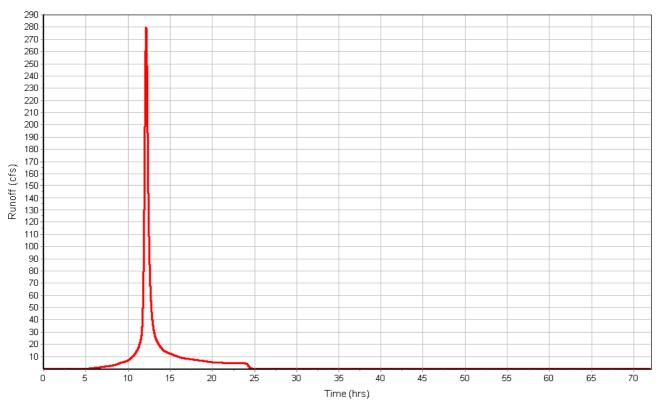
Total Rainfall (in)	3.10
Total Runoff (in)	2.22
Peak Runoff (cfs)	279.69
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0.00:25:53

### Subbasin : A-1

## Rainfall Intensity Graph



## Runoff Hydrograph



## Subbasin : Undeveloped

### Input Data

Area (ac)	0.52
Peak Rate Factor	
Weighted Curve Number	84.00
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

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	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	84.00
Composite Area & Weighted CN	0.52		84.00

## Time of Concentration

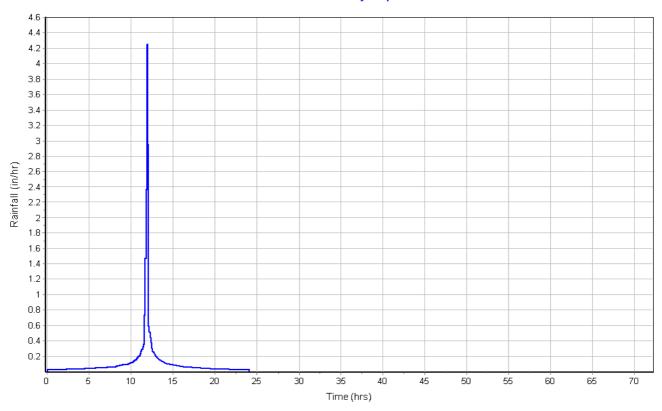
User-Defined TOC override (minutes): 5

### **Subbasin Runoff Results**

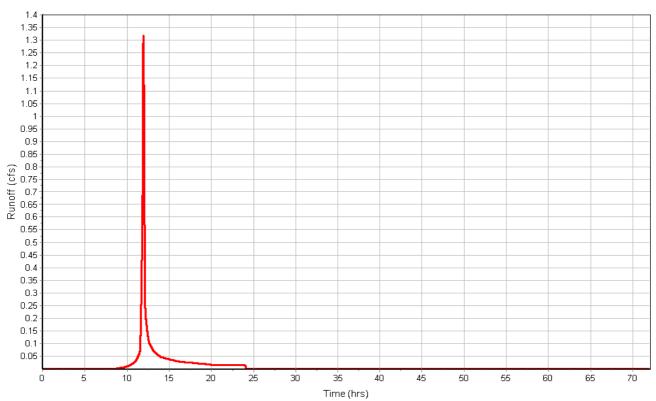
Total Rainfall (in)	3.10
Total Runoff (in)	1.60
Peak Runoff (cfs)	1.32
Weighted Curve Number	84.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Subbasin : Undeveloped

## Rainfall Intensity Graph



## Runoff Hydrograph



## **Junction Input**

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(in)
1 Jun-01	0.00	6.00	6.00	0.00	0.00	6.00	0.00	0.00	0.00

## **Junction Results**

S	N Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
	ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
			Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
						Attained					Occurrence		
		(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	279.96	279.96	0.00	0.00	0.00	6.00	0.00	0.00	0 00:00	0 00:00	0.00	0.00

## **Pipe Input**

	SN Element	Length	Inlet	Inlet	Outlet	Outlet 7	Γotal	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional	Initial Flap	No. of
	ID		Invert	Invert	Invert	Invert [	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses	Flow Gate	Barrels
			Elevation	Offset	Elevation	Offset			Height							
_		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)					(cfs)	
_	1 Link-01	426.71	0.00	0.00	0.00	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	0.5000	0.5000	0.0000	0.00 No	1

## Pipe Results

ID Flow Peak Flow Capacity Design Flow Velocity Time Depth Depth/ Surcharg	ad Number Condition
	sa Hambor Condition
Occurrence Ratio Total Depth	
Ratio	
(cfs) (days hh:mm) (cfs) (ft/sec) (min) (ft) (m	in)
1 Link-01 279.96 0 12:07 0.00 0.00 0.00 0.00 0.00 0.00 0.	00



## **Project Description**

File Name ...... Existing Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

## **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	Feb 18, 2023	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	2
Subbasins	2
Nodes	2
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	1
Channels	0
Pipes	1
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN F	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
II	D	Source	ID	Type	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	2-Year	Cumulative	inches	Missouri	Jackson	2	3.71	SCS Type II 24-hr

## **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 A-1	132.96	484.00	91.58	3.71	2.80	371.89	349.78	0 00:25:53
2 Undeveloped	0.52	484.00	84.00	3.71	2.12	1.10	1.74	0 00:05:00

## **Node Summary**

S	N Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	Junction	0.00	6.00	0.00	6.00	0.00	350.13	0.00	0.00	6.00	0 00:00	0.00	0.00
	2 Out-01	Outfall	0.00					350.13	0.00					

# Link Summary

S	N Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
	ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
			Node			Elevation	Elevation						Ratio			Total Depth	
																Ratio	
					(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
	1 Link-01	Pipe	Jun-01	Out-01	426.71	0.00	0.00	0.0000	0.000	0.0150	350.13	0.00	0.00	0.00	0.00	0.00	0.00

## **Subbasin Hydrology**

#### Subbasin: A-1

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
50 - 75% grass cover, Fair	0.00	D	84.00
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$ 

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)
P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation:

V = 16.1345 \* (Sf^0.5) (unpaved surface)
V = 20.3282 \* (Sf^0.5) (paved surface)
V = 15.0 \* (Sf^0.5) (grassed waterway surface)
V = 10.0 \* (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 \* (Sf^0.5) (cultivated straight rows surface)
V = 7.0 \* (Sf^0.5) (short grass pasture surface)
V = 5.0 \* (Sf^0.5) (woodland surface)
V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / WpTc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

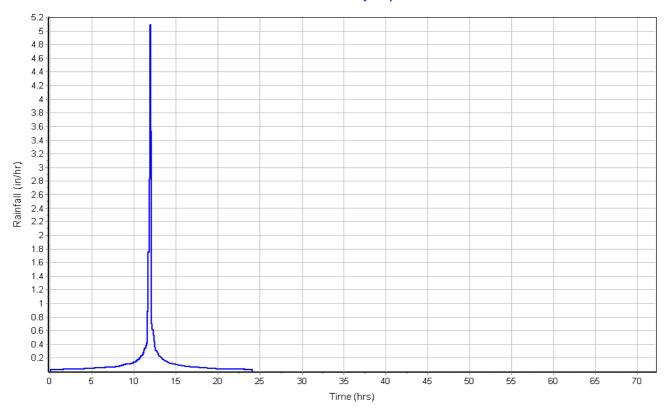
n = Manning's roughness

	Subarea	Subarea	
Sheet Flow Computations	A	В	С
Manning's Roughness :	.3	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.50	0.00	0.00
Velocity (ft/sec):	0.10	0.00	0.00
Computed Flow Time (min) :	16.31	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0.00	0.00
Computed Flow Time (min) :	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) :	7.01	0.00	0.00
Total TOC (min)25.89			

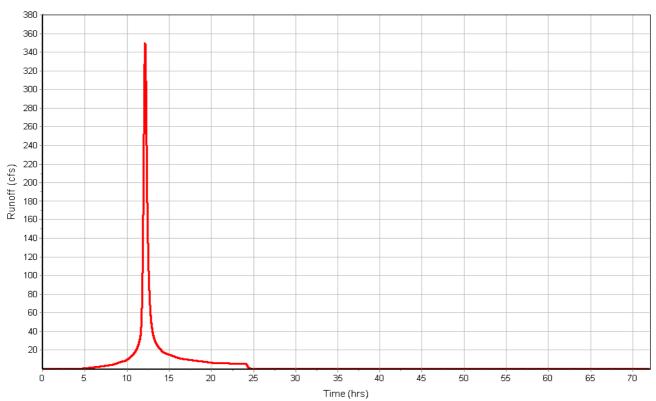
## Subbasin Runoff Results

Total Rainfall (in)	3.71
Total Runoff (in)	2.80
Peak Runoff (cfs)	349.78
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

## Rainfall Intensity Graph



## Runoff Hydrograph



## Subbasin : Undeveloped

### Input Data

Area (ac)	0.52
Peak Rate Factor	
Weighted Curve Number	84.00
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

iiposite oui ve ivallibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	84.00
Composite Area & Weighted CN	0.52		84.00

### Time of Concentration

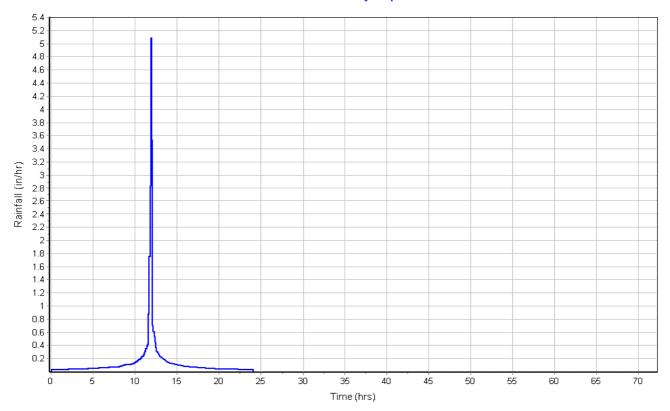
User-Defined TOC override (minutes): 5

### **Subbasin Runoff Results**

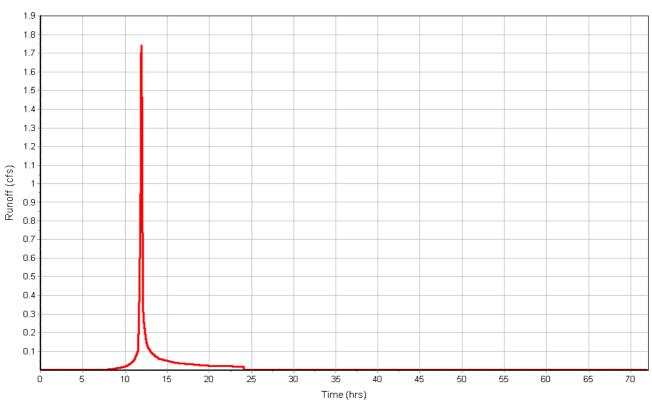
Total Rainfall (in)	3.71
Total Runoff (in)	2.12
Peak Runoff (cfs)	1.74
Weighted Curve Number	84.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Subbasin : Undeveloped

## Rainfall Intensity Graph



## Runoff Hydrograph



## **Junction Input**

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(in)
1 Jun-01	0.00	6.00	6.00	0.00	0.00	6.00	0.00	0.00	0.00

## **Junction Results**

	SN Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
	ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
			Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
						Attained					Occurrence		
_		(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	350.13	350.13	0.00	0.00	0.00	6.00	0.00	0.00	0 00:00	0 00:00	0.00	0.00

# **Pipe Input**

	SN Element	Length	Inlet	Inlet	Outlet	Outlet 7	Γotal	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional	Initial Flap	No. of
	ID		Invert	Invert	Invert	Invert [	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses	Flow Gate	Barrels
			Elevation	Offset	Elevation	Offset			Height							
_		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)					(cfs)	
_	1 Link-01	426.71	0.00	0.00	0.00	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	0.5000	0.5000	0.0000	0.00 No	1

## Pipe Results

ID Flow Peak Flow Capacity Design Flow Velocity Time Depth Depth/ Surchar	
ib flow reaktion capacity besign flow velocity fille beptil beptil suicilal	rged Number Condition
Occurrence Ratio Total Depth	
Ratio	
(cfs) (days hh:mm) (cfs) (ft/sec) (min) (ft) (i	min)



# **Project Description**

File Name ...... Existing Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	,	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	2
Subbasins	2
Nodes	2
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	1
Channels	0
Pipes	1
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
	ID	Source	ID	Type	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	10 Year	Cumulative	inches	Missouri	Jackson	10	5.67	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 A-1	132.96	484.00	91.58	5.67	4.70	624.78	574.93	0 00:25:53
2 Undeveloped	0.52	484.00	84.00	5.67	3.89	2.02	3.14	0 00:05:00

# **Node Summary**

SN Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
			Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
									Attained		Occurrence		
		(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1 Jun-01	Junction	0.00	6.00	0.00	6.00	0.00	575.48	0.00	0.00	6.00	0 00:00	0.00	0.00
2 Out-01	Outfall	0.00					575.48	0.00					

# Link Summary

SN Ele	ment	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID		Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
			Node			Elevation E	Elevation						Ratio			Total Depth	
																Ratio	
					(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Linl	k-01	Pipe	Jun-01	Out-01	426.71	0.00	0.00	0.0000	0.000	0.0150	575.48	0.00	0.00	0.00	0.00	0.00	0.00

## **Subbasin Hydrology**

#### Subbasin: A-1

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
50 - 75% grass cover, Fair	0.00	D	84.00
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$ 

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation:

V = 16.1345 \* (Sf^0.5) (unpaved surface)
V = 20.3282 \* (Sf^0.5) (paved surface)
V = 15.0 \* (Sf^0.5) (grassed waterway surface)
V = 10.0 \* (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 \* (Sf^0.5) (cultivated straight rows surface)
V = 7.0 \* (Sf^0.5) (short grass pasture surface)
V = 5.0 \* (Sf^0.5) (woodland surface)
V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

#### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / WpTc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

n = Manning's roughness

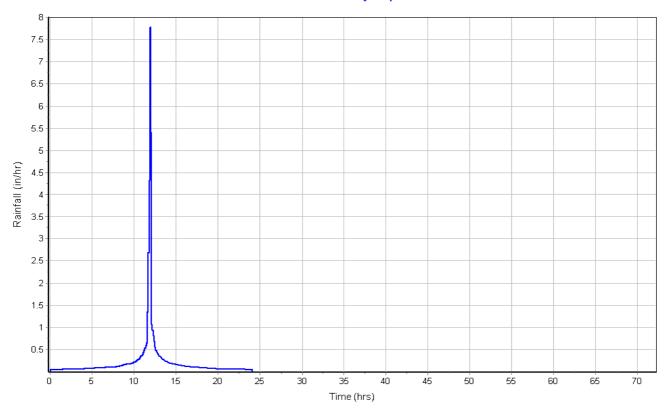
Chart Flan Commutations	Subarea	Subarea	
Sheet Flow Computations	.3	B	<u>C</u>
Manning's Roughness :		0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.50	0.00	0.00
Velocity (ft/sec) :	0.10	0.00	0.00
Computed Flow Time (min):	16.31	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec) :	2.87	0.00	0.00
Computed Flow Time (min) :	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) :	7.01	0.00	0.00
Total TOC (min)25.89			

## Subbasin Runoff Results

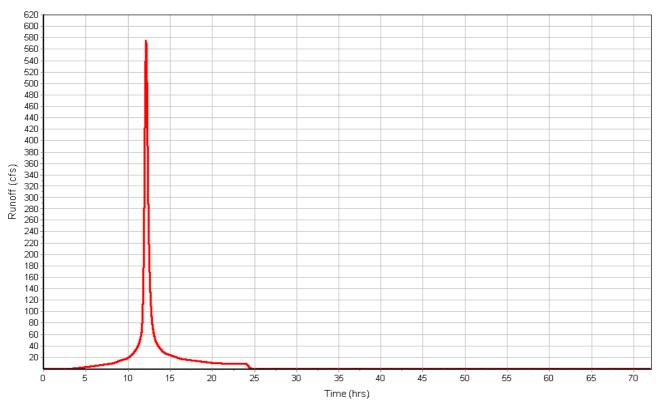
Total Rainfall (in)	5.67
Total Runoff (in)	4.70
Peak Runoff (cfs)	574.93
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

Subbasin : A-1

## Rainfall Intensity Graph



## Runoff Hydrograph



## Subbasin : Undeveloped

### Input Data

Area (ac)	0.52
Peak Rate Factor	
Weighted Curve Number	84.00
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

iiposite oui ve ivallibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	84.00
Composite Area & Weighted CN	0.52		84.00

## Time of Concentration

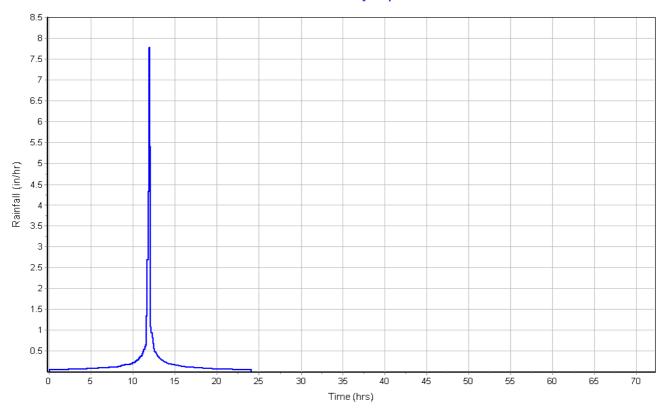
User-Defined TOC override (minutes): 5

### **Subbasin Runoff Results**

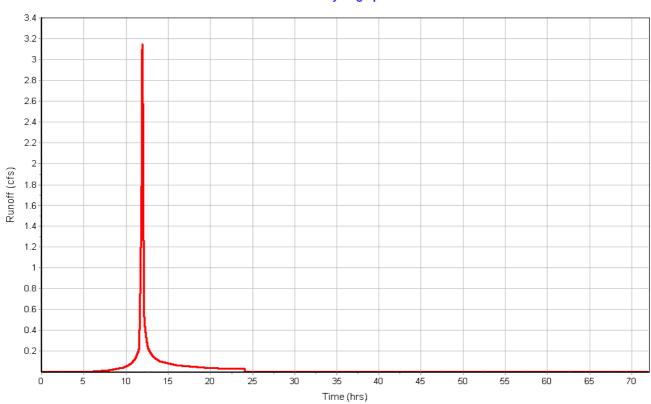
Total Rainfall (in)	5.67
Total Runoff (in)	3.89
Peak Runoff (cfs)	3.14
Weighted Curve Number	84.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Subbasin : Undeveloped

## Rainfall Intensity Graph



## Runoff Hydrograph



## **Junction Input**

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(in)
1 Jun-01	0.00	6.00	6.00	0.00	0.00	6.00	0.00	0.00	0.00

## **Junction Results**

	SN Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
	ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
			Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
						Attained					Occurrence		
_		(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	575.48	575.48	0.00	0.00	0.00	6.00	0.00	0.00	0 00:00	0 00:00	0.00	0.00

# **Pipe Input**

	SN Element	Length	Inlet	Inlet	Outlet	Outlet 7	Γotal	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional	Initial Flap	No. of
	ID		Invert	Invert	Invert	Invert [	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses	Flow Gate	Barrels
			Elevation	Offset	Elevation	Offset			Height							
_		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)					(cfs)	
_	1 Link-01	426.71	0.00	0.00	0.00	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	0.5000	0.5000	0.0000	0.00 No	1

## Pipe Results

Number Condition
Number Condition



# **Project Description**

File Name ...... Existing Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	Feb 18, 2023	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	2
Subbasins	2
Nodes	2
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	1
Channels	0
Pipes	1
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
	ID	Source	ID	Type	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	100 Year	Cumulative	inches	Missouri	Jackson	100	9.25	SCS Type II 24-hr

## **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 A-1	132.96	484.00	91.58	9.25	8.23	1094.39	977.27	0 00:25:53
2 Undeveloped	0.52	484.00	84.00	9.25	7.30	3.80	5.72	0 00:05:00

# **Node Summary**

SN	Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1	Jun-01	Junction	0.00	6.00	0.00	6.00	0.00	978.28	0.00	0.00	6.00	0 00:00	0.00	0.00
2	Out-01	Outfall	0.00					978.28	0.00					

# **Link Summary**

SN E	lement	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
10	)	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
			Node			Elevation	Elevation						Ratio			Total Depth	
																Ratio	
					(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 L	ink-01	Pipe	Jun-01	Out-01	426.71	0.00	0.00	0.0000	0.000	0.0150	978.28	0.00	0.00	0.00	0.00	0.00	0.00

## **Subbasin Hydrology**

#### Subbasin: A-1

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
50 - 75% grass cover, Fair	0.00	D	84.00
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$ 

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation:

V = 16.1345 \* (Sf^0.5) (unpaved surface)
V = 20.3282 \* (Sf^0.5) (paved surface)
V = 15.0 \* (Sf^0.5) (grassed waterway surface)
V = 10.0 \* (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 \* (Sf^0.5) (cultivated straight rows surface)
V = 7.0 \* (Sf^0.5) (short grass pasture surface)
V = 5.0 \* (Sf^0.5) (woodland surface)
V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

#### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / WpTc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

n = Manning's roughness

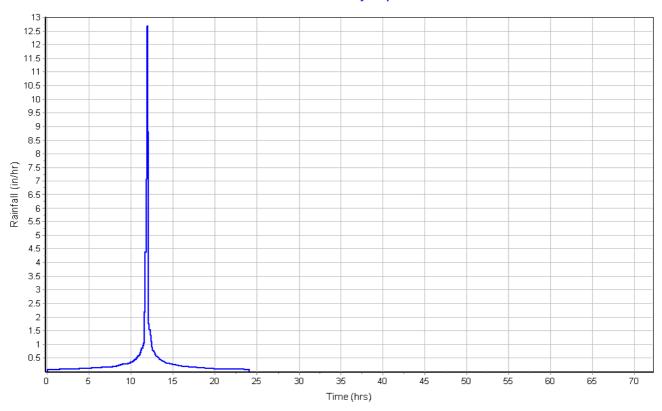
Sheet Flow Computations	Subarea A	Subarea B	Subarea C
Manning's Roughness :	.3	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.50	0.00	0.00
Velocity (ft/sec):	0.10	0.00	0.00
Computed Flow Time (min) :	16.31	0.00	0.00
Compated Flow Time (min).	10.51	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0.00	0.00
Computed Flow Time (min):	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) :	7.01	0.00	0.00
Total TOC (min)25.89			

## Subbasin Runoff Results

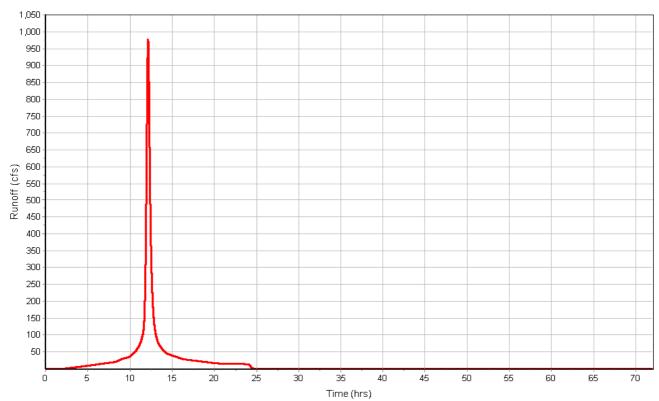
Total Rainfall (in)	9.25
Total Runoff (in)	8.23
Peak Runoff (cfs)	977.27
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

### Subbasin : A-1

## Rainfall Intensity Graph



## Runoff Hydrograph



## Subbasin : Undeveloped

### Input Data

Area (ac)	0.52
Peak Rate Factor	
Weighted Curve Number	84.00
Rain Gage ID	Rain Gage-01

### **Composite Curve Number**

iiposite oui ve ivallibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	84.00
Composite Area & Weighted CN	0.52		84.00

### Time of Concentration

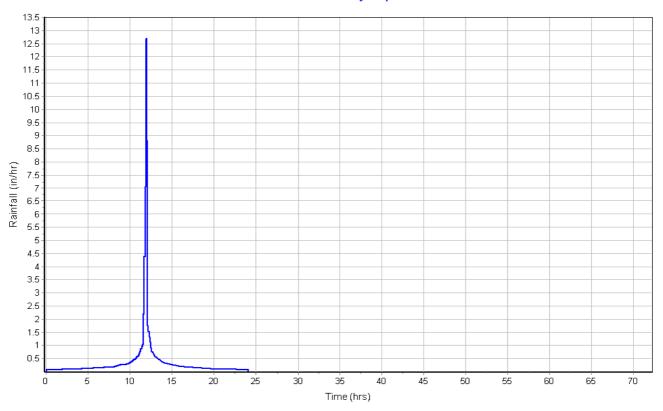
User-Defined TOC override (minutes): 5

### **Subbasin Runoff Results**

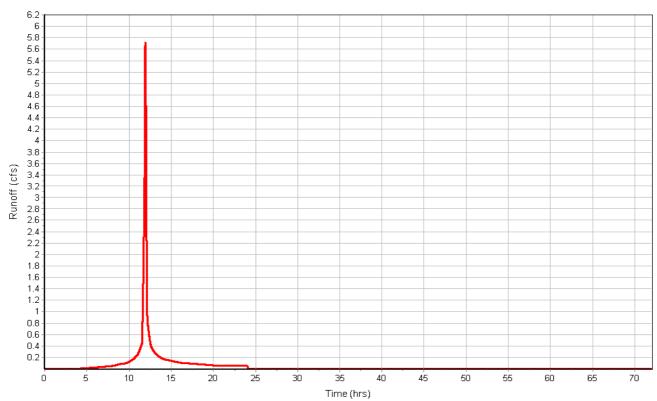
Total Rainfall (in)	9.25
Total Runoff (in)	
Peak Runoff (cfs)	5.72
Weighted Curve Number	84.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Subbasin : Undeveloped

## Rainfall Intensity Graph



## Runoff Hydrograph



## **Junction Input**

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(in)
1 Jun-01	0.00	6.00	6.00	0.00	0.00	6.00	0.00	0.00	0.00

## **Junction Results**

SN Element	Peak Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
ID	Inflow Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
	Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
				Attained					Occurrence		
	(cfs) (cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1 Jun-01	978.28 978.28	0.00	0.00	0.00	6.00	0.00	0.00	0 00:00	0 00:00	0.00	0.00

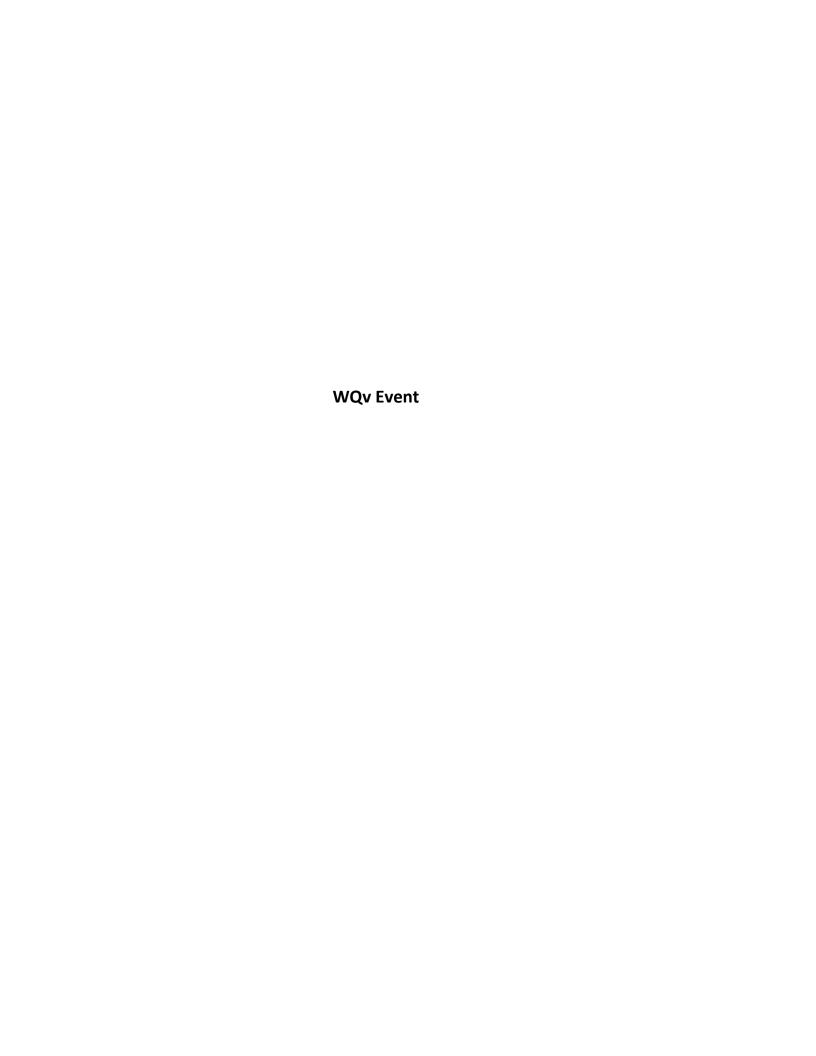
# **Pipe Input**

	SN Element	Length	Inlet	Inlet	Outlet	Outlet 7	Γotal	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional	Initial Flap	No. of
	ID		Invert	Invert	Invert	Invert [	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses	Flow Gate	Barrels
			Elevation	Offset	Elevation	Offset			Height							
_		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)					(cfs)	
_	1 Link-01	426.71	0.00	0.00	0.00	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	0.5000	0.5000	0.0000	0.00 No	1

## Pipe Results

ID Flow Book Flow Committee Design Flow Make Trans Book Book Committee	
ID Flow Peak Flow Capacity Design Flow Velocity Time Depth Depth/ Surcha	rged Number Condition
Occurrence Ratio Total Depth	
Ratio	
(cfs) (days hh:mm) (cfs) (ft/sec) (min) (ft)	(min)
1 Link-01 978.28 0 12:07 0.00 0.00 0.00 0.00 0.00	0.00





# **Project Description**

File Name ...... Proposed Conditions\_NOAA.SPF

# **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qt
Rain Gages	1
Subbasins	2
Nodes	3
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	1
Links	3
Channels	0
Pipes	1
Pumps	0
Orifices	2
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County		Rainfall Depth	Rainfall Distribution
								(years)	(inches)	
49		Time Series	WQv	Cumulative	inches	Missouri	Jackson	1.00	1.37	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	(ac) 132.96	484.00	91.58	(in) 1.37	(in) 0.67	(ac-in) 88.82	(cfs) 85.12	(days hh:mm:ss) 0 00:25:53

# **Node Summary**

SN Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
			Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
									Attained		Occurrence		
		(ft)	(ft)	(ft)	(ft)	(ft²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1 1-Jun	Junction	101.00	106.00	0.00	0.00	0.00	0.02	101.04	0.00	4.96	0 00:00	0.00	0.00
2 Out-01	Outfall	100.00					85.10	100.04					
3 Stor-01	Storage Node	100.00	106.00	0.00		0.00	0.73	101.10				0.00	0.00

# **Link Summary**

SN Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-01	Pipe	1-Jun	Out-01	50.00	101.00	100.00	2.0000	36.000	0.0150	0.02	81.75	0.00	1.19	0.04	0.01	0.00 Calculated
2 Orifice-01	Orifice	Stor-01	1-Jun		100.00	101.00		3.000		0.02						
3 Orifice-04	Orifice	Stor-01	1-Jun		100.00	101.00		4.000		0.00						

### **Subbasin Hydrology**

### Subbasin: Sub-01

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83
1/4 acre lots, 38% impervious	1.71	D	87
Urban commercial, 85% imp	19.01	С	94
Urban commercial, 85% imp	74.72	D	95
Multi-Family	3.11	С	90
Paved roads with curbs & sewers	0.4	D	98
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

Tc = (0.007 \* ((n \* Lf)^0.8)) / ((P^0.5) \* (Sf^0.4))

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation :

V = 16.1345 \* (Sf^0.5) (unpaved surface)

V = 20.3282 \* (Sf^0.5) (paved surface)

V = 15.0 \* (Sf^0.5) (grassed waterway surface)

 $V = 10.0 * (Sf^0.5)$  (nearly bare & untilled surface)  $V = 9.0 * (Sf^0.5)$  (cultivated straight rows surface)

 $V = 7.0 * (Sf^0.5)$  (short grass pasture surface)

V = 5.0 \* (Sf^0.5) (woodland surface)

V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

V = (1.49 \* (R^(2/3)) \* (Sf^0.5)) / n

R = Aq / Wp

Tc = (Lf / V) / (3600 sec/hr)

### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

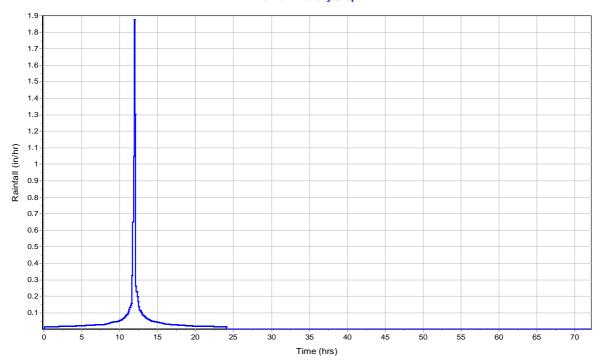
 $n \ = Manning's \ roughness$ 

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	0.3	0	0
Flow Length (ft):	100	0	0
Slope (%):	2	0	0
2 yr, 24 hr Rainfall (in) :	3.5	0	0
Velocity (ft/sec):	0.1	0	0
Computed Flow Time (min):	16.31	0	0
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0	0
Slope (%):	2	0	0
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0	0
Computed Flow Time (min) :	2.57	0	0
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	0.013	0	0
Flow Length (ft):	2975	0	0
Channel Slope (%):	1	0	0
Cross Section Area (ft²):	3.425	0	0
Wetted Perimeter (ft):	7.06	0	0
Velocity (ft/sec):	7.08	0	0
Computed Flow Time (min) :	7.01	0	0
Total TOC (min)25.89			

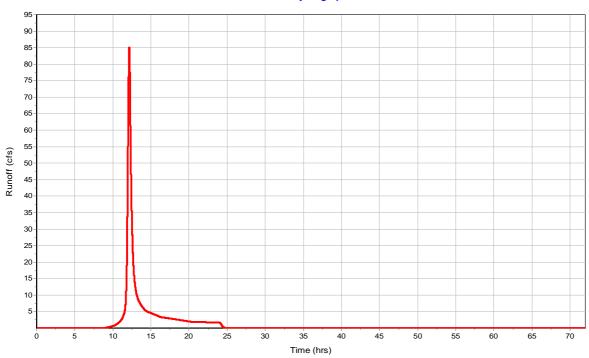
## **Subbasin Runoff Results**

Total Rainfall (in)	1.37
Total Runoff (in)	0.67
Peak Runoff (cfs)	85.12
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

### Rainfall Intensity Graph



### Runoff Hydrograph



### Subbasin: Sub-02

### Input Data

Area (ac)	0.52
Peak Rate Factor	484
Weighted Curve Number	. 95
Pain Gane ID	Rain Gage-01

### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	95
Composite Area & Weighted CN	0.52		95

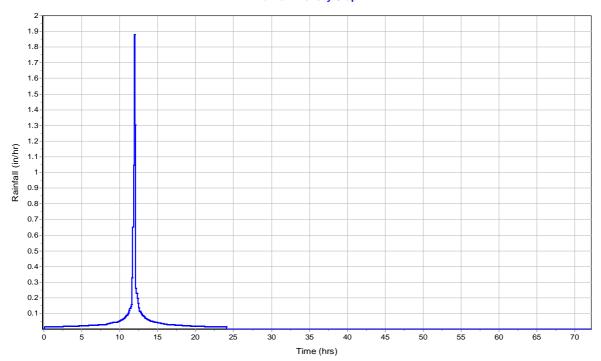
### **Time of Concentration**

User-Defined TOC override (minutes): 5

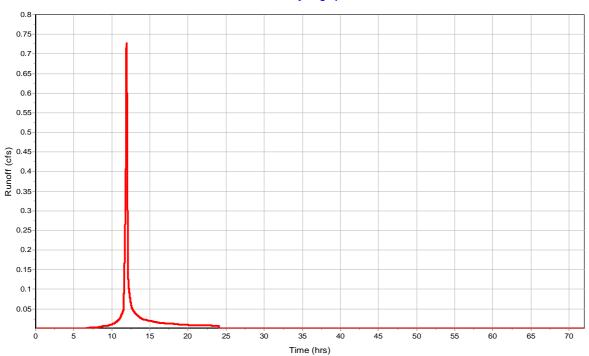
### **Subbasin Runoff Results**

Total Rainfall (in)	1.37
Total Runoff (in)	0.89
Peak Runoff (cfs)	0.73
Weighted Curve Number	95
Time of Concentration (days hh:mm:ss)	0 00:05:00

### Rainfall Intensity Graph



## Runoff Hydrograph





# **Project Description**

File Name ...... Proposed Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	1
Subbasins	2
Nodes	3
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	1
Links	3
Channels	0
Pipes	1
Pumps	0
Orifices	2
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

S	N Rain Gage		Data Source		Rain	State	County		Rainfall	
	ID	Source	ID	Туре	Units			Period (years)	(inches)	Distribution
4	9	Time Series	1 Year	Cumulative	inches	Missouri	Jackson	1.00	3.10	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID	7.1.00	Factor	3					Concentration
ID		ractor		ırve Rainfall Runoff Runoff			Kulloll	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	132.96	484.00	91.58	3.10	2.22	294.77	279.69	0 00:25:53
2 Sub-02	0.52	484.00	95.00	3.10	2.55	1.32	1.97	0 00:05:00

# **Node Summary**

SN	Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Туре	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1	1-Jun	Junction	101.00	106.00	0.00	0.00	0.00	0.21	101.12	0.00	4.88	0 00:00	0.00	0.00
2	Out-01	Outfall	100.00					279.90	100.11					
3	Stor-01	Storage Node	100.00	106.00	0.00		0.00	1.97	101.89				0.00	0.00

# **Link Summary**

SN Element	Elemen	t From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-01	Pipe	1-Jun	Out-01	50.00	101.00	100.00	2.0000	36.000	0.0150	0.21	81.75	0.00	2.41	0.11	0.04	0.00 Calculated
2 Orifice-0	1 Orifice	Stor-01	1-Jun		100.00	101.00		3.000		0.21						
3 Orifice-0		Stor-01			100.00	101.00		4.000		0.00						

### **Subbasin Hydrology**

### Subbasin: Sub-01

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83
1/4 acre lots, 38% impervious	1.71	D	87
Urban commercial, 85% imp	19.01	С	94
Urban commercial, 85% imp	74.72	D	95
Multi-Family	3.11	С	90
Paved roads with curbs & sewers	0.4	D	98
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

Tc = (0.007 \* ((n \* Lf)^0.8)) / ((P^0.5) \* (Sf^0.4))

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

### Shallow Concentrated Flow Equation :

V = 16.1345 \* (Sf^0.5) (unpaved surface)

V = 20.3282 \* (Sf^0.5) (paved surface)

V = 15.0 \* (Sf^0.5) (grassed waterway surface)

 $V = 10.0 * (Sf^0.5)$  (nearly bare & untilled surface)  $V = 9.0 * (Sf^0.5)$  (cultivated straight rows surface)

 $V = 7.0 * (Sf^0.5)$  (short grass pasture surface)

V = 5.0 \* (Sf^0.5) (woodland surface)

V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

V = (1.49 \* (R^(2/3)) \* (Sf^0.5)) / n

R = Aq / Wp

Tc = (Lf / V) / (3600 sec/hr)

### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

 $Aq = Flow Area (ft^2)$ 

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

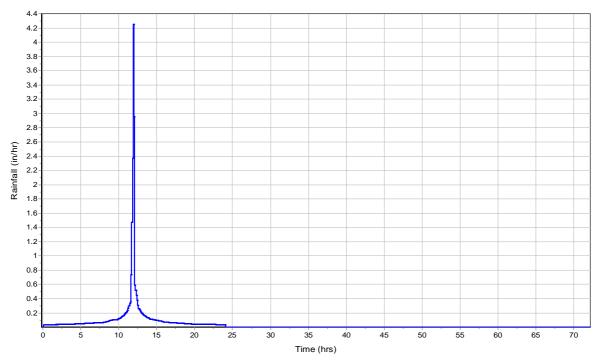
 $n \ = Manning's \ roughness$ 

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	0.3	0	0
Flow Length (ft):	100	0	0
Slope (%):	2	0	0
2 yr, 24 hr Rainfall (in) :	3.5	0	0
Velocity (ft/sec):	0.1	0	0
Computed Flow Time (min) :	16.31	0	0
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0	0
Slope (%):	2	0	0
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0	0
Computed Flow Time (min):	2.57	0	0
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	0.013	0	0
Flow Length (ft):	2975	0	0
Channel Slope (%):	1	0	0
Cross Section Area (ft²) :	3.425	0	0
Wetted Perimeter (ft):	7.06	0	0
Velocity (ft/sec):	7.08	0	0
Computed Flow Time (min) :	7.01	0	0
Total TOC (min)25.89			

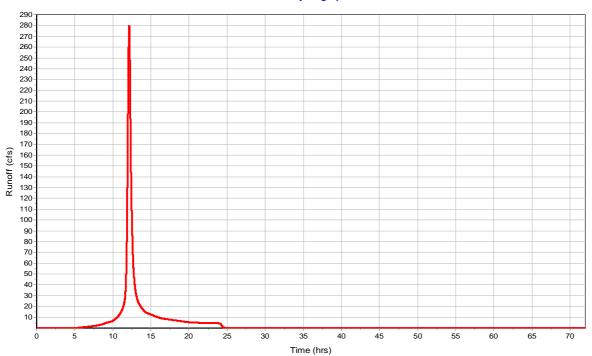
## **Subbasin Runoff Results**

Total Rainfall (in)	3.1
Total Runoff (in)	2.22
Peak Runoff (cfs)	279.69
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

## Rainfall Intensity Graph



### Runoff Hydrograph



### Subbasin: Sub-02

### Input Data

Area (ac)	0.52
Peak Rate Factor	484
Weighted Curve Number	. 95
Pain Gane ID	Rain Gage-01

### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	95
Composite Area & Weighted CN	0.52		95

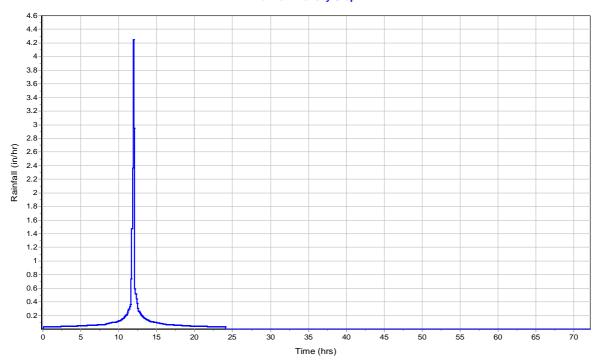
### **Time of Concentration**

User-Defined TOC override (minutes): 5

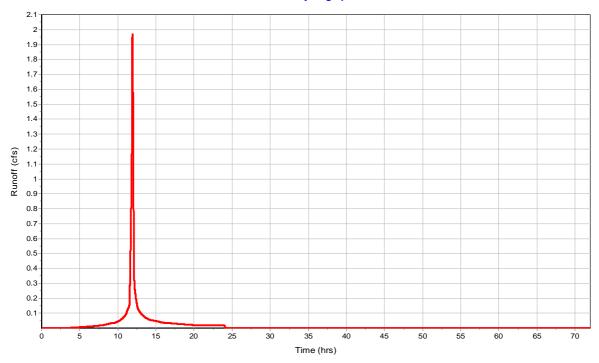
### **Subbasin Runoff Results**

Total Rainfall (in)	3.1
Total Runoff (in)	2.55
Peak Runoff (cfs)	1.97
Weighted Curve Number	95
Time of Concentration (days hh:mm:ss)	0 00:05:00

## Rainfall Intensity Graph



## Runoff Hydrograph





# **Project Description**

File Name ...... Proposed Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qty
Rain Gages	1
Subbasins	2
Nodes	3
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	1
Links	3
Channels	0
Pipes	1
Pumps	0
Orifices	2
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County		Rainfall Depth	Rainfall Distribution
								(years)	(inches)	
49		Time Series	2-Year	Cumulative	inches	Missouri	Jackson	2.00	3.71	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	132.96	484.00	91.58	3.71	2.80	371.89	349.78	0 00:25:53
2 Sub-02	0.52	484.00	95.00	3.71	3.15	1.64	2.40	0 00:05:00

# **Node Summary**

SN	I Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
-	l 1-Jun	Junction	101.00	106.00	0.00	0.00	0.00	0.25	101.13	0.00	4.87	0 00:00	0.00	0.00
2	2 Out-01	Outfall	100.00					350.02	100.12					
3	Stor-01	Storage Node	100.00	106.00	0.00		0.00	2.40	102.22				0.00	0.00

# **Link Summary**

SN Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
				()	()	()	( /	()		()	()					
1 Link-01	Pipe	1-Jun	Out-01	50.00	101.00	100.00	. ,	36.000	0.0150	( /	81.75	0.00	2.54	0.12	0.04	0.00 Calculated
1 Link-01 2 Orifice-01		1-Jun Stor-01				. , ,	. ,	. ,	0.0150	( /	. ,	0.00	2.54	. ,	0.04	0.00 Calculated

### **Subbasin Hydrology**

### Subbasin: Sub-01

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83
1/4 acre lots, 38% impervious	1.71	D	87
Urban commercial, 85% imp	19.01	С	94
Urban commercial, 85% imp	74.72	D	95
Multi-Family	3.11	С	90
Paved roads with curbs & sewers	0.4	D	98
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

Tc = (0.007 \* ((n \* Lf)^0.8)) / ((P^0.5) \* (Sf^0.4))

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

### Shallow Concentrated Flow Equation :

V = 16.1345 \* (Sf^0.5) (unpaved surface)

V = 20.3282 \* (Sf^0.5) (paved surface)

V = 15.0 \* (Sf^0.5) (grassed waterway surface)

 $V = 10.0 * (Sf^0.5)$  (nearly bare & untilled surface)  $V = 9.0 * (Sf^0.5)$  (cultivated straight rows surface)

 $V = 7.0 * (Sf^0.5)$  (short grass pasture surface)

V = 5.0 \* (Sf^0.5) (woodland surface)

V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

### Channel Flow Equation :

V = (1.49 \* (R^(2/3)) \* (Sf^0.5)) / n

R = Aq / Wp

Tc = (Lf / V) / (3600 sec/hr)

### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

 $Aq = Flow Area (ft^2)$ 

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

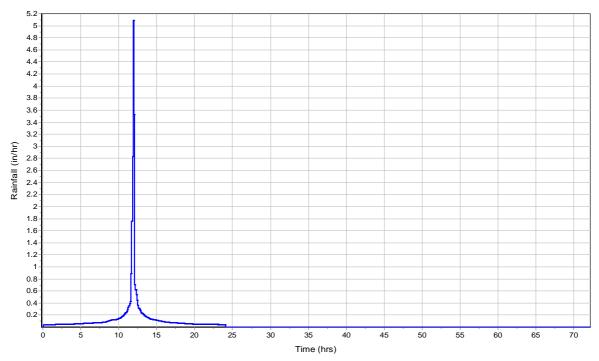
 $n \ = Manning's \ roughness$ 

	Subarea	Subarea	Subarea
Sheet Flow Computations	A	В	С
Manning's Roughness :	0.3	0	0
Flow Length (ft):	100	0	0
Slope (%):	2	0	0
2 yr, 24 hr Rainfall (in) :	3.5	0	0
Velocity (ft/sec):	0.1	0	0
Computed Flow Time (min) :	16.31	0	0
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0	0
Slope (%):	2	0	0
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0	0
Computed Flow Time (min) :	2.57	0	0
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness:	0.013	0	0
Flow Length (ft):	2975	0	0
Channel Slope (%):	1	0	0
Cross Section Area (ft²):	3.425	0	0
Wetted Perimeter (ft):	7.06	0	0
Velocity (ft/sec):	7.08	0	0
Computed Flow Time (min):	7.01	0	0
Total TOC (min)25.89			

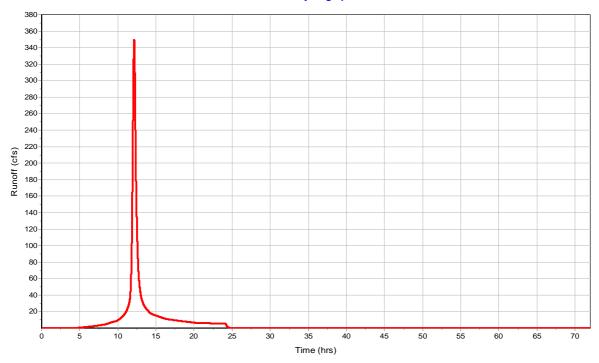
### **Subbasin Runoff Results**

Total Rainfall (in)	3.71
Total Runoff (in)	2.8
Peak Runoff (cfs)	349.78
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

## Rainfall Intensity Graph



### Runoff Hydrograph



### Subbasin: Sub-02

### Input Data

Area (ac)	0.52
Peak Rate Factor	484
Weighted Curve Number	. 95
Pain Gane ID	Rain Gage-01

### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	95
Composite Area & Weighted CN	0.52		95

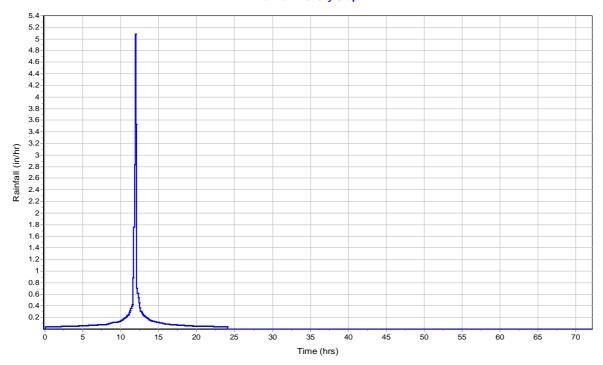
### **Time of Concentration**

User-Defined TOC override (minutes): 5

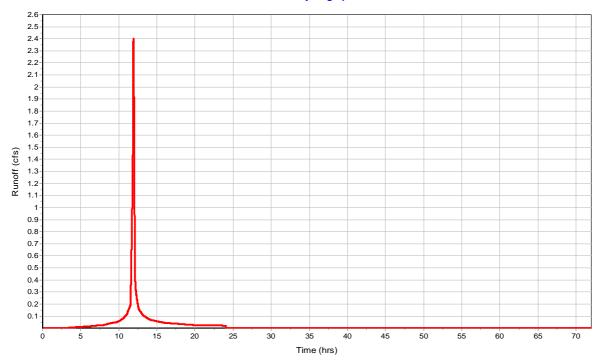
### **Subbasin Runoff Results**

Total Rainfall (in)	3.71
Total Runoff (in)	3.15
Peak Runoff (cfs)	2.4
Weighted Curve Number	95
Time of Concentration (days hh:mm:ss)	0 00:05:00

## Rainfall Intensity Graph



### Runoff Hydrograph





# **Project Description**

File Name ...... Proposed Conditions\_NOAA.SPF

## **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:00:05	days hh:mm:ss
Routing Time Step	1	seconds

## **Number of Elements**

	Qt
Rain Gages	1
Subbasins	2
Nodes	3
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	1
Links	3
Channels	0
Pipes	1
Pumps	0
Orifices	2
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

## **Rainfall Details**

SN	Rain Gage	_	Data Source		Rain	State	County		Rainfall	
	ID	Source	ID	Туре	Units				Depth (inches)	Distribution
49	)	Time Series	10 Year	Cumulative	inches	Missouri	Jackson	10.00	5.67	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	(ac)	484.00	91.58	(in) 5.67	. ,	(ac-in) 624.78	( /	(days hh:mm:ss) 0 00:25:53

# **Node Summary**

S	N Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
	1 1-Jun	Junction	101.00	106.00	0.00	0.00	0.00	0.35	101.15	0.00	4.85	0 00:00	0.00	0.00
	2 Out-01	Outfall	100.00					575.24	100.14					
	3 Stor-01	Storage Node	100.00	106.00	0.00		0.00	3.77	103.27				0.00	0.00

# **Link Summary**

SN Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow/	Peak Flow	Peak Flow	Peak Flow	Total Time Reported
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Design Flow	Velocity	Depth	Depth/	Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-01	Pipe	1-Jun	Out-01	50.00	101.00	100.00	2.0000	36.000	0.0150	0.35	81.75	0.00	2.78	0.14	0.05	0.00 Calculated
2 Orifice-01	Orifice	Stor-01	1-Jun		100.00	101.00		3.000		0.35						
3 Orifice-04	Orifico	Stor-01	1 lun		100.00	101.00		4.000		0.00						

# **Subbasin Hydrology**

#### Subbasin: Sub-01

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83
1/4 acre lots, 38% impervious	1.71	D	87
Urban commercial, 85% imp	19.01	С	94
Urban commercial, 85% imp	74.72	D	95
Multi-Family	3.11	С	90
Paved roads with curbs & sewers	0.4	D	98
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

Tc = (0.007 \* ((n \* Lf)^0.8)) / ((P^0.5) \* (Sf^0.4))

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation :

V = 16.1345 \* (Sf^0.5) (unpaved surface)

V = 20.3282 \* (Sf^0.5) (paved surface)

V = 15.0 \* (Sf^0.5) (grassed waterway surface)

 $V = 10.0 * (Sf^0.5)$  (nearly bare & untilled surface)  $V = 9.0 * (Sf^0.5)$  (cultivated straight rows surface)

 $V = 7.0 * (Sf^0.5)$  (short grass pasture surface)

V = 5.0 \* (Sf^0.5) (woodland surface)

V = 2.5 \* (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

#### Channel Flow Equation :

V = (1.49 \* (R^(2/3)) \* (Sf^0.5)) / n

R = Aq / Wp

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

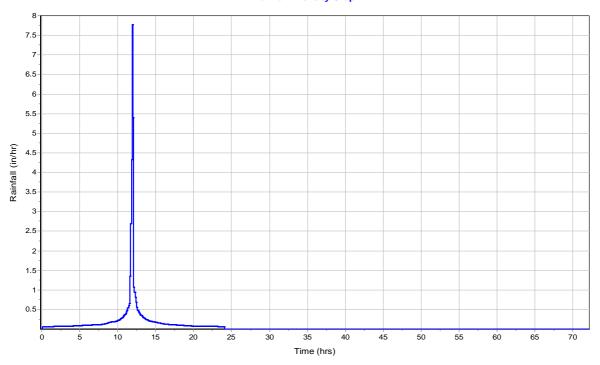
 $n \ = Manning's \ roughness$ 

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	0.3	0	0
Flow Length (ft):	100	0	0
Slope (%):	2	0	0
2 yr, 24 hr Rainfall (in) :	3.5	0	0
Velocity (ft/sec):	0.1	0	0
Computed Flow Time (min):	16.31	0	0
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0	0
Slope (%):	2	0	0
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0	0
Computed Flow Time (min) :	2.57	0	0
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	0.013	0	0
Flow Length (ft):	2975	0	0
Channel Slope (%):	1	0	0
Cross Section Area (ft²):	3.425	0	0
Wetted Perimeter (ft):	7.06	0	0
Velocity (ft/sec):	7.08	0	0
Computed Flow Time (min) :	7.01	0	0
Total TOC (min)25.89			

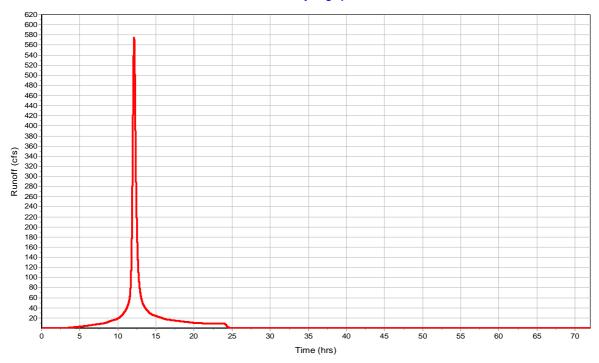
# **Subbasin Runoff Results**

Total Rainfall (in)	5.67
Total Runoff (in)	4.7
Peak Runoff (cfs)	574.93
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0 00:25:53

# Rainfall Intensity Graph



#### **Runoff Hydrograph**



# Input Data

Area (ac)	0.52
Peak Rate Factor	484
Weighted Curve Number	. 95
Pain Gane ID	Rain Gage-01

#### **Composite Curve Number**

32	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	95
Composite Area & Weighted CN	0.52		95

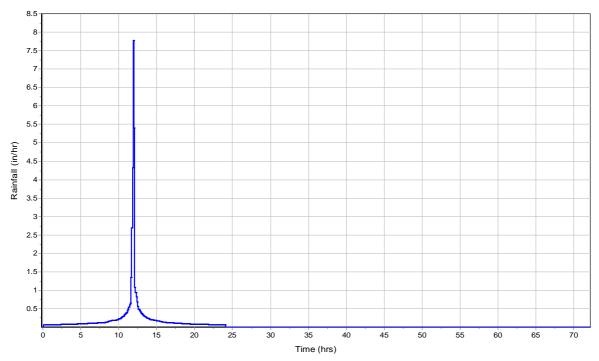
#### **Time of Concentration**

User-Defined TOC override (minutes): 5

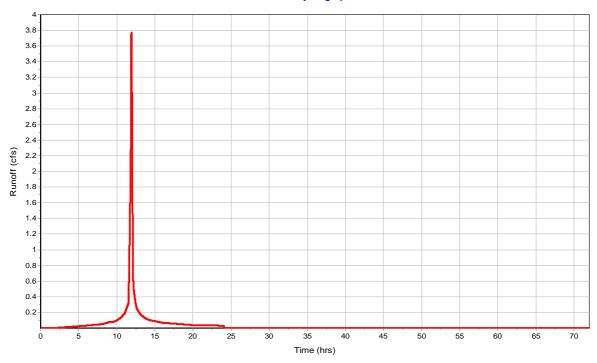
#### **Subbasin Runoff Results**

Total Rainfall (in)	5.67
Total Runoff (in)	5.08
Peak Runoff (cfs)	3.78
Weighted Curve Number	95
Time of Concentration (days hh:mm:ss)	0 00:05:00

# Rainfall Intensity Graph



#### **Runoff Hydrograph**





# **Project Description**

File Name ...... Proposed Conditions.SPF

# **Project Options**

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

# **Analysis Options**

Start Analysis On	Feb 15, 2023	00:00:00
End Analysis On	Feb 18, 2023	00:00:00
Start Reporting On	Feb 15, 2023	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:01:00	days hh:mm:ss
Routing Time Step	5	seconds

# **Number of Elements**

	Qty
Rain Gages	1
Subbasins	2
Nodes	3
Junctions	1
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	1
Links	3
Channels	0
Pipes	1
Pumps	0
Orifices	2
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

# **Rainfall Details**

SN	Rain Gage	Data	Data Source	Rainfall	Rain	State	County	Return	Rainfall	Rainfall
	ID	Source	ID	Туре	Units			Period	Depth	Distribution
								(years)	(inches)	
1		Time Series	100 Year	Cumulative	inches	Missouri	Jackson	100	7.70	SCS Type II 24-hr

# **Subbasin Summary**

SN Subbasin	Area	Peak Rate	Weighted	Total	Total	Total	Peak	Time of
ID		Factor	Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
			Number			Volume		
	(ac)			(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	132.96	484.00	91.58	7.70	6.70	890.43	804.27	0 00:25:53
2 Sub-02	0.52	484.00	95.00	7.70	7.10	3.69	5.18	0 00:05:00

# **Node Summary**

5	SN Element	Element	Invert	Ground/Rim	Initial	Surcharge	Ponded	Peak	Max HGL	Max	Min	Time of	Total	Total Time
	ID	Туре	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
				Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
										Attained		Occurrence		
_			(ft)	(ft)	(ft)	(ft)	(ft <sup>2</sup> )	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
	1 Jun-01	Junction	101.00	106.00	0.00	0.00	0.00	0.82	101.22	0.00	4.78	0 00:00	0.00	0.00
	2 Out-01	Outfall	100.00					803.29	100.21					
	3 Stor-01	Storage Node	100.00	106.00	0.00		0.00	5.18	105.74				0.00	0.00

# **Subbasin Hydrology**

#### Subbasin: Sub-01

#### **Input Data**

Area (ac)	132.96
Peak Rate Factor	484.00
Weighted Curve Number	91.58
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
1/4 acre lots, 38% impervious	34.01	С	83.00
1/4 acre lots, 38% impervious	1.71	D	87.00
Urban commercial, 85% imp	19.01	С	94.00
Urban commercial, 85% imp	74.72	D	95.00
Multi-Family	3.11	С	90.00
Paved roads with curbs & sewers	0.40	D	98.00
Composite Area & Weighted CN	132.96		91.58

#### **Time of Concentration**

TOC Method: SCS TR-55

Sheet Flow Equation :

Tc = (0.007 \* ((n \* Lf)^0.8)) / ((P^0.5) \* (Sf^0.4))

#### Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)
P = 2 yr, 24 hr Rainfall (inches)
Sf = Slope (ft/ft)

#### Shallow Concentrated Flow Equation :

 $V = 16.1345 * (Sf^0.5) (unpaved surface) \\ V = 20.3282 * (Sf^0.5) (paved surface) \\ V = 15.0 * (Sf^0.5) (grassed waterway surface) \\ V = 10.0 * (Sf^0.5) (nearly bare & untilled surface) \\ V = 9.0 * (Sf^0.5) (cultivated straight rows surface) \\ V = 7.0 * (Sf^0.5) (short grass pasture surface) \\ V = 5.0 * (Sf^0.5) (woodland surface) \\ V = 2.5 * (Sf^0.5) (forest w/heavy litter surface) \\ Tc = (Lf / V) / (3600 sec/hr) \\ \label{eq:velocity}$ 

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

#### Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$ 

R = Aq / Wp

Tc = (Lf / V) / (3600 sec/hr)

#### Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec) Sf = Slope (ft/ft)

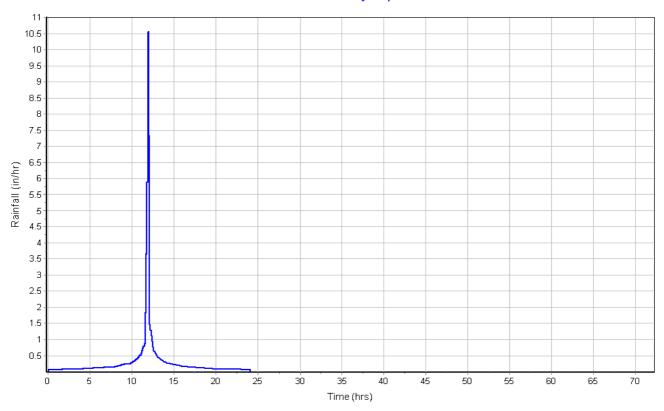
n = Manning's roughness

Sheet Flow Computations	Subarea A	Subarea B	Subarea C
Manning's Roughness :	.3	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	2	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.50	0.00	0.00
Velocity (ft/sec):	0.10	0.00	0.00
Computed Flow Time (min) :	16.31	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	443	0.00	0.00
Slope (%):	2	0.00	0.00
Surface Type :	Paved	Unpaved	Unpaved
Velocity (ft/sec):	2.87	0.00	0.00
Computed Flow Time (min):	2.57	0.00	0.00
	Subarea	Subarea	Subarea
Channel Flow Computations	Α	В	С
Manning's Roughness :	.013	0.00	0.00
Flow Length (ft):	2975	0.00	0.00
Channel Slope (%):	1	0.00	0.00
Cross Section Area (ft²):	3.425	0.00	0.00
Wetted Perimeter (ft):	7.06	0.00	0.00
Velocity (ft/sec):	7.08	0.00	0.00
Computed Flow Time (min) :	7.01	0.00	0.00
Total TOC (min)25.89			

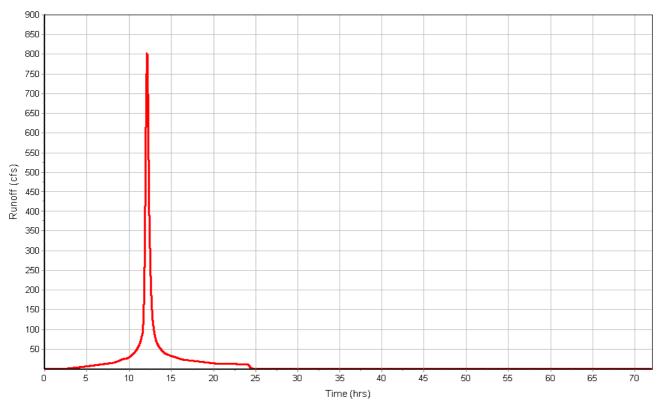
# Subbasin Runoff Results

Total Rainfall (in)	7.70
Total Runoff (in)	6.70
Peak Runoff (cfs)	804.27
Weighted Curve Number	91.58
Time of Concentration (days hh:mm:ss)	0.00:25:53

# Rainfall Intensity Graph



# Runoff Hydrograph



#### **Input Data**

Area (ac)	0.52
Peak Rate Factor	484.00
Weighted Curve Number	95.00
Rain Gage ID	Rain Gage-01

#### **Composite Curve Number**

iiposite oui ve ivallibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.52	-	95.00
Composite Area & Weighted CN	0.52		95.00

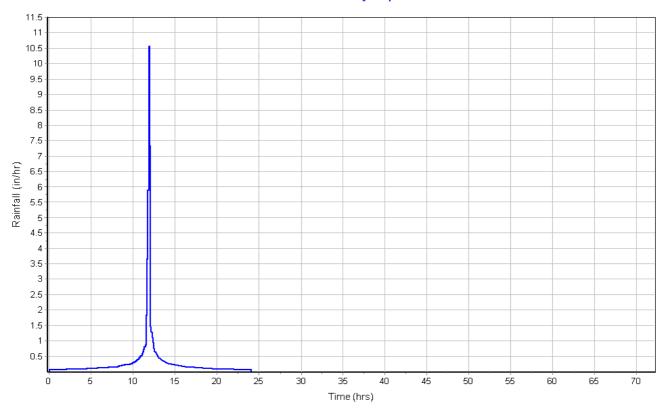
# Time of Concentration

User-Defined TOC override (minutes): 5

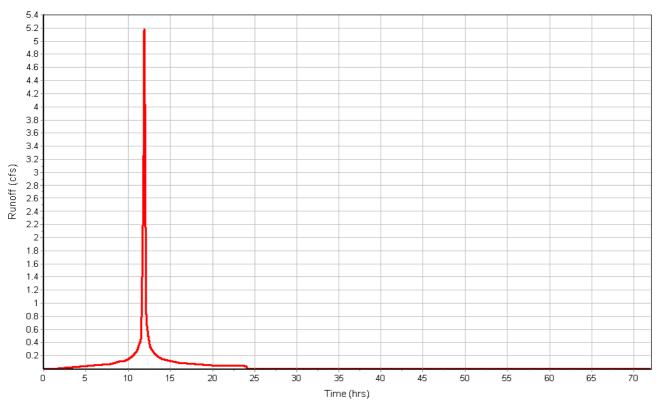
#### **Subbasin Runoff Results**

Total Rainfall (in)	7.70
Total Runoff (in)	
Peak Runoff (cfs)	5.18
Weighted Curve Number	95.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

# Rainfall Intensity Graph



# Runoff Hydrograph



# **Junction Results**

SN Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
		Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
					Attained					Occurrence		
	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1 Jun-01	0.82	0.00	101.22	0.22	0.00	4.78	101.03	0.03	0 12:09	0 00:00	0.00	0.00

# **APPENDIX D**

Soil Maps

#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 24, Aug 31, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Aug 30, 2022—Sep 8. 2022 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

# **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	С	232.8	60.9%
10128	Sharpsburg-Urban land complex, 2 to 5 percent slopes	D	6.9	1.8%
10180	Udarents-Urban land- Sampsel complex, 2 to 5 percent slopes	С	33.7	8.8%
10181	Udarents-Urban land- Sampsel complex, 5 to 9 percent slopes	С	15.5	4.0%
99012	Urban land, upland, 5 to 9 percent slopes		93.4	24.4%
Totals for Area of Inter	est		382.3	100.0%

# **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

# **APPENDIX E**

**FEMA** 

#### NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible undated or additional flood hazard information

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodemays have been determined, users are encouraged to consult the Flood and/or floodemays flow been determined, users are encouraged to consult the Flood within the Flood Insurance Study (FIS) pages that accompanies this FIRM. User should be aware that BFEs aboun on the FIRM represent rounded whole-lood should not be used as the sole source of flood elevation enterminent. Accordingly, flood elevation data presented in the FIG floopers should be utilized in conjunction with the FIRM for purposes of construction and findinglial management.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood insurance Pergarm. Floodway widths and other pertinent floodway data are provided in the Flood insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Flazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Missouri State Plane West Zone (FIPS sone 2403). The horizontal datum was MAD 83, GRS 1980 septemed. Utherarces in datum, softend projection or UNI zones used in the stifferences in map features across jurisdiction boundaries. These differences do not effect the accuracy of this FIRM.

Flood devotations on this map are referenced to the Noth American Verliad Dobumt of 1888. Thesis food devotations must be compared to startinus and ground absolutions referenced to the same verifical diatum. For information regarding conversion between the National Geodetic Verlica Dobum of 1980 and the North American Verlical Datum of 1980. Visit the National Geodetic Survey website at http://www.mas.enae.gov or confect for National Geodetic Survey website at the National Cedebitic Durincy of the following the National Cedebitic Survey website at the National Cedebitic Survey website at the National Cedebitic Survey at the following the National Cedebitic Survey websites at the National Cedeb

NGA, N/NGS12 National Geodetic Survey 55MC-3, #9202

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the Nationa Geodetic Survey at (301) 713-3242, or visit its website at <a href="http://www.ngs.npaa.gov">http://www.ngs.npaa.gov</a>.

The profile baselines depicted on this map represent the hydraulic modeling baseline that match the flood profiles in the FIS report. As a result of improved topographic data the profile baseline, in some cases, may deviate significantly from the channe centertine or appear outside the SFHA.

Based on updated topographic information, this map reflects more detailed and up to dote stream channel configurations and floodplain delineations than those shown on the previous Infilm for this jurisdaction. As a result the Flood Profiles and Floodway Data tables for multiple streams in the Flood Insurance. Shally Report (which contains authorisative hydraulic data) may reflect stream channel distances that differ from what is shown on the map. Also, the road to floodplain relationships for unrevised streams may differ from what

corporate limits shown on this map are based on the best data available at the time

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses, and a Listing of Communities table containing National Flood insurance Program dates for each community as well as a little of the panels on which each community

For information on available products associated with this FIRM visit the Map Service Center (MSC) website at <a href="http://msc.fema.gov">http://msc.fema.gov</a>, Available products may include previously issued Letters of Map Change a Flood Insurance Study Report and/or digital versions of this map. Many of these products can be ordered obtained directly from the MSC website.

2825000 ET 2830000 FT 041 201 27 51 1005000 FT Prarie Lee Lake

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD It chance flood (100-year flood), also known as the base flood, is the fix of bridge grainlef or exceeded in any place year. The Special Rood Haze sto floodings the fix of modified by the fixed flood in the fixed flood in the fixed flood flood flood.

ZONE AE Base Fluid Elevations determined. ZONE AH

Flood deaths of 1 to 3 feet (usually areas of nonding): Base Flood Fleiotion

Coastal flood zone with velocity hazard (wave action); no Dase Flood Elevation reserves of

FLOODWAY AREAS IN ZONE AE

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 squar mile; and areas protected by levees from 1% annual chance flood.

Areas determined to be subside the 0.2% annual chance floodolain.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAS)

(LZ% Approx) Chance Moodplain Boundar Clondway boundary

> Zone D boundary CROS and CRA houndary

Doundary dividing Special Flood Hazard Area Zones and bound dwiding Special Flood Hazard Areas of different Base Flood Ele-flood darkles on flood valveilies

Base Flood Elevation line and value; elevation in feet Base Flood Elevation value whate uniform within zone; elevation is fast 4

(23) - - - - - (23)

.....

(EL 987)

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) Western Hemisphere

5000-foot ticks: Missouri State Plane West Zone (FIPS Zone 2403), Transverse Mercator projection DX5510 × • MI 5

MAP REPUSITURIES Refer to Map Repositories list on Map Index

EFFECTIVE DATE(3) OF REVISION(3) TO THIS PANEL January 20, 2017 - to change Special Flood Hazard Areas.

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

MAP SCALE 1" = 500"





MAP REVISED JANUARY 20, 2017

MAP NUMBER

29095C0436G

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# LEE'S SUMMIT DOWNTOWN MARKET DRAINAGE STUDY

Lee's Summit, MO

July 2023

Olsson Project No. 022-00393