

To: Lee's Summit Senior Community, LLC

5051 S. National Avenue, Ste. 4-110

Springfield, Missouri 65810

From: Anderson Engineering, Inc.

941 W 141st Terrace Kansas City, MO 64145

Date: March 10, 2023

Subject: The Princeton Senior Living Revised Drainage Memo

The purpose of this memorandum is to determine the impacts of converting the existing extended dry detention basin to a wet bottom detention basin on the analyzed drainage area. Reference *Appendix A* for an exhibit of proposed improvements.

Per the approved stormwater report, dated July 19th, 2019, 2 drainage areas DEV 10 (2.94 Ac.) and DEV 20 (2.40 Ac.) flow to Bioretention Facilities #1 and #2, respectively, then to the extended dry detention basin. Drainage area, DEV 30 (4.08 Ac.) flows through an underground stormwater system directly to the existing extended dry detention basin. The extended dry detention basin, along with drainage areas DEV12 and OUT11, discharge to Point of Interest #1. The approved stormwater report shows that the discharge from the site is within acceptable levels. Reference *Appendix B* for pages from the approved drainage report.

The proposed wet bottom detention basin was designed minimizing impacts to the approved drainage analysis and extended dry detention basin design. The wet bottom detention pond is proposed to be 5 ft deep with a 3:1 side slope. The existing extended dry detention basin outfall structure's elevation is 1013.19 and the permanent pool elevation of the wet bottom detention basin will be maintained at that elevation. No modifications to the primary outlet works are proposed. The permanent pool elevation will be at or below all receiving and discharge elevations and thus, in the event that the permanent pool needs to be drained, a pump will be utilized. By maintaining the existing outfall elevation and excavating the current bottom basin slope to the existing outlet, the overall volume for the detention will be increased. Reference *Table 1* below for an existing vs. proposed stage-storage curve comparison. Reference *Table 2* for revised outflow data. Reference *Appendix C* for revised detention calculation reports.

Table 1: Existing vs. Proposed Stage-Storage

Stage (ft)	Elevation (ft)	Ex. Contour Area (sf)	Prop. Contour Area (sf)	Ex. Total Storage (ft³)	Prop. Total Storage (ft³)	Total Volume Difference (cf)
0.00	1013.00	0	6,640	0	0	0
1.00	1014.00	4,594	8,130	1,531	7,372	+5,841
2.00	1015.00	11,499	10,733	9,317	16,772	+7,455
3.00	1016.00	15,079	15,079	22,565	29,615	+7,050
4.00	1017.00	17,882	17,882	39,024	46,074	+7,050
5.00	1018.00	20,841	20,841	58,364	65,415	+7,051
6.00	1019.00	24,958	24,958	80,744	88,281	+7,537
7.00	1020.00	27,232	27,232	106,319	114,366	+8,047
8.00	1021.00	30,663	30,663	135,246	143,293	+8,047
9.00	1022.00	34,251	34,251	167,683	175,730	+8,047

Table 2: Developed Condition Summary*

	Q _{2-yr} (cfs)	Q _{10-yr} (cfs)	Q100 _{-yr} (cfs)	100-yr WSE (ft)
Allowable	4.71	18.84	28.26	1020.80
Ex. Dry Det. Discharge	1.24	5.91	15.89	1020.77
Pro. Det. Discharge	0.97	3.93	15.78	1020.59
Ex. Vs Pro. Difference	-0.27	-1.98	-0.11	-0.19

^{*}Reference approved drainage study Table 4A, pg. 8 of 99 for developed conditions analysis summary point of interest #1.

Conclusions and Recommendations

The impacts of converting the existing extended dry detention basin to a wet bottom detention basin has been analyzed for this memorandum. It has been determined that by maintaining the existing outfall elevation the detention basin volume has increased and the overall water surface elevation has decreased. The proposed detention basin improvements have also been shown to decrease the overall 100-yr water surface elevation.

Please feel free to contact me with any additional questions or comments.

Thank you,

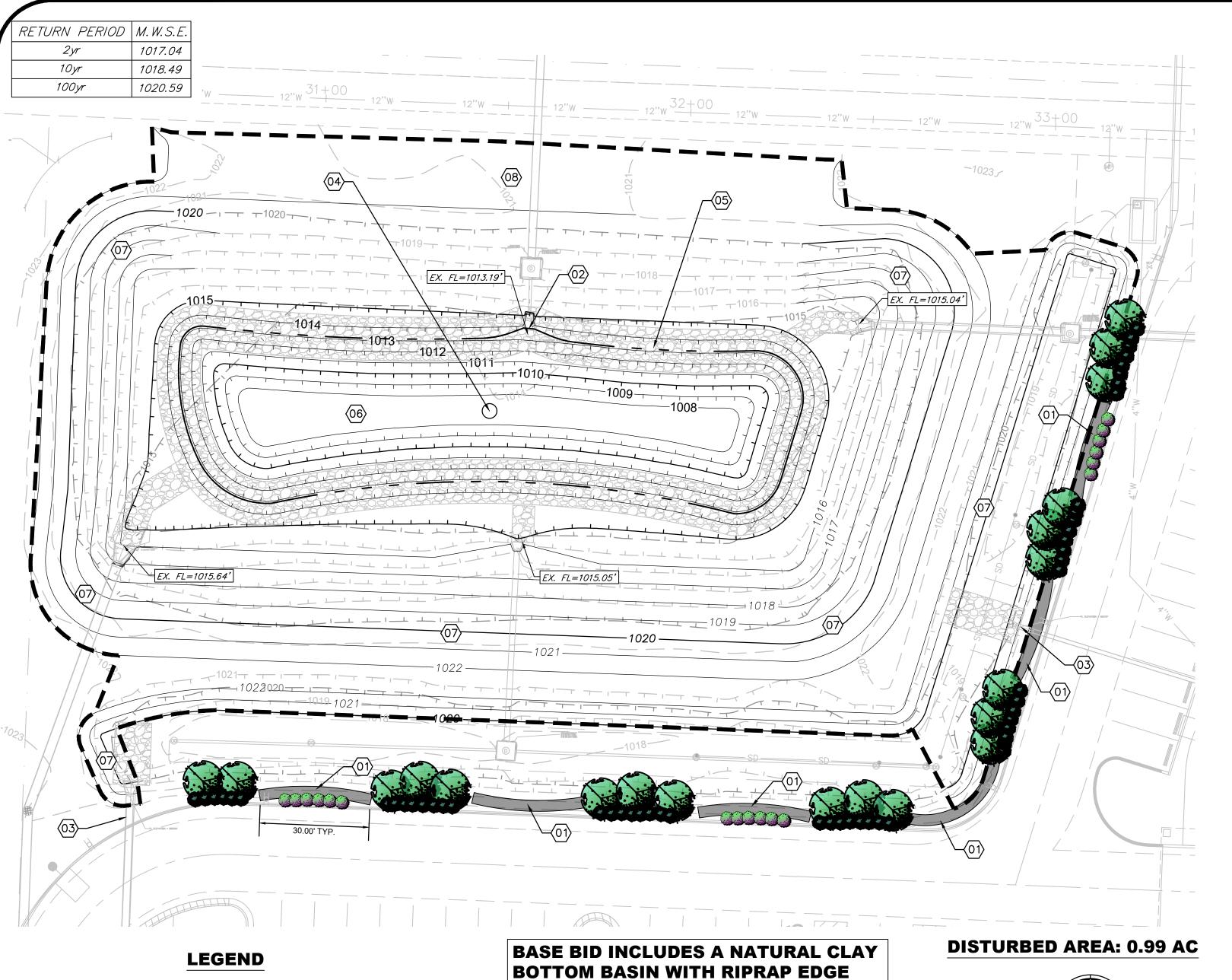
Trevor Fox, PE

Anderson Engineering, Inc.

2

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APPENDIX AProposed Improvements



TREATMENT.NOTE BID ALTERNATES ON SHEET C100 AND C101





GENERAL NOTES

ALL TOPSOIL, VEGETATION, ROOT STRUCTURES, AND DELETERIOUS MATERIALS SHALL BE STRIPPED FROM THE GROUND SURFACE PRIOR TO THE PLACEMENT OF EMBANKMENTS.

FINISH GRADE 5' CONTOUR

FINISH GRADE 1' CONTOUR

EXISTING GRADE 5' CONTOUR

EXISTING GRADE 1' CONTOUR

PERMANENT POOL ELEVATION (1013.19)

STONE EDGE TREATMENT

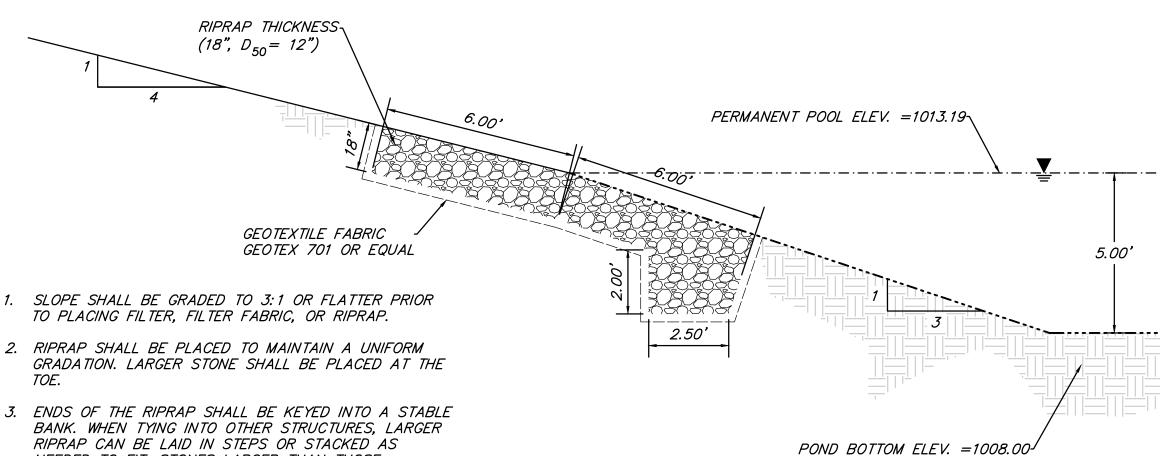
STACKED LEDGESTONE

DISTURBED AREA

- 2. ALL DISTURBED AREAS THAT ARE NOT TO BE PAVED (GREEN SPACES) SHALL BE FINISH GRADED WITH A MINIMUM OF SIX INCHES OF TOPSOIL.
- FINISHED GRADES SHALL NOT BE STEEPER THAN 3:1.
- EXISTING GRADE CONTOURS SHOWN AT 1 FOOT INTERVALS. PROPOSED GRADE CONTOURS SHOWN AT 1
- HAUL OFF AND MATERIAL IMPORT SHALL NOT BE AN EXCLUDED ITEM IN THE BASE BID. ALL EXCAVATION SHALL BE CONSIDERED NON-CLASSIFIED. NO ADDITIONAL PAYMENT WILL BE MADE FOR ROCK EXCAVATION OR BLASTING.
- ALL DISTURBED AREAS ARE TO RECEIVE TOPSOIL (6"), SEED/SOD, MULCH AND WATER UNTIL A HEALTHY STAND OF GRASS IS ESTABLISHED. RE—SEEDING SHALL BE REQUIRED.
- WITHIN FORTY—EIGHT HOURS PRIOR TO ANY ASPHALT OR CONCRETE PAVING, THE SUBGRADE SHALL BE PROOF-ROLLED WITH A FULLY LOADED TANDEM WHEEL DUMP TRUCK AND OBSERVED BY THE ON-SITE GEOTECHNICAL ENGINEER. AREAS OF THE SUBGRADE WITH EXCESSIVE RUTTING AND/OR PUMPING SHALL BE RE-WORKED OR REMOVED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS. FLY ASH OR GRANULAR MATERIAL MAY BE ADDED BY THE CONTRACTOR (AS APPROVED BY THE ON-SITE GEOTECHNICAL ENGINEER) TO STABILIZE THE SUBGRADE.
- REFERENCE GEOTECHNICAL REPORT FOR BUILDING PAD PREPARATION. CONTRACTOR SHALL OPERATE UNDER THE TERMS AND PERMITS INCLUDED IN THE STORMWATER POLLUTION PREVENTION PLAN (SWPPP) PREPARED FOR THIS PROJECT AND PERMITTED THROUGH THE STATE OF MISSOURI. CONTRACTOR SHALL EMPLOY A QUALIFIED PERSON TO CONDUCT REGULAR INSPECTIONS OF THE SITE EROSION CONTROL MEASURES AND DOCUMENT SUCH INSPECTIONS IN THE SWPPP DOCUMENT MAINTAINED BY THE CONTRACTOR.
- THE CONTRACTOR SHALL ADHERE TO ALL TERMS & CONDITIONS AS OUTLINED IN THE PERMIT FOR STORMWATER DISCHARGE ASSOCIATED WITH THE CONSTRUCTION ACTIVITIES AS ISSUED BY THE CITY OF
- 11. REFERENCE OLSSON GEOTECHNICAL REPORT, DATED FEBRUARY 15, 2019, FOR BORING LOGS EXPLORATION *RESULTS*

KEYED NOTES

- BID ALTERNATE: INSTALL STACKED LEDGESTONE IN ARC AS SHOWN. CONTRACTOR TO STACK STONE AS NECESSARY UNTIL 24" MIN. ABOVE EXISTING FLUSH CURB IS EXPOSED. CONTRACTOR TO COORDINATE COLOR WITH OWNER.
- EXISTING CONCRETE HEADWALL W/ FLOW CONTROL ASSEMBLY TO REMAIN. CONTRACTOR SHALL NOT DISTURB EXISTING CONCRETE HEADWALL.
- EXISTING STORM SEWER TO REMAIN. CONTRACTOR SHALL NOT DISTURB EXISTING STORM SEWER.
- INSTALL SCOTT AERATOR (DA-20) WITH SCOTT NIGHT GLO LED LIGHTING KIT, OR APPROVED EQUAL, AS SHOWN ON PLANS. REFERENCE MEP PLANS FOR ELECTRICAL ROUTING AND POWER REQUIREMENTS. CONTRACTOR TO COORDINATE WITH OWNER ON HORSEPOWER REQUIREMENT FOR DESIRED SPRAY HEIGHT AND DIAMETER
- INSTALL RIPRAP EDGE TREATMENT PER POND EDGE TREATMENT DETAIL ON BID ALTERNATE: INSTALL CONCRETE WALL EDGE TREATMENT. GRADING AND DETAIL PER SHEET C101.
- WET BOTTOM RETENTION BASIN. CONTRACTOR TO PROVIDE THE FOLLOWING BID ALTERNATES FOR POND BOTTOM LINING.
 - 1. 18" BENTONITE CLAY LINER TO PERMANENT POOL ELEVATION 2. 45 MIL. EPDM POND LINER INSTALLATION.
- CONTRACTOR TO REESTABLISH EXISTING CONTOURS AS SHOWN ON PLAN TO PROVIDED MIN. REQUIRED DETENTION VOLUME.
- CONTRACTOR TO VERIFY EMERGENCY SPILLWAY ELEVATIONS.



RIPRAP CAN BE LAID IN STEPS OR STACKED AS NEEDED TO FIT. STONES LARGER THAN THOSE DESIGNED FOR FLOW SHALL BE USED FOR THIS

- 4. REMAINING DISTURBED AREAS SHALL BE GRADED AND PERMANENTLY SEEDED AND MULCHED.
- 5. RIPRAP SHALL BE GREY LIMESTONE, OR APPROVED EQUAL. AND SHALL MEET MODOT STANDARDS FOR SOUNDNESS, ABRASION, AND DURABILITY

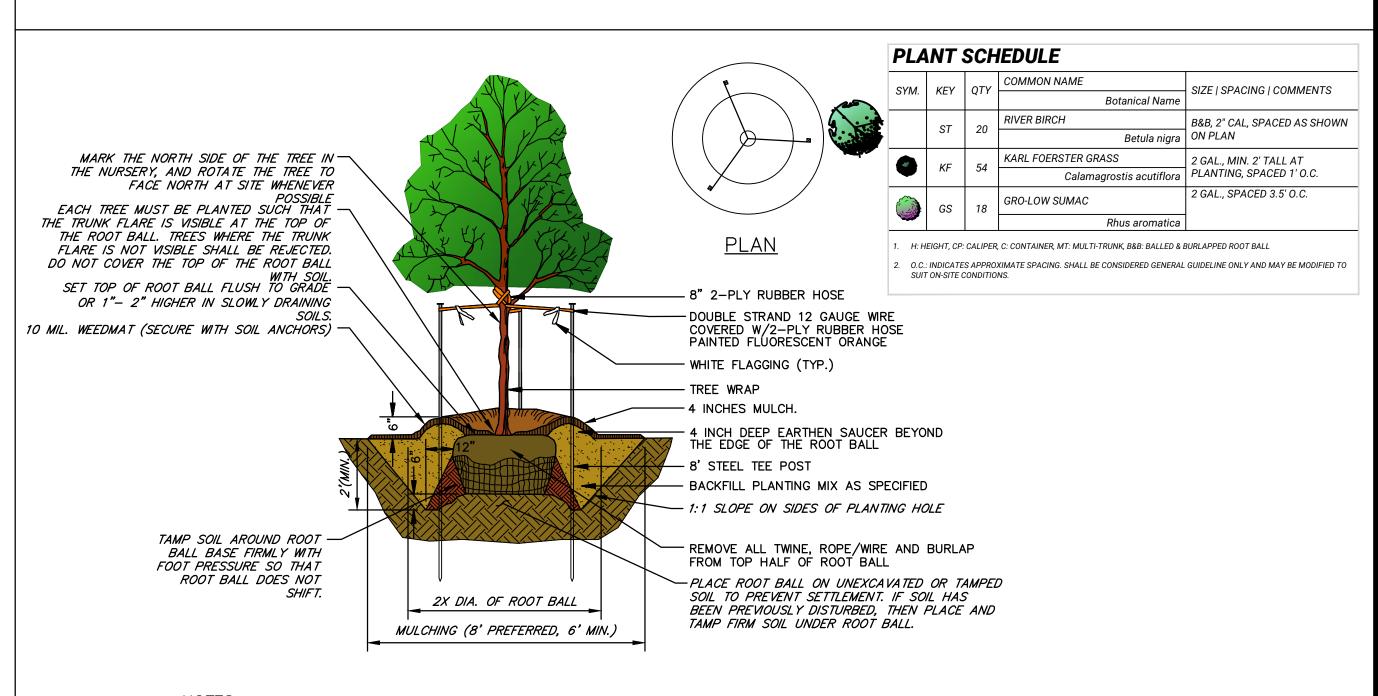
POND EDGE TREATMENT DETAIL

SCALE: N.T.S.



- CONTRACTOR TO CUT INTO EXISTING SLOPE AND PLACE STONE ON A STABLE SHELF LEAVING 24" OF STONE EXPOSED AT CURB EDGE.
- 2. CONTRACTOR TO COORDINATE WITH OWNER ON STONE COLOR FROM SUPPLIER. PHOTOS PROVIDED AS REFERENCE ONLY.

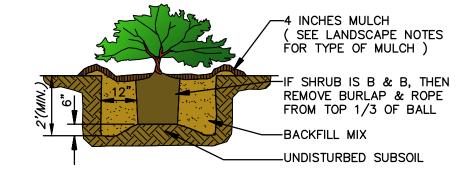
STACKED LEDGESTONE LANDSCAPING (BID ALTERNATE)



- 1. DO NOT HEAVILY PRUNE TREE AT PLANTING. PRUNE ONLY CROSSOVER LIMBS, CO-DOMINANT LEADERS, AND BROKEN OR DEAD BRANCHES. SOME INTERIOR TWIGS AND LATERAL BRANCHES MAY BE PRUNED; HOWEVER, DO NOT REMOVE THE TERMINAL BUDS OF BRANCHES THAT EXTEND TO THE EDGE OF THE CROWN.
- 2. STAKE AND/OR WRAP TREES ONLY UPON THE APPROVAL OF THE LANDSCAPE ARCHITECT. 3. BACKFILL WITH EXISTING SOIL IN SANDY LOAM SOILS. ADD 20% MAX. BY VOLUME COMPOSTED ORGANIC MATERIAL TO THE EXISTING SOIL.
- 4. SEE LANDSCAPE PLAN NOTES FOR TYPE OF MULCH TO BE USED. 5. REMOVE TEE POSTS, WIRE WRAPPED IN RUBBER HOSE AND FLAGGING AFTER ONE COMPLETE GROWING SEASON (MARCH-OCTOBER).

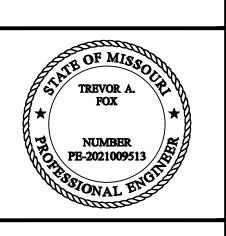
TREE PLANTING DETAIL

N.T.S.



LANDSCAPE DETAILS (BID ALTERNATE)

	DRAWING INFO.	DNT	ЭЭГ		2/17/23	ISSUED FOR: FOR REVIEW	23KC10002	
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	REVISIONS	DESCRIPTION						© COPYRIGHT ANDERSON ENGINEERING, INC. 2023
1		NO.						



SHEET NUMBER

APPENDIX BApproved Drainage Report

FINAL STORMWATER DRAINAGE STUDY FOR LEE'S SUMMIT SENIOR LIVING COMMUNITY

SE Oldham Parkway Lee Summit, Missouri

South Prairie Lee Watershed

Prepared for:

Lee's Summit Senior Community, LLC 5051 S. National Avenue, Ste. 4-110 Springfield, Missouri Phone: 417-893-6006



2nd Submittal July 2019

Prepared By: Trevor Drake
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Missouri Engineering Certificate of Authority #001592
Olsson Project No. 018-1450



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June 2019

APPENDICES

APPENDIX A Hydrology & Detention Calculations

APPENDIX B FEMA Firmette

APPENDIX C APWA \ MARC BMP Level of Service & Water Quality Calculations

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1. GENERAL INFORMATION

The following stormwater report is for the Lee's Summit Senior Living Community located near the southern boundary of the South Prairie Lee Watershed on the south side of Oldham Parkway approximately 0.4 miles east of Todd George Parkway. The proposed 157,515-sqft facility will be on a 10.45 acre± site that is currently vacant pasture land. In the existing condition the site generally flows from south to the north towards Oldham Parkway. A subtle ridge line splits the site into two sub-drainage areas. The western onsite drainage area discharges to the Oldham Parkway drainage swale at the northwest corner of the site (POI #1). The swale drains to a 5'x5' RCB culvert that flows north underneath the Oldham Parkway, US Route 50, and Blue Parkway to the E. Fork Little Blue River through an unnamed tributary. The eastern onsite drainage area intercepts offsite runoff from approximately 5-acres of agricultural land from the east. Runoff continues to flow north and northeast to an existing 30" RCP culvert (POI #2) that discharges north underneath Oldham Parkway, US Route 50, and Blue Parkway. Storm water continues north to an existing wet detention facility located south of Shenandoah Drive.

Stormwater runoff from the proposed Lee's Summit Senior Living Community will be collected and conveyed through onsite storm sewer, that is routed to proposed bioretention and extended dry detention facilities. These facilities will discharge the water in compliance with the KC APWA "Comprehensive Control Strategy" to the proposed public storm sewer that will be installed with the Oldham Parkway street improvements.

According the FEMA Flood Map Service Center the site is <u>not</u> located in a flood hazard area per map #29095C049G dated 01/20/2017. The FEMA FIRMette has been included in Appendix B.

Per the National Wetlands Inventory, the site has no "blue line" streams or wetlands are located on site.

Soil data was taken from the USDA Natural Resources Conservation Service – Web Soil Survey of Jackson, County Missouri. The Web soil survey categorize soils on the proposed Lee's Summit Senior Living Community as:

TABLE 1. SITE SOIL CLASSIFICATION

Map Unit	Map Unit Name	Percent Slopes	Rating	Area in AOI (acres)	Percent of AOI
10000	Arisburg Silt Loam	1 to 5	С	15.9	85.9%
10082	Arisburg-Urban land complex	1 to 5	С	2.6	14.1%

^{*}see Web Soil Survey pdf located in Appendix A

2. METHODOLOGY

This Stormwater Drainage Study has been prepared to evaluate the hydrologic impact generated by the development of the Lee's Summit Senior Living Community and adjacent public street improvements. The base data for models prepared for this report have been obtained through topographic surveys, online maps, and aerial imagery.

The following method was used to study and model existing and proposed conditions for stormwater runoff:

- TR-55 Unit Hydrograph Method
 - 2-year, 10-year, 100-year Return Frequency Storms
 - o 24-Hour SCS Type II Rainfall Distribution
 - o SCS Runoff Curve Numbers Per SCS TR-55
 - SCS TR-55 Methods for determining Time of Concentration and Travel Time

Rainfall depth & duration data were taken from the National Oceanic and Atmospheric Administration (NOAA). A summary of the rainfall data used in the calculations are presented in Table 2.

TABLE 2. RAINFALL PRECIPITATION

Annual Exceedance Probability (AEP)	Rainfall Depth (inches)
1-year	3.71
10-year	5.66
100-year	9.25

^{*}Hydraflow reports have been provided in Appendix A

3. EXISTING CONDITIONS ANALYSIS

Existing conditions where modeled assuming pasture in good condition. This assumption was used to calculate existing condition flow rates and the level service required for proposed BMP

implementation. Discharge from the proposed development will adhere to APWA and Lee's Summit discharge requirements. Refer to Figure 1 for existing condition sub-drainage area locations, runoff curve numbers, and sub-drainage area acreage.

In the existing condition, the site generally flows from south to the north towards Oldham Parkway. A subtle ridge line splits the site into two sub-drainage areas. The western onsite drainage area (EX10) discharges to the Oldham Parkway drainage swale at the northwest corner of the site (POI #1). The swale drains to a 5'x5' RCB culvert that flows north underneath the Oldham Parkway, US Route 50, and Blue Parkway to the E. Fork Little Blue River through an unnamed tributary.

The eastern onsite drainage area (EX20) intercepts offsite runoff from approximately 5-acres of pasture land from the east (OFF20). Runoff continues to flow north and northeast to an existing 30" RCP culvert (POI #2) that discharges north underneath Oldham Parkway, US Route 50, and Blue Parkway. Storm water continues north to an existing wet detention facility located south of Shenandoah Drive.

The following table(s), Table 3A & 3B, summarizes the results of the existing conditions analysis:

TABLE 3A. EXISTING CONDITIONS ANALYSIS SUMMARY POINT OF INTEREST #1

Subarea	Existing	Existing	Existing
	Q _{2-year}	Q _{10-year}	Q _{100-year}
	(cfs)	(cfs)	(cfs)
EX POI #1	16.24	34.88	72.52

TABLE 3B. EXISTING CONDITIONS ANALYSIS SUMMARY POINT OF INTEREST #2

Subarea	Existing	Existing	Existing
	Q _{2-year}	Q _{10-year}	Q _{100-year}
	(cfs)	(cfs)	(cfs)
EX PO1 #2	16.94	36.47	75.73

4. PROPOSED CONDITIONS ANALYSIS

The proposed conditions section of this analysis assumes completion of the Lee's Summit Senior Living Community and adjacent public street improvements. A CN value of 98 was used for all building and pavement surfaces. A CN values of 80 was used for all developed open space. As in the existing conditions, the proposed conditions stormwater runoff model was created and ran for the 2, 10, and 100-year storm events. The complete output for the Hydraflow model has been included in Appendix A. Refer to Figure 2 for developed subdrainage area locations, runoff curve numbers, and sub-drainage area acreage.

In the developed condition drainage area DEV 10 flows into Bio Detention Facility #1 before flowing into the proposed dry detention basin. Drainage area DEV 20 is routed through Bio Detention Facility #2 before it is discharged to the dry detention basin. Drainage area DEV 30 is conveyed into the dry detention basin through an underground storm sewer system. The detention facility discharges to Point of Interest #1, Discharge from the detention basin will be less than allowable flow rates established using the "Comprehensive Control Strategy". Additionally, the dry detention will provide a 40-hour minimum extended drainage time of the 90% storm runoff volume. Stormwater flow from the detention facility, DA12 and OFF11 combine at Point of Interest #1 located immediately upstream of the existing 5'x5' box culvert to flows north beneath Oldham Parkway.

Point of Interest #2 accepts the accumulation of flow from OFF 20, DA 21, and DA 22. Offsite and public right-of-way stormwater runoff is collected in an underground storm sewer system and conveyed to the 30-inch concrete pipe that flows north beneath Oldham Parkway.

The following tables contain input data and summarize the computed results of the developed conditions analysis:

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TABLE 4A. DEVELOPED CONDITIONS ANALYSIS SUMMARY POINT OF INTEREST #1

Subarea	Drainage Area (acres)	Curve Number	Tc (Minutes)	Developed Q _{2-year} (cfs)	Developed Q _{10-year} (cfs)	Developed Q _{100-year} (cfs)
DEV 10	2.94	92	5	13.29	21.46	36.24
BIO #1				12.54	20.61	35.10
DEV 20	2.40	89	5	10.01	16.75	28.97
BIO #2				8.13	15.53	25.01
DEV 30	4.08	89	5	17.02	28.48	49.26
DRY DET. DISCHARGE	9.42			1.24	5.91	15.89
ALLOWABLE				4.71	18.84	28.26
DA 12 (R/W)	1.21	87	5	4.75	8.15	14.36
OFF 11	8.28	74	25.6	10.78	23.30	48.68

TABLE 4B. DEVELOPED CONDITIONS ANALYSIS SUMMARY POINT OF INTEREST #2

Subarea	Drainage Area (acres)	Curve Number	Tc (Minutes)	Developed Q _{2-year} (cfs)	Developed Q _{10-year} (cfs)	Developed Q _{100-year} (cfs)
DA 21 (R/W)	1.5	88	5	6.07	10.29	17.96
DA 22 (R/W)	0.54	85	5	1.98	3.50	6.28
OFF 20	5.39	75	32.7	6.44	13.67	28.27

TABLE 5A. DRY DETENTION FACILITY SUMMARY

Return Frequency	Developed Q _{DEV} (cfs)	Detention Volume (cf)	WSE (ft)
2	1.24	43,010	1017.21
10	5.91	72,321	1018.62
100	15.89	128,492	1020.77

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TABLE 5B. BIO DETENTION #1 FACILITY SUMMARY

Return Frequency	Developed Q _{DEV} (cfs)	Detention Volume (cf)	WSE (ft)
2	12.54	8,754	1021.24
10	20.61	9,607	1021.33
100	35.10	10,893	1021.48

TABLE 5C. BIO DETENTION #2 FACILITY SUMMARY

Return Frequency	Developed Q _{DEV} (cfs)	Detention Volume (cf)	WSE (ft)
2	8.13	8,037	1022.79
10	15.53	9,138	1022.94
100	25.10	10,956	1023.15

TABLE 6A. POINT OF INTEREST #1 SUMMARY

Return Frequency	Existing Q _{pre} (cfs)	Developed Q _{DEV} (cfs)
2	16.24	11.96
10	34.88	28.37
100	72.52	66.43

TABLE 6B. POINT OF INTEREST #2 SUMMARY

Return Frequency	Existing Q _{pre} (cfs)	Developed Q _{DEV} (cfs)
2	16.94	10.95
10	36.47	20.60
100	75.73	39.30

5. POST CONSTRUCTION WATER QUALITY

Water quality volume treatment calculations were determined using the 2012 APWA/MARC BMP manual level of surface calculations. The level of surface calculation considered all onsite development. Existing offsite right-of-way and proposed public right-of-way will not be conveyed through onsite BMPs. Water quality level of service and water quality volume calculations are provided in Appendix C.

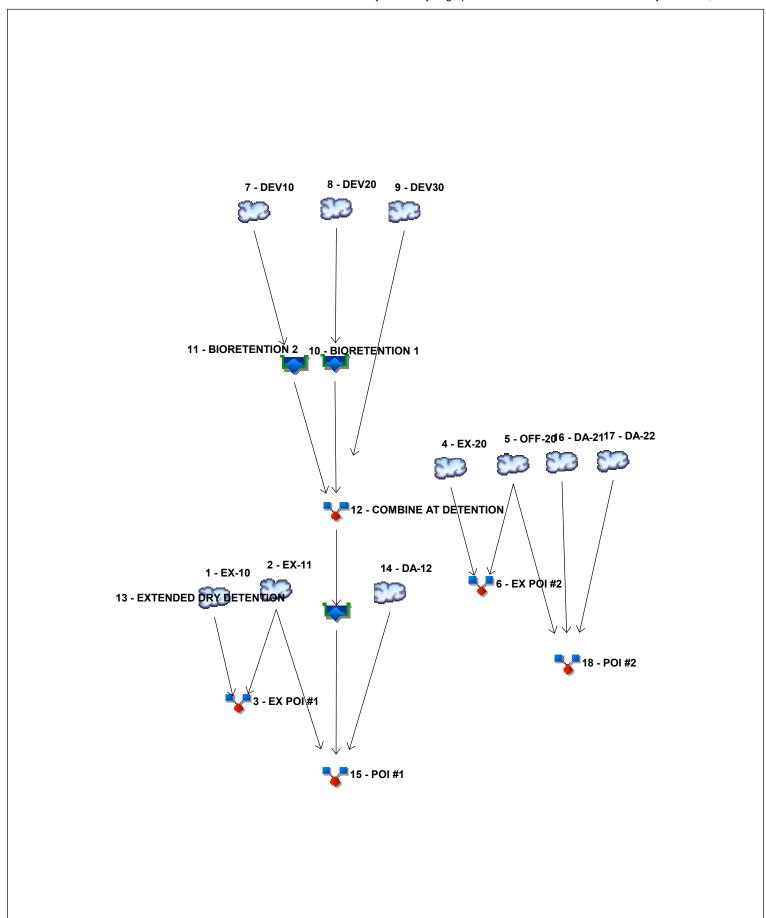
6. CONCLUSIONS & RECOMMENDATIONS

The Lee's Summit Senior Living Community has been evaluated in this report to show that the stormwater discharge from the site will remain within the acceptable levels. A new detention basin and two new biodetention basins are to be constructed to handle the increased runoff created from the development.

In conclusion, all peak discharges at the points of interest for all events are below the predevelopment flow rates. Additionally, post construction storm water BMPs will be provided to meet the required level of service for this development. See Appendix F for City of Lee's Summit BMP Level of Service Worksheet.

It is therefore requested that Lee's Summit, Missouri approve this "Lee's Summit Senior Living Community Final Stormwater Drainage Study." This study will be verified with the final construction documents for the construction with the development.

APPENDIX CRevised Calculation Report



Project: PRINCETON DETENTION BASIN-REV1 2023-01-27.gpw

Friday, 01 / 27 / 2023

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

		<u> </u>				Hydrafi	ow Hydrographs	s Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v20
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	5.462	2	730	20,656				EX-10
2	SCS Runoff	10.78	2	730	41,034				EX-11
3	Combine	16.24	2	730	61,691	1, 2			EX POI #1
4	SCS Runoff	10.77	2	730	40,985				EX-20
5	SCS Runoff	6.443	2	734	28,774				OFF-20
6	Combine	16.94	2	730	69,759	4, 5			EX POI #2
7	SCS Runoff	13.29	2	716	28,396				DEV10
8	SCS Runoff	10.01	2	716	20,843				DEV20
9	SCS Runoff	17.02	2	716	35,433				DEV30
10	Reservoir	12.54	2	718	21,778	7	1021.24	8,754	BIORETENTION 1
11	Reservoir	8.128	2	720	14,839	8	1022.78	8,038	BIORETENTION 2
12	Combine	36.65	2	718	72,051	9, 10, 11			COMBINE AT DETENTION
13	Reservoir	0.974	2	890	68,048	12	1017.04	46,809	EXTENDED DRY DETENTION
14	SCS Runoff	4.750	2	716	9,768				DA-12
15	Combine	11.64	2	730	118,850	2, 13, 14			POI #1
16	SCS Runoff	6.074	2	716	12,562				DA-21
17	SCS Runoff	1.984	2	716	4,044				DA-22
18	Combine	10.95	2	718	45,380	5, 16, 17			POI #2
					1			1	

PRINCETON DETENTION BASIN-REV1 2023 Retu27. @priod: 2 Year

Friday, 01 / 27 / 2023

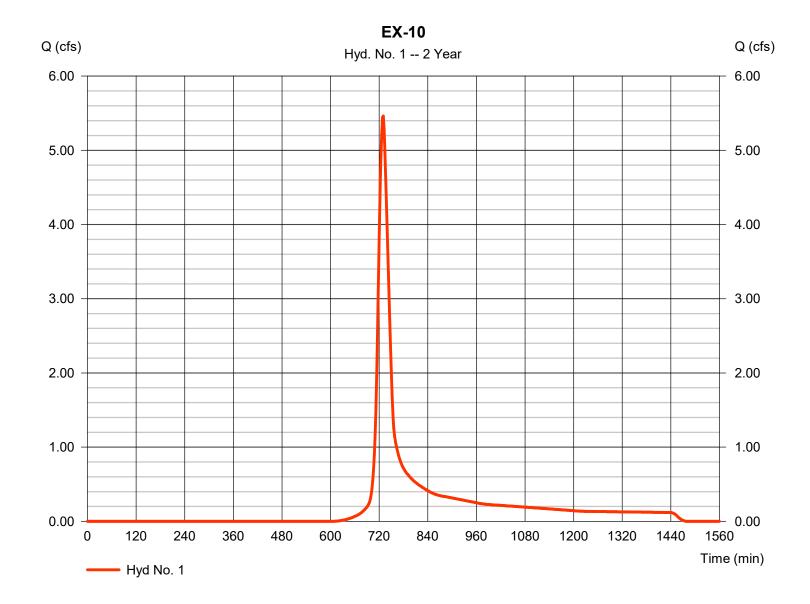
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 1

EX-10

Hydrograph type = SCS Runoff Peak discharge = 5.462 cfsStorm frequency = 2 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 20,656 cuft Curve number Drainage area = 3.980 ac= 75 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.30 min = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



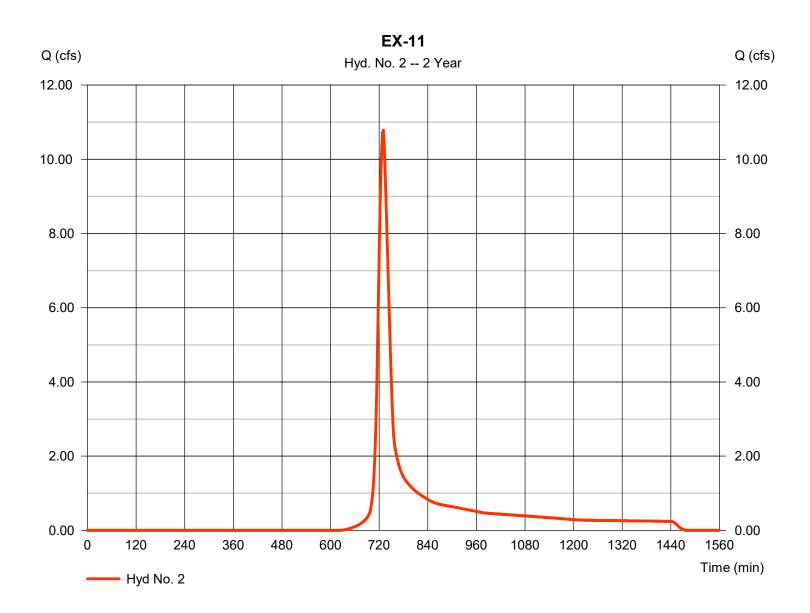
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 2

EX-11

Hydrograph type = SCS Runoff Peak discharge = 10.78 cfsStorm frequency = 2 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 41,034 cuft Drainage area = 8.280 ac Curve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 25.60 min = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



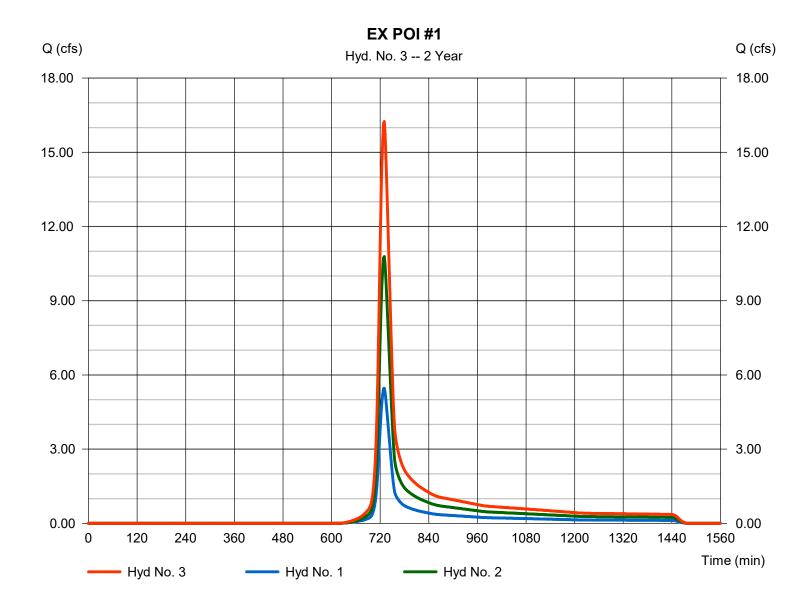
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 3

EX POI #1

= 16.24 cfsHydrograph type = Combine Peak discharge Time to peak Storm frequency = 2 yrs= 730 min Time interval = 2 min Hyd. volume = 61,691 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 12.260 ac



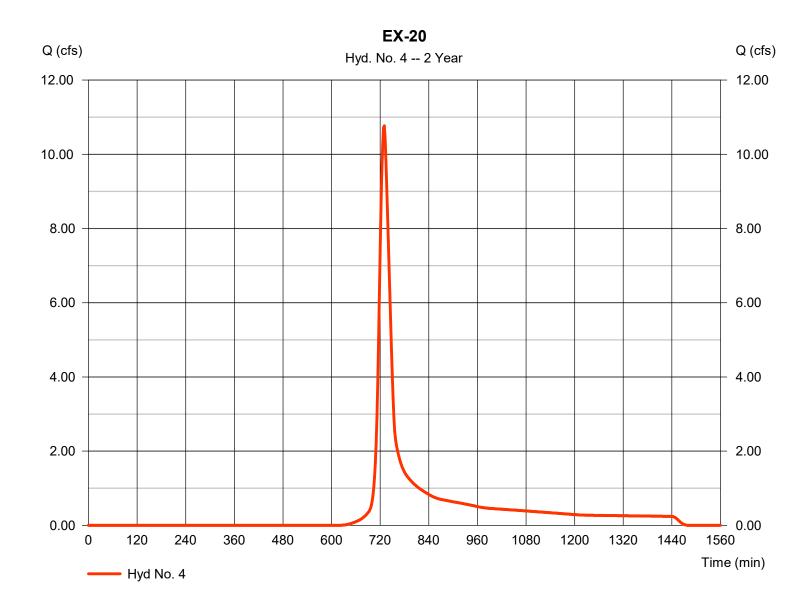
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 4

EX-20

Hydrograph type = SCS Runoff Peak discharge = 10.77 cfsStorm frequency = 2 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 40,985 cuftDrainage area = 8.270 ac Curve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 25.10 min = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



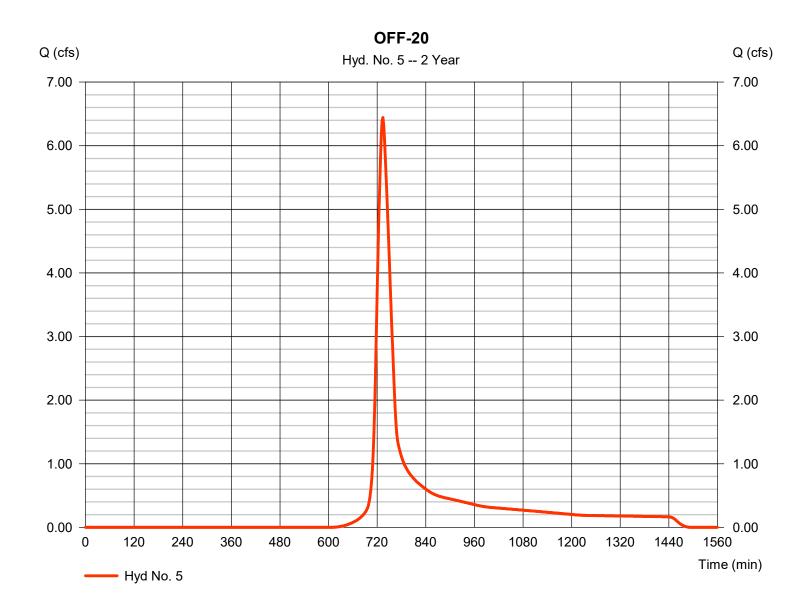
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 5

OFF-20

Hydrograph type = SCS Runoff Peak discharge $= 6.443 \, \text{cfs}$ Storm frequency = 2 yrsTime to peak = 734 min Time interval = 2 min Hyd. volume = 28,774 cuft Drainage area = 5.390 acCurve number = 75 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 32.70 min = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



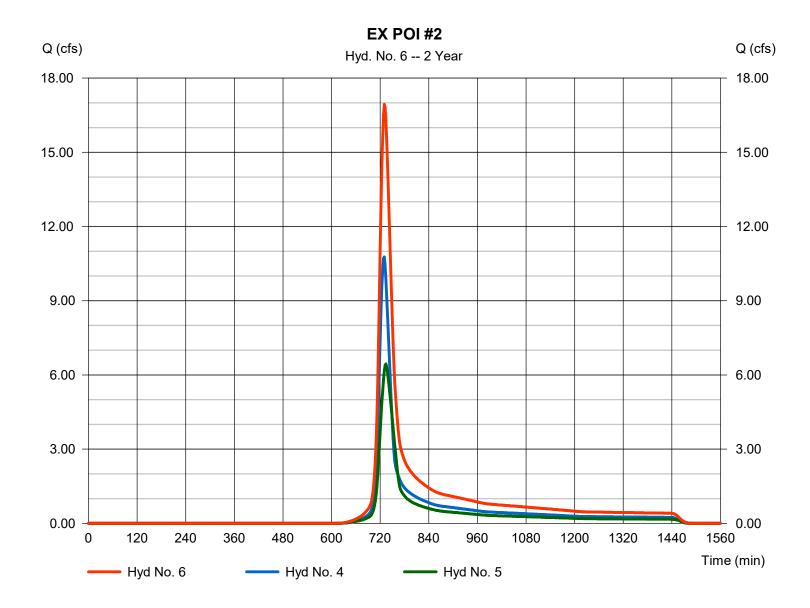
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 6

EX POI #2

Hydrograph type = Combine Peak discharge = 16.94 cfsTime to peak Storm frequency = 2 yrs= 730 min Time interval = 2 min Hyd. volume = 69,759 cuftInflow hyds. = 4,5 Contrib. drain. area = 13.660 ac



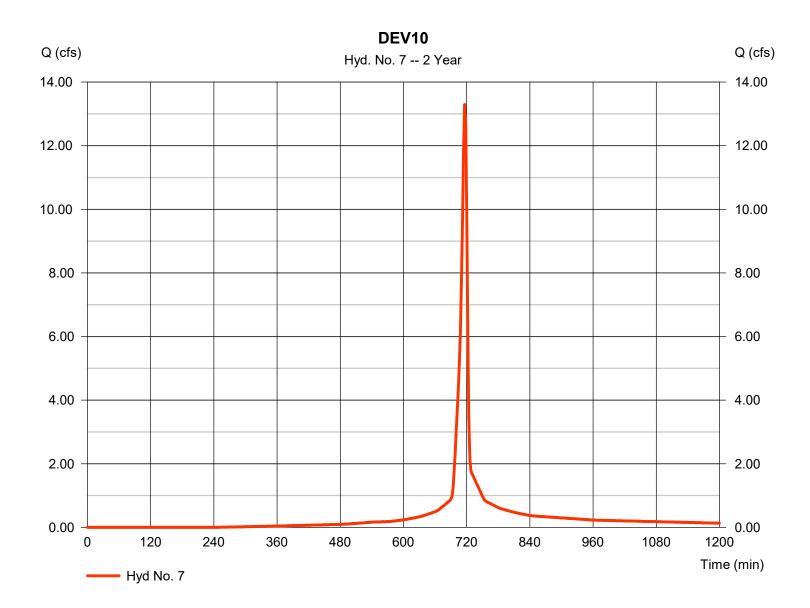
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Friday, 01 / 27 / 2023

Hyd. No. 7

DEV10

Hydrograph type = SCS Runoff Peak discharge = 13.29 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 28,396 cuft Drainage area Curve number = 2.940 ac= 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



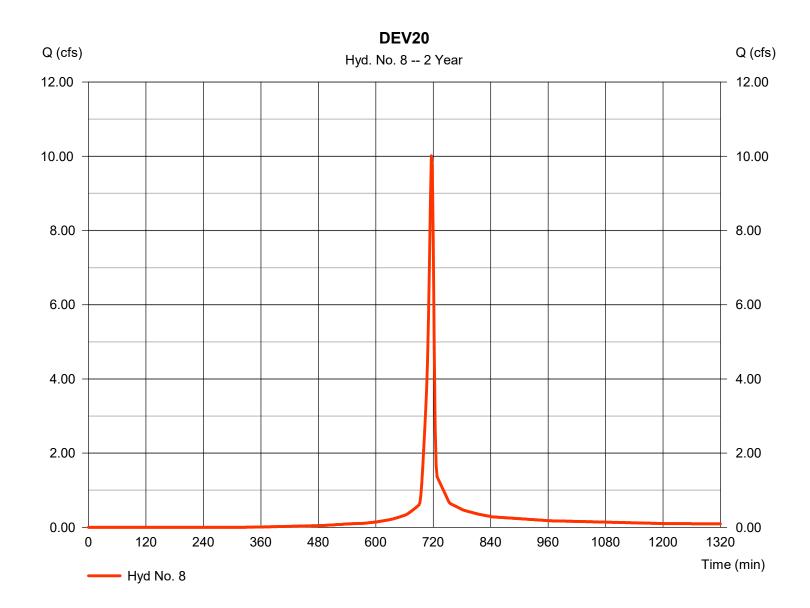
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Friday, 01 / 27 / 2023

Hyd. No. 8

DEV20

Hydrograph type = SCS Runoff Peak discharge = 10.01 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 20,843 cuft Drainage area Curve number = 2.400 ac= 89 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



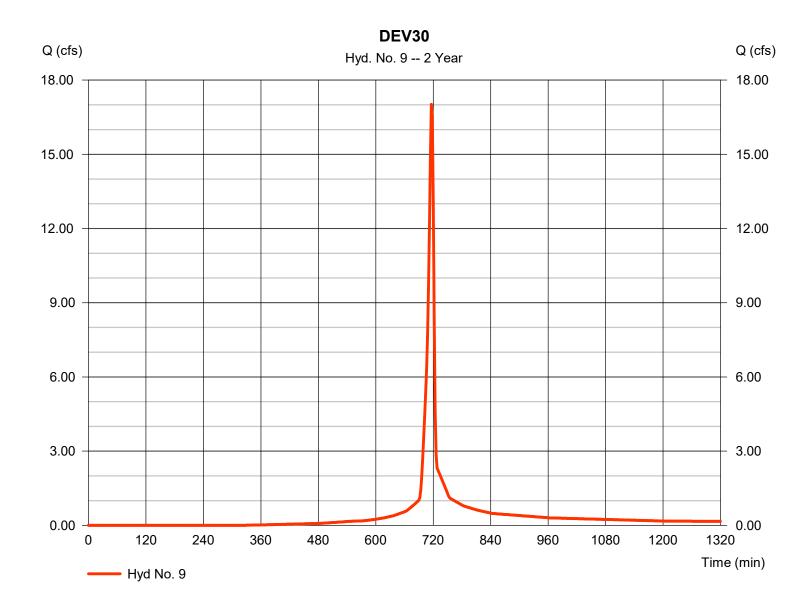
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 9

DEV₃₀

Hydrograph type = SCS Runoff Peak discharge = 17.02 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 35,433 cuft Drainage area = 4.080 acCurve number = 89 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

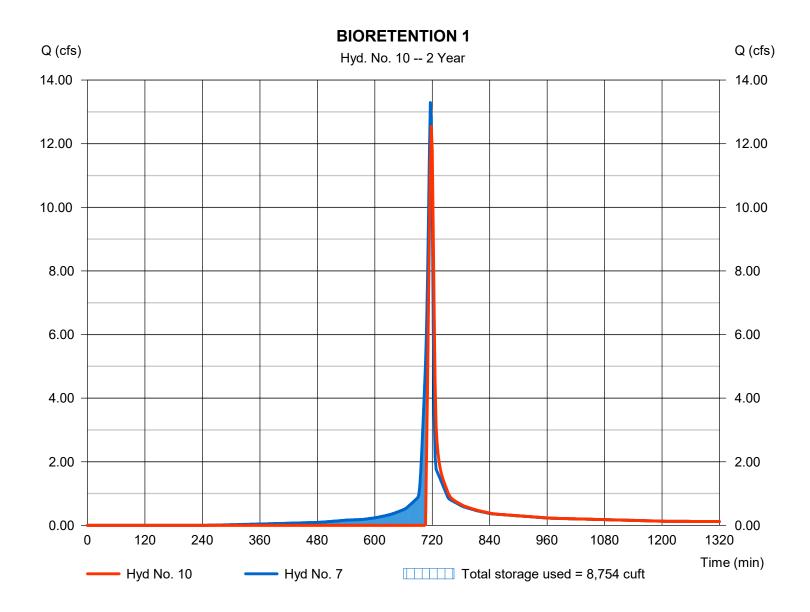
Friday, 01 / 27 / 2023

Hyd. No. 10

BIORETENTION 1

Hydrograph type Peak discharge = 12.54 cfs= Reservoir Storm frequency = 2 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 21,778 cuft Inflow hyd. No. = 7 - DEV10 Max. Elevation = 1021.24 ft= BIORETENTION 1 = 8,754 cuft Reservoir name Max. Storage

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Pond No. 1 - BIORETENTION 1

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1020.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	1020.00	5,489	0	0
1.00	1021.00	7,817	6,618	6,618
2.00	1022.00	10,202	8,982	15,600
3.00	1023.00	12,644	11,400	27,000

Culvert / Orifice Structures Weir Structures [B] [C] [PrfRsr] [A] [C] [D] [A] [B] Rise (in) = 24.00 Inactive Inactive 0.00 Crest Len (ft) = 32.00 100.00 Inactive 0.00 = 24.000.00 0.00 0.00 Crest El. (ft) = 1021.00 1022.00 0.00 0.00 Span (in) No. Barrels = 2 1 0 Weir Coeff. = 3.33 3.33 3.33 3.33 1 = 1015.29 0.00 0.00 0.00 = Rect Broad Invert El. (ft) Weir Type = 58.56 0.00 0.00 0.00 Multi-Stage Length (ft) = Yes No No No = 0.500.00 0.00 n/a Slope (%) N-Value = .013 .013 .013 n/a = 0.000 (by Contour) = 0.600.60 0.60 0.60 Exfil.(in/hr) Orifice Coeff. Multi-Stage = n/a No No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stane	/ Storage	/ Discharge	Table
Staue .	Joinaue	/ DISCHALUE	Iable

Stage ft	Storage cuft	Elevation ft	Clv A cfs	CIv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	1020.00	0.00				0.00	0.00					0.000
1.00	6,618	1021.00	58.27 ic				0.00	0.00					0.000
2.00	15,600	1022.00	70.71 ic				70.71 s	0.00					70.71
3.00	27,000	1023.00	78.12 ic				78.08 s	333.00					411.08

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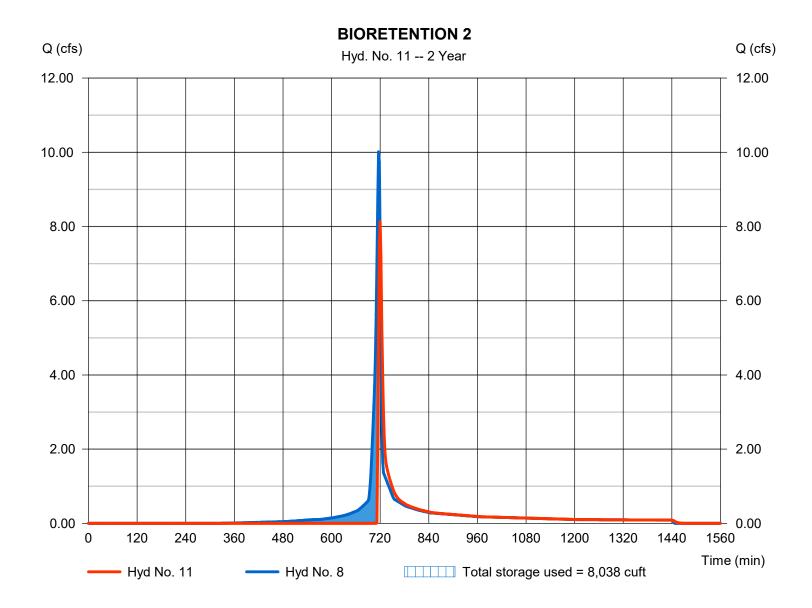
Friday, 01 / 27 / 2023

Hyd. No. 11

BIORETENTION 2

Hydrograph type Peak discharge = 8.128 cfs= Reservoir Storm frequency = 2 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 14,839 cuft Inflow hyd. No. Max. Elevation = 1022.78 ft= 8 - DEV20 Reservoir name = BIORETENTION #2 Max. Storage = 8,038 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Pond No. 2 - BIORETENTION #2

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1021.50 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	1021.50	4,007	0	0
0.50	1022.00	5,756	2,427	2,427
1.50	1023.00	8,647	7,152	9,579
2.50	1024.00	11,639	10,105	19,684

Culvert / Orifice Structures Weir Structures [B] [C] [PrfRsr] [A] [B] [C] [D] [A] Rise (in) = 24.00Inactive Inactive Inactive Crest Len (ft) = 16.00 Inactive Inactive 0.00 = 24.000.00 0.00 0.00 Crest El. (ft) = 1022.50 0.00 0.00 0.00 Span (in) No. Barrels = 1 1 1 0 Weir Coeff. = 3.333.33 3.33 3.33 = 1017.01 0.00 0.00 0.00 = Rect Broad Broad Invert El. (ft) Weir Type = 303.540.00 0.00 0.00 Multi-Stage Length (ft) = Yes No No No = 0.500.00 0.00 n/a Slope (%)

N-Value = .013 .013 .013 n/a 0.60 = 0.000 (by Contour) = 0.600.60 0.60 Exfil.(in/hr) Orifice Coeff. Multi-Stage = n/a No No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage.	/ Storage	/ Discharge	Table
Staue	Storage	/ Discharge	i abie

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	CIv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	1021.50	0.00				0.00						0.000
0.50	2,427	1022.00	22.04 oc				0.00						0.000
1.50	9,579	1023.00	22.04 oc				18.84						18.84
2.50	19,684	1024.00	28.01 oc				27.98 s						27.98

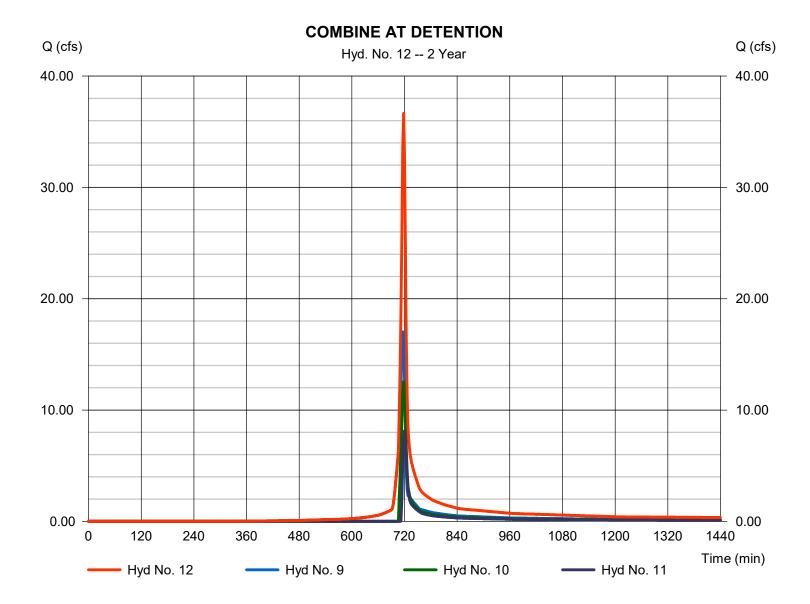
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Friday, 01 / 27 / 2023

Hyd. No. 12

COMBINE AT DETENTION

Hydrograph type = Combine Peak discharge = 36.65 cfsStorm frequency Time to peak = 2 yrs= 718 min Time interval = 2 min Hyd. volume = 72,051 cuftInflow hyds. = 9, 10, 11 Contrib. drain. area = 4.080 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

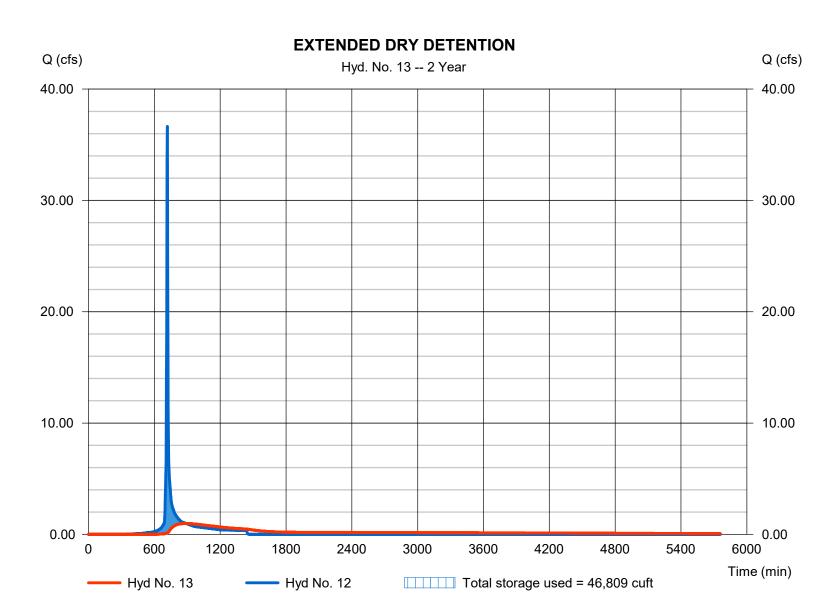
Friday, 01 / 27 / 2023

Hyd. No. 13

EXTENDED DRY DETENTION

Hydrograph type Peak discharge = 0.974 cfs= Reservoir Time to peak Storm frequency = 2 yrs= 890 min Time interval = 2 min Hyd. volume = 68,048 cuft Inflow hyd. No. = 12 - COMBINE AT DETENTIOMax. Elevation = 1017.04 ft= EXTENDED DRY DETENTIONMax. Storage Reservoir name = 46,809 cuft

Storage Indication method used.



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Friday, 01 / 27 / 2023

Pond No. 3 - EXTENDED DRY DETENTION

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1013.00 ft

Stage / Storage Table

Stage (ft)	ge (ft) Elevation (ft) Conto		Incr. Storage (cuft)	Total storage (cuft)
0.00	1013.00	6,640	0	0
1.00	1014.00	8,130	7,372	7,372
2.00	1015.00	10,733	9,400	16,772
3.00	1016.00	15,079	12,843	29,615
4.00	1017.00	17,882	16,459	46,074
5.00	1018.00	20,841	19,341	65,415
6.00	1019.00	24,958	22,866	88,281
7.00	1020.00	27,232	26,084	114,366
8.00	1021.00	30,663	28,928	143,293
9.00	1022.00	34,251	32,437	175,730

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	2.00	Inactive	0.00	Crest Len (ft)	= 0.33	11.00	Inactive	0.00
Span (in)	= 15.00	2.00	0.00	0.00	Crest El. (ft)	= 1016.25	1018.50	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 1011.71	1013.19	0.00	0.00	Weir Type	= Rect	Rect		
Length (ft)	= 69.50	0.50	0.00	0.00	Multi-Stage	= Yes	Yes	No	No
Slope (%)	= 0.50	0.50	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	CIv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	1013.00	0.00	0.00			0.00	0.00					0.000
1.00	7,372	1014.00	3.48 oc	0.09 ic			0.00	0.00					0.090
2.00	16,772	1015.00	3.48 oc	0.14 ic			0.00	0.00					0.138
3.00	29,615	1016.00	3.48 oc	0.17 ic			0.00	0.00					0.173
4.00	46,074	1017.00	3.48 oc	0.20 ic			0.71	0.00					0.917
5.00	65,415	1018.00	3.48 oc	0.23 ic			2.54	0.00					2.772
6.00	88,281	1019.00	13.82 oc	0.06 ic			2.41 s	11.35 s					13.82
7.00	114,366	1020.00	15.18 oc	0.01 ic			1.17 s	13.99 s					15.17
8.00	143,293	1021.00	16.19 oc	0.01 ic			0.93 s	15.22 s					16.16
9.00	175,730	1022.00	17.13 oc	0.00 ic			0.84 s	16.14 s					16.99

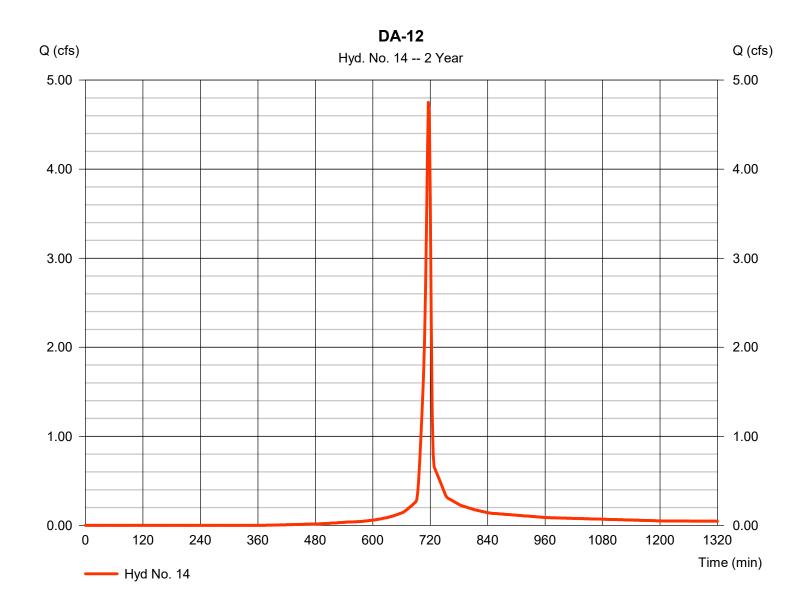
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Friday, 01 / 27 / 2023

Hyd. No. 14

DA-12

Hydrograph type = SCS Runoff Peak discharge = 4.750 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 9,768 cuftDrainage area = 1.210 acCurve number = 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



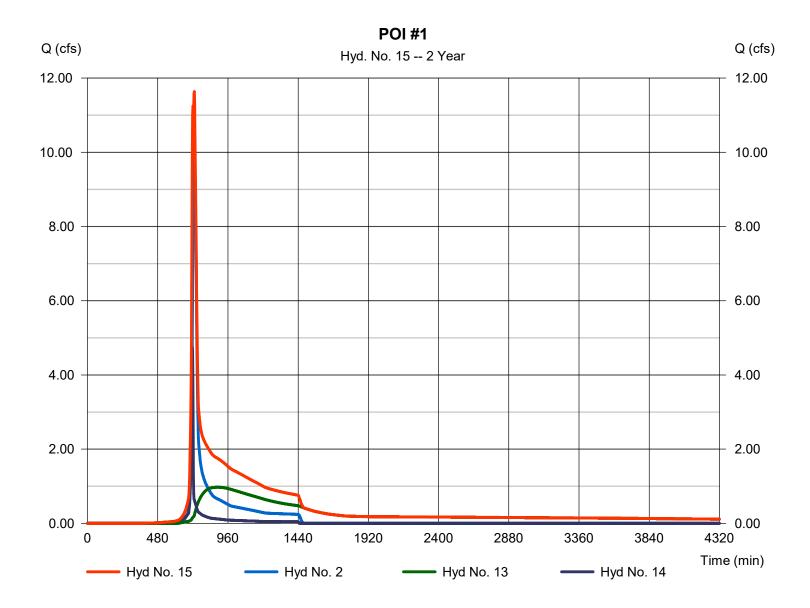
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Friday, 01 / 27 / 2023

Hyd. No. 15

POI #1

Hydrograph type = Combine Peak discharge = 11.64 cfsTime to peak Storm frequency = 2 yrs= 730 min Time interval = 2 min Hyd. volume = 118,850 cuft Inflow hyds. = 2, 13, 14 Contrib. drain. area = 9.490 ac



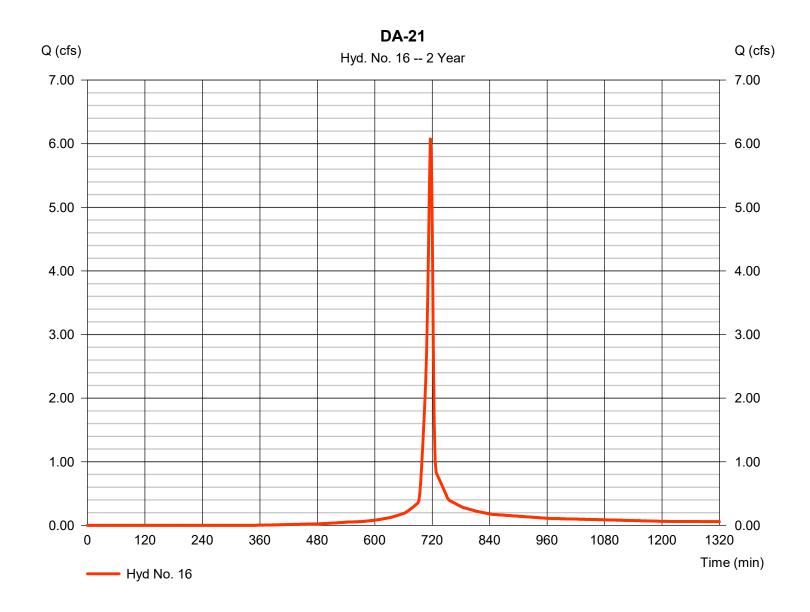
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Friday, 01 / 27 / 2023

Hyd. No. 16

DA-21

Hydrograph type = SCS Runoff Peak discharge = 6.074 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 12,562 cuft Drainage area = 1.500 acCurve number = 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



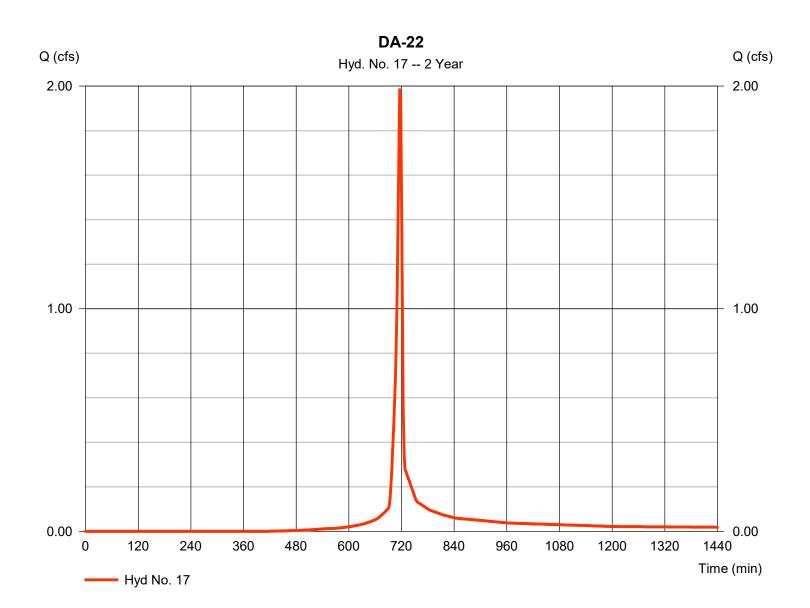
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Friday, 01 / 27 / 2023

Hyd. No. 17

DA-22

Hydrograph type = SCS Runoff Peak discharge = 1.984 cfsStorm frequency = 2 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 4,044 cuftDrainage area = 0.540 acCurve number = 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.71 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



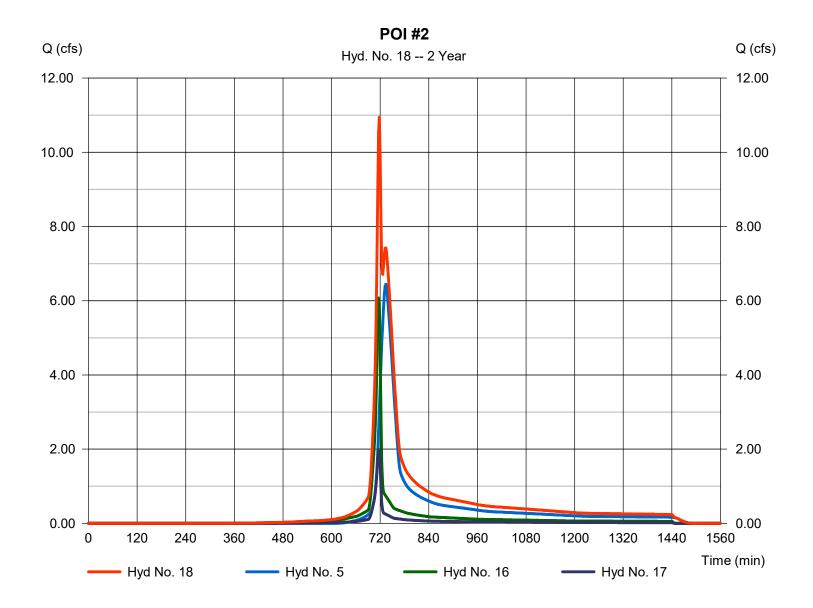
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Friday, 01 / 27 / 2023

Hyd. No. 18

POI #2

Hydrograph type = Combine Peak discharge = 10.95 cfsTime to peak Storm frequency = 2 yrs= 718 min Time interval = 2 min Hyd. volume = 45,380 cuftInflow hyds. = 5, 16, 17 Contrib. drain. area = 7.430 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

о.	ydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1 SC	CS Runoff	11.58	2	728	42,585				EX-10
2 SC	CS Runoff	23.30	2	728	85,835				EX-11
3 Co	ombine	34.88	2	728	128,420	1, 2			EX POI #1
4 SC	CS Runoff	23.27	2	728	85,731				EX-20
5 SC	CS Runoff	13.67	2	732	59,320				OFF-20
6 Cd	ombine	36.47	2	730	145,051	4, 5			EX POI #2
7 SC	CS Runoff	21.46	2	716	47,379				DEV10
8 SC	CS Runoff	16.75	2	716	35,991				DEV20
9 sc	CS Runoff	28.48	2	716	61,185				DEV30
10 Re	eservoir	20.60	2	718	40,761	7	1021.33	9,608	BIORETENTION 1
11 Re	eservoir	15.54	2	718	29,987	8	1022.94	9,139	BIORETENTION 2
12 Co	ombine	63.60	2	718	131,933	9, 10, 11			COMBINE AT DETENTION
13 Re	eservoir	3.932	2	764	127,545	12	1018.49	76,695	EXTENDED DRY DETENTION
14 SC	CS Runoff	8.155	2	716	17,264				DA-12
15 Co	ombine	27.70	2	728	230,644	2, 13, 14			POI #1
16 SC	CS Runoff	10.29	2	716	21,945				DA-21
17 SC	CS Runoff	3.500	2	716	7,319				DA-22
18 Co	ombine	20.60	2	718	88,584	5, 16, 17			POI #2

PRINCETON DETENTION BASIN-REV1 2023 Retu27 . Igpriod: 10 Year

Friday, 01 / 27 / 2023

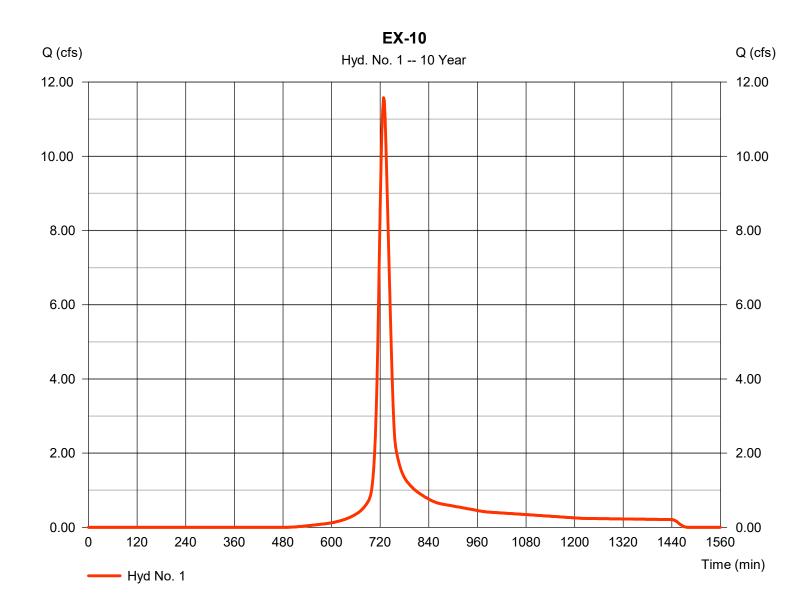
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Friday, 01 / 27 / 2023

Hyd. No. 1

EX-10

Hydrograph type = SCS Runoff Peak discharge = 11.58 cfsStorm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 42,585 cuft Drainage area Curve number = 3.980 ac= 75 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.30 min = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



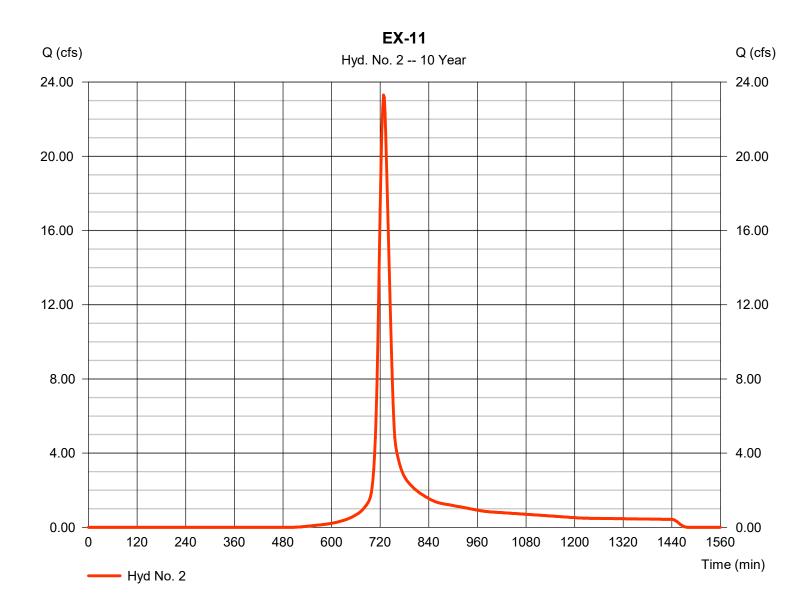
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Friday, 01 / 27 / 2023

Hyd. No. 2

EX-11

Hydrograph type = SCS Runoff Peak discharge = 23.30 cfsStorm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 85,835 cuft Drainage area = 8.280 acCurve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 25.60 min = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



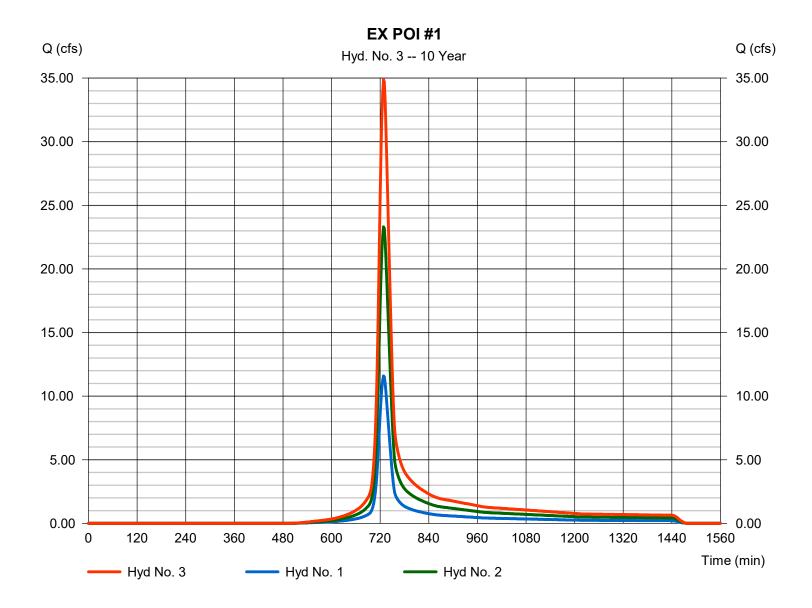
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Friday, 01 / 27 / 2023

Hyd. No. 3

EX POI #1

Hydrograph type = Combine Peak discharge = 34.88 cfsStorm frequency Time to peak = 10 yrs= 728 min Time interval = 2 min Hyd. volume = 128,420 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 12.260 ac



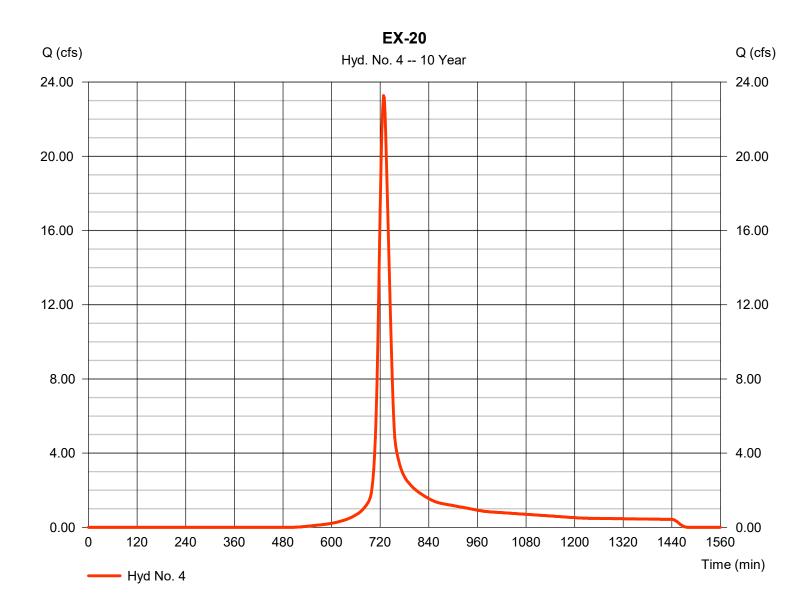
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Friday, 01 / 27 / 2023

Hyd. No. 4

EX-20

Hydrograph type = SCS Runoff Peak discharge = 23.27 cfsStorm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 85,731 cuft Drainage area = 8.270 acCurve number = 74 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 25.10 min = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



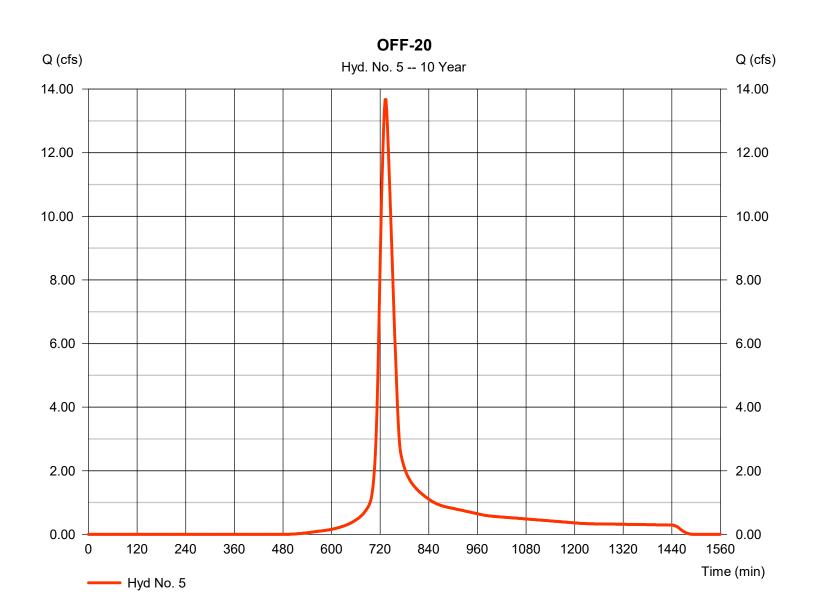
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Friday, 01 / 27 / 2023

Hyd. No. 5

OFF-20

Hydrograph type = SCS Runoff Peak discharge = 13.67 cfsStorm frequency = 10 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 59,320 cuftDrainage area = 5.390 acCurve number = 75 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 32.70 min = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



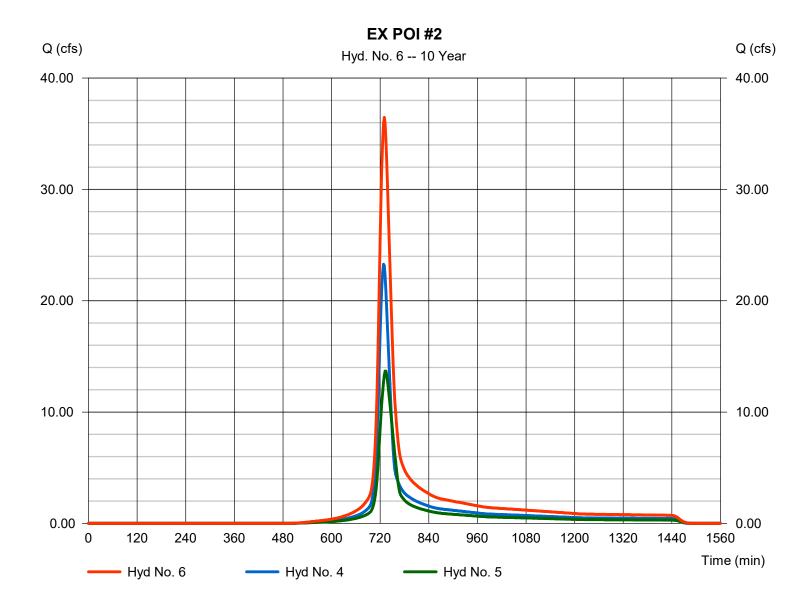
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 6

EX POI #2

Hydrograph type = Combine Peak discharge = 36.47 cfsTime to peak Storm frequency = 10 yrs= 730 min Time interval = 2 min Hyd. volume = 145,051 cuft Inflow hyds. = 4, 5 Contrib. drain. area = 13.660 ac



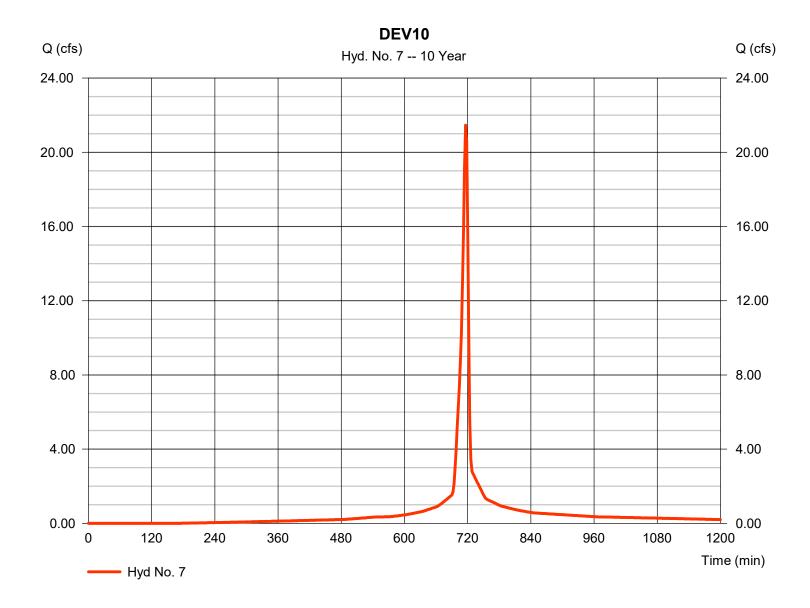
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 7

DEV10

Hydrograph type = SCS Runoff Peak discharge = 21.46 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 47,379 cuftDrainage area Curve number = 2.940 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



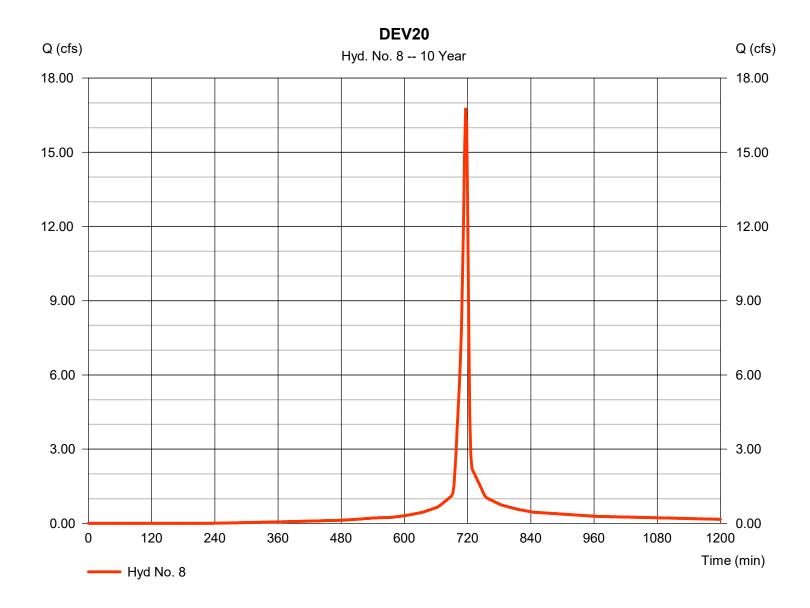
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 8

DEV20

Hydrograph type = SCS Runoff Peak discharge = 16.75 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 35,991 cuft Drainage area = 2.400 acCurve number = 89 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



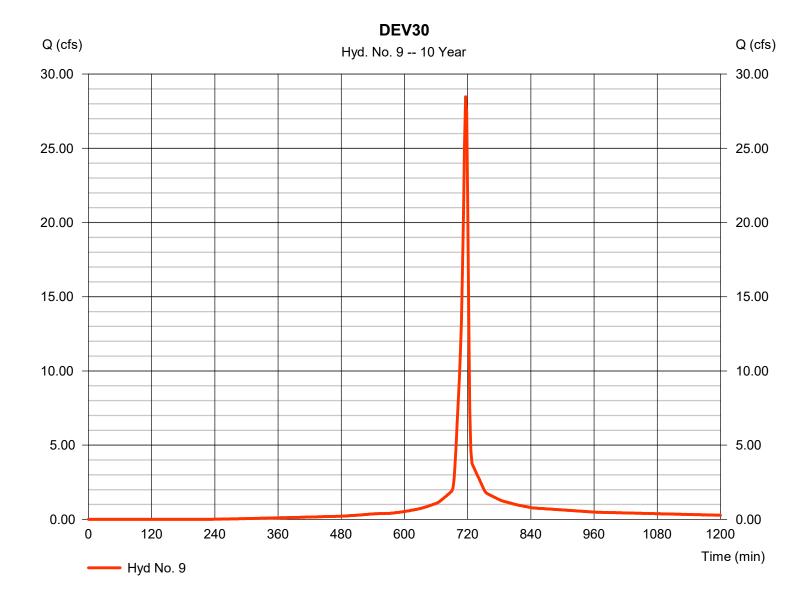
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 9

DEV₃₀

Hydrograph type = SCS Runoff Peak discharge = 28.48 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 61,185 cuft Drainage area = 4.080 acCurve number = 89 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

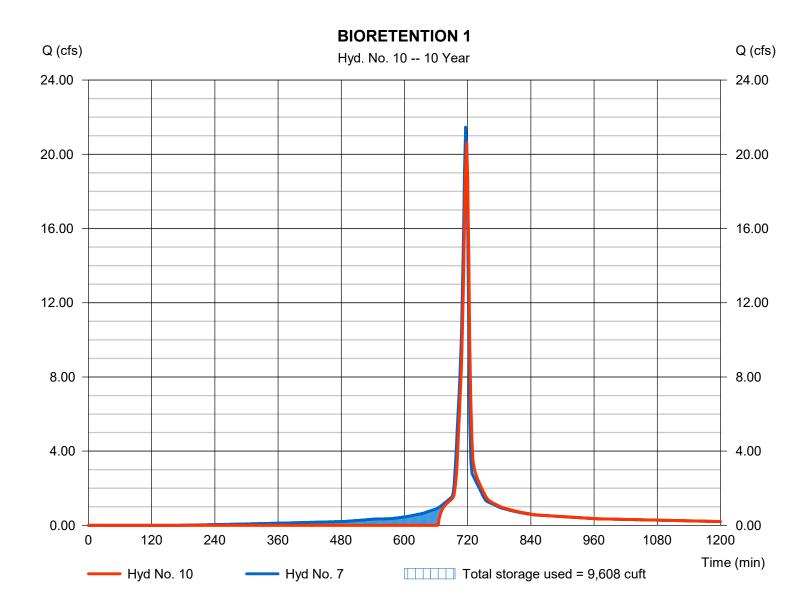
Friday, 01 / 27 / 2023

Hyd. No. 10

BIORETENTION 1

Hydrograph type = Reservoir Peak discharge = 20.60 cfsStorm frequency = 10 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 40,761 cuftInflow hyd. No. = 7 - DEV10 Max. Elevation = 1021.33 ft= BIORETENTION 1 Reservoir name Max. Storage = 9,608 cuft

Storage Indication method used.



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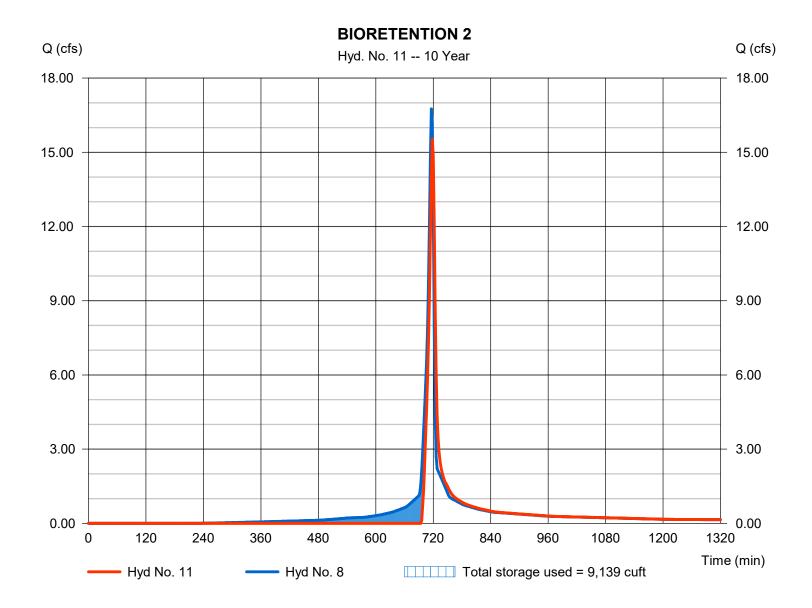
Friday, 01 / 27 / 2023

Hyd. No. 11

BIORETENTION 2

Hydrograph type = Reservoir Peak discharge = 15.54 cfsStorm frequency = 10 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 29,987 cuft Inflow hyd. No. Max. Elevation = 1022.94 ft= 8 - DEV20 Reservoir name = BIORETENTION #2 Max. Storage = 9,139 cuft

Storage Indication method used.



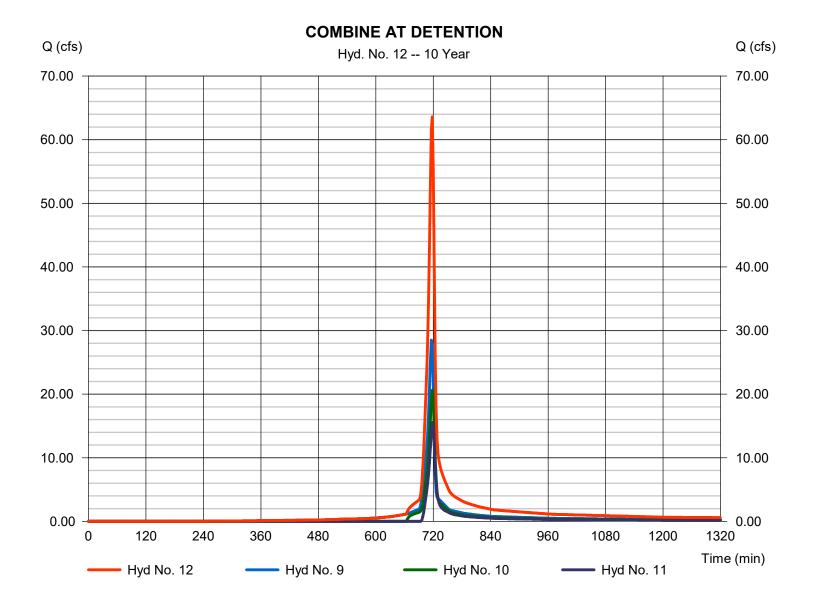
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Friday, 01 / 27 / 2023

Hyd. No. 12

COMBINE AT DETENTION

Hydrograph type = Combine Peak discharge = 63.60 cfsStorm frequency Time to peak = 10 yrs= 718 min Time interval = 2 min Hyd. volume = 131,933 cuft Inflow hyds. = 9, 10, 11 Contrib. drain. area = 4.080 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

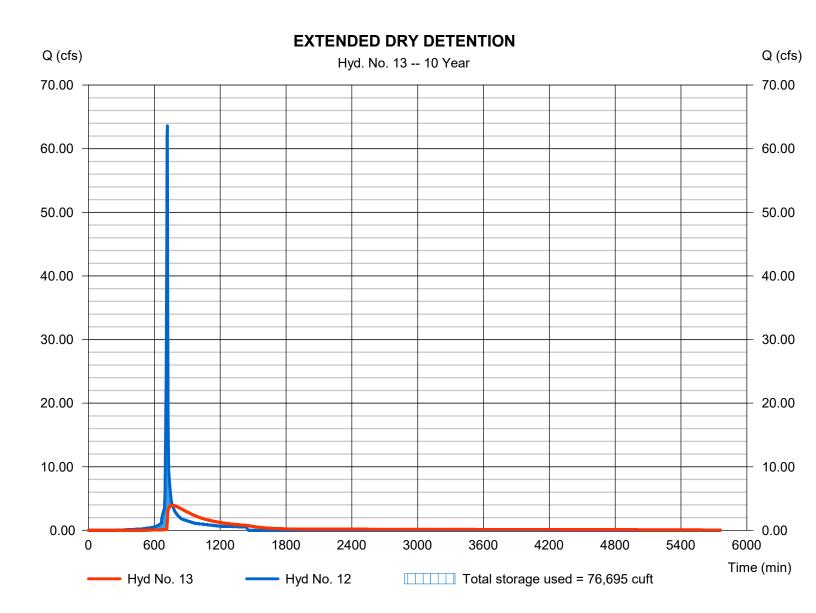
Friday, 01 / 27 / 2023

Hyd. No. 13

EXTENDED DRY DETENTION

Hydrograph type Peak discharge = 3.932 cfs= Reservoir Storm frequency Time to peak = 10 yrs= 764 min Time interval = 2 min Hyd. volume = 127,545 cuft Inflow hyd. No. = 12 - COMBINE AT DETENTIOMax. Elevation = 1018.49 ft= EXTENDED DRY DETENTIONMax. Storage = 76,695 cuft Reservoir name

Storage Indication method used.



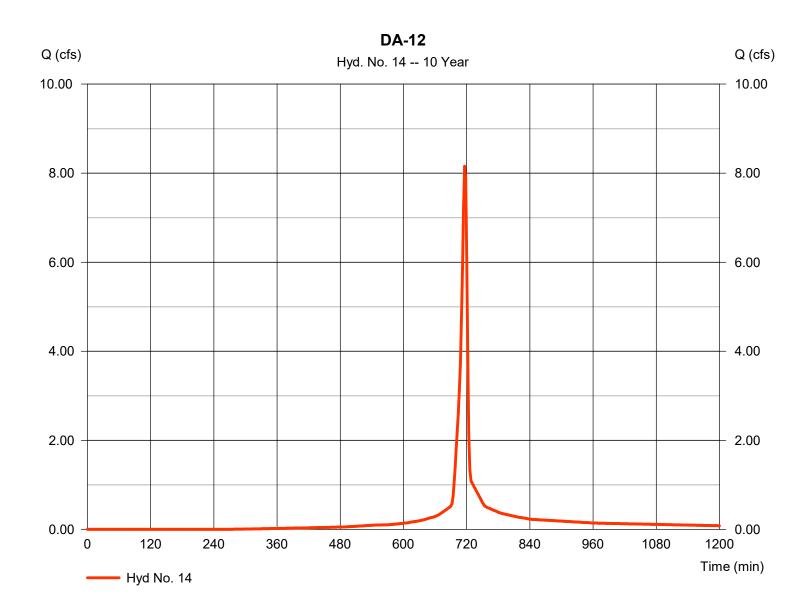
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 14

DA-12

Hydrograph type = SCS Runoff Peak discharge = 8.155 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 17,264 cuft Drainage area = 1.210 ac Curve number = 87 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



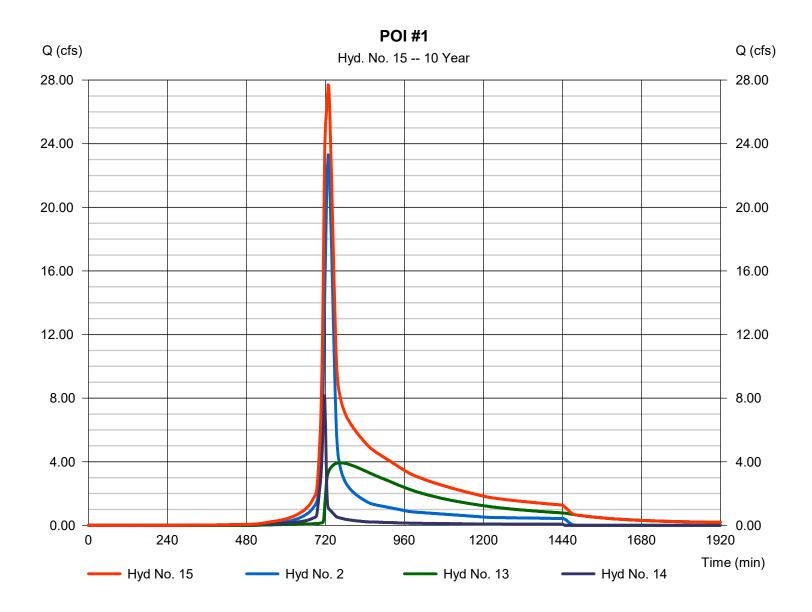
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Hyd. No. 15

POI #1

Hydrograph type = Combine Peak discharge = 27.70 cfsTime to peak Storm frequency = 10 yrs= 728 min Time interval = 2 min Hyd. volume = 230,644 cuft Inflow hyds. = 2, 13, 14 Contrib. drain. area = 9.490 ac



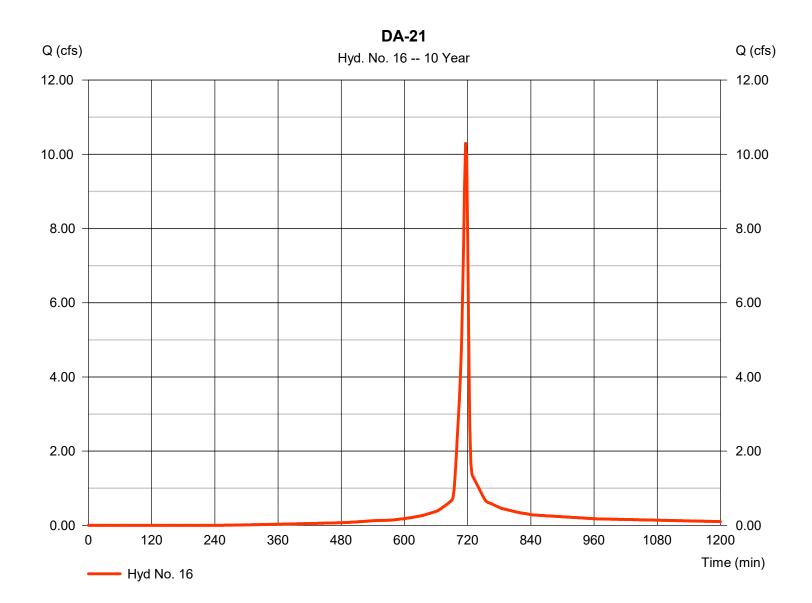
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Friday, 01 / 27 / 2023

Hyd. No. 16

DA-21

Hydrograph type = SCS Runoff Peak discharge = 10.29 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 21,945 cuft Drainage area = 1.500 acCurve number = 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



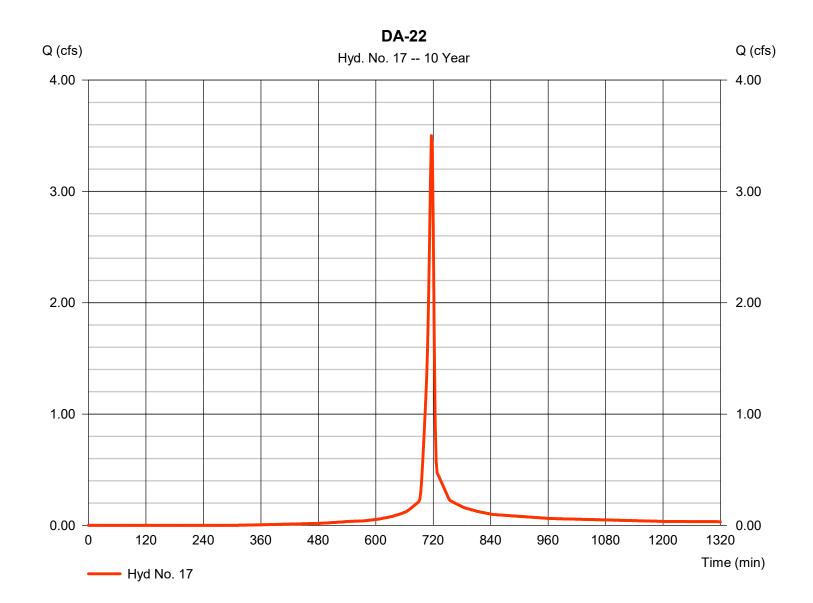
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Friday, 01 / 27 / 2023

Hyd. No. 17

DA-22

Hydrograph type = SCS Runoff Peak discharge = 3.500 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 7,319 cuftDrainage area Curve number = 0.540 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.66 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



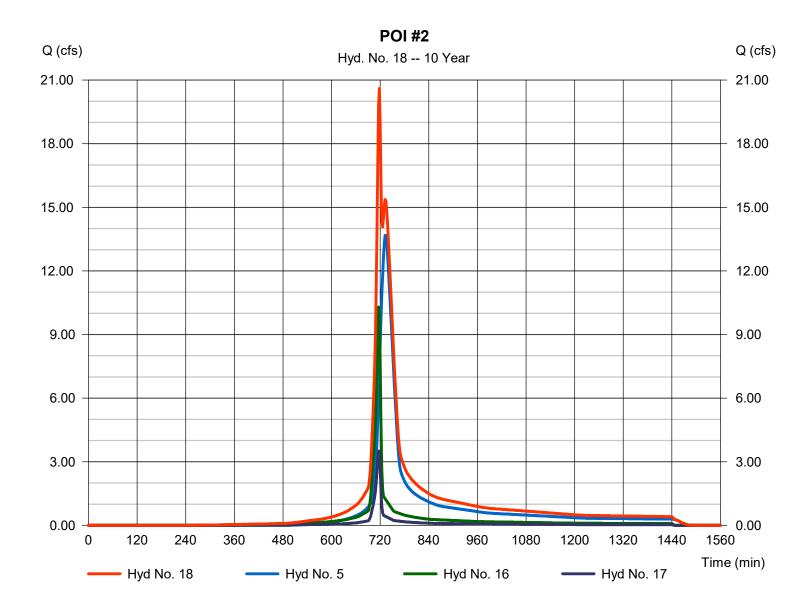
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Friday, 01 / 27 / 2023

Hyd. No. 18

POI #2

Hydrograph type = Combine Peak discharge = 20.60 cfsStorm frequency Time to peak = 10 yrs= 718 min Time interval = 2 min Hyd. volume = 88,584 cuft Inflow hyds. = 5, 16, 17 Contrib. drain. area = 7.430 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	23.85	2	728	87,924				EX-10
2	SCS Runoff	48.68	2	728	179,217				EX-11
3	Combine	72.52	2	728	267,141	1, 2			EX POI #1
4	SCS Runoff	48.62	2	728	179,000				EX-20
5	SCS Runoff	28.27	2	732	122,475				OFF-20
6	Combine	75.73	2	730	301,476	4, 5			EX POI #2
7	SCS Runoff	36.24	2	716	82,868				DEV10
8	SCS Runoff	28.97	2	716	64,654				DEV20
9	SCS Runoff	49.26	2	716	109,912				DEV30
10	Reservoir	35.10	2	718	76,250	7	1021.48	10,894	BIORETENTION 1
11	Reservoir	25.01	2	718	58,651	8	1023.14	10,956	BIORETENTION 2
12	Combine	107.32	2	718	244,813	9, 10, 11			COMBINE AT DETENTION
13	Reservoir	15.78	2	732	240,103	12	1020.59	131,403	EXTENDED DRY DETENTION
14	SCS Runoff	14.36	2	716	31,586				DA-12
15	Combine	66.32	2	728	450,905	2, 13, 14			POI #1
16	SCS Runoff	17.96	2	716	39,783				DA-21
17	SCS Runoff	6.284	2	716	13,644				DA-22
18	Combine	39.30	2	718	175,902	5, 16, 17			POI #2

PRINCETON DETENTION BASIN-REV1 2023 Refultation. 100 Year

Friday, 01 / 27 / 2023

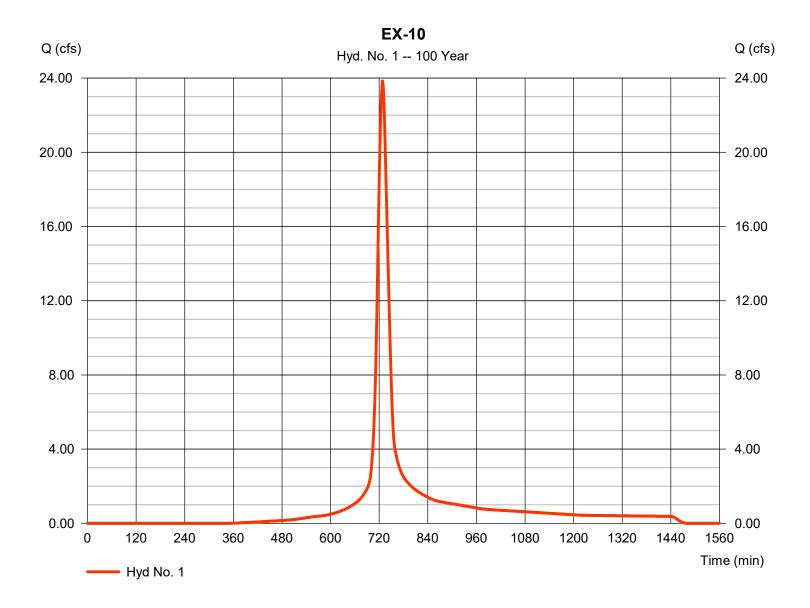
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Friday, 01 / 27 / 2023

Hyd. No. 1

EX-10

Hydrograph type = SCS Runoff Peak discharge = 23.85 cfsStorm frequency = 100 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 87,924 cuft Drainage area Curve number = 3.980 ac= 75 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 26.30 min = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



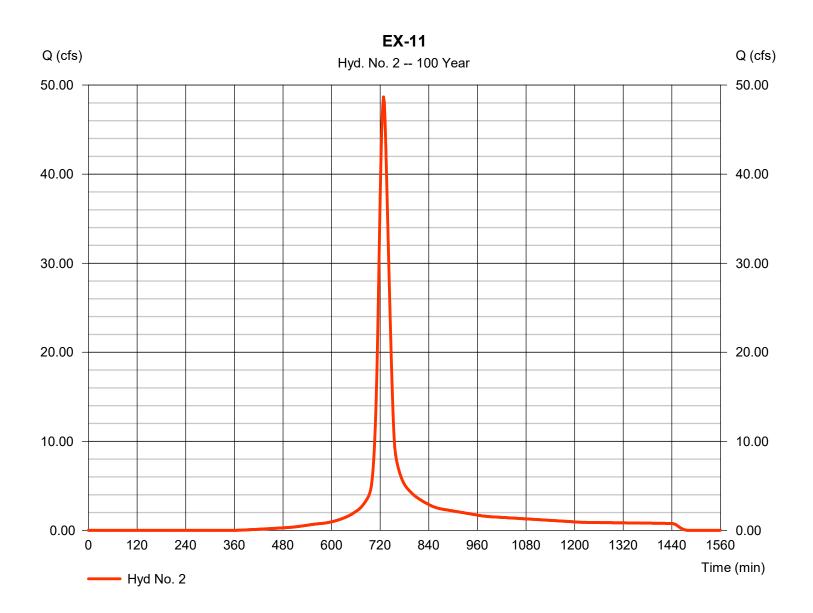
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Friday, 01 / 27 / 2023

Hyd. No. 2

EX-11

Hydrograph type = SCS Runoff Peak discharge = 48.68 cfsStorm frequency = 100 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 179,217 cuft Drainage area = 8.280 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 25.60 min = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



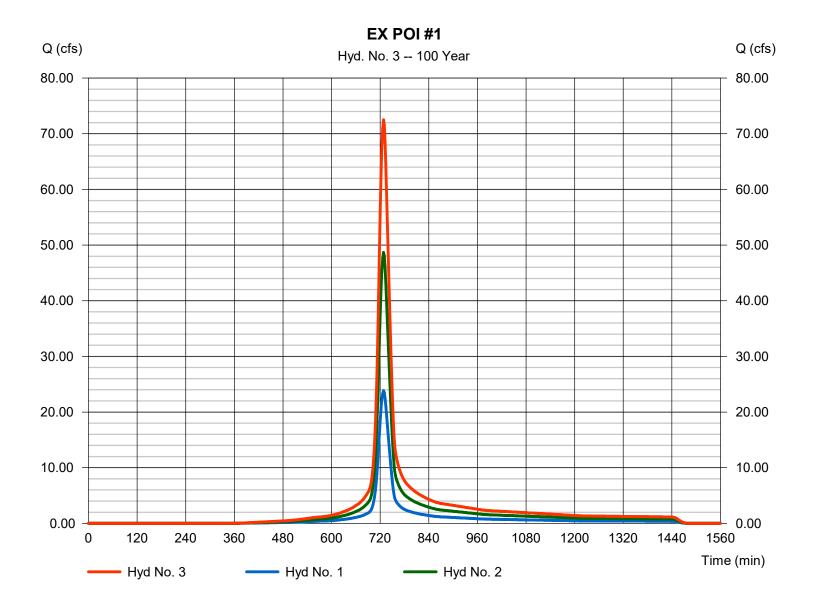
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Friday, 01 / 27 / 2023

Hyd. No. 3

EX POI #1

= 72.52 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 100 yrs= 728 min Time interval = 2 min Hyd. volume = 267,141 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 12.260 ac



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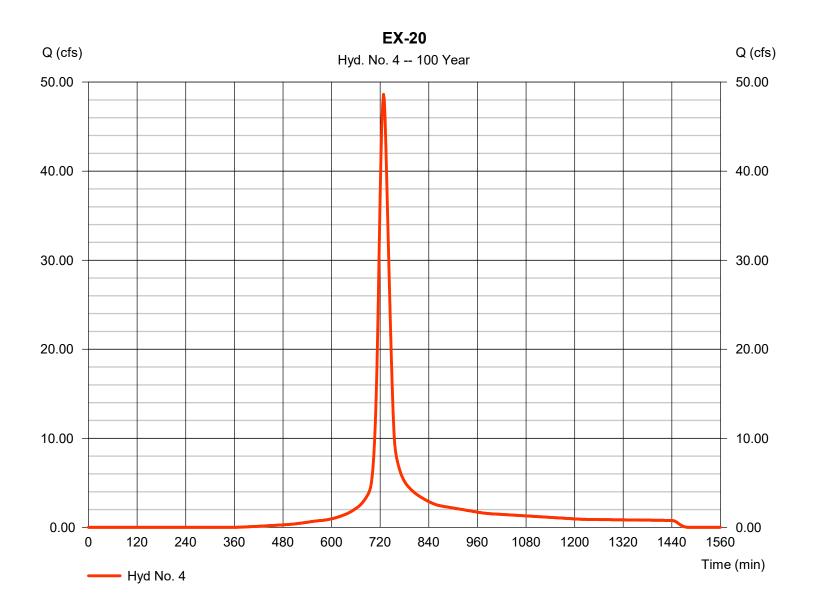
Friday, 01 / 27 / 2023

Hyd. No. 4

EX-20

Hydrograph type = SCS Runoff Peak discharge = 48.62 cfsStorm frequency = 100 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 179,000 cuftDrainage area = 8.270 acCurve number = 74 = 0 ftBasin Slope = 0.0 %Hydraulic length

Tc method = User Time of conc. (Tc) = 25.10 min
Total precip. = 9.25 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



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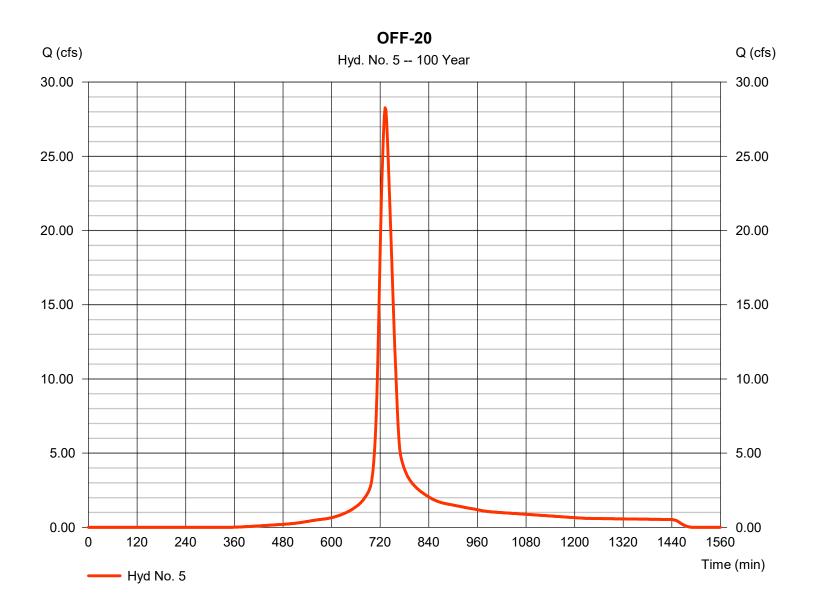
Friday, 01 / 27 / 2023

Hyd. No. 5

OFF-20

Hydrograph type = SCS Runoff Peak discharge = 28.27 cfsStorm frequency = 100 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 122,475 cuft Drainage area = 5.390 acCurve number = 75 = 0 ftBasin Slope = 0.0 %Hydraulic length

Tc method = User Time of conc. (Tc) = 32.70 min
Total precip. = 9.25 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



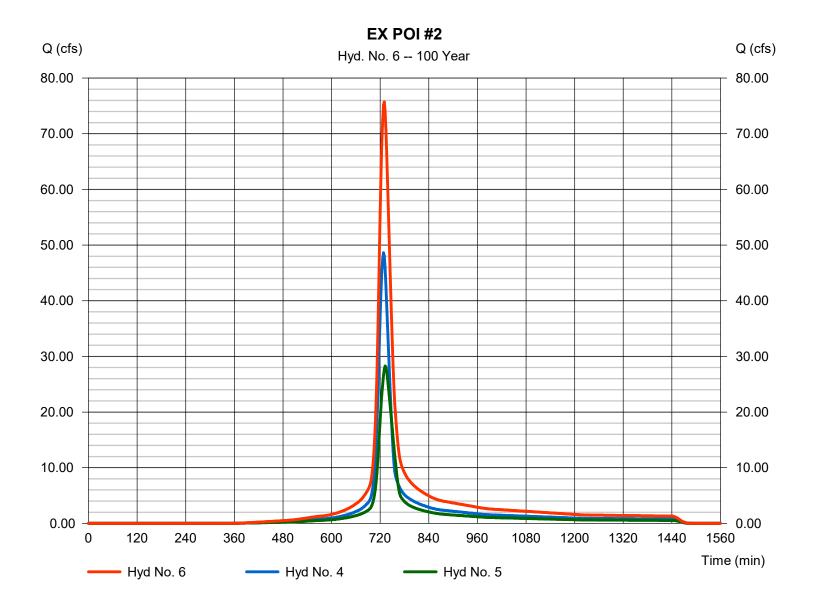
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Friday, 01 / 27 / 2023

Hyd. No. 6

EX POI #2

Hydrograph type = Combine Peak discharge = 75.73 cfsStorm frequency Time to peak = 100 yrs= 730 min Time interval = 2 min Hyd. volume = 301,476 cuft Inflow hyds. = 4, 5 Contrib. drain. area = 13.660 ac



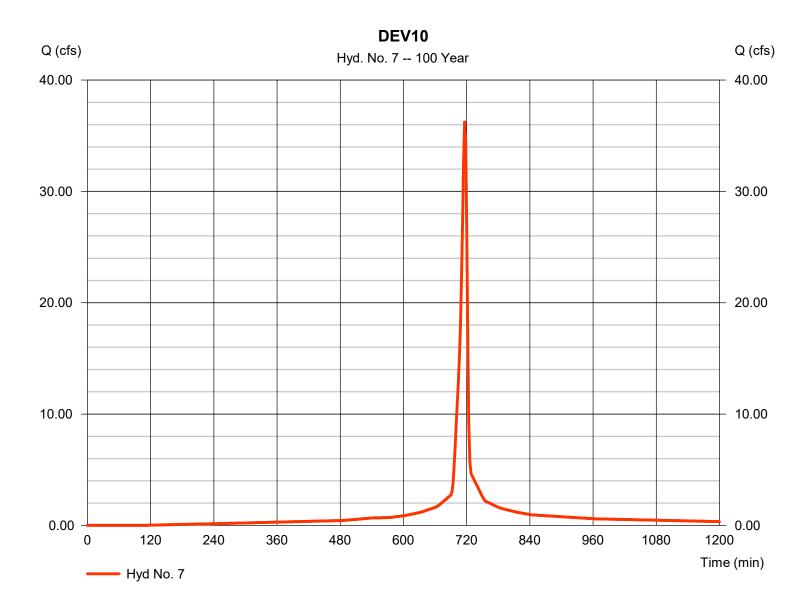
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Friday, 01 / 27 / 2023

Hyd. No. 7

DEV10

= 36.24 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 82,868 cuft Drainage area = 2.940 acCurve number = 92 = 0.0 % Hydraulic length = 0 ftBasin Slope Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



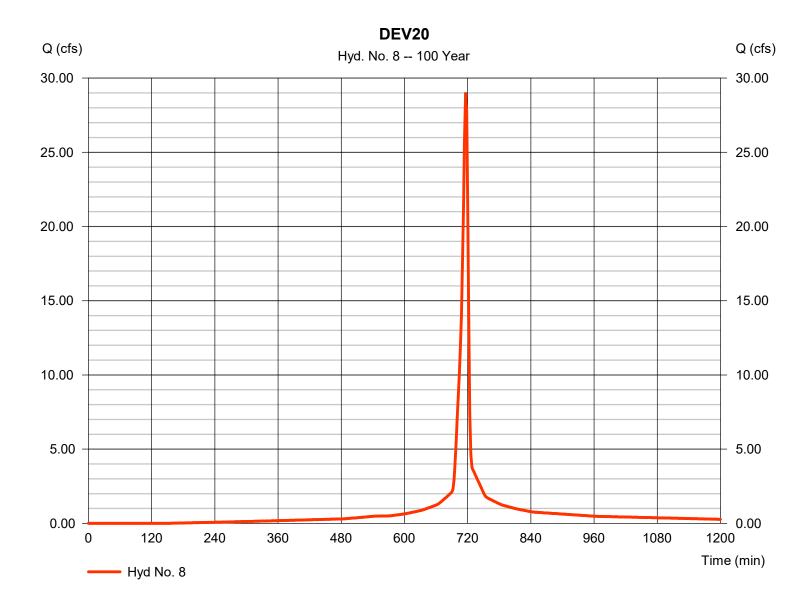
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Friday, 01 / 27 / 2023

Hyd. No. 8

DEV20

Hydrograph type = SCS Runoff Peak discharge = 28.97 cfsStorm frequency = 100 yrsTime to peak = 716 min = 64,654 cuft Time interval = 2 min Hyd. volume Drainage area = 2.400 acCurve number = 89 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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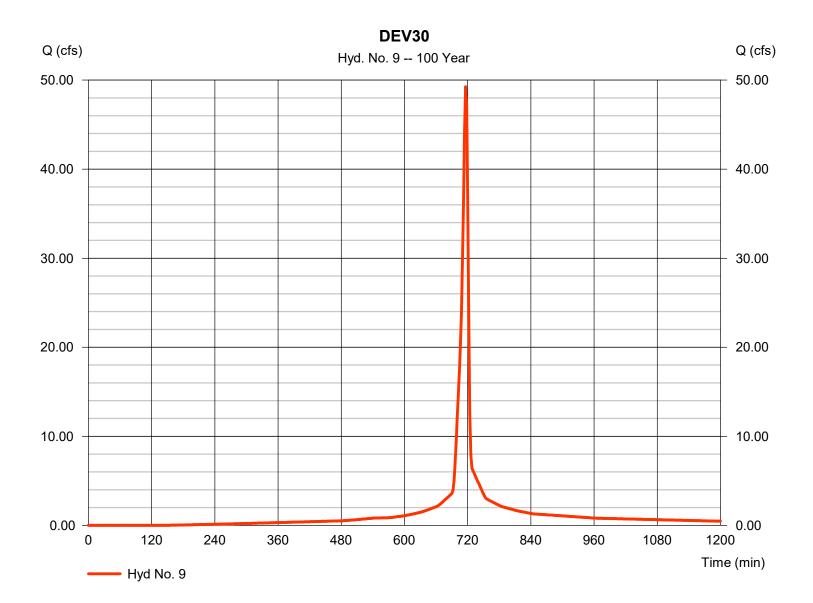
Friday, 01 / 27 / 2023

Hyd. No. 9

DEV₃₀

Hydrograph type = SCS Runoff Peak discharge = 49.26 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 109,912 cuft Drainage area Curve number = 4.080 ac= 89

Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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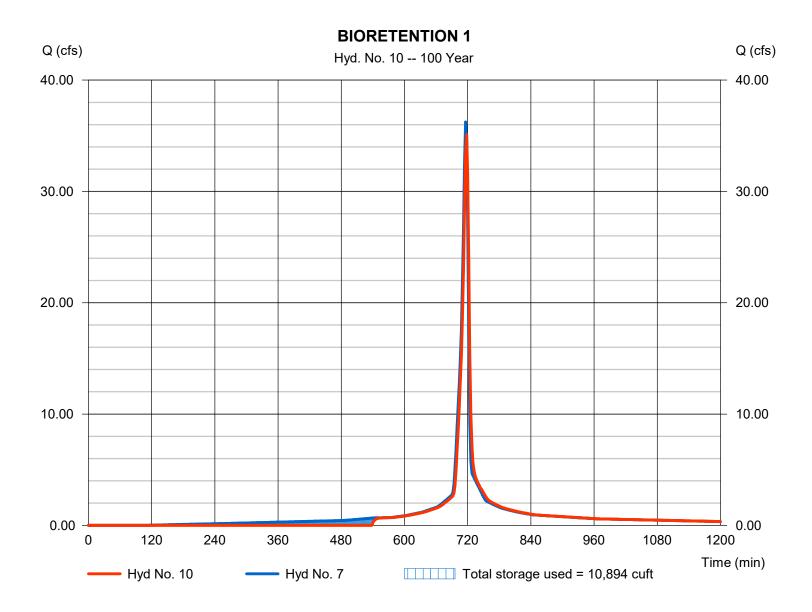
Friday, 01 / 27 / 2023

Hyd. No. 10

BIORETENTION 1

Hydrograph type = Reservoir Peak discharge = 35.10 cfsStorm frequency = 100 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 76,250 cuftInflow hyd. No. Max. Elevation = 1021.48 ft = 7 - DEV10 = BIORETENTION 1 Reservoir name Max. Storage = 10,894 cuft

Storage Indication method used.



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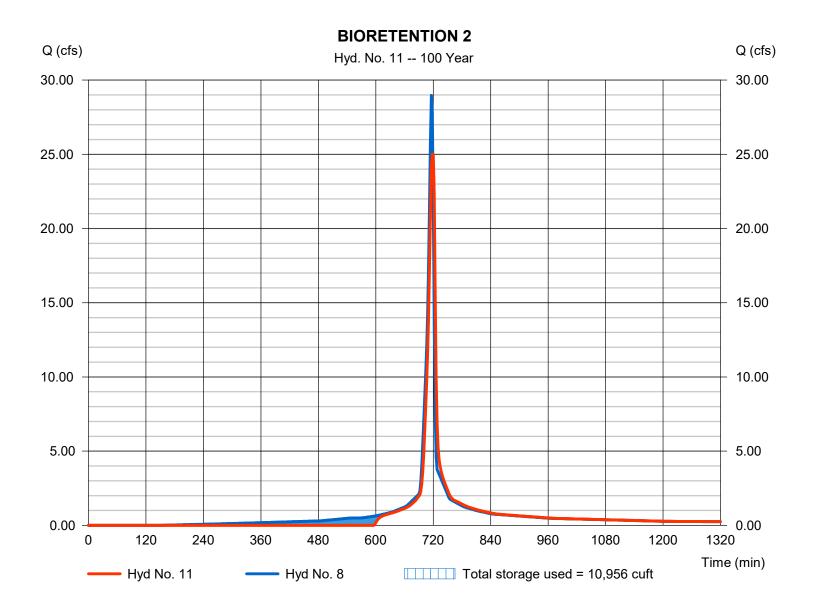
Friday, 01 / 27 / 2023

Hyd. No. 11

BIORETENTION 2

= Reservoir Hydrograph type Peak discharge = 25.01 cfsStorm frequency = 100 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 58,651 cuftInflow hyd. No. Max. Elevation = 1023.14 ft= 8 - DEV20 Reservoir name = BIORETENTION #2 Max. Storage = 10,956 cuft

Storage Indication method used.



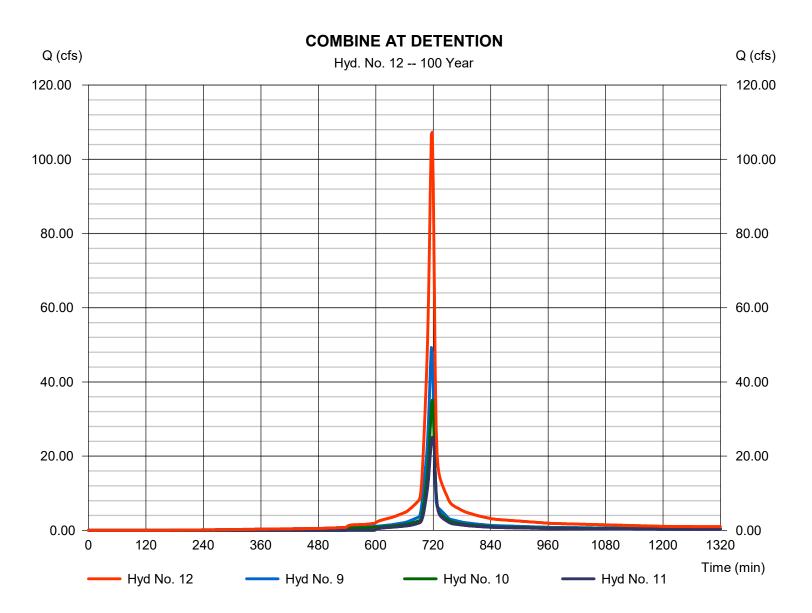
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Friday, 01 / 27 / 2023

Hyd. No. 12

COMBINE AT DETENTION

Hydrograph type = Combine Peak discharge = 107.32 cfsStorm frequency Time to peak = 100 yrs= 718 min Time interval = 2 min Hyd. volume = 244,813 cuft Inflow hyds. = 9, 10, 11Contrib. drain. area = 4.080 ac



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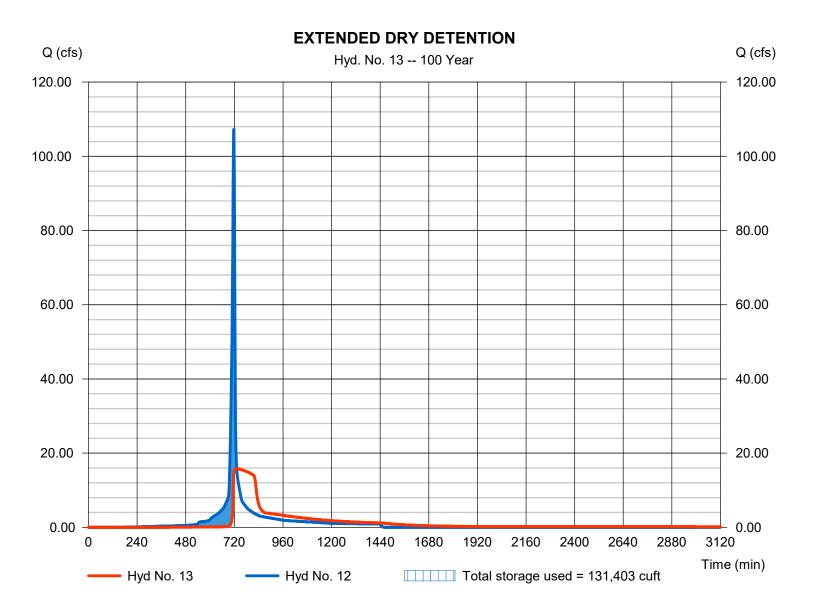
Friday, 01 / 27 / 2023

Hyd. No. 13

EXTENDED DRY DETENTION

Hydrograph type Peak discharge = 15.78 cfs= Reservoir Storm frequency Time to peak = 100 yrs= 732 min Time interval = 2 min Hyd. volume = 240,103 cuft Inflow hyd. No. = 12 - COMBINE AT DETENTIOMax. Elevation = 1020.59 ft= EXTENDED DRY DETENTIONMax. Storage Reservoir name = 131,403 cuft

Storage Indication method used.



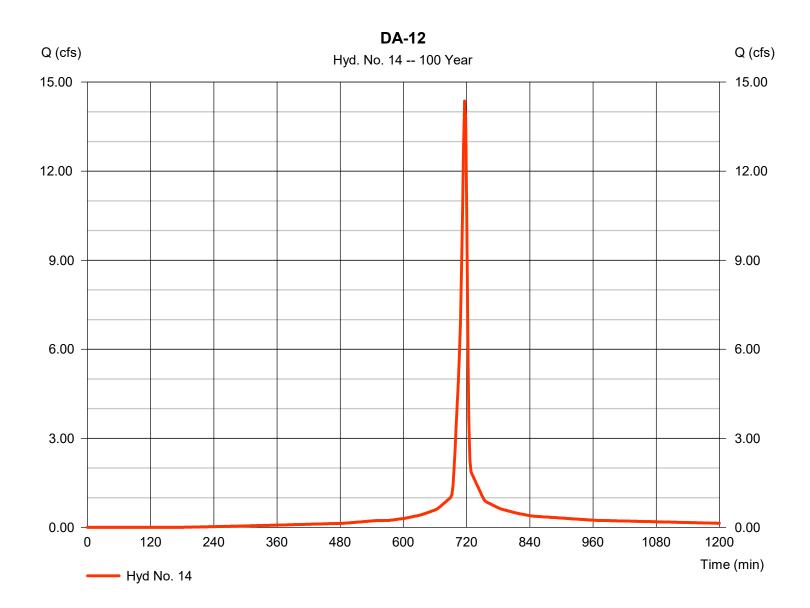
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Friday, 01 / 27 / 2023

Hyd. No. 14

DA-12

Hydrograph type = SCS Runoff Peak discharge = 14.36 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 31,586 cuft Drainage area = 1.210 ac Curve number = 87 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



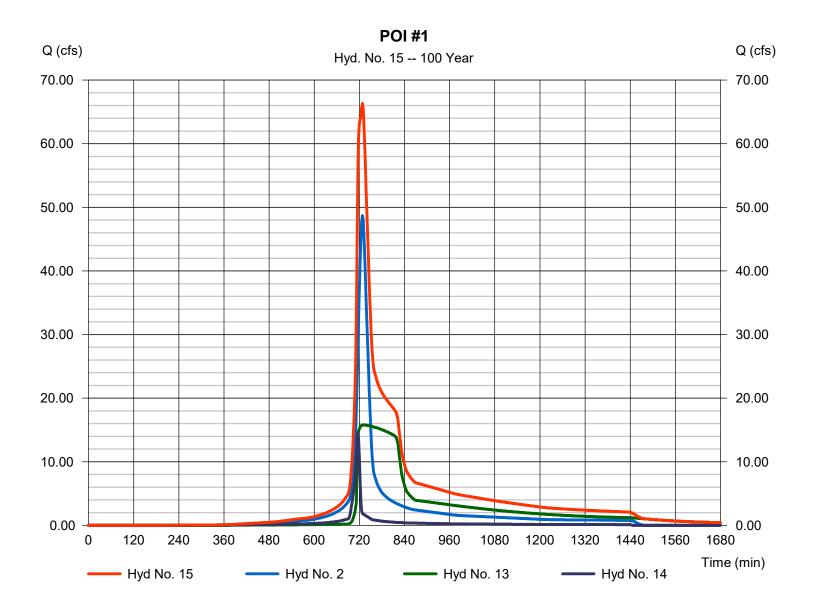
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Friday, 01 / 27 / 2023

Hyd. No. 15

POI #1

Hydrograph type = Combine Peak discharge = 66.32 cfsStorm frequency Time to peak = 100 yrs= 728 min Time interval = 2 min Hyd. volume = 450,905 cuft Inflow hyds. = 2, 13, 14 Contrib. drain. area = 9.490 ac



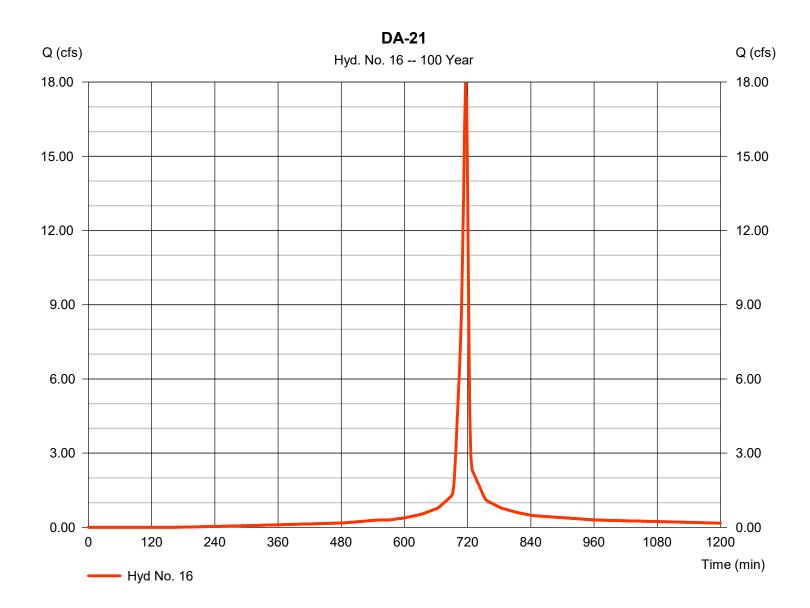
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Friday, 01 / 27 / 2023

Hyd. No. 16

DA-21

Hydrograph type = SCS Runoff Peak discharge = 17.96 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 39,783 cuft Drainage area = 1.500 acCurve number = 88 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



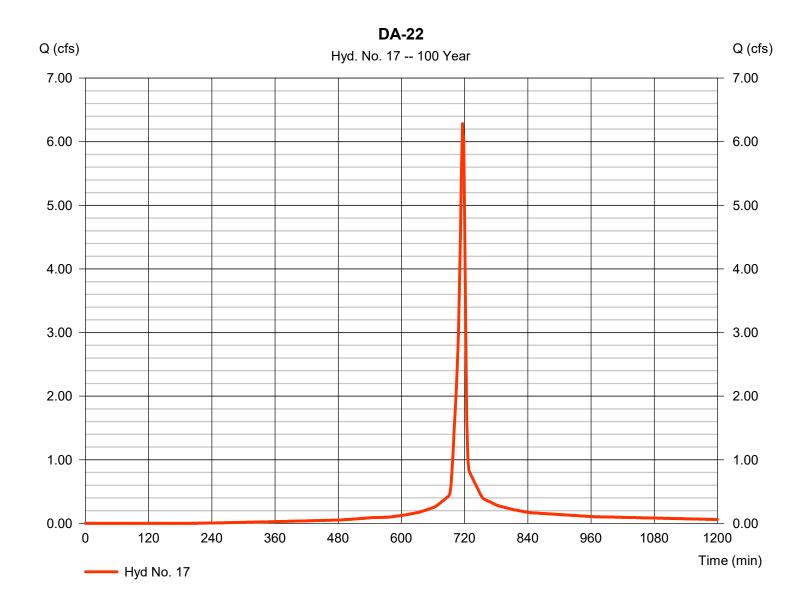
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Friday, 01 / 27 / 2023

Hyd. No. 17

DA-22

Hydrograph type = SCS Runoff Peak discharge = 6.284 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 13.644 cuft Drainage area Curve number = 0.540 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 9.25 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



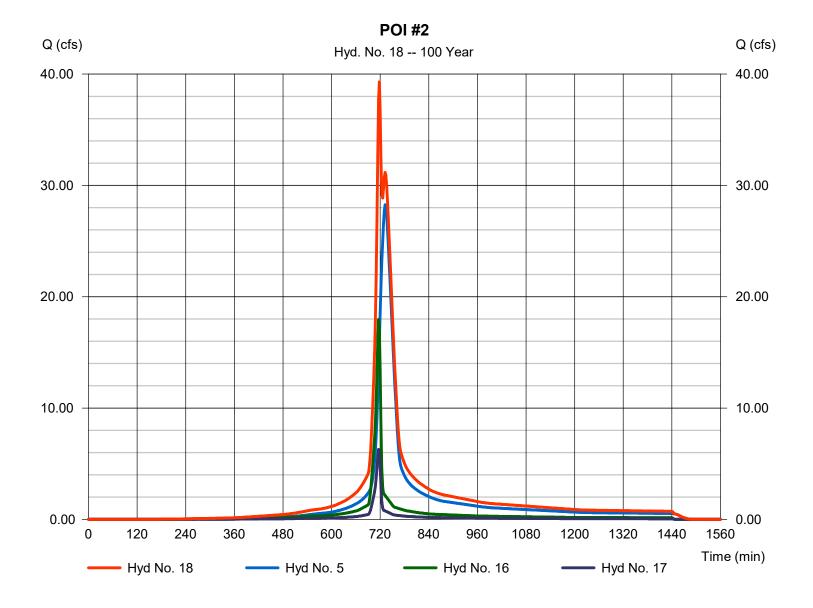
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Friday, 01 / 27 / 2023

Hyd. No. 18

POI #2

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min Inflow hyds. = 5, 16, 17 Peak discharge = 39.30 cfs
Time to peak = 718 min
Hyd. volume = 175,902 cuft
Contrib. drain. area = 7.430 ac



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Friday, 01 / 27 / 2023

Return Period	Intensity-Duration-Frequency Equation Coefficients (FHA)										
(Yrs)	В	D	E	(N/A)							
1	0.0000	0.0000	0.0000								
2	69.8703	13.1000	0.8658								
3	0.0000	0.0000	0.0000								
5	79.2597	14.6000	0.8369								
10	88.2351	15.5000	0.8279								
25	102.6072	16.5000	0.8217								
50	114.8193	17.2000	0.8199								
100	127.1596	17.8000	0.8186								

File name: Grandview, MO.IDF

Intensity = B / (Tc + D)^E

Return		Intensity Values (in/hr)													
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60			
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
2	5.69	4.61	3.89	3.38	2.99	2.69	2.44	2.24	2.07	1.93	1.81	1.70			
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
5	6.57	5.43	4.65	4.08	3.65	3.30	3.02	2.79	2.59	2.42	2.27	2.15			
10	7.24	6.04	5.21	4.59	4.12	3.74	3.43	3.17	2.95	2.77	2.60	2.46			
25	8.25	6.95	6.03	5.34	4.80	4.38	4.02	3.73	3.48	3.26	3.07	2.91			
50	9.04	7.65	6.66	5.92	5.34	4.87	4.49	4.16	3.88	3.65	3.44	3.25			
100	9.83	8.36	7.30	6.50	5.87	5.36	4.94	4.59	4.29	4.03	3.80	3.60			

Tc = time in minutes. Values may exceed 60.

Precip. file name: C:\Users\AE\Desktop\LEES SUMMIT PRINCETON DB.pcp

		R	ainfall P	recipitat	ion Tab	le (in)		
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	0.00	3.71	0.00	0.00	5.66	0.00	0.00	9.25
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00