LOW PRESSURE SANITARY SEWER STUDY

WOODLAND OAKS SW Corner Colbern & Blackwell

Site Acreage: 20.81 Acres

Lee's Summit, MO

PREPARED BY:



Revision

Date	Comment	Ву
4-6-22	Full LPS w/ Revised Alignment	AEP
6-14-22	Revised per City Comments Dated 5-17-22	AEP

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Matthew J. Schlicht, PE

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3. GENERAL INFORMATION

This study has been prepared to evaluate a low pressure sewer (LPS) alternative for complete sanitary service of the proposed single family residential subdivision, Woodland Oaks. Due to topographic challenges in addition to potential capacity issues with adjacent gravity sanitary sewers a LPS system is required to serve the development. The proposed development shall consist of 42 single family residential lots. The site is located at the southwest corner of Colbern Road and Blackwell Road. The property is bound by Colbern Road to the north, Blackwell Road to the east, Woodland Shores a single family residential subdivision to the south and a large acre single family tract to the west. Woodland Oaks is tributary to Lake Jacomo which is located to the northwest just across Colbern Road. The site is a tract of land located in the SE ¼ of Section 27, Township 48 North, and Range 31 West. See Exhibit A for an aerial view of the site along with the surrounding area.

4. METHODOLOGY

LPS capacity and hydraulic criteria shall at a minimum conform to Missouri Department of Natural Resources (MDNR) Minimum Design Requirements as outlined in 10 CSR 20-8.

- Velocity. Design shall be based on the most probable number of pumping units expected to operate simultaneously or on some other acceptable method of computing the peak pumpage rate. Environment One Corporation (E/One) Design Assistant 9 Software will be used to determine most probable number of pumping units expected to operate simultaneously along with associated peak velocities. E/One is a leader in the LPS field and has numerous time tested systems operating successfully throughout Missouri.
- A cleansing velocity of at least two feet per second (2 fps), at least once and preferably several times per day, shall be achieved. Projected velocities may be found in the E/One design report located in the Appendix.
- Minimum size. The minimum diameter sewer main pipe shall not be less than one and a half inches (1.5"). The minimum 1.5" forcemain size will handle a maximum of three homes. The use of 1.5" main in lieu of 2" will depend on lot layout and configuration.
- Service Line Connection. The minimum diameter service line pipe shall be one and one quarter inches (1.25"). Per discussion with the City a lateral assembly consisting of both a ball and check valve shall be located 5 feet from the forcemain. The City will own and maintain everything downstream of the isolation ball valve. The HOA or Private Resident shall own, operate and maintain the lateral assembly and all appurtenances upstream including the simplex grinder pump station and control panel. The LPS system shall terminate at the edge of the sanitary easement with a capped 1.25" service line.
- Simplex grinder pump station shall not serve multiple equivalent dwelling units (EDU) if owned, operated, and maintained by individual homeowners; and not serve commercial facilities.
- Storage volume. A grinder pump vault shall have a storage volume of at least seventy (70) gallons.
- Design Flow. Single family lots are projected to produce average daily flows of 370 gpd each (100 gpd per capita x 3.7 capita/dwelling). Peak hour demand per lot is 1,617 gpd or 1.12 gpm (370 gpd x 4.37 Peak Factor) well below the proposed pump capacity of 11 gpm. A pump curve for the proposed grinder pumps may be found in the Appendix.
- The roughness coefficient, C for the proposed pipe shall be 120.

In addition to developing a scouring velocity of 2 fps in the system a maximum fluid retention time in the system should be less than 24 hours to minimize creation of septic conditions. These two parameters along with total dynamic head will be the basis of design for the proposed forcemains.

5. LPS SYSTEM DESIGN

The development consists of 42 lots all of which will be served by the LPS system. The LPS forcemain will be comprised of a main trunk starting at NE Woodland Oak Circle and running along NE Woodland Oak Drive. The forcemain will exit the development and head south along the west right-of-way of Blackwell Road. The forcemain will then turn west at the south right-of-way of NE Woodland Shores Drive and terminate at the southeast corner of NE Woodland Shores Drive and NE Woodland Shores Circle. The forcemain will be connected to an existing 8" PVC gravity main located approximately 35 feet south of manhole 26-305 for further gravity conveyance downstream to the Woodland Shores Pump Station. Two branches will be included in the design to serve residences along NE Lashbrook Circle and NE Cherrybark Court. A proposed general layout for the LPS system may be found in Exhibit B.

Service lines and all upstream appurtenances shall be 1.25". Service line shall be HDPE SDR-11 and terminate at the edge of easement with a pipe cap. All lateral assemblies shall be placed 5' from the forcemain to minimize non-isolatable service line while allowing emergency shutoff of the residence. The public forcemain will commence just downstream of the ball valve. The lateral assembly which consists of the ball and check valve shall be privately owned along with all line and appurtenances upstream including the simplex grinder station and the control panel.

5.1 GRINDER PUMPS

The low-pressure sewer system design was based on the DH071 grinder pump manufactured by E/One Sewer Systems. These units feature a 1 horsepower motor and have a typical discharge of 11 gpm at 40 psi. They have a storage capacity of 70 gallons and are rated by the manufacturer for up to 700 gallons per day. The manufacturer's pump curve may be found in Exhibit C. Each pump will have an internal check valve and will be installed with a gate valve on the service lateral near the property line. Additionally, each pump will be installed with a control panel that includes a high level alarm. The grinder pump stations and additional service line shall be installed with construction of the homes.

5.2 FORCEMAIN

The forcemain design was completed using software developed by E-One along with guidance provided by the pump manufacturer. The design involves breaking the system down into zones, with each zone defined by a given number of pump connections. Zone 1 is typically located furthest away from the receiving structure with subsequent zones being added at all branches and changes in pipe size. The branch structure facilitates pipe sizing for each zone based upon a statistically probable number of simultaneous pump operations. Pipe sizes were determined by requiring a minimum velocity of 2 feet per second for average daily flows, as well as maintaining a maximum fluid retention time in the system of less than 24 hours. The required pipe material is HDPE SDR-11. All branches shall terminate with an end of line flushing assembly. The City has requested an odor/corrosion control system be furnished. The proposed odor control system shall be a liquid chemical feed type. The chemical employed shall be Bioxide a non-reactive nitrate salt. The Bioxide provides nitrate oxygen which reacts with sulfide compounds to eliminate/minimize the production of hydrogen sulfide. System sizing was based on the more conservative prevention versus removal methodology. In the simplified model, prevention is based on providing 4.8 moles of NO3 per mole of Sulfide which requires 9.282 lbs of NO3 per lb of sulfide. The system will average 0.016 MGD at buildout. The dissolved sulfides in the wastewater where assumed to be 2 mg/L for standard domestic wastewater. The dissolved sulfide load at buildout is 0.27 lbs/day. The nitrate load at buildout is 2.51 lbs/day. The Bioxide treatment ratio is 2.1 gallons of Bioxide per pound of Sulfide. The stoichiometric Bioxide requirement is 0.567 gallons per day (1.50 ml/min) at buildout. A configurable peristaltic dosage pump with a dosage range of (0.1 - 300 ml/min) was selected. This pump has plenty of room on both the lower and upper ends to dial in the process. The storage sizing should be based on

maximum seasonal Bioxide usage and product availability/pricing structure from the supplier. A 300 gallon chemical feed tank was chosen to provide maximum flexibility for the City. The chemical feed pump is configurable and has the ability to change doses based on timing.

The City has also requested air release valve/vault be provided at the forcemain high points. There will be two ARI Model D-025 2" air release valves located on the 3" common forcemain. See Exhibit H for air release valve recommendations from ARI the City approved vendor. The City also requests two manholes both upstream and downstream of the tie-in point be internally coated with epoxy. The proposed layout only has one manhole upstream of the tie-in point therefore only one manhole will be epoxy coated upstream.

The forcemain was modeled with eight zones. Zone 1 was placed farthest from the outlet or gravity tie-in point while Zone 8 consisted of the last run of forcemain which tied into the existing gravity system offsite. Forcemain consisted of both 2 and 3 inch segments. The maximum pressure in the system occurred in Zone 1 at 152.52 feet of head, which is less than the 185 feet recommended by the pump manufacturer. Zone 1 consists of the first three lots on Forcemain 1. Maximum scouring velocities of 2 fps were obtained in all eight zones with the lowest scouring velocity occurring in Zones 1, 3 and 6 at 2.38 fps. The maximum retention time was calculated at 2.03 hours in Zone 1. The proposed peak flow from the LPS system as determined by E-One Design Software was determined to be 66 gpm or 0.147 cfs as provided by 6 simultaneous pumps operating. The final design calculations are summarized and provided in Exhibit D.

6. RECEIVING GRAVITY SEWER CAPACITY ANALYSIS

The Woodland Shores gravity sanitary sewer capacity analysis was terminated at the Woodland Shores pump station wetwell labeled 62-002PS, see Sanitary Sewer Map, located in Exhibit E, for both the existing sanitary sewer system layout along with proposed development location and tie-in point. There are currently 57.98 +/-acres tributary to wetwell 62-002PS, see Exhibit F Sanitary Sewer Tributary Area Map from original CES study. The existing serviceable area outlined by CES appears to be reasonable and has been utilized for this analysis. The proposed development will utilize the east branch of the sewer system to convey flow. All tributary area has been accounted for to wetwell 62-002PS as stipulated by the City's design criteria. The proposed development consists of 42 single family residences to be served by a LPS system. The proposed peak flow for the proposed development as determined by E-One Software (66 gpm or 0.147 cfs) was added to the Peak Flow column at upstream manhole 26-305 and carried thru to the wetwell 26-002PS. The proposed development may be served by the existing downstream sewer system with no surcharging anticipated as outlined in Exhibit G Sanitary Sewer Capacity Analysis.

7. CONCLUSIONS & RECOMMENDATIONS

An LPS system and existing gravity system will be able to provide sanitary sewer service for 42 residences in the proposed development without any adverse impacts to the community or downstream sanitary system. We recommend that an LPS system as described in this report be constructed to service the 42 residences as shown on the general layout.

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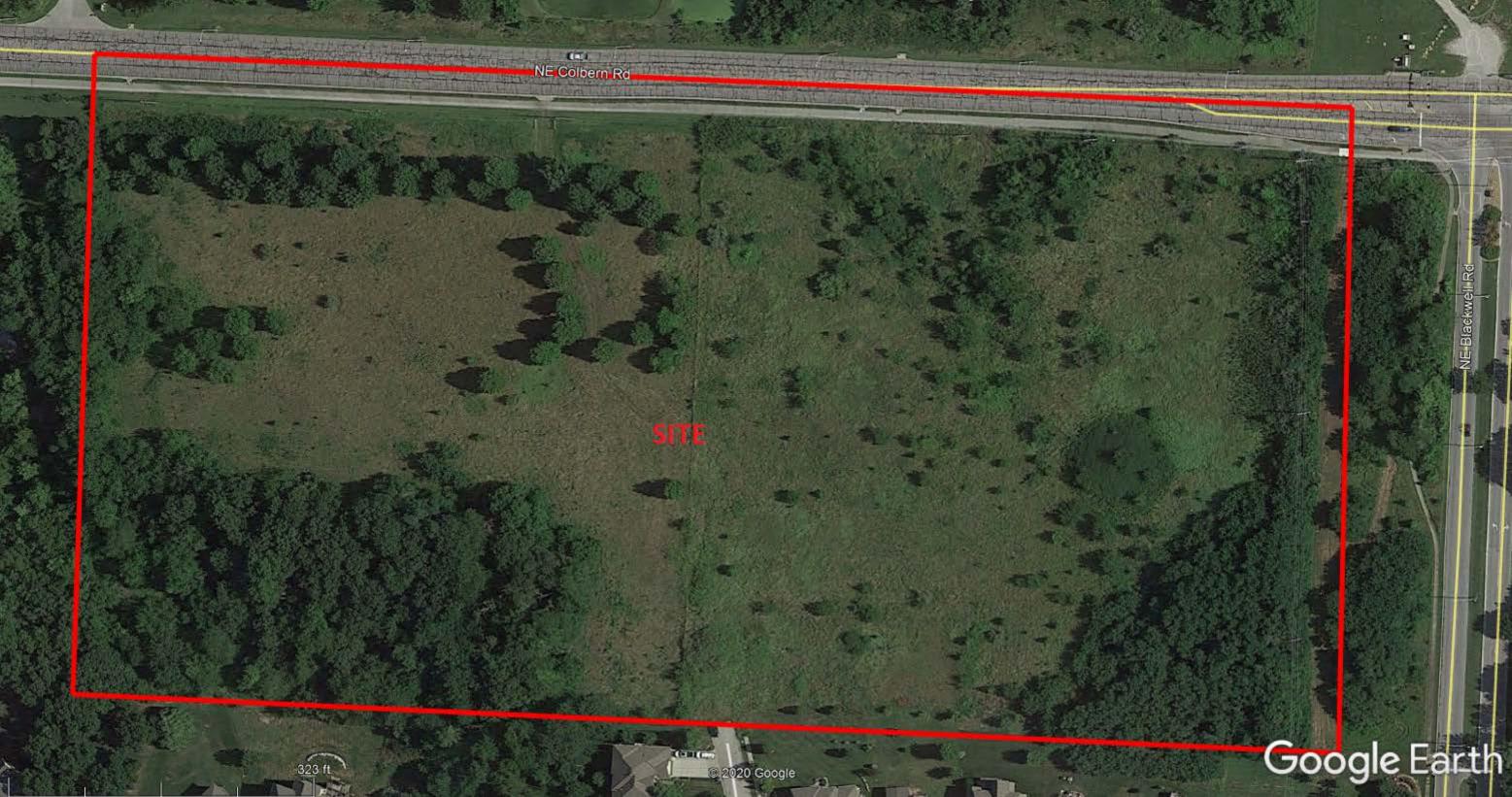
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Exhibit A **Aerial Images**



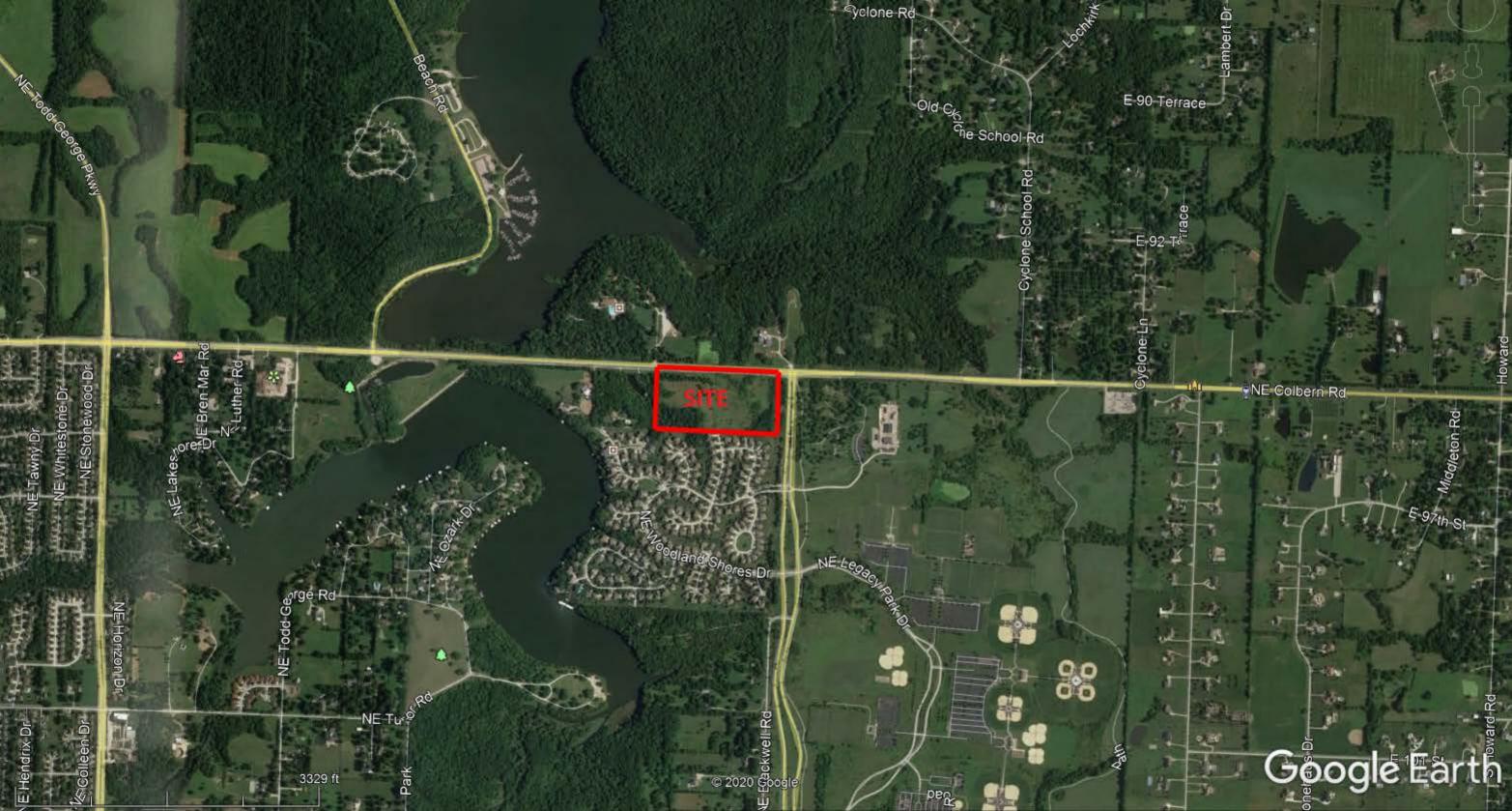


Exhibit B Sanitary Sewer General Layout



Exhibit C E/One Grinder Pump Flow Curve

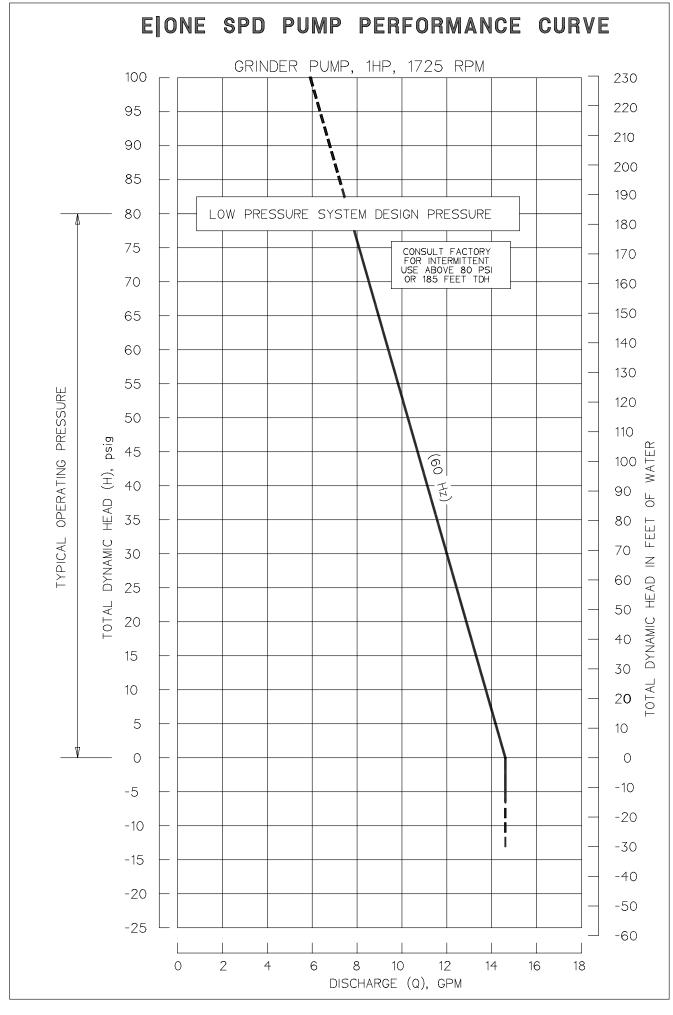


Exhibit D E/One Design Summary

Prepared By:

April 6, 2022

Zone	Connects				Max Flow	Max	Max Flow	Pipe Size	Max	Length of Main	Friction Loss	Friction	Accum Fric	Max Main	Minimum Pump	Static Head	Total
Number	to Zone				Per Pump	Sim Ops	(GPM)	(inches)	Velocity	this Zone	Factor	Loss This	Loss (feet)	Elevation	Elevation	(feet)	Dynamic
		in Zone	in Zone		(gpm)				(FPS)		(ft/100 ft)	Zone					Head (ft)
This spreadsheet was calculated using pipe diameters for: SDR11HDPE Friction loss calculations were based on a Constant for inside roughness"C" of: 120												20					
1.00	2.00	3	3	370	11.00	2	22.00	2.00	2.38	145.14	1.80	2.61	97.52	980.00	925.00	55.00	152.52
2.00	5.00	14	17	370	11.00	4	44.00	2.00	4.76	864.19	6.49	56.08	94.91	980.00	925.00	55.00	149.91
3.00	4.00	3	3	370	11.00	2	22.00	2.00	2.38	80.96	1.80	1.46	56.29	980.00	941.00	39.00	95.29
4.00	5.00	4	7	370	11.00	3	33.00	2.00	3.57	420.05	3.81	16.00	54.83	980.00	940.00	40.00	94.83
5.00	8.00	7	31	370	11.00	6	66.00	3.00	3.29	409.30	2.08	8.52	38.83	980.00	941.00	39.00	77.83
6.00	7.00	3	3	370	11.00	2	22.00	2.00	2.38	80.70	1.80	1.45	48.66	980.00	941.00	39.00	87.66
7.00	8.00	5	8	370	11.00	3	33.00	2.00	3.57	443.75	3.81	16.90	47.21	980.00	941.00	39.00	86.21
8.00	8.00	3	42	370	11.00	6	66.00	3.00	3.29	1,456.22	2.08	30.31	30.31	980.00	947.00	33.00	63.31

Zone Number	Connects to Zone	Accumulated Total of Pumps this Zone	Pipe Size (inches)	Gallons per 100 lineal feet	Length of Zone	Capacity of Zone	Average Daily Flow	Average Fluid Changes per Day	Average Retention Time (Hr)	Accumulated Retention Time (Hr)
This spread	This spreadsheet was calculated using pipe diameters for: SDR11HDPE Gals per Day per Dwelling									
1.00	2.00	3	2.00	15.40	145.14	22.36	1,110	49.65	0.48	2.03
2.00	5.00	17	2.00	15.40	864.19	133.11	6,290	47.25	0.51	1.55
3.00	4.00	3	2.00	15.40	80.96	12.47	1,110	89.01	0.27	1.91
4.00	5.00	7	2.00	15.40	420.05	64.70	2,590	40.03	0.60	1.64
5.00	8.00	31	3.00	33.47	409.30	136.98	11,470	83.74	0.29	1.04
6.00	7.00	3	2.00	15.40	80.70	12.43	1,110	89.30	0.27	1.58
7.00	8.00	8	2.00	15.40	443.75	68.35	2,960	43.31	0.55	1.31
8.00	8.00	42	3.00	33.47	1,456.22	487.35	15,540	31.89	0.75	0.75

Exhibit E Sanitary Sewer Map



Exhibit F Sanitary Sewer Tributary Area Map

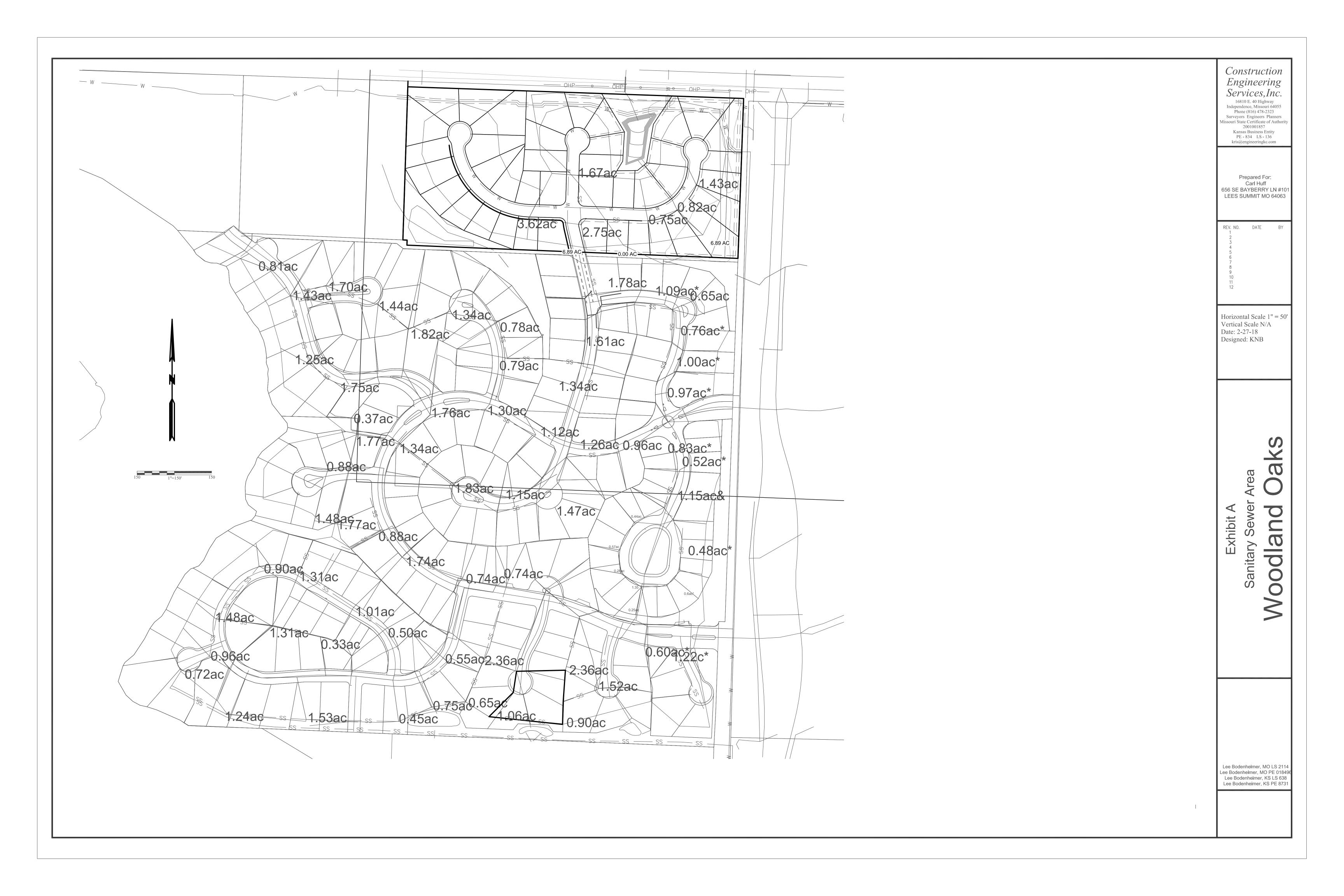


Exhibit G Sanitary Sewer Capacity Analysis

			Wood	dland Oaks -	Sanitary :	Sewer Ca	oacitv An	alvsis: Cit	v of Lee	's Summit	Criteria	at Ultimat	e Buildout			
		U.S. Str.	Cum.					, , , , , ,	,				Segment		Surcharge	
D.S. Str.	U.S. Str.	Area	Area	Peak Flow	FL IN	FL OUT	Length	Slope	Dia	Material	n	Capacity	Condition	Rim El.	Depth	U.S. Str.
		(ac.)	(ac.)	(cfs)			(ft)	(ft/ft)	(ft)			(cfs)			(ft)	
26-002PS	26-166	0.01	57.98	1.625	902	902.9	7.37	0.1221	0.67	PVC	0.014	3.948	GRAVITY	916.07	0.00	26-166
26-166	26-167	35.91	57.97	1.624	903	903.96	14.36	0.0669	0.67	PVC	0.014	2.921	GRAVITY	916.68	0.00	26-167
26-167	26-178	1.24	22.06	0.794	904.04	915.01	251.41	0.0436	0.67	PVC	0.014	2.360	GRAVITY	923.31	0.00	26-178
26-178	26-179	1.53	20.82	0.762	915.21	918.62	302.68	0.0113	0.67	PVC	0.014	1.199	GRAVITY	929.47	0.00	26-179
26-179	26-180	0.45	19.29	0.722	918.72	920.71	385.5	0.0052	0.67	PVC	0.014	0.812	GRAVITY	942.37	0.00	26-180
26-180	26-181	1.30	18.84	0.710	920.81	921.80	144.69	0.0068	0.67	DIP	0.015	0.872	GRAVITY	944.90	0.00	26-181
26-181	26-182	3.75	17.54	0.675	921.95	922.96	133	0.0076	0.67	DIP	0.015	0.919	GRAVITY	947.08	0.00	26-182
26-182	26-183	0	13.79	0.573	923.04	923.64	92.09	0.0065	0.67	DIP	0.015	0.851	GRAVITY	945.64	0.00	26-183
26-183	26-184	0	13.79	0.573	923.79	926.03	330.76	0.0068	0.67	PVC	0.014	0.930	GRAVITY	933.94	0.00	26-184
26-184	26-185	2.36	13.79	0.573	926.18	927.29	87.96	0.0126	0.67	PVC	0.014	1.269	GRAVITY	935.49	0.00	26-185
26-185	26-186	1.52	11.43	0.507	927.39	929.99	149.14	0.0174	0.67	PVC	0.014	1.492	GRAVITY	936.19	0.00	26-186
26-186	26-187	0	9.91	0.463	930.17	938.26	221.61	0.0365	0.67	PVC	0.014	2.159	GRAVITY	951.11	0.00	26-187
26-187	26-188	3.44	9.91	0.463	938.55	938.87	42.27	0.0076	0.67	PVC	0.014	0.983	GRAVITY	950.62	0.00	26-188
26-188	26-200	0.25	6.47	0.362	938.92	939.68	80.32	0.0095	0.67	PVC	0.014	1.099	GRAVITY	949.80	0.00	26-200
26-200	26-299	2.43	6.22	0.355	939.78	948.75	130.58	0.0687	0.67	DIP	0.015	2.764	GRAVITY	963.48	0.00	26-299
26-299	26-300	0.28	3.79	0.284	950.15	951.9	103.01	0.0170	0.67	PVC	0.014	1.473	GRAVITY	965.37	0.00	26-300
26-300	26-301	0.57	3.51	0.275	952.9	957.6	94.87	0.0495	0.67	PVC	0.014	2.515	GRAVITY	969.22	0.00	26-301
26-301	26-302	0.44	2.94	0.257	959.6	962.94	134.21	0.0249	0.67	PVC	0.014	1.782	GRAVITY	975.33	0.00	26-302
26-302	26-303	1.15	2.5	0.242	963.14	964.36	126.94	0.0096	0.67	PVC	0.014	1.108	GRAVITY	976.54	0.00	26-303
26-303	26-304	0.52	1.35	0.202	964.86	966.35	179.26	0.0083	0.67	PVC	0.014	1.030	GRAVITY	978.90	0.00	26-304
26-304	26-305	0.83	0.83	0.182	966.55	967.72	117.28	0.0100	0.67	PVC	0.014	1.128	GRAVITY	979.94	0.00	26-305

^{*}U.S. Str. Areas in bold account for additional upstream branch flow.

0.147 cfs

was added to Peak Flow at 26-305 and carried to Structure 26-002PS

^{**}Woodland Oaks Peak Flow = 66 GPM

Exhibit H ARV Sizing Recommendation

Anthony Philipsheck

From: Kim Sorensen < Kim.Sorensen@aquestia.com>

Sent: Sunday, June 12, 2022 2:13 PM

To: Anthony Philipsheck

Cc: Brett Warga

Subject: RE: Thank you for Requesting a Sign up for ARIAVcad.

Anthony,

Our ARIavCAD analysis software does not lend itself well to this type of sewer net work. It is intended more for single pipe transmission force mains. I reviewed the report and it appears that all of the pipes are small, less than 4". I know for certain the D-025 will be the right valve for this application for those small pipes. These valves should be located at all of the high points in the system. Please be aware the D-025 requires 1 PSI to seal as measured at the valve seal elevation. This pressure will be 1 PSI +/- less than the pipeline pressure at the valve location. I would recommend that you check static and operational pressures at the valve locations.

Please let me know if you have any questions.

Regards,

Please note the e-mail address change: kim.sorensen@aquestia.com

D. Kim Sorensen, P.E. Senior Applications Engineer kim.sorensen@aquestia,com

Phone: 801-254-2226 Mobile: 801-875-9155 Toll Free: 888-7-ARIUSA (888-727-4872) www.ariusa.com |

www.dorot.com | www.controlvalves.com

----Original Message-----

From: Anthony Philipsheck <aphilipsheck@es-kc.com>

Sent: Friday, June 10, 2022 3:01 PM

To: Kim Sorensen < kim.sorensen@aguestia.com>

Subject: FW: Thank you for Requesting a Sign up for ARIAVcad.

Kim,

I would like to get help sizing an air release valve or two potentially for a Low Pressure Sewer System. The City of Lee's Summit Missouri only has ARI Model D-26 on their approved air release valve list.

See study attached for proposed project.

Any help you can provide is greatly appreciated.

Thanks,

Anthony Philipsheck Engineering Solutions 50 SE 30th Street Lee's Summit, MO 64082 P (816) 623-9888 ext. 5 F (816) 623-9849 www.engineeringsolutionskc.com

----Original Message-----

From: pesa.support@tomisystems.com [mailto:pesa.support@tomisystems.com]

Sent: Friday, June 10, 2022 3:50 PM

To: aphilipsheck@es-kc.com

Subject: Thank you for Requesting a Sign up for ARIAVcad.

Thank-you for your ARIavCAD registration, your request is under approval review.

The approval process may take a few days so if you have an urgent air valve analysis sizing need you may contact A.R.I Application engineer who will assist you in the analysis process:

D. Kim Sorensen, P.E. Senior Applications Engineer Aquestia USA Kim.Sorensen@aquestia.com 801.875.9155 (Cell) 801.254,2226 (Office)