LOW PRESSURE SANITARY SEWER STUDY

WOODLAND OAKS SW Corner Colbern & Blackwell

Site Acreage: 20.81 Acres

Lee's Summit, MO

PREPARED BY:



THEW ILICH

Revision

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| Date | Comment | By |
| 4-6-22 | Full LPS w/ Revised Alignment | AEP |
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Matthew J. Schlicht, PE

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3. GENERAL INFORMATION

This study has been prepared to evaluate a low pressure sewer (LPS) alternative for complete sanitary service of the proposed single family residential subdivision, Woodland Oaks. Due to topographic challenges in addition to potential capacity issues with adjacent gravity sanitary sewers a LPS system is required to serve the development. The proposed development shall consist of 42 single family residential lots. The site is located at the southwest corner of Colbern Road and Blackwell Road. The property is bound by Colbern Road to the north, Blackwell Road to the east, Woodland Oaks is tributary to Lake Jacomo which is located to the northwest just across Colbern Road. The site is a tract of land located in the SE ¼ of Section 27, Township 48 North, and Range 31 West. See Exhibit A for an aerial view of the site along with the surrounding area.

4. METHODOLOGY

LPS capacity and hydraulic criteria shall at a minimum conform to Missouri Department of Natural Resources (MDNR) Minimum Design Requirements as outlined in 10 CSR 20-8.

- Velocity. Design shall be based on the most probable number of pumping units expected to operate simultaneously or on some other acceptable method of computing the peak pumpage rate. Environment One Corporation (E/One) Design Assistant 9 Software will be used to determine most probable number of pumping units expected to operate simultaneously along with associated peak velocities. E/One is a leader in the LPS field and has numerous time tested systems operating successfully throughout Missouri.
- A cleansing velocity of at least two feet per second (2 fps), at least once and preferably several times per day, shall be achieved. Projected velocities may be found in the E/One design report located in the Appendix.
- Minimum size. The minimum diameter sewer main pipe shall not be less than one and a half inches (1.5"). The minimum 1.5" forcemain size will handle a maximum of three homes. The use of 1.5" main in lieu of 2" will depend on lot layout and configuration.
- Service Line Connection. The minimum diameter service line pipe shall be one and one quarter inches (1.25"). Per discussion with the City a lateral assembly consisting of both a ball and check valve shall be located 5 feet from the forcemain. The City will own and maintain everything downstream of the isolation ball valve. The HOA or Private Resident shall own, operate and maintain the lateral assembly and all appurtenances upstream including the simplex grinder pump station and control panel. The LPS system shall terminate at the edge of the sanitary easement with a capped 1.25" service line.
- Simplex grinder pump station shall not serve multiple equivalent dwelling units (EDU) if owned, operated, and maintained by individual homeowners; and not serve commercial facilities.
- Storage volume. A grinder pump vault shall have a storage volume of at least seventy (70) gallons.
- Design Flow. Single family lots are projected to produce average daily flows of 370 gpd each (100 gpd per capita x 3.7 capita/dwelling). Peak hour demand per lot is 1,617 gpd or 1.12 gpm (370 gpd x 4.37 Peak Factor) well below the proposed pump capacity of 11 gpm. A pump curve for the proposed grinder pumps may be found in the Appendix.
- The roughness coefficient, C for the proposed pipe shall be 120.

In addition to developing a scouring velocity of 2 fps in the system a maximum fluid retention time in the system should be less than 24 hours to minimize creation of septic conditions. These two parameters along with total dynamic head will be the basis of design for the proposed forcemains.

5. LPS SYSTEM DESIGN

The development consists of 42 lots all of which will be served by the LPS system. The LPS forcemain will be comprised of a main trunk starting at NE Woodland Oak Circle and running along NE Woodland Oak Drive. The forcemain will exit the development and head south along the west right-of-way of Blackwell Road. The forcemain will then turn west at the south right-of-way of NE Woodland Shores Drive and terminate at the southeast corner of NE Woodland Shores Drive and NE Woodland Shores Circle. The forcemain will be connected to an existing 8" PVC gravity main located approximately 35 feet south of manhole 26-305 for further gravity conveyance downstream to the Woodland Shores Pump Station. Two branches will be included in the design to serve residences along NE Lashbrook Circle and NE Cherrybark Court. A proposed general layout for the LPS system may be found in Exhibit B.

Service lines and all upstream appurtenances shall be 1.25". Service line shall be HDPE SDR-11 and terminate at the edge of easement with a pipe cap. All lateral assemblies shall be placed 5' from the forcemain to minimize non-isolatable service line while allowing emergency shutoff of the residence. The public forcemain will commence just downstream of the ball valve. The lateral assembly which consists of the ball and check valve shall be privately owned along with all line and appurtenances upstream including the simplex grinder station and the control panel.

5.1 GRINDER PUMPS

The low-pressure sewer system design was based on the DH071 grinder pump manufactured by E/One Sewer Systems. These units feature a 1 horsepower motor and have a typical discharge of 11 gpm at 40 psi. They have a storage capacity of 70 gallons and are rated by the manufacturer for up to 700 gallons per day. The manufacturer's pump curve may be found in Exhibit C. Each pump will have an internal check valve and will be installed with a gate valve on the service lateral near the property line. Additionally, each pump will be installed with a control panel that includes a high level alarm. The grinder pump stations and additional service line shall be installed with construction of the homes.

5.2 FORCEMAIN

The forcemain design was completed using software developed by E-One along with guidance provided by the pump manufacturer. The design involves breaking the system down into zones, with each zone defined by a given number of pump connections. Zone 1 is typically located furthest away from the receiving structure with subsequent zones being added at all branches and changes in pipe size. The branch structure facilitates pipe sizing for each zone based upon a statistically probable number of simultaneous pump operations. Pipe sizes were determined by requiring a minimum velocity of 2 feet per second for average daily flows, as well as maintaining a maximum fluid retention time in the system of less than 24 hours. The required pipe material is HDPE SDR-11. All branches shall terminate with an end of line flushing assembly. The City has requested an odor/corrosion control system be furnished along with an air release valve/vault at the forcemain high point. The City also requests two manholes both upstream and downstream of the tie-in point be coated with epoxy. The proposed layout only has one manhole upstream of the tie-in point therefore only one manhole will be epoxy coated upstream.

The forcemain was modeled with eight zones. Zone 1 was placed farthest from the outlet or gravity tie-in point while Zone 8 consisted of the last run of forcemain which tied into the existing gravity system offsite. Forcemain consisted of both 2 and 3 inch segments. The maximum pressure in the system occurred in Zone 1 at 152.52 feet of head, which is less than the 185 feet recommended by the pump manufacturer. Zone 1 consists of the first three lots on Forcemain 1. Maximum scouring velocities of 2 fps were obtained in all eight zones with the lowest scouring velocity occurring in Zones 1, 3 and 6 at 2.38 fps. The maximum retention time was

calculated at 2.03 hours in Zone 1. The proposed peak flow from the LPS system as determined by E-One Design Software was determined to be 66 gpm or 0.147 cfs as provided by 6 simultaneous pumps operating. The final design calculations are summarized and provided in Exhibit D.

6. RECEIVING GRAVITY SEWER CAPACITY ANALYSIS

The Woodland Shores gravity sanitary sewer capacity analysis was terminated at the Woodland Shores pump station wetwell labeled 62-002PS, see Sanitary Sewer Map, located in Exhibit E, for both the existing sanitary sewer system layout along with proposed development location and tie-in point. There are currently 57.98 +/- acres tributary to wetwell 62-002PS, see Exhibit F Sanitary Sewer Tributary Area Map from original CES study. The existing serviceable area outlined by CES appears to be reasonable and has been utilized for this analysis. The proposed development will utilize the east branch of the sewer system to convey flow. All tributary area has been accounted for to wetwell 62-002PS as stipulated by the City's design criteria. The proposed development consists of 42 single family residences to be served by a LPS system. The proposed peak flow for the proposed development as determined by E-One Software (66 gpm or 0.147 cfs) was added to the Peak Flow column at upstream manhole 26-305 and carried thru to the wetwell 26-002PS. The proposed development may be served by the existing downstream sewer system with no surcharging anticipated as outlined in Exhibit G Sanitary Sewer Capacity Analysis.

7. CONCLUSIONS & RECOMMENDATIONS

An LPS system and existing gravity system will be able to provide sanitary sewer service for 42 residences in the proposed development without any adverse impacts to the community or downstream sanitary system. We recommend that an LPS system as described in this report be constructed to service the 42 residences as shown on the general layout.













GRAPHIC SCALE



SANITARY GENERAL LAYOUT

GENERAL NOTE:

1 ~ ALL CONSTRUCTION SHALL CONFORM TO THE CITY OF LEE'S SUMMIT DESIGN AND CONSTRUCTION MANUAL AS ADOPTED BY ORDINANCE 5813.

2 ~ TRENCH CHECKS SHALL BE INSTALL AT ALL SANITARY WYES LOCATION.



Exhibit C

E/One Grinder Pump Flow Curve



ESD 08-0022 REV. 2, 6/08



PRELIMINARY PRESSURE SEWER - PIPE SIZING AND BRANCH ANALYSIS

Prepared By:

April 6, 2022

| Zone | Connects | Number | Accum | Gals/day | Max Flow | Max | Max Flow | Pipe Size | Max | Length of Main | Friction Loss | Friction | Accum Fric | Max Main | Minimum Pump | Static Head | Total |
|---|----------|----------|---------|----------|----------|---------|----------|-----------|----------|----------------|---------------|-----------|-------------|-----------|--------------|-------------|-----------|
| Number | to Zone | of Pumps | Pumps | per Pump | Per Pump | Sim Ops | (GPM) | (inches) | Velocity | this Zone | Factor | Loss This | Loss (feet) | Elevation | Elevation | (feet) | Dynamic |
| | | in Zone | in Zone | | (gpm) | | | | (FPS) | | (ft/100 ft) | Zone | | | | | Head (ft) |
| This spreadsheet was calculated using pipe diameters for: SDR11HDPE Friction loss calculations were based on a Constant for inside roughness "C" of | | | | | | | | | " of: 1 | 20 | | | | | | | |
| 1.00 | 2.00 | 3 | 3 | 370 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 145.14 | 1.80 | 2.61 | 97.52 | 980.00 | 925.00 | 55.00 | 152.52 |
| 2.00 | 5.00 | 14 | 17 | 370 | 11.00 | 4 | 44.00 | 2.00 | 4.76 | 864.19 | 6.49 | 56.08 | 94.91 | 980.00 | 925.00 | 55.00 | 149.91 |
| 3.00 | 4.00 | 3 | 3 | 370 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 80.96 | 1.80 | 1.46 | 56.29 | 980.00 | 941.00 | 39.00 | 95.29 |
| 4.00 | 5.00 | 4 | 7 | 370 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 420.05 | 3.81 | 16.00 | 54.83 | 980.00 | 940.00 | 40.00 | 94.83 |
| 5.00 | 8.00 | 7 | 31 | 370 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 409.30 | 2.08 | 8.52 | 38.83 | 980.00 | 941.00 | 39.00 | 77.83 |
| 6.00 | 7.00 | 3 | 3 | 370 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 80.70 | 1.80 | 1.45 | 48.66 | 980.00 | 941.00 | 39.00 | 87.66 |
| 7.00 | 8.00 | 5 | 8 | 370 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 443.75 | 3.81 | 16.90 | 47.21 | 980.00 | 941.00 | 39.00 | 86.21 |
| 8.00 | 8.00 | 3 | 42 | 370 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 1,456.22 | 2.08 | 30.31 | 30.31 | 980.00 | 947.00 | 33.00 | 63.31 |

| Zone Number | Connects to Zone | Accumulated Total of Pumps this Zone | Pipe Size (inches) | Gallons per 100 lineal feet | Length of Zone | Capacity of Zone | Capacity of Zone Average Daily Flow | | Average Retention Time (Hr) | Accumulated Retention Time (Hr) | |
|---|---------------------|--|--------------------|--------------------------------|----------------|------------------|-------------------------------------|-------|--------------------------------|------------------------------------|--|
| This spreadsheet was calculated using pipe diameters for: SDR11HDPE | | | | | | | | | er Dwelling | 370 | |
| 1.00 | 2.00 | 3 | 2.00 | 15.40 | 145.14 | 22.36 | 1,110 | 49.65 | 0.48 | 2.03 | |
| 2.00 | 5.00 | 17 | 2.00 | 15.40 | 864.19 | 133.11 | 6,290 | 47.25 | 0.51 | 1.55 | |
| 3.00 | 4.00 | 3 | 2.00 | 15.40 | 80.96 | 12.47 | 1,110 | 89.01 | 0.27 | 1.91 | |
| 4.00 | 5.00 | 7 | 2.00 | 15.40 | 420.05 | 64.70 | 2,590 | 40.03 | 0.60 | 1.64 | |
| 5.00 | 8.00 | 31 | 3.00 | 33.47 | 409.30 | 136.98 | 11,470 | 83.74 | 0.29 | 1.04 | |
| 6.00 | 7.00 | 3 | 2.00 | 15.40 | 80.70 | 12.43 | 1,110 | 89.30 | 0.27 | 1.58 | |
| 7.00 | 8.00 | 8 | 2.00 | 15.40 | 443.75 | 68.35 | 2,960 | 43.31 | 0.55 | 1.31 | |
| 8.00 | 8.00 | 42 | 3.00 | 33.47 | 1,456.22 | 487.35 | 15,540 | 31.89 | 0.75 | 0.75 | |

Exhibit F

Sanitary Sewer Tributary Area Map

| Cor Eng Ser 168 Indepem Pho Surveyo Missouri St Kan PE kris@ | Stru gined ViCe, 310 E. 40 H idence, Mis ons Engine ate Certific 20010018 sas Busine 2 - 834 L engineerin Preparec Carl H BAYBEF SUMMIT | <i>ection</i> <i>ering</i> <i>s, Inc.</i> Highway ssouri 64055 78-2323 ers Planners cate of Authority 357 ss Entity S - 136 ngkc.com |
|--|---|---|
| REV. NO. 1 2 3 4 5 6 7 8 9 10 11 12 | DAT | E BY |
| Vertica Date: 2 Designo | 1 Scale -27-18 ed: KN | N/A B |
| Exhibit A | Sanitary Sewer Area | Woodland Oaks |
| Lee Bod Lee Bod Lee Bod Lee Bod | enheimer, nheimer, denheime lenheime | °, MO LS 2114 MO PE 018496 er, KS LS 638 r, KS PE 8731 |

| | Woodland Oaks - Sanitary Sewer Capacity Analysis: City of Lee's Summit Criteria at Ultimate Buildout | | | | | | | | | | | | | | | |
|-----------|--|-----------|-------|-----------|--------|--------|--------|---------|------|----------|-------|----------|-----------|---------|-----------|-----------|
| | | U.S. Str. | Cum. | | | | | | | | | | Segment | | Surcharge | |
| D.S. Str. | U.S. Str. | Area | Area | Peak Flow | FL IN | FL OUT | Length | Slope | Dia | Material | n | Capacity | Condition | Rim El. | Depth | U.S. Str. |
| | | (ac.) | (ac.) | (cfs) | | | (ft) | (ft/ft) | (ft) | | | (cfs) | | | (ft) | |
| 26-002PS | 26-166 | 0.01 | 57.98 | 1.625 | 902 | 902.9 | 7.37 | 0.1221 | 0.67 | PVC | 0.014 | 3.948 | GRAVITY | 916.07 | 0.00 | 26-166 |
| 26-166 | 26-167 | 35.91 | 57.97 | 1.624 | 903 | 903.96 | 14.36 | 0.0669 | 0.67 | PVC | 0.014 | 2.921 | GRAVITY | 916.68 | 0.00 | 26-167 |
| 26-167 | 26-178 | 1.24 | 22.06 | 0.794 | 904.04 | 915.01 | 251.41 | 0.0436 | 0.67 | PVC | 0.014 | 2.360 | GRAVITY | 923.31 | 0.00 | 26-178 |
| 26-178 | 26-179 | 1.53 | 20.82 | 0.762 | 915.21 | 918.62 | 302.68 | 0.0113 | 0.67 | PVC | 0.014 | 1.199 | GRAVITY | 929.47 | 0.00 | 26-179 |
| 26-179 | 26-180 | 0.45 | 19.29 | 0.722 | 918.72 | 920.71 | 385.5 | 0.0052 | 0.67 | PVC | 0.014 | 0.812 | GRAVITY | 942.37 | 0.00 | 26-180 |
| 26-180 | 26-181 | 1.30 | 18.84 | 0.710 | 920.81 | 921.80 | 144.69 | 0.0068 | 0.67 | DIP | 0.015 | 0.872 | GRAVITY | 944.90 | 0.00 | 26-181 |
| 26-181 | 26-182 | 3.75 | 17.54 | 0.675 | 921.95 | 922.96 | 133 | 0.0076 | 0.67 | DIP | 0.015 | 0.919 | GRAVITY | 947.08 | 0.00 | 26-182 |
| 26-182 | 26-183 | 0 | 13.79 | 0.573 | 923.04 | 923.64 | 92.09 | 0.0065 | 0.67 | DIP | 0.015 | 0.851 | GRAVITY | 945.64 | 0.00 | 26-183 |
| 26-183 | 26-184 | 0 | 13.79 | 0.573 | 923.79 | 926.03 | 330.76 | 0.0068 | 0.67 | PVC | 0.014 | 0.930 | GRAVITY | 933.94 | 0.00 | 26-184 |
| 26-184 | 26-185 | 2.36 | 13.79 | 0.573 | 926.18 | 927.29 | 87.96 | 0.0126 | 0.67 | PVC | 0.014 | 1.269 | GRAVITY | 935.49 | 0.00 | 26-185 |
| 26-185 | 26-186 | 1.52 | 11.43 | 0.507 | 927.39 | 929.99 | 149.14 | 0.0174 | 0.67 | PVC | 0.014 | 1.492 | GRAVITY | 936.19 | 0.00 | 26-186 |
| 26-186 | 26-187 | 0 | 9.91 | 0.463 | 930.17 | 938.26 | 221.61 | 0.0365 | 0.67 | PVC | 0.014 | 2.159 | GRAVITY | 951.11 | 0.00 | 26-187 |
| 26-187 | 26-188 | 3.44 | 9.91 | 0.463 | 938.55 | 938.87 | 42.27 | 0.0076 | 0.67 | PVC | 0.014 | 0.983 | GRAVITY | 950.62 | 0.00 | 26-188 |
| 26-188 | 26-200 | 0.25 | 6.47 | 0.362 | 938.92 | 939.68 | 80.32 | 0.0095 | 0.67 | PVC | 0.014 | 1.099 | GRAVITY | 949.80 | 0.00 | 26-200 |
| 26-200 | 26-299 | 2.43 | 6.22 | 0.355 | 939.78 | 948.75 | 130.58 | 0.0687 | 0.67 | DIP | 0.015 | 2.764 | GRAVITY | 963.48 | 0.00 | 26-299 |
| 26-299 | 26-300 | 0.28 | 3.79 | 0.284 | 950.15 | 951.9 | 103.01 | 0.0170 | 0.67 | PVC | 0.014 | 1.473 | GRAVITY | 965.37 | 0.00 | 26-300 |
| 26-300 | 26-301 | 0.57 | 3.51 | 0.275 | 952.9 | 957.6 | 94.87 | 0.0495 | 0.67 | PVC | 0.014 | 2.515 | GRAVITY | 969.22 | 0.00 | 26-301 |
| 26-301 | 26-302 | 0.44 | 2.94 | 0.257 | 959.6 | 962.94 | 134.21 | 0.0249 | 0.67 | PVC | 0.014 | 1.782 | GRAVITY | 975.33 | 0.00 | 26-302 |
| 26-302 | 26-303 | 1.15 | 2.5 | 0.242 | 963.14 | 964.36 | 126.94 | 0.0096 | 0.67 | PVC | 0.014 | 1.108 | GRAVITY | 976.54 | 0.00 | 26-303 |
| 26-303 | 26-304 | 0.52 | 1.35 | 0.202 | 964.86 | 966.35 | 179.26 | 0.0083 | 0.67 | PVC | 0.014 | 1.030 | GRAVITY | 978.90 | 0.00 | 26-304 |
| 26-304 | 26-305 | 0.83 | 0.83 | 0.182 | 966.55 | 967.72 | 117.28 | 0.0100 | 0.67 | PVC | 0.014 | 1.128 | GRAVITY | 979.94 | 0.00 | 26-305 |

*U.S. Str. Areas in bold account for additional upstream branch flow.

**Woodland Oaks Peak Flow = 66 GPM

0.147 cfs

was added to Peak Flow at 26-305 and carried to Structure 26-002PS