

Final Stormwater Management Plan

Market Street Center

M291 and SW Market Street
Lee's Summit, Missouri

Prepared by:



PLANNING
ENGINEERING
IMPLEMENTATION

PHELPS ENGINEERING, INC

1270 N. Winchester
Olathe, Kansas 66061
(913) 393-1155
Fax (913) 393-1166
www.phelpsengineering.com

Developer: Foresight Real Estate Services, LLC
105 N. Stewart Ct, Suite 225
Liberty, MO 64068

PEI #210639
February 4, 2022

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- WQV 40 Hour Drawdown Calculation
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1. INTRODUCTION

This report is a final stormwater management plan for the proposed Market Street Center development prepared by Phelps Engineering, Inc.

The proposed site is bounded by SW Market Street to the north, Missouri Highway 291 to the east, an existing commercial development to the west, and an existing commercial development to the south. The proposed development is approximately 5.03 acres and consists of 1 commercial building and parking lot. The existing site consists of undeveloped open space.

The property lies within Zone X, defined as areas determined to be outside the 0.2% annual chance floodplain, as shown on the flood insurance rate map prepared by the Federal Emergency Management Agency for the City of Lee's Summit, Community No. 290172, Jackson County, Missouri, Map No. 29095C0291G, and dated January 20, 2017.

See the Vicinity Map below.



2. STORMWATER REQUIREMENTS

Stormwater design criteria are in accordance with City of Lee's, Missouri Technical Specifications and Design Criteria.

Stormwater detention and BMPs shall be provided per APWA 5608.4.C.1, comprehensive control measures, as follows:

1. Post-development peak discharge rates from the site shall not exceed those indicated below:

- 50% storm peak rate less than or equal to 0.5 cfs per site acre
- 10% storm peak rate less than or equal to 2.0 cfs per site acre
- 1% storm peak rate less than or equal to 3.0 cfs per site acre

The calculated allowable release rates are:

- 50% storm (2-year) - $0.5 \text{ cfs} \times 5.03 \text{ acres} = 2.51 \text{ cfs}$
- 10% storm (10-year) - $2.0 \text{ cfs} \times 5.03 \text{ acres} = 10.06 \text{ cfs}$
- 1% storm (100-year) - $3.0 \text{ cfs} \times 5.03 \text{ acres} = 15.09 \text{ cfs}$

2. 40-hour extended detention of runoff from the local 90% mean annual event (1.37"/24-hour rainfall).

3. SITE SOIL CONDITIONS

Soils data for the property was determined using the NRCS Web Soil Survey for Jackson County. The property consists of Arisburg-Urban land complex, Udarents-Urban land-Sampsel complex, Arisburg silt loam, and Sampsel silty clay loam, which designates the site as Type C Hydrologic Soil Group (HSG). The site watershed soil properties and the Existing Drainage Map can be found in Appendix A of this report.

4. EXISTING CONDITIONS

The existing property consists of undeveloped open space. The property surface drains southeasterly to an existing 12" culver which discharges to the MODOT right of way ditch.

There are 3 point discharges from off-site drainage areas that will be routed through the site. See the off-site drainage area map included in Appendix A.

#1 – An existing 48" storm sewer discharges onto the property at the northern end of the site. This discharge point consists of a portion of SW Market Street right of way drainage and a portion of the southern existing Walmart development.

#2 – An existing 12" storm sewer discharges onto the property at the western end of the site. This discharge point consists of the existing Firestone development.

#3 – An existing 36" storm sewer discharges onto the property at the southwest corner of the site. This discharge point consists of the existing commercial development west of SW Market Street.

5. PROPOSED CONDITIONS

The proposed development consists of a single proposed office building and parking lot, resulting in 0.75 acres of impervious area. A future development is planned on Lot 2. This development was assumed to consist of 1.78 acres of future impervious area and was included in this analysis.

The proposed development will capture and route stormwater via a new private underground enclosed storm sewer system. Stormwater runoff will be routed to the proposed detention basin at the southern extent of the site. See Appendix B of this report for Proposed Drainage Map.

The proposed detention basin has a bottom elevation of 995.50 and a top of berm elevation of 1004.00. The basin consists of a 4'x4' outlet control structure with a 1.5" orifice and 18" outlet pipe. The orifice was sized to drawdown the water quality volume, generated by the 5.03 acre site, over 40 hours. See the water quality drawdown calculations in Appendix B. Orifice opens are provided above the water quality volume to detain the 2-year, 10-year, and 100-year events.

The outlet pipe will discharge at the southeast corner of the property and convey stormwater to the existing MODOT ditch, matching the existing conditions. The detention basin provides a total available storage of 75,410 cubic feet which equates to approximately 15,000 CF / acre.

6. STORMWATER DETENTION RESULTS

Composite CNs were determined using SCS TR-55 methods. The SCS Type II 24 hour duration storm event was utilized for the stormwater analysis. A minimum time of concentration of 5 minutes was utilized for all drainage areas based on the size of the site. For the preliminary stormwater study, the entire site was assumed to be routed to the detention basin. There is a very small amount of surface runoff along the eastern property line that will bypass the detention basin. This area will be further analyzed with the Final Stormwater Management Study.

The proposed drainage sub-basin characteristics and composite curve numbers are shown in Table 1 below. See Appendix B of this report for the Proposed Drainage Map.

Table 1 – Proposed Runoff Conditions

Drainage Sub-Basin	Open Space (acres)	Impervious (acres)	Total (acres)	Composite CN	Time of Conc. (min)
Bypass	0.83	0.00	0.83	74	5.0
Detention	1.87	2.33	4.20	87	5.0

Using HydroCAD, the proposed 2-year, 10-year, and 100-year site peak discharge was determined with the proposed detention basin included. The proposed 100-year site peak discharge and allowable release rate is shown in Table 2 below. The proposed detention basin results are shown in Table 3 below.

See Appendix B of this report for proposed HydroCAD calculations.

Table 2 – Proposed Runoff Results

Storm Event	Allowable Release Rate (cfs)	Peak Discharge (cfs)
2-Year	2.51	2.46
10-Year	10.06	9.06
100-Year	15.09	14.98

Table 3 – Proposed Detention Basin Results

Basin	Detention Inflow (cfs)	Detention Outflow (cfs)	Maximum WSEL (ft.)	Maximum Storage (cf)
2-Year	16.61	1.70	999.20	17,018
10-Year	28.39	6.25	1,000.44	28,419
100-Year	44.00	9.11	1,001.89	44,940

7. CONCLUSION

The detention basin results in a proposed peak discharge less than the allowable release rates for the 2-year, 10-year, and 100-year storm events meeting APWA 5608.4.C.1 comprehensive control measures.

The detention basin provides an orifice opening sized to ensure 40-hour extended detention of runoff from the local 90% mean annual event (1.37"/24-hour rainfall) meeting APWA 5608.4.C.1 comprehensive control measures.

The proposed plan meets all City of Lee's Summit stormwater requirements.

This report and attached appendices complete Phelps Engineering Inc.'s submittal of the Final Stormwater Management Plan for Market Street Center. Please feel free to contact PEI at (913) 393-1155 if you require additional information.

Sincerely,

PHELPS ENGINEERING, INC.

Judd D. Claussen, P.E.

Enclosures



APPENDIX A

A. Site Conditions

- NRCS Web Soil Survey
- Existing Drainage Map



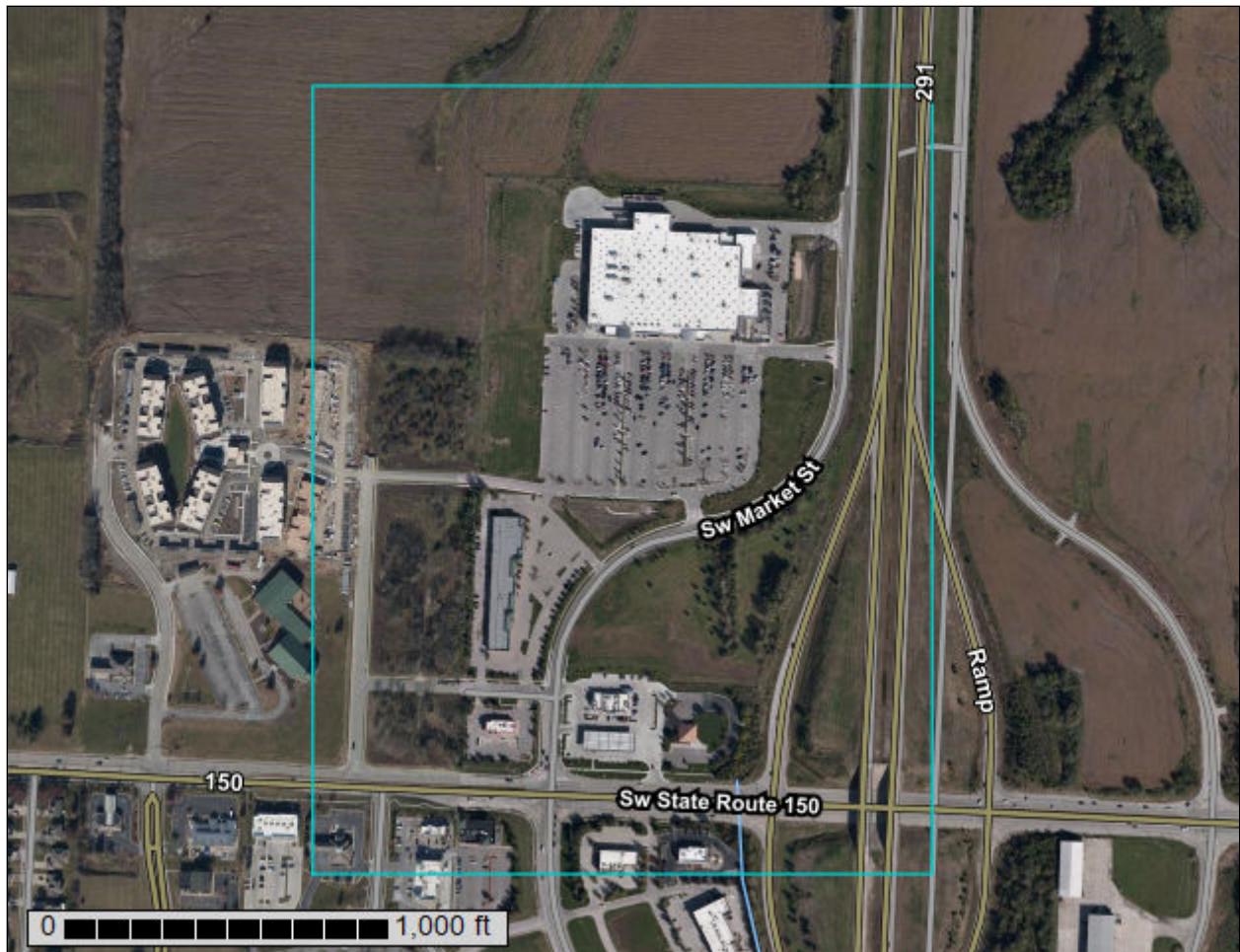
United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Jackson County, Missouri



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units).

Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

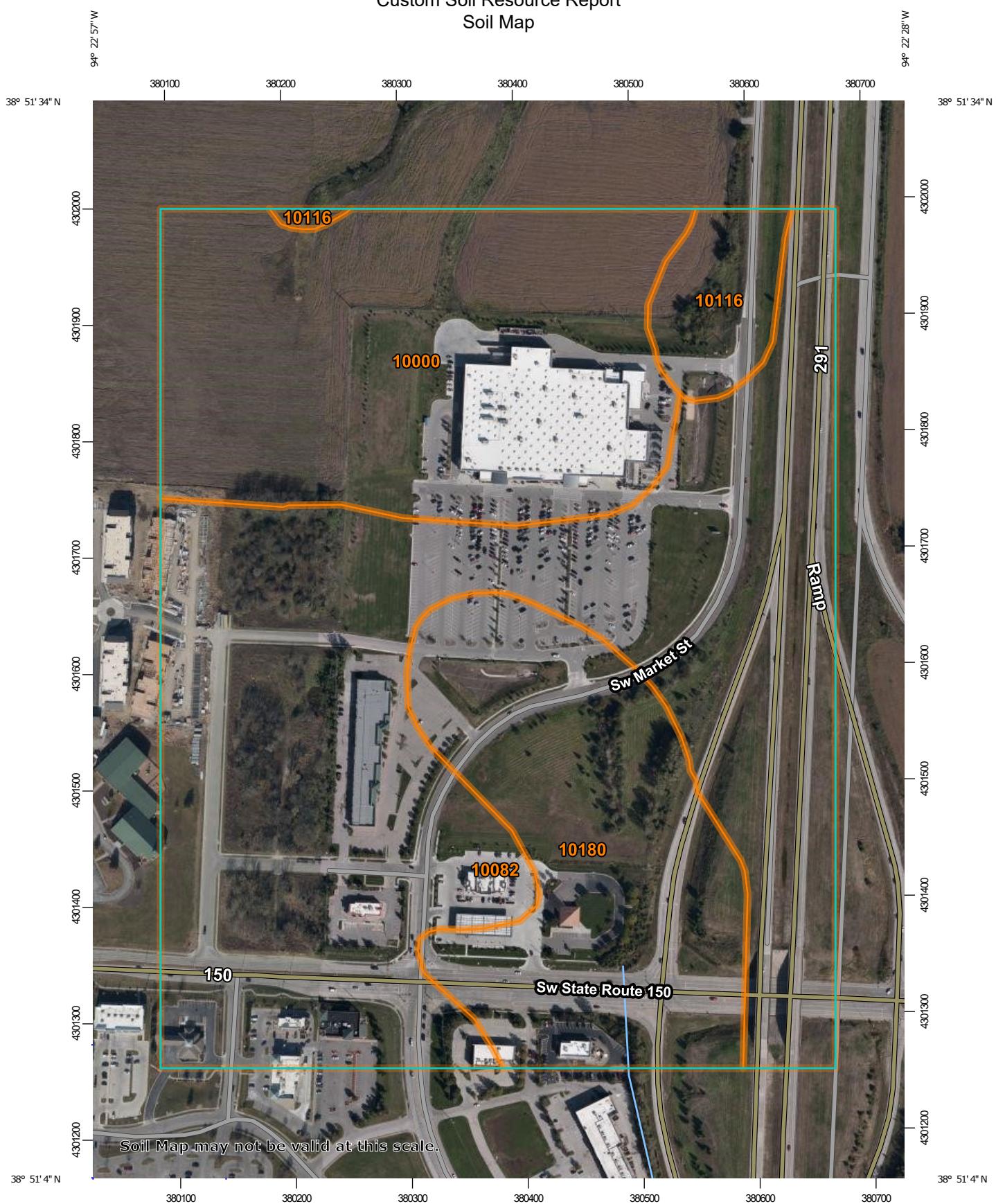
Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report
Soil Map



Map Scale: 1:4,510 if printed on A portrait (8.5" x 11") sheet.

0 50 100 200 300 Meters

0 200 400 800 1200 Feet

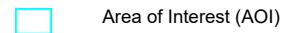
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 15N WGS84



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MAP LEGEND

Area of Interest (AOI)



Area of Interest (AOI)

Soils



Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip

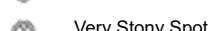


Sodic Spot

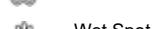
Spoil Area



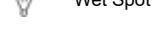
Stony Spot



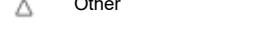
Very Stony Spot



Wet Spot

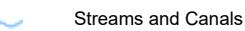


Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



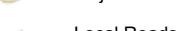
Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri

Survey Area Data: Version 23, Sep 1, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 6, 2019—Nov 16, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
10000	Arisburg silt loam, 1 to 5 percent slopes	27.9	26.2%
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	54.1	50.7%
10116	Samsel silty clay loam, 2 to 5 percent slopes	4.0	3.7%
10180	Udarents-Urban land-Samsel complex, 2 to 5 percent slopes	20.7	19.4%
Totals for Area of Interest		106.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Jackson County, Missouri

10000—Arisburg silt loam, 1 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w22b

Elevation: 610 to 1,130 feet

Mean annual precipitation: 39 to 43 inches

Mean annual air temperature: 50 to 55 degrees F

Frost-free period: 177 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Arisburg and similar soils: 87 percent

Minor components: 13 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Arisburg

Setting

Landform: Interfluviums

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam

A - 6 to 13 inches: silt loam

Bt - 13 to 19 inches: silty clay loam

Btg - 19 to 56 inches: silty clay loam

BCg - 56 to 79 inches: silty clay loam

Properties and qualities

Slope: 1 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.60 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: High (about 11.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: R107BY007MO - Loess Upland Prairie

Hydric soil rating: No

Minor Components

Sharpsburg

Percent of map unit: 5 percent
Landform: Ridges
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: R109XY002MO - Loess Upland Prairie
Hydric soil rating: No

Greentown

Percent of map unit: 5 percent
Landform: Hillslopes
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Convex
Ecological site: R109XY002MO - Loess Upland Prairie
Hydric soil rating: No

Haig

Percent of map unit: 3 percent
Landform: Flats
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Convex
Ecological site: R109XY001MO - Claypan Summit Prairie
Hydric soil rating: Yes

10082—Arisburg-Urban land complex, 1 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w7Id
Elevation: 750 to 1,130 feet
Mean annual precipitation: 39 to 45 inches
Mean annual air temperature: 50 to 55 degrees F
Frost-free period: 177 to 220 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Arisburg and similar soils: 61 percent
Urban land: 30 percent
Minor components: 9 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Arisburg

Setting

Landform: Interfluves
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluvial
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam
A - 6 to 13 inches: silt loam
Bt - 13 to 19 inches: silty clay loam
Btg - 19 to 56 inches: silty clay loam
BCg - 56 to 79 inches: silty clay loam

Properties and qualities

Slope: 1 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.60 in/hr)
Depth to water table: About 18 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 11.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Ecological site: R107BY007MO - Loess Upland Prairie
Hydric soil rating: No

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 8
Hydric soil rating: No

Minor Components

Sampsel

Percent of map unit: 3 percent
Landform: Hills
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Concave
Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna
Hydric soil rating: Yes

Greenton

Percent of map unit: 3 percent

Custom Soil Resource Report

Landform: Hillslopes

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Side slope

Down-slope shape: Convex

Across-slope shape: Convex

Ecological site: R109XY002MO - Loess Upland Prairie

Hydric soil rating: No

Sharpsburg

Percent of map unit: 3 percent

Landform: Ridges

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Interfluvium

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: R109XY002MO - Loess Upland Prairie

Hydric soil rating: No

10116—Sampsel silty clay loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2qkzy

Elevation: 600 to 900 feet

Mean annual precipitation: 33 to 41 inches

Mean annual air temperature: 50 to 55 degrees F

Frost-free period: 177 to 220 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Sampsel and similar soils: 95 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Sampsel

Setting

Landform: Hillslopes

Landform position (two-dimensional): Foothillslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave

Across-slope shape: Convex, concave

Parent material: Residuum weathered from shale

Typical profile

Ap - 0 to 11 inches: silty clay loam

Bt - 11 to 80 inches: silty clay

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C/D
Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna
Other vegetative classification: Grass/Prairie (Herbaceous Vegetation)
Hydric soil rating: No

10180—Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1n85h
Elevation: 600 to 900 feet
Mean annual precipitation: 33 to 43 inches
Mean annual air temperature: 50 to 57 degrees F
Frost-free period: 175 to 220 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Udarents and similar soils: 41 percent
Urban land: 39 percent
Sampsel and similar soils: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udarents

Setting

Landform position (two-dimensional): Summit
Landform position (three-dimensional): Crest
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Mine spoil or earthy fill

Typical profile

C1 - 0 to 5 inches: silt loam
C2 - 5 to 80 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very high

Custom Soil Resource Report

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.14 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: R107BY002MO - Deep Loess Upland Prairie

Other vegetative classification: Mixed/Transitional (Mixed Native Vegetation)

Hydric soil rating: No

Description of Urban Land

Setting

Landform: Interfluviums

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Interfluve

Across-slope shape: Convex

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Description of Sampsel

Setting

Landform: Hillslopes

Landform position (two-dimensional): Foothillslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave

Across-slope shape: Convex

Parent material: Residuum weathered from shale

Typical profile

Ap - 0 to 13 inches: silty clay loam

Bt - 13 to 80 inches: silty clay

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 0 to 18 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Custom Soil Resource Report

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C/D

Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna

Other vegetative classification: Grass/Prairie (Herbaceous Vegetation)

Hydric soil rating: No

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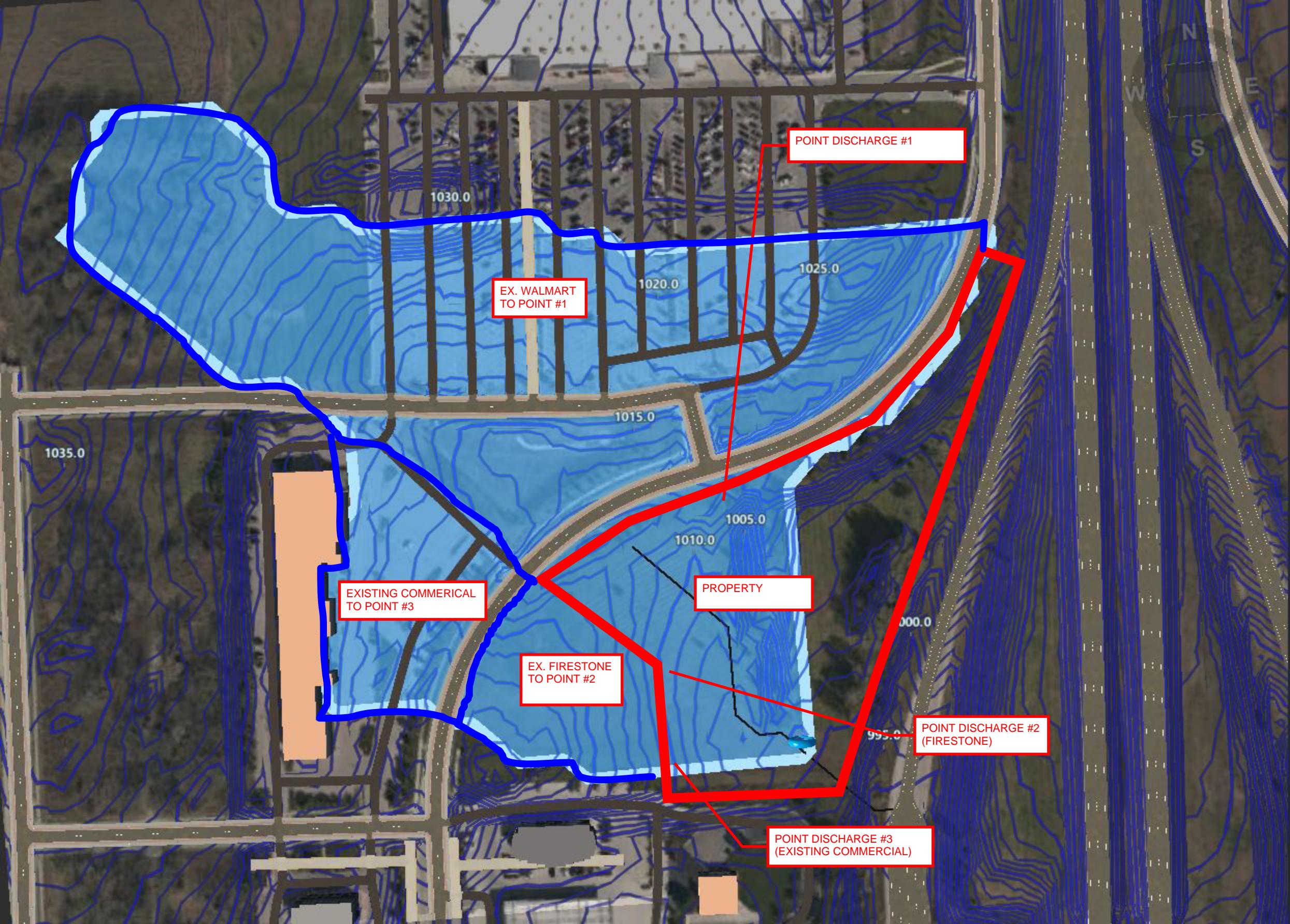
Custom Soil Resource Report

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Type	Manual Style
Geometry	Watershed/Blue
Area	737866.06 sq.ft.
Channel Length	442.59 '
Channel Slope	1.55 %
Elevations (High/Low)	1011.89'/1005.05'
Hydrology Data	User Defined
Hydrology Method	
Peak Flow (AEP)	
1/10	0.0 cfs
1/50	0.0 cfs
1/100	0.0 cfs



APPENDIX B

B. Detention & BMPs

- Proposed Drainage Map
- Proposed Detention Basin Details
- WQV 40 Hour Drawdown Calculation
- Proposed HydroCAD Model



Olathe, Kansas 66061
(913) 393-1155
Fax (913) 393-1166
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M291 AND SW MARKET STREET
CITY OF LEE'S SUMMIT, JACKSON COUNTY, MISSOURI



EXTENDED DRY DETENTION BASIN

TREATMENT AREA=9.43 ACRES

% IMPERVIOUS=25.87%

LEADER QUALITY VOLUME ELEM - 000-07

BOTTOM OF BASIN=980.00
TOP OF BERM=987.00

LEGEND

- EXISTING MINOR CONTOUR
 - EXISTING MAJOR CONTOUR
 - PROPOSED MINOR CONTOUR
 - PROPOSED MAJOR CONTOUR
 - 100-YEAR WSE
 - EMERGENCY SPILLWAY
 - PROPOSED STORM PIPE

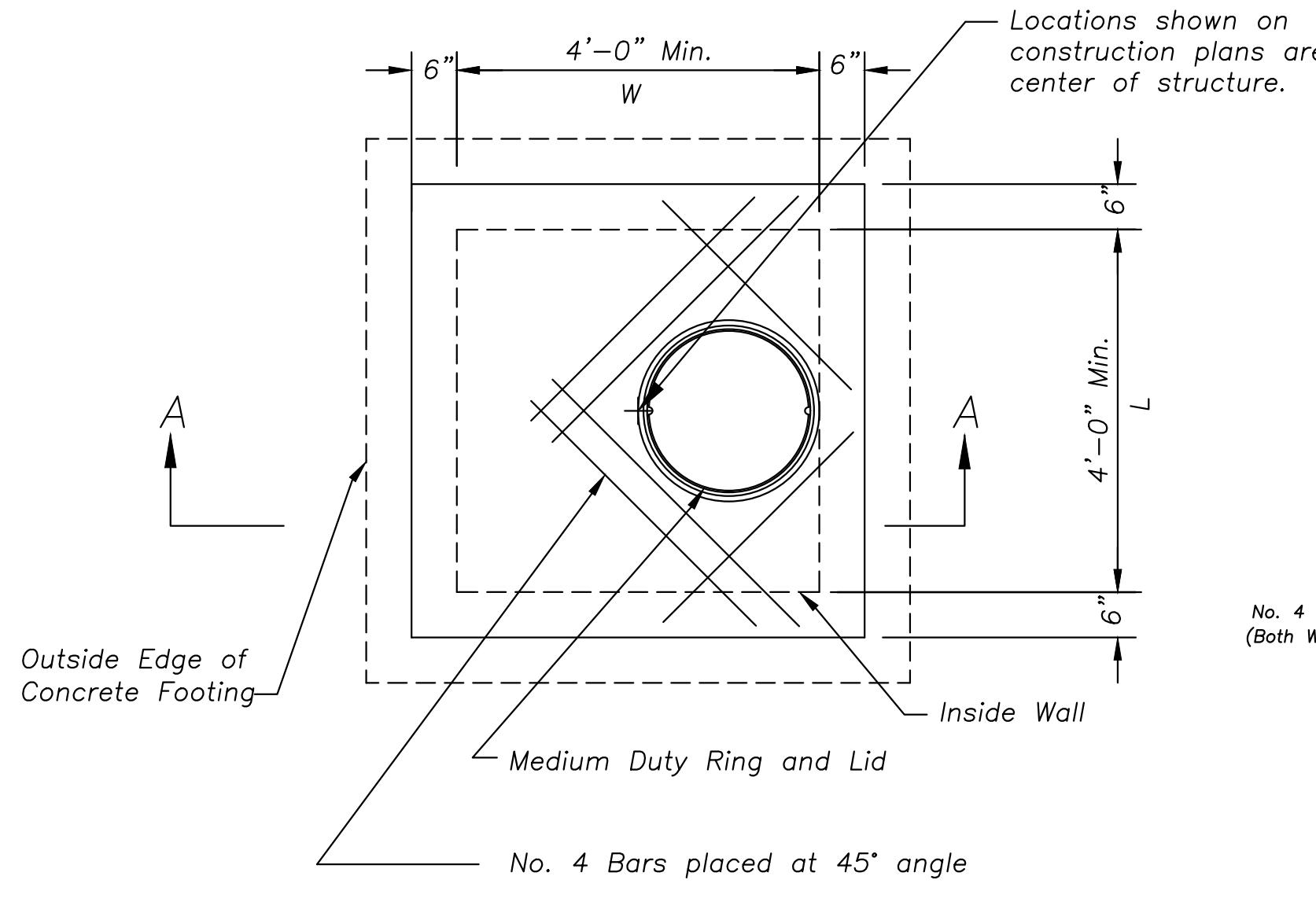
20 YEAR OVERFLOW

100-YEAR OVERFLOW
10-Year Inflow $Q_{100} = 44.00 \text{ CFS}$
10-Year WSE = 1002.0'

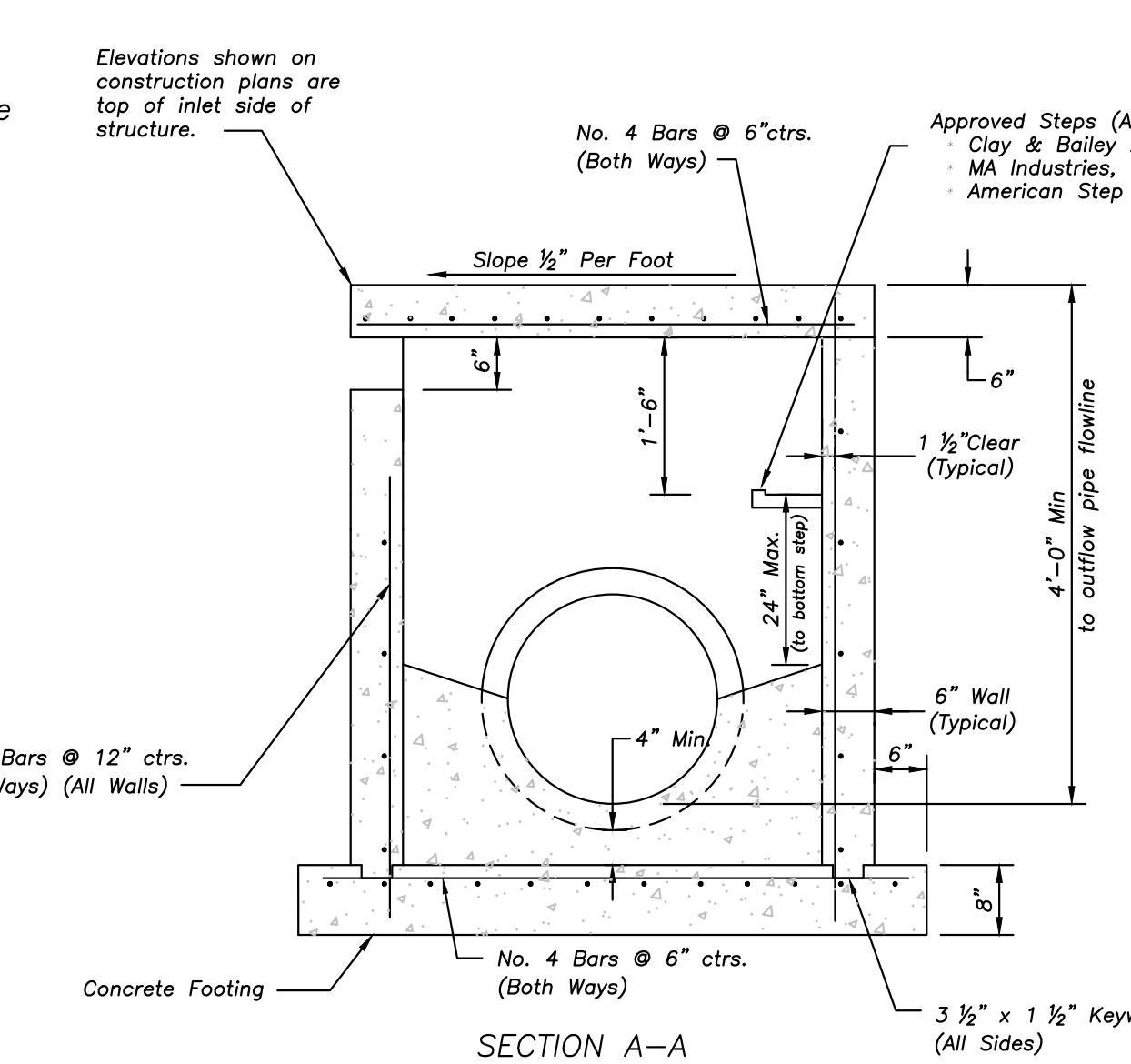
Emergency Spillway Elevation = 1002.5'
Emergency Spillway Width = 40'

$$0\text{-Year Emergency Spillway Flow Depth, } H = 0.5' \text{ (1003.0')} \\ = CLH^{1.5} \quad 44.00 = (3.1)(40)(H)^{1.5}$$

Retention Basin Berm Elevation = 1004.0'



Plan



OUTLET CONTROL DETAIL

SCALE: M

Outlet Control Structure Notes

Gen

1. All storm sewer structures shall be pre-cast or poured in place. If pre-cast structures are used for publicly financed, maintained or administered construction, the tops shall be poured in place and the wall steel shall be left exposed to a height 2" below the finish top elevation, or as directed by the City Engineer.
 2. Pre-cast shop drawings are to be approved by the City Engineer for publicly financed or administered projects. Pre-cast shop drawings for privately financed projects are to be submitted to the Engineering Services Division of the Planning and Development Services Department.
 3. Do not scale these drawings for dimensions or clearances. Any questions regarding dimensions shall be brought to the attention of the City Engineer prior to construction.
 4. The first dimension listed in the construction notes is the "L" dimension. The second dimension is the "W" dimension. The concrete thickness and reinforcement shown is for boxes with ("L"+"H") and ("W"+"H") less than or equal to 20. For boxes with either of these calculations greater than 20, a special design is required.

C

5. Concrete used in this work shall be KCMMB4K, as approved by the Kansas City Metropolitan Materials Board, and shall meet the requirements of the **Lee's Summit** Municipal Code.
 6. Concrete construction shall meet the applicable requirements of Standard Specifications for State Road and Bridge Construction, Kansas Department of Transportation, latest edition, except as modified in the **Lee's Summit** Municipal Code.
 7. Inlet floors shall be shaped with non-reinforced concrete inverts to provide smooth flow.
 8. Bevel all exposed edges with $\frac{3}{4}$ " triangular molding.

Reinforcing Steel

 9. Reinforcing steel shall be new billet, minimum Grade 60 as per ASTM A615, and shall be bent cold.
 10. All dimensions relative to reinforcing steel are to centerline of bars. 2" clearance shall be provided throughout unless noted otherwise. Tolerance of $+/- \frac{1}{8}$ " shall be permitted.
 11. All lap splices not shown shall be a minimum of 40 bar diameters in length.
 12. All reinforcing steel shall be supported on fabricated steel bar supports @ 3'-0" maximum spacing.
 13. All dowels shall be accurately placed and securely tied in place prior to placement of bottom slab concrete. Sticking of dowels into fresh or partially hardened concrete will not be acceptable.

Construction

 14. The bottom slab shall be at least 24 hours old before placing sidewall concrete. All sidewall forms shall remain in place a minimum of 24 hours after sidewalls are poured before removal, and after removal shall be immediately treated with membrane curing compound.
 15. Pipe connections to pre-cast structures shall have a minimum of 6" of concrete around the entire pipe within 2' of the structure.
 16. Material selection and compaction requirements for backfill around structures shall be as specified in the Manual of Infrastructure Standards, as promulgated by the City Engineer.

Design Procedure Form: WQV 40 Hour Drawdown Calculations
Main Worksheet

Designer: DAF
 Checked By: JDC
 Company: Phelps Engineering, Inc
 Date: 2/4/2022
 Project: 291 and Market Street
 Location: Lee's Summit MO

I. Basin Water Quality Volume

Step 1) Tributary area to EDW, A_T (ac) A_T (ac) = 4.20

Step 2) Calculate WQv using methodology in Section 6 WQv (ac-ft) = 0.26
 WQv (cf) = 11,473

IIa. Water Quality Outlet Type

Step 1) Set water quality outlet type:
 Type 1 = single orifice Outlet Type = 1
 Type 2 = perforated riser or plate
 Type 3 = v-notch weir

Vb. Water Quality Pool Outlet, Single Orifice

Step 1) Depth of water quality volume above permanent pool, Z_{WQ} (ft) Z_{WQ} (ft) = 3

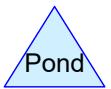
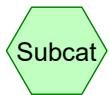
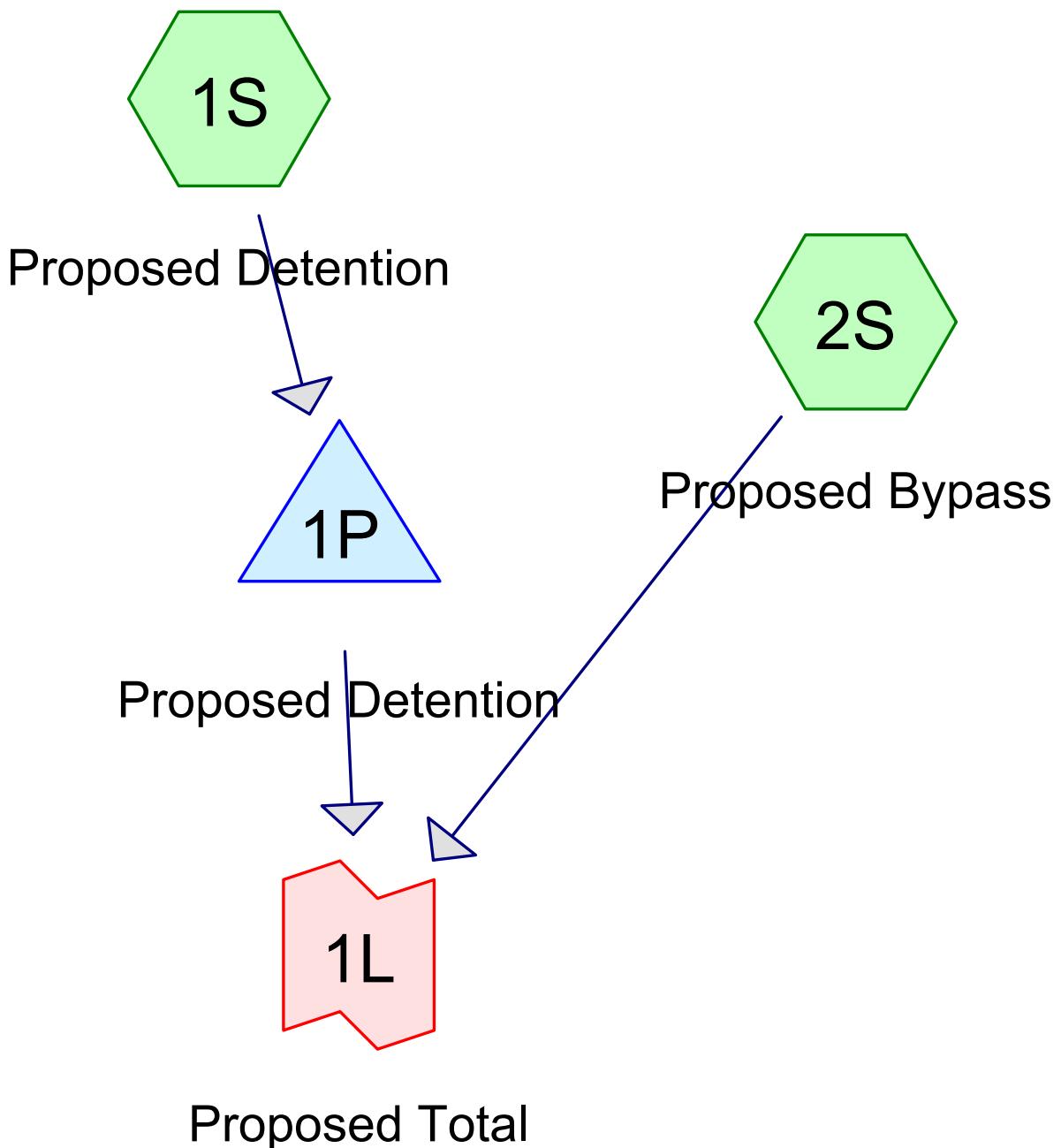
Step 2) Average head of water quality volume over invert of orifice, H_{WQ} (ft)
 $H_{WQ} = 0.5 * Z_{WQ}$ H_{WQ} (ft) = 1.5

Step 3) Average water quality outflow rate, Q_{WQ} (cfs)
 $Q_{WQ} = (WQv * 43,560)/(40 * 3,600)$ Q_{WQ} (cfs) = 0.08

Step 4) Set value of orifice discharge coefficient, C_o
 $C_o = 0.66$ when thickness of riser/weir plate is = or < orifice diameter
 $C_o = 0.80$ when thickness of riser/weir plate is > orifice diameter C_o = 0.66

Step 5) Water quality outlet orifice diameter (minimum of 4 inches), D_o (in)
 $D_o = 12 * 2 * (Q_{WQ}/(C_o * \pi * (2 * g * H)^{0.5}))^{0.5}$ D_o (in) = 1.50
 (If orifice diameter < 4 inches, use outlet type 2 or 3) 1.5"

Step 6) To size outlet orifice for EDW with an irregular stage-volume relationship, use the Single Orifice Worksheet



Routing Diagram for Proposed

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Proposed

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Page 2

Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	Jackson - 10 YR	Type II 24-hr		Default	24.00	1	5.30	2
2	Jackson - 100 YR	Type II 24-hr		Default	24.00	1	7.70	2
3	Jackson - 2 YR	Type II 24-hr		Default	24.00	1	3.50	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.700	74	>75% Grass cover, Good, HSG C (1S, 2S)
2.330	98	Paved parking, HSG C (1S)
5.030	85	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
5.030	HSG C	1S, 2S
0.000	HSG D	
0.000	Other	
5.030		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.700	0.000	0.000	2.700	>75% Grass cover, Good	1S, 2S
0.000	0.000	2.330	0.000	0.000	2.330	Paved parking	1S
0.000	0.000	5.030	0.000	0.000	5.030	TOTAL AREA	

Proposed

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)
1	1P	995.50	995.00	48.3	0.0104	0.013	0.0	18.0	0.0

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Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Proposed DetentionRunoff Area=4.200 ac 55.48% Impervious Runoff Depth=3.85"
Tc=5.0 min CN=87 Runoff=28.39 cfs 1.348 af**Subcatchment 2S: Proposed Bypass**Runoff Area=0.830 ac 0.00% Impervious Runoff Depth=2.61"
Tc=5.0 min CN=74 Runoff=4.01 cfs 0.180 af**Pond 1P: Proposed Detention**Peak Elev=1,000.44' Storage=28,419 cf Inflow=28.39 cfs 1.348 af
Outflow=6.25 cfs 1.244 af**Link 1L: Proposed Total**Inflow=9.06 cfs 1.424 af
Primary=9.06 cfs 1.424 af**Total Runoff Area = 5.030 ac Runoff Volume = 1.528 af Average Runoff Depth = 3.65"**
53.68% Pervious = 2.700 ac 46.32% Impervious = 2.330 ac

Proposed

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Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Summary for Subcatchment 1S: Proposed Detention

Runoff = 28.39 cfs @ 11.96 hrs, Volume= 1.348 af, Depth= 3.85"
 Routed to Pond 1P : Proposed Detention

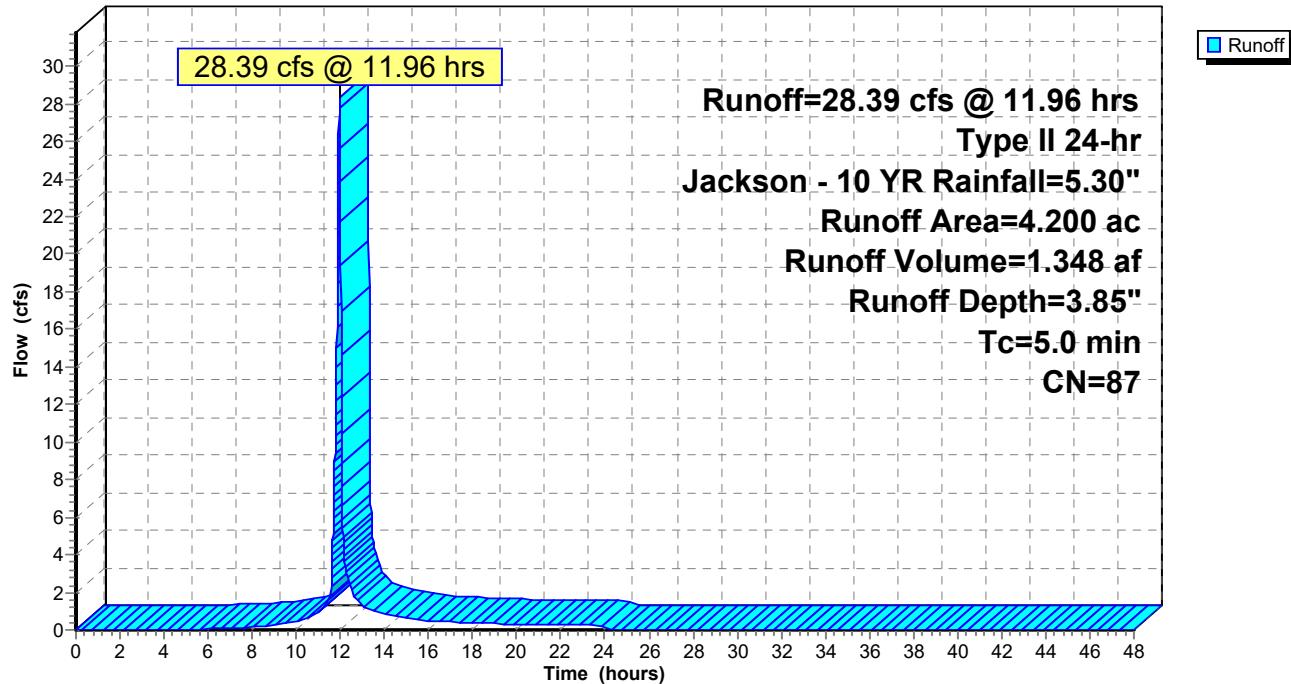
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
 Type II 24-hr Jackson - 10 YR Rainfall=5.30"

Area (ac)	CN	Description
1.870	74	>75% Grass cover, Good, HSG C
2.330	98	Paved parking, HSG C
4.200	87	Weighted Average
1.870		44.52% Pervious Area
2.330		55.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 1S: Proposed Detention

Hydrograph



Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Hydrograph for Subcatchment 1S: Proposed Detention

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	5.30	3.85	0.00
0.50	0.03	0.00	0.00	27.00	5.30	3.85	0.00
1.00	0.06	0.00	0.00	27.50	5.30	3.85	0.00
1.50	0.09	0.00	0.00	28.00	5.30	3.85	0.00
2.00	0.12	0.00	0.00	28.50	5.30	3.85	0.00
2.50	0.15	0.00	0.00	29.00	5.30	3.85	0.00
3.00	0.18	0.00	0.00	29.50	5.30	3.85	0.00
3.50	0.22	0.00	0.00	30.00	5.30	3.85	0.00
4.00	0.25	0.00	0.00	30.50	5.30	3.85	0.00
4.50	0.29	0.00	0.00	31.00	5.30	3.85	0.00
5.00	0.33	0.00	0.01	31.50	5.30	3.85	0.00
5.50	0.38	0.00	0.03	32.00	5.30	3.85	0.00
6.00	0.42	0.01	0.06	32.50	5.30	3.85	0.00
6.50	0.47	0.02	0.08	33.00	5.30	3.85	0.00
7.00	0.52	0.03	0.11	33.50	5.30	3.85	0.00
7.50	0.58	0.04	0.13	34.00	5.30	3.85	0.00
8.00	0.64	0.06	0.16	34.50	5.30	3.85	0.00
8.50	0.70	0.09	0.22	35.00	5.30	3.85	0.00
9.00	0.78	0.12	0.29	35.50	5.30	3.85	0.00
9.50	0.86	0.16	0.34	36.00	5.30	3.85	0.00
10.00	0.96	0.20	0.45	36.50	5.30	3.85	0.00
10.50	1.08	0.27	0.63	37.00	5.30	3.85	0.00
11.00	1.25	0.37	0.95	37.50	5.30	3.85	0.00
11.50	1.50	0.54	1.72	38.00	5.30	3.85	0.00
12.00	3.51	2.19	23.82	38.50	5.30	3.85	0.00
12.50	3.90	2.54	2.14	39.00	5.30	3.85	0.00
13.00	4.09	2.72	1.34	39.50	5.30	3.85	0.00
13.50	4.23	2.85	1.02	40.00	5.30	3.85	0.00
14.00	4.35	2.96	0.80	40.50	5.30	3.85	0.00
14.50	4.44	3.04	0.71	41.00	5.30	3.85	0.00
15.00	4.52	3.12	0.64	41.50	5.30	3.85	0.00
15.50	4.60	3.19	0.57	42.00	5.30	3.85	0.00
16.00	4.66	3.25	0.49	42.50	5.30	3.85	0.00
16.50	4.72	3.31	0.46	43.00	5.30	3.85	0.00
17.00	4.78	3.36	0.44	43.50	5.30	3.85	0.00
17.50	4.83	3.41	0.41	44.00	5.30	3.85	0.00
18.00	4.88	3.46	0.38	44.50	5.30	3.85	0.00
18.50	4.93	3.50	0.36	45.00	5.30	3.85	0.00
19.00	4.97	3.54	0.33	45.50	5.30	3.85	0.00
19.50	5.01	3.58	0.31	46.00	5.30	3.85	0.00
20.00	5.05	3.61	0.28	46.50	5.30	3.85	0.00
20.50	5.08	3.64	0.27	47.00	5.30	3.85	0.00
21.00	5.11	3.67	0.27	47.50	5.30	3.85	0.00
21.50	5.15	3.70	0.26	48.00	5.30	3.85	0.00
22.00	5.18	3.74	0.26				
22.50	5.21	3.77	0.25				
23.00	5.24	3.79	0.24				
23.50	5.27	3.82	0.24				
24.00	5.30	3.85	0.23				
24.50	5.30	3.85	0.00				
25.00	5.30	3.85	0.00				
25.50	5.30	3.85	0.00				
26.00	5.30	3.85	0.00				

Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Summary for Subcatchment 2S: Proposed Bypass

Runoff = 4.01 cfs @ 11.96 hrs, Volume= 0.180 af, Depth= 2.61"
Routed to Link 1L : Proposed Total

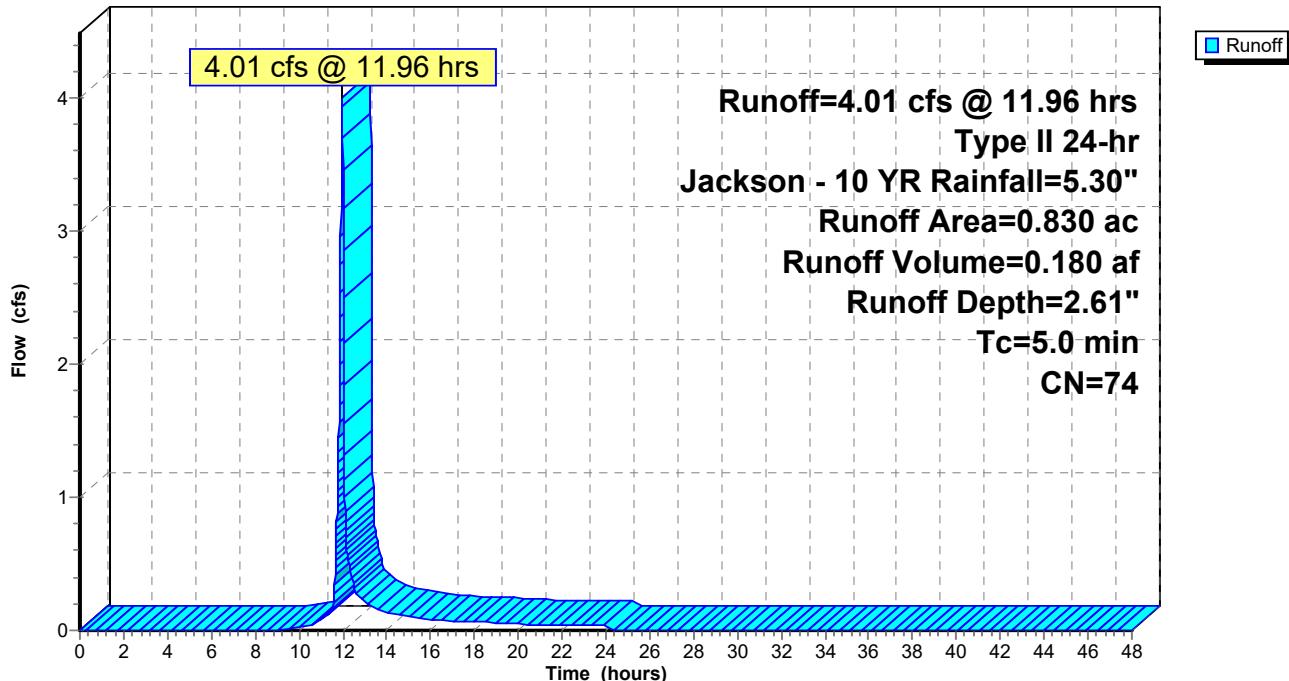
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
Type II 24-hr Jackson - 10 YR Rainfall=5.30"

Area (ac)	CN	Description
0.830	74	>75% Grass cover, Good, HSG C
0.000	98	Paved parking, HSG C
0.830	74	Weighted Average
0.830		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	Direct Entry,				

Subcatchment 2S: Proposed Bypass

Hydrograph



Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Hydrograph for Subcatchment 2S: Proposed Bypass

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	5.30	2.61	0.00
0.50	0.03	0.00	0.00	27.00	5.30	2.61	0.00
1.00	0.06	0.00	0.00	27.50	5.30	2.61	0.00
1.50	0.09	0.00	0.00	28.00	5.30	2.61	0.00
2.00	0.12	0.00	0.00	28.50	5.30	2.61	0.00
2.50	0.15	0.00	0.00	29.00	5.30	2.61	0.00
3.00	0.18	0.00	0.00	29.50	5.30	2.61	0.00
3.50	0.22	0.00	0.00	30.00	5.30	2.61	0.00
4.00	0.25	0.00	0.00	30.50	5.30	2.61	0.00
4.50	0.29	0.00	0.00	31.00	5.30	2.61	0.00
5.00	0.33	0.00	0.00	31.50	5.30	2.61	0.00
5.50	0.38	0.00	0.00	32.00	5.30	2.61	0.00
6.00	0.42	0.00	0.00	32.50	5.30	2.61	0.00
6.50	0.47	0.00	0.00	33.00	5.30	2.61	0.00
7.00	0.52	0.00	0.00	33.50	5.30	2.61	0.00
7.50	0.58	0.00	0.00	34.00	5.30	2.61	0.00
8.00	0.64	0.00	0.00	34.50	5.30	2.61	0.00
8.50	0.70	0.00	0.00	35.00	5.30	2.61	0.00
9.00	0.78	0.00	0.00	35.50	5.30	2.61	0.00
9.50	0.86	0.01	0.01	36.00	5.30	2.61	0.00
10.00	0.96	0.02	0.02	36.50	5.30	2.61	0.00
10.50	1.08	0.04	0.04	37.00	5.30	2.61	0.00
11.00	1.25	0.07	0.07	37.50	5.30	2.61	0.00
11.50	1.50	0.15	0.16	38.00	5.30	2.61	0.00
12.00	3.51	1.25	3.47	38.50	5.30	2.61	0.00
12.50	3.90	1.52	0.34	39.00	5.30	2.61	0.00
13.00	4.09	1.66	0.21	39.50	5.30	2.61	0.00
13.50	4.23	1.77	0.16	40.00	5.30	2.61	0.00
14.00	4.35	1.85	0.13	40.50	5.30	2.61	0.00
14.50	4.44	1.93	0.12	41.00	5.30	2.61	0.00
15.00	4.52	1.99	0.10	41.50	5.30	2.61	0.00
15.50	4.60	2.05	0.09	42.00	5.30	2.61	0.00
16.00	4.66	2.10	0.08	42.50	5.30	2.61	0.00
16.50	4.72	2.15	0.08	43.00	5.30	2.61	0.00
17.00	4.78	2.19	0.07	43.50	5.30	2.61	0.00
17.50	4.83	2.23	0.07	44.00	5.30	2.61	0.00
18.00	4.88	2.27	0.06	44.50	5.30	2.61	0.00
18.50	4.93	2.31	0.06	45.00	5.30	2.61	0.00
19.00	4.97	2.34	0.06	45.50	5.30	2.61	0.00
19.50	5.01	2.37	0.05	46.00	5.30	2.61	0.00
20.00	5.05	2.40	0.05	46.50	5.30	2.61	0.00
20.50	5.08	2.43	0.05	47.00	5.30	2.61	0.00
21.00	5.11	2.45	0.04	47.50	5.30	2.61	0.00
21.50	5.15	2.48	0.04	48.00	5.30	2.61	0.00
22.00	5.18	2.51	0.04				
22.50	5.21	2.53	0.04				
23.00	5.24	2.56	0.04				
23.50	5.27	2.58	0.04				
24.00	5.30	2.61	0.04				
24.50	5.30	2.61	0.00				
25.00	5.30	2.61	0.00				
25.50	5.30	2.61	0.00				
26.00	5.30	2.61	0.00				

Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Summary for Pond 1P: Proposed Detention

Inflow Area = 4.200 ac, 55.48% Impervious, Inflow Depth = 3.85" for Jackson - 10 YR event

Inflow = 28.39 cfs @ 11.96 hrs, Volume= 1.348 af

Outflow = 6.25 cfs @ 12.10 hrs, Volume= 1.244 af, Atten= 78%, Lag= 8.2 min

Primary = 6.25 cfs @ 12.10 hrs, Volume= 1.244 af

Routed to Link 1L : Proposed Total

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 1,000.44' @ 12.10 hrs Surf.Area= 10,208 sf Storage= 28,419 cf

Plug-Flow detention time= 299.5 min calculated for 1.243 af (92% of inflow)

Center-of-Mass det. time= 258.0 min (1,053.1 - 795.0)

Volume	Invert	Avail.Storage	Storage Description
#1	995.50'	75,410 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
995.50	100	0	0
996.00	1,400	375	375
997.00	4,400	2,900	3,275
1,004.00	16,210	72,135	75,410

Device	Routing	Invert	Outlet Devices
#1	Primary	995.50'	18.0" Round Culvert L= 48.3' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 995.50' / 995.00' S= 0.0104 '/' Cc= 0.900 n= 0.013, Flow Area= 1.77 sf
#2	Device 1	995.50'	1.5" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	998.50'	12.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	999.20'	15.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#5	Device 1	1,002.00'	288.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=6.25 cfs @ 12.10 hrs HW=1,000.44' (Free Discharge)

- ↑ 1=Culvert (Passes 6.25 cfs of 17.42 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.13 cfs @ 10.64 fps)
- 3=Orifice/Grate (Orifice Controls 3.13 cfs @ 6.26 fps)
- 4=Orifice/Grate (Orifice Controls 2.99 cfs @ 4.78 fps)
- 5=Orifice/Grate (Controls 0.00 cfs)

Proposed

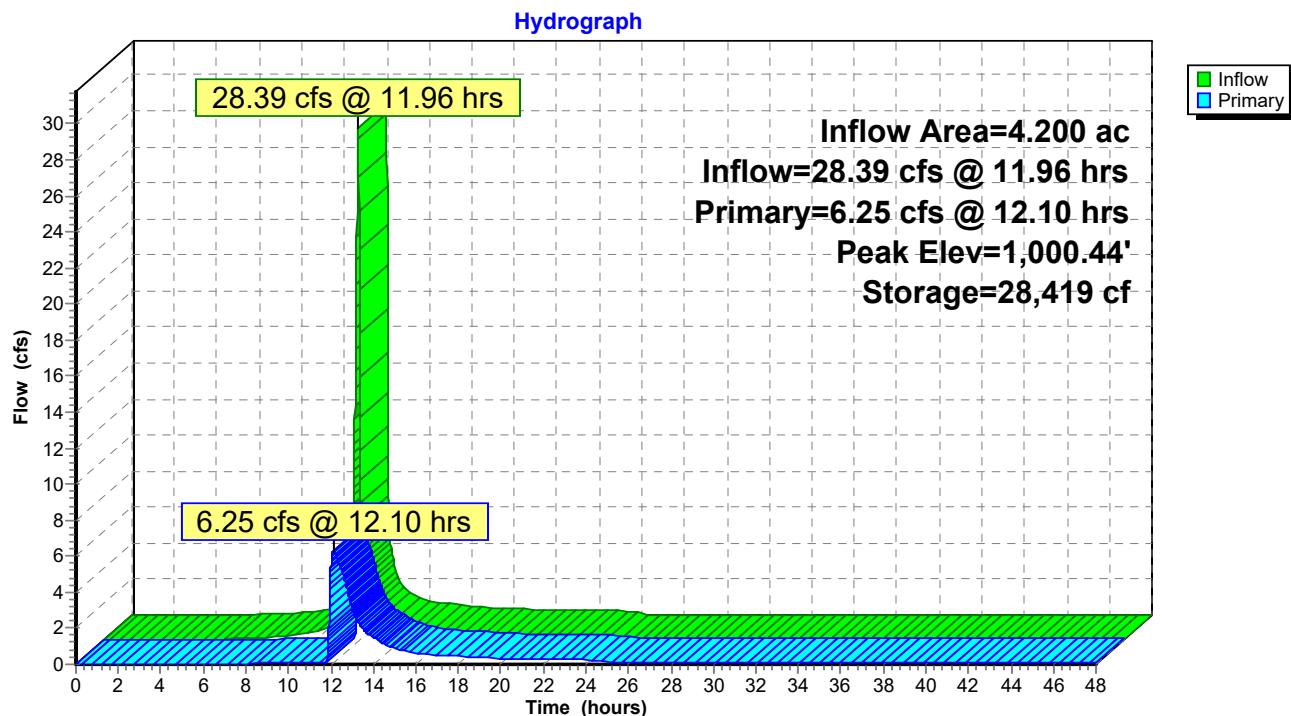
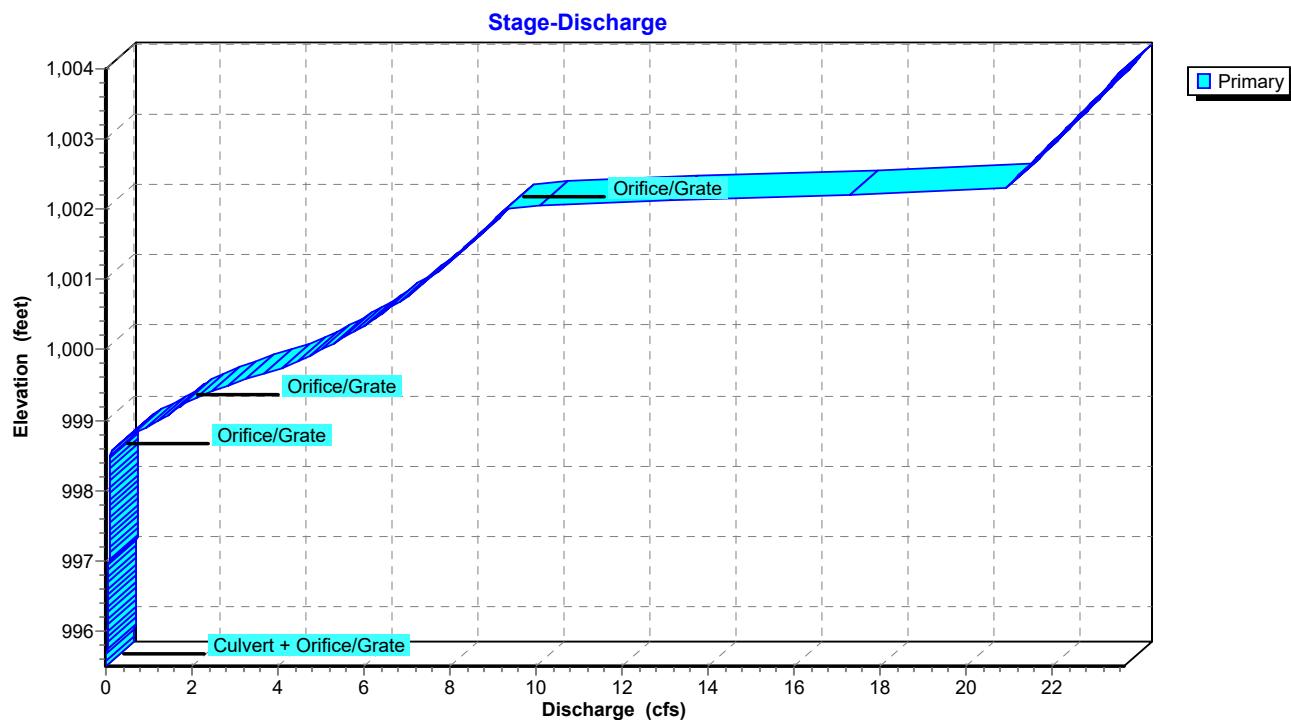
Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Pond 1P: Proposed Detention**Pond 1P: Proposed Detention**

Proposed

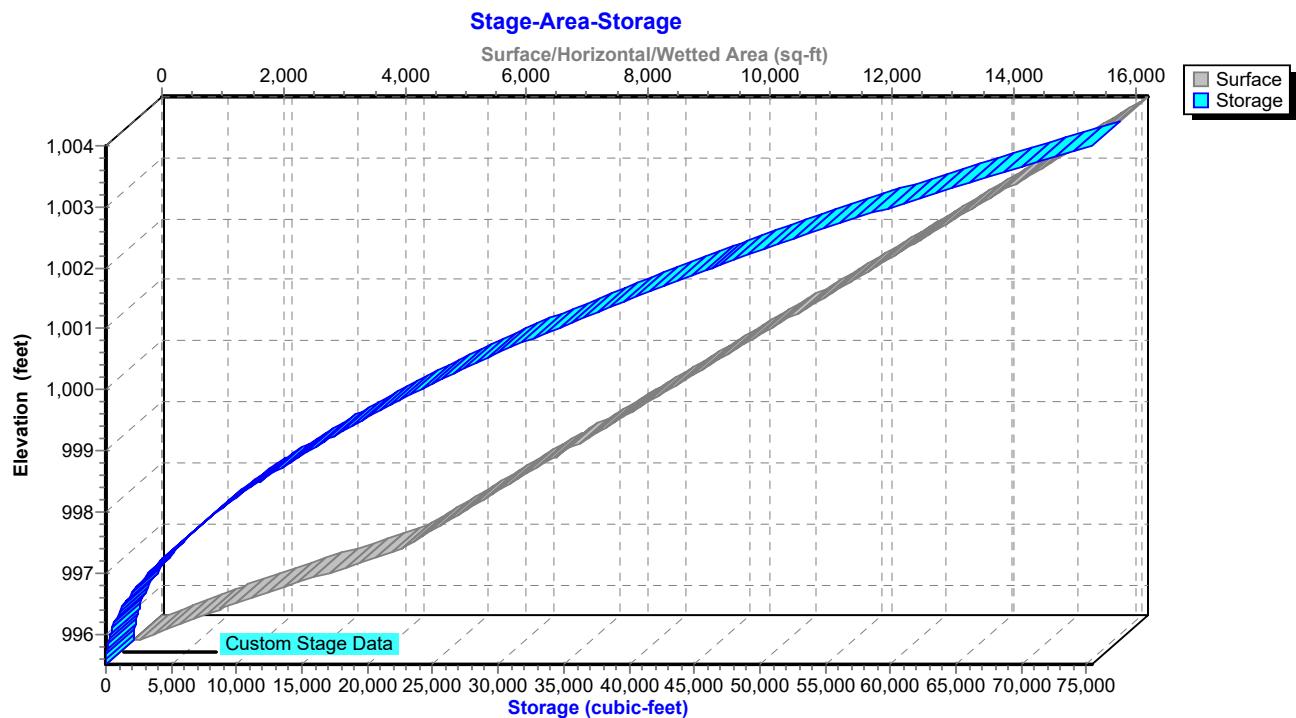
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Pond 1P: Proposed Detention

Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Hydrograph for Pond 1P: Proposed Detention

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
0.00	0.00	0	995.50	0.00
1.00	0.00	0	995.50	0.00
2.00	0.00	0	995.50	0.00
3.00	0.00	0	995.50	0.00
4.00	0.00	0	995.50	0.00
5.00	0.01	7	995.53	0.00
6.00	0.06	81	995.71	0.02
7.00	0.11	267	995.92	0.04
8.00	0.16	602	996.14	0.04
9.00	0.29	1,220	996.42	0.05
10.00	0.45	2,268	996.75	0.06
11.00	0.95	4,382	997.24	0.08
12.00	23.82	25,794	1,000.18	5.56
13.00	1.34	20,050	999.56	3.13
14.00	0.80	16,290	999.11	1.51
15.00	0.64	14,627	998.89	0.90
16.00	0.49	13,945	998.80	0.64
17.00	0.44	13,561	998.75	0.51
18.00	0.38	13,339	998.72	0.44
19.00	0.33	13,149	998.69	0.38
20.00	0.28	12,965	998.67	0.33
21.00	0.27	12,831	998.65	0.29
22.00	0.26	12,758	998.64	0.27
23.00	0.24	12,700	998.63	0.26
24.00	0.23	12,648	998.62	0.25
25.00	0.00	12,051	998.54	0.13
26.00	0.00	11,650	998.48	0.10
27.00	0.00	11,288	998.43	0.10
28.00	0.00	10,930	998.38	0.10
29.00	0.00	10,575	998.32	0.10
30.00	0.00	10,223	998.27	0.10
31.00	0.00	9,875	998.22	0.10
32.00	0.00	9,530	998.16	0.10
33.00	0.00	9,189	998.11	0.09
34.00	0.00	8,851	998.05	0.09
35.00	0.00	8,517	998.00	0.09
36.00	0.00	8,187	997.94	0.09
37.00	0.00	7,861	997.89	0.09
38.00	0.00	7,538	997.83	0.09
39.00	0.00	7,219	997.78	0.09
40.00	0.00	6,905	997.72	0.09
41.00	0.00	6,594	997.67	0.09
42.00	0.00	6,287	997.61	0.08
43.00	0.00	5,985	997.56	0.08
44.00	0.00	5,687	997.50	0.08
45.00	0.00	5,393	997.44	0.08
46.00	0.00	5,103	997.39	0.08
47.00	0.00	4,818	997.33	0.08
48.00	0.00	4,538	997.27	0.08

Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Stage-Discharge for Pond 1P: Proposed Detention

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
995.50	0.00	998.15	0.10	1,000.80	7.07	1,003.45	22.83
995.55	0.00	998.20	0.10	1,000.85	7.18	1,003.50	22.91
995.60	0.01	998.25	0.10	1,000.90	7.28	1,003.55	22.99
995.65	0.02	998.30	0.10	1,000.95	7.39	1,003.60	23.07
995.70	0.02	998.35	0.10	1,001.00	7.49	1,003.65	23.15
995.75	0.03	998.40	0.10	1,001.05	7.59	1,003.70	23.22
995.80	0.03	998.45	0.10	1,001.10	7.69	1,003.75	23.30
995.85	0.03	998.50	0.10	1,001.15	7.79	1,003.80	23.38
995.90	0.03	998.55	0.14	1,001.20	7.88	1,003.85	23.46
995.95	0.04	998.60	0.20	1,001.25	7.98	1,003.90	23.53
996.00	0.04	998.65	0.29	1,001.30	8.07	1,003.95	23.61
996.05	0.04	998.70	0.39	1,001.35	8.17	1,004.00	23.69
996.10	0.04	998.75	0.51	1,001.40	8.26		
996.15	0.05	998.80	0.63	1,001.45	8.35		
996.20	0.05	998.85	0.77	1,001.50	8.44		
996.25	0.05	998.90	0.92	1,001.55	8.53		
996.30	0.05	998.95	1.08	1,001.60	8.62		
996.35	0.05	999.00	1.24	1,001.65	8.71		
996.40	0.05	999.05	1.38	1,001.70	8.79		
996.45	0.06	999.10	1.50	1,001.75	8.88		
996.50	0.06	999.15	1.61	1,001.80	8.96		
996.55	0.06	999.20	1.71	1,001.85	9.05		
996.60	0.06	999.25	1.84	1,001.90	9.13		
996.65	0.06	999.30	2.01	1,001.95	9.21		
996.70	0.06	999.35	2.20	1,002.00	9.29		
996.75	0.06	999.40	2.40	1,002.05	10.23		
996.80	0.07	999.45	2.62	1,002.10	11.89		
996.85	0.07	999.50	2.85	1,002.15	14.01		
996.90	0.07	999.55	3.09	1,002.20	16.50		
996.95	0.07	999.60	3.35	1,002.25	19.32		
997.00	0.07	999.65	3.61	1,002.30	20.93		
997.05	0.07	999.70	3.88	1,002.35	21.02		
997.10	0.07	999.75	4.11	1,002.40	21.10		
997.15	0.07	999.80	4.32	1,002.45	21.19		
997.20	0.08	999.85	4.51	1,002.50	21.27		
997.25	0.08	999.90	4.69	1,002.55	21.36		
997.30	0.08	999.95	4.86	1,002.60	21.44		
997.35	0.08	1,000.00	5.02	1,002.65	21.53		
997.40	0.08	1,000.05	5.18	1,002.70	21.61		
997.45	0.08	1,000.10	5.33	1,002.75	21.69		
997.50	0.08	1,000.15	5.48	1,002.80	21.78		
997.55	0.08	1,000.20	5.62	1,002.85	21.86		
997.60	0.08	1,000.25	5.75	1,002.90	21.94		
997.65	0.09	1,000.30	5.89	1,002.95	22.02		
997.70	0.09	1,000.35	6.02	1,003.00	22.11		
997.75	0.09	1,000.40	6.14	1,003.05	22.19		
997.80	0.09	1,000.45	6.27	1,003.10	22.27		
997.85	0.09	1,000.50	6.39	1,003.15	22.35		
997.90	0.09	1,000.55	6.51	1,003.20	22.43		
997.95	0.09	1,000.60	6.63	1,003.25	22.51		
998.00	0.09	1,000.65	6.74	1,003.30	22.59		
998.05	0.09	1,000.70	6.85	1,003.35	22.67		
998.10	0.09	1,000.75	6.96	1,003.40	22.75		

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Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Stage-Area-Storage for Pond 1P: Proposed Detention

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
995.50	100	0	1,000.80	10,811	32,176
995.60	360	23	1,000.90	10,980	33,266
995.70	620	72	1,001.00	11,149	34,372
995.80	880	147	1,001.10	11,317	35,495
995.90	1,140	248	1,001.20	11,486	36,636
996.00	1,400	375	1,001.30	11,655	37,793
996.10	1,700	530	1,001.40	11,823	38,967
996.20	2,000	715	1,001.50	11,992	40,157
996.30	2,300	930	1,001.60	12,161	41,365
996.40	2,600	1,175	1,001.70	12,330	42,589
996.50	2,900	1,450	1,001.80	12,498	43,831
996.60	3,200	1,755	1,001.90	12,667	45,089
996.70	3,500	2,090	1,002.00	12,836	46,364
996.80	3,800	2,455	1,002.10	13,004	47,656
996.90	4,100	2,850	1,002.20	13,173	48,965
997.00	4,400	3,275	1,002.30	13,342	50,291
997.10	4,569	3,723	1,002.40	13,511	51,634
997.20	4,737	4,189	1,002.50	13,679	52,993
997.30	4,906	4,671	1,002.60	13,848	54,369
997.40	5,075	5,170	1,002.70	14,017	55,763
997.50	5,244	5,686	1,002.80	14,185	57,173
997.60	5,412	6,219	1,002.90	14,354	58,600
997.70	5,581	6,768	1,003.00	14,523	60,044
997.80	5,750	7,335	1,003.10	14,692	61,504
997.90	5,918	7,918	1,003.20	14,860	62,982
998.00	6,087	8,519	1,003.30	15,029	64,476
998.10	6,256	9,136	1,003.40	15,198	65,988
998.20	6,425	9,770	1,003.50	15,366	67,516
998.30	6,593	10,421	1,003.60	15,535	69,061
998.40	6,762	11,088	1,003.70	15,704	70,623
998.50	6,931	11,773	1,003.80	15,873	72,202
998.60	7,099	12,475	1,003.90	16,041	73,797
998.70	7,268	13,193	1,004.00	16,210	75,410
998.80	7,437	13,928			
998.90	7,606	14,680			
999.00	7,774	15,449			
999.10	7,943	16,235			
999.20	8,112	17,038			
999.30	8,280	17,857			
999.40	8,449	18,694			
999.50	8,618	19,547			
999.60	8,787	20,418			
999.70	8,955	21,305			
999.80	9,124	22,209			
999.90	9,293	23,129			
1,000.00	9,461	24,067			
1,000.10	9,630	25,022			
1,000.20	9,799	25,993			
1,000.30	9,968	26,981			
1,000.40	10,136	27,987			
1,000.50	10,305	29,009			
1,000.60	10,474	30,048			
1,000.70	10,642	31,103			

Proposed

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Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Summary for Link 1L: Proposed Total

Inflow Area = 5.030 ac, 46.32% Impervious, Inflow Depth > 3.40" for Jackson - 10 YR event

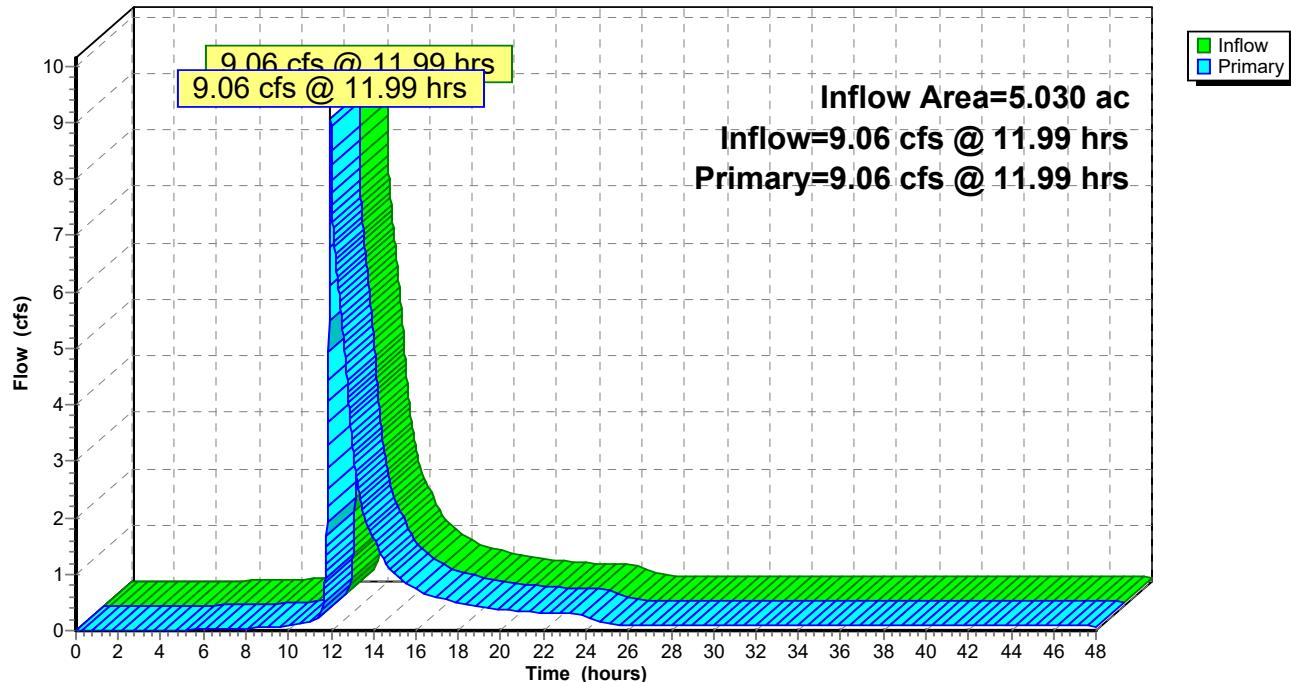
Inflow = 9.06 cfs @ 11.99 hrs, Volume= 1.424 af

Primary = 9.06 cfs @ 11.99 hrs, Volume= 1.424 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Link 1L: Proposed Total

Hydrograph



Proposed

Type II 24-hr Jackson - 10 YR Rainfall=5.30"

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Hydrograph for Link 1L: Proposed Total

Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)
0.00	0.00	0.00	0.00	26.50	0.10	0.00	0.10
0.50	0.00	0.00	0.00	27.00	0.10	0.00	0.10
1.00	0.00	0.00	0.00	27.50	0.10	0.00	0.10
1.50	0.00	0.00	0.00	28.00	0.10	0.00	0.10
2.00	0.00	0.00	0.00	28.50	0.10	0.00	0.10
2.50	0.00	0.00	0.00	29.00	0.10	0.00	0.10
3.00	0.00	0.00	0.00	29.50	0.10	0.00	0.10
3.50	0.00	0.00	0.00	30.00	0.10	0.00	0.10
4.00	0.00	0.00	0.00	30.50	0.10	0.00	0.10
4.50	0.00	0.00	0.00	31.00	0.10	0.00	0.10
5.00	0.00	0.00	0.00	31.50	0.10	0.00	0.10
5.50	0.01	0.00	0.01	32.00	0.10	0.00	0.10
6.00	0.02	0.00	0.02	32.50	0.09	0.00	0.09
6.50	0.03	0.00	0.03	33.00	0.09	0.00	0.09
7.00	0.04	0.00	0.04	33.50	0.09	0.00	0.09
7.50	0.04	0.00	0.04	34.00	0.09	0.00	0.09
8.00	0.04	0.00	0.04	34.50	0.09	0.00	0.09
8.50	0.05	0.00	0.05	35.00	0.09	0.00	0.09
9.00	0.06	0.00	0.06	35.50	0.09	0.00	0.09
9.50	0.07	0.00	0.07	36.00	0.09	0.00	0.09
10.00	0.09	0.00	0.09	36.50	0.09	0.00	0.09
10.50	0.11	0.00	0.11	37.00	0.09	0.00	0.09
11.00	0.15	0.00	0.15	37.50	0.09	0.00	0.09
11.50	0.25	0.00	0.25	38.00	0.09	0.00	0.09
12.00	9.03	0.00	9.03	38.50	0.09	0.00	0.09
12.50	5.56	0.00	5.56	39.00	0.09	0.00	0.09
13.00	3.35	0.00	3.35	39.50	0.09	0.00	0.09
13.50	2.13	0.00	2.13	40.00	0.09	0.00	0.09
14.00	1.64	0.00	1.64	40.50	0.09	0.00	0.09
14.50	1.27	0.00	1.27	41.00	0.09	0.00	0.09
15.00	1.00	0.00	1.00	41.50	0.09	0.00	0.09
15.50	0.84	0.00	0.84	42.00	0.08	0.00	0.08
16.00	0.72	0.00	0.72	42.50	0.08	0.00	0.08
16.50	0.64	0.00	0.64	43.00	0.08	0.00	0.08
17.00	0.58	0.00	0.58	43.50	0.08	0.00	0.08
17.50	0.54	0.00	0.54	44.00	0.08	0.00	0.08
18.00	0.50	0.00	0.50	44.50	0.08	0.00	0.08
18.50	0.47	0.00	0.47	45.00	0.08	0.00	0.08
19.00	0.44	0.00	0.44	45.50	0.08	0.00	0.08
19.50	0.41	0.00	0.41	46.00	0.08	0.00	0.08
20.00	0.38	0.00	0.38	46.50	0.08	0.00	0.08
20.50	0.35	0.00	0.35	47.00	0.08	0.00	0.08
21.00	0.34	0.00	0.34	47.50	0.08	0.00	0.08
21.50	0.32	0.00	0.32	48.00	0.08	0.00	0.08
22.00	0.32	0.00	0.32				
22.50	0.31	0.00	0.31				
23.00	0.30	0.00	0.30				
23.50	0.29	0.00	0.29				
24.00	0.29	0.00	0.29				
24.50	0.18	0.00	0.18				
25.00	0.13	0.00	0.13				
25.50	0.11	0.00	0.11				
26.00	0.10	0.00	0.10				

Proposed

Prepared by {enter your company name here}

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Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Proposed DetentionRunoff Area=4.200 ac 55.48% Impervious Runoff Depth=6.16"
Tc=5.0 min CN=87 Runoff=44.00 cfs 2.155 af**Subcatchment 2S: Proposed Bypass**Runoff Area=0.830 ac 0.00% Impervious Runoff Depth=4.66"
Tc=5.0 min CN=74 Runoff=7.04 cfs 0.322 af**Pond 1P: Proposed Detention**Peak Elev=1,001.89' Storage=44,940 cf Inflow=44.00 cfs 2.155 af
Outflow=9.11 cfs 2.049 af**Link 1L: Proposed Total**Inflow=14.98 cfs 2.371 af
Primary=14.98 cfs 2.371 af**Total Runoff Area = 5.030 ac Runoff Volume = 2.477 af Average Runoff Depth = 5.91"**
53.68% Pervious = 2.700 ac 46.32% Impervious = 2.330 ac

Proposed

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Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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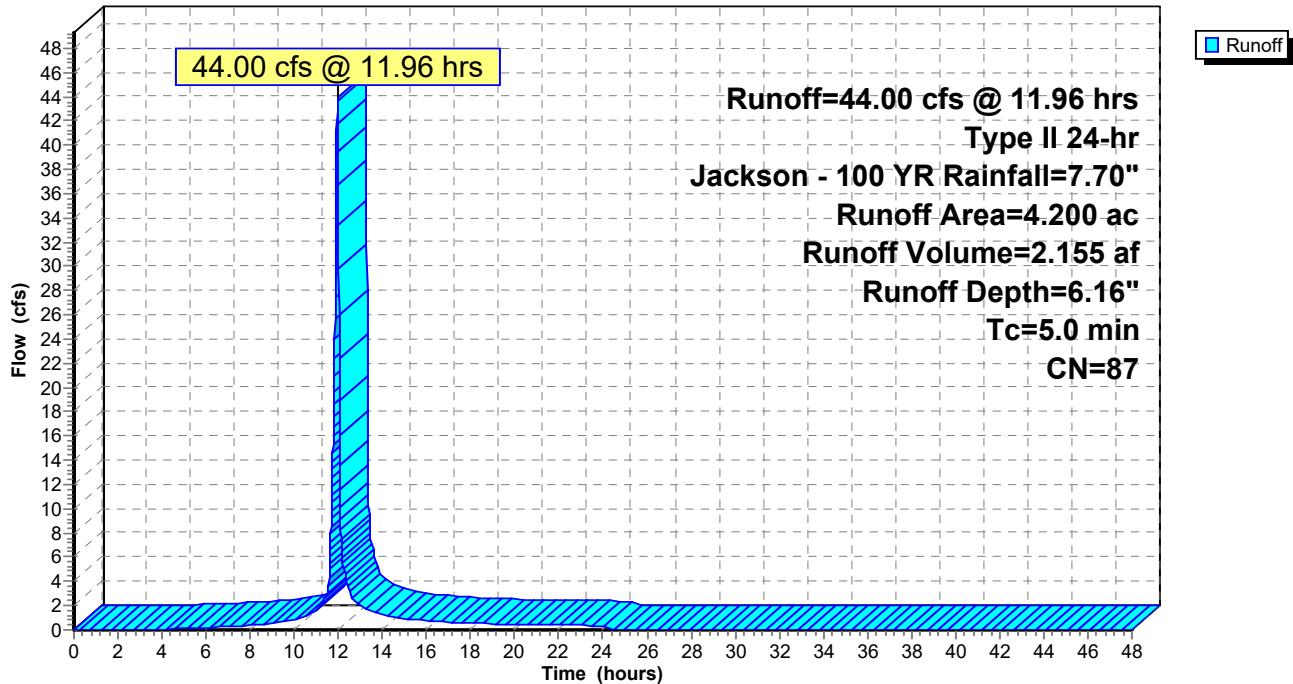
Summary for Subcatchment 1S: Proposed Detention

Runoff = 44.00 cfs @ 11.96 hrs, Volume= 2.155 af, Depth= 6.16"
 Routed to Pond 1P : Proposed Detention

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
 Type II 24-hr Jackson - 100 YR Rainfall=7.70"

Area (ac)	CN	Description
1.870	74	>75% Grass cover, Good, HSG C
2.330	98	Paved parking, HSG C
4.200	87	Weighted Average
1.870		44.52% Pervious Area
2.330		55.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 1S: Proposed Detention**Hydrograph**

Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Hydrograph for Subcatchment 1S: Proposed Detention

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	7.70	6.16	0.00
0.50	0.04	0.00	0.00	27.00	7.70	6.16	0.00
1.00	0.08	0.00	0.00	27.50	7.70	6.16	0.00
1.50	0.12	0.00	0.00	28.00	7.70	6.16	0.00
2.00	0.17	0.00	0.00	28.50	7.70	6.16	0.00
2.50	0.22	0.00	0.00	29.00	7.70	6.16	0.00
3.00	0.27	0.00	0.00	29.50	7.70	6.16	0.00
3.50	0.32	0.00	0.01	30.00	7.70	6.16	0.00
4.00	0.37	0.00	0.04	30.50	7.70	6.16	0.00
4.50	0.43	0.01	0.07	31.00	7.70	6.16	0.00
5.00	0.49	0.02	0.10	31.50	7.70	6.16	0.00
5.50	0.55	0.04	0.14	32.00	7.70	6.16	0.00
6.00	0.62	0.06	0.18	32.50	7.70	6.16	0.00
6.50	0.69	0.08	0.22	33.00	7.70	6.16	0.00
7.00	0.76	0.11	0.27	33.50	7.70	6.16	0.00
7.50	0.84	0.14	0.31	34.00	7.70	6.16	0.00
8.00	0.92	0.18	0.35	34.50	7.70	6.16	0.00
8.50	1.02	0.23	0.46	35.00	7.70	6.16	0.00
9.00	1.13	0.30	0.59	35.50	7.70	6.16	0.00
9.50	1.26	0.37	0.65	36.00	7.70	6.16	0.00
10.00	1.39	0.46	0.84	36.50	7.70	6.16	0.00
10.50	1.57	0.58	1.15	37.00	7.70	6.16	0.00
11.00	1.81	0.76	1.68	37.50	7.70	6.16	0.00
11.50	2.18	1.05	2.92	38.00	7.70	6.16	0.00
12.00	5.11	3.67	36.67	38.50	7.70	6.16	0.00
12.50	5.66	4.19	3.25	39.00	7.70	6.16	0.00
13.00	5.94	4.46	2.03	39.50	7.70	6.16	0.00
13.50	6.15	4.66	1.54	40.00	7.70	6.16	0.00
14.00	6.31	4.82	1.21	40.50	7.70	6.16	0.00
14.50	6.45	4.95	1.07	41.00	7.70	6.16	0.00
15.00	6.57	5.07	0.96	41.50	7.70	6.16	0.00
15.50	6.68	5.17	0.85	42.00	7.70	6.16	0.00
16.00	6.78	5.26	0.74	42.50	7.70	6.16	0.00
16.50	6.86	5.35	0.69	43.00	7.70	6.16	0.00
17.00	6.94	5.42	0.65	43.50	7.70	6.16	0.00
17.50	7.02	5.50	0.61	44.00	7.70	6.16	0.00
18.00	7.09	5.57	0.57	44.50	7.70	6.16	0.00
18.50	7.16	5.63	0.53	45.00	7.70	6.16	0.00
19.00	7.22	5.69	0.50	45.50	7.70	6.16	0.00
19.50	7.28	5.75	0.46	46.00	7.70	6.16	0.00
20.00	7.33	5.80	0.42	46.50	7.70	6.16	0.00
20.50	7.38	5.85	0.40	47.00	7.70	6.16	0.00
21.00	7.43	5.89	0.40	47.50	7.70	6.16	0.00
21.50	7.48	5.94	0.39	48.00	7.70	6.16	0.00
22.00	7.52	5.99	0.38				
22.50	7.57	6.03	0.37				
23.00	7.61	6.07	0.37				
23.50	7.66	6.12	0.36				
24.00	7.70	6.16	0.35				
24.50	7.70	6.16	0.00				
25.00	7.70	6.16	0.00				
25.50	7.70	6.16	0.00				
26.00	7.70	6.16	0.00				

Proposed

Prepared by {enter your company name here}

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Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Summary for Subcatchment 2S: Proposed Bypass

Runoff = 7.04 cfs @ 11.96 hrs, Volume= 0.322 af, Depth= 4.66"
Routed to Link 1L : Proposed Total

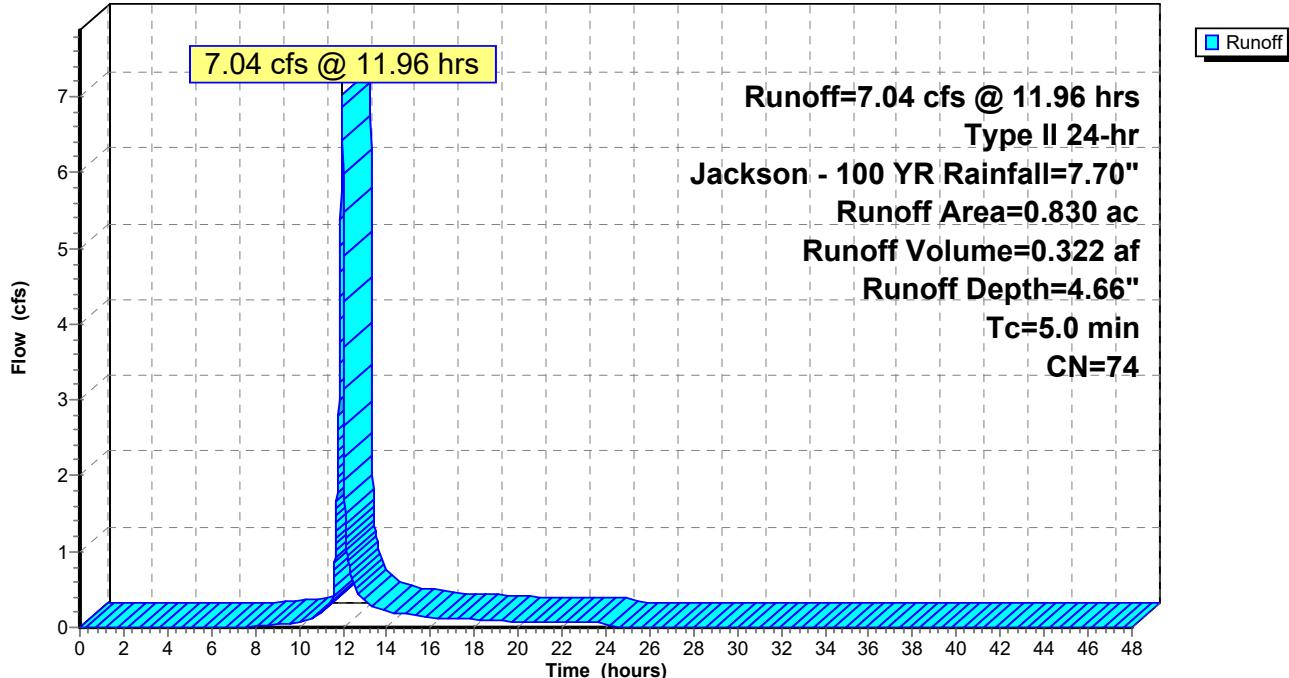
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
Type II 24-hr Jackson - 100 YR Rainfall=7.70"

Area (ac)	CN	Description
0.830	74	>75% Grass cover, Good, HSG C
0.000	98	Paved parking, HSG C
0.830	74	Weighted Average
0.830		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	Direct Entry,				

Subcatchment 2S: Proposed Bypass

Hydrograph



Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Hydrograph for Subcatchment 2S: Proposed Bypass

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	7.70	4.66	0.00
0.50	0.04	0.00	0.00	27.00	7.70	4.66	0.00
1.00	0.08	0.00	0.00	27.50	7.70	4.66	0.00
1.50	0.12	0.00	0.00	28.00	7.70	4.66	0.00
2.00	0.17	0.00	0.00	28.50	7.70	4.66	0.00
2.50	0.22	0.00	0.00	29.00	7.70	4.66	0.00
3.00	0.27	0.00	0.00	29.50	7.70	4.66	0.00
3.50	0.32	0.00	0.00	30.00	7.70	4.66	0.00
4.00	0.37	0.00	0.00	30.50	7.70	4.66	0.00
4.50	0.43	0.00	0.00	31.00	7.70	4.66	0.00
5.00	0.49	0.00	0.00	31.50	7.70	4.66	0.00
5.50	0.55	0.00	0.00	32.00	7.70	4.66	0.00
6.00	0.62	0.00	0.00	32.50	7.70	4.66	0.00
6.50	0.69	0.00	0.00	33.00	7.70	4.66	0.00
7.00	0.76	0.00	0.00	33.50	7.70	4.66	0.00
7.50	0.84	0.01	0.01	34.00	7.70	4.66	0.00
8.00	0.92	0.01	0.02	34.50	7.70	4.66	0.00
8.50	1.02	0.03	0.03	35.00	7.70	4.66	0.00
9.00	1.13	0.05	0.04	35.50	7.70	4.66	0.00
9.50	1.26	0.08	0.05	36.00	7.70	4.66	0.00
10.00	1.39	0.11	0.07	36.50	7.70	4.66	0.00
10.50	1.57	0.17	0.11	37.00	7.70	4.66	0.00
11.00	1.81	0.27	0.18	37.50	7.70	4.66	0.00
11.50	2.18	0.44	0.36	38.00	7.70	4.66	0.00
12.00	5.11	2.45	5.99	38.50	7.70	4.66	0.00
12.50	5.66	2.90	0.56	39.00	7.70	4.66	0.00
13.00	5.94	3.14	0.35	39.50	7.70	4.66	0.00
13.50	6.15	3.31	0.27	40.00	7.70	4.66	0.00
14.00	6.31	3.45	0.21	40.50	7.70	4.66	0.00
14.50	6.45	3.57	0.19	41.00	7.70	4.66	0.00
15.00	6.57	3.67	0.17	41.50	7.70	4.66	0.00
15.50	6.68	3.77	0.15	42.00	7.70	4.66	0.00
16.00	6.78	3.85	0.13	42.50	7.70	4.66	0.00
16.50	6.86	3.92	0.12	43.00	7.70	4.66	0.00
17.00	6.94	3.99	0.12	43.50	7.70	4.66	0.00
17.50	7.02	4.06	0.11	44.00	7.70	4.66	0.00
18.00	7.09	4.12	0.10	44.50	7.70	4.66	0.00
18.50	7.16	4.18	0.10	45.00	7.70	4.66	0.00
19.00	7.22	4.24	0.09	45.50	7.70	4.66	0.00
19.50	7.28	4.29	0.08	46.00	7.70	4.66	0.00
20.00	7.33	4.33	0.07	46.50	7.70	4.66	0.00
20.50	7.38	4.38	0.07	47.00	7.70	4.66	0.00
21.00	7.43	4.42	0.07	47.50	7.70	4.66	0.00
21.50	7.48	4.46	0.07	48.00	7.70	4.66	0.00
22.00	7.52	4.50	0.07				
22.50	7.57	4.54	0.07				
23.00	7.61	4.58	0.07				
23.50	7.66	4.62	0.06				
24.00	7.70	4.66	0.06				
24.50	7.70	4.66	0.00				
25.00	7.70	4.66	0.00				
25.50	7.70	4.66	0.00				
26.00	7.70	4.66	0.00				

Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

Prepared by {enter your company name here}

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Summary for Pond 1P: Proposed Detention

Inflow Area = 4.200 ac, 55.48% Impervious, Inflow Depth = 6.16" for Jackson - 100 YR event

Inflow = 44.00 cfs @ 11.96 hrs, Volume= 2.155 af

Outflow = 9.11 cfs @ 12.10 hrs, Volume= 2.049 af, Atten= 79%, Lag= 8.6 min

Primary = 9.11 cfs @ 12.10 hrs, Volume= 2.049 af

Routed to Link 1L : Proposed Total

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 1,001.89' @ 12.10 hrs Surf.Area= 12,647 sf Storage= 44,940 cf

Plug-Flow detention time= 215.9 min calculated for 2.049 af (95% of inflow)

Center-of-Mass det. time= 186.9 min (968.9 - 782.0)

Volume	Invert	Avail.Storage	Storage Description
#1	995.50'	75,410 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
995.50	100	0	0
996.00	1,400	375	375
997.00	4,400	2,900	3,275
1,004.00	16,210	72,135	75,410

Device	Routing	Invert	Outlet Devices
#1	Primary	995.50'	18.0" Round Culvert L= 48.3' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 995.50' / 995.00' S= 0.0104 '/' Cc= 0.900 n= 0.013, Flow Area= 1.77 sf
#2	Device 1	995.50'	1.5" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	998.50'	12.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	999.20'	15.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#5	Device 1	1,002.00'	288.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=9.11 cfs @ 12.10 hrs HW=1,001.89' (Free Discharge)

- ↑ 1=Culvert (Passes 9.11 cfs of 20.20 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.15 cfs @ 12.11 fps)
- 3=Orifice/Grate (Orifice Controls 4.26 cfs @ 8.53 fps)
- 4=Orifice/Grate (Orifice Controls 4.70 cfs @ 7.52 fps)
- 5=Orifice/Grate (Controls 0.00 cfs)

Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

Prepared by {enter your company name here}

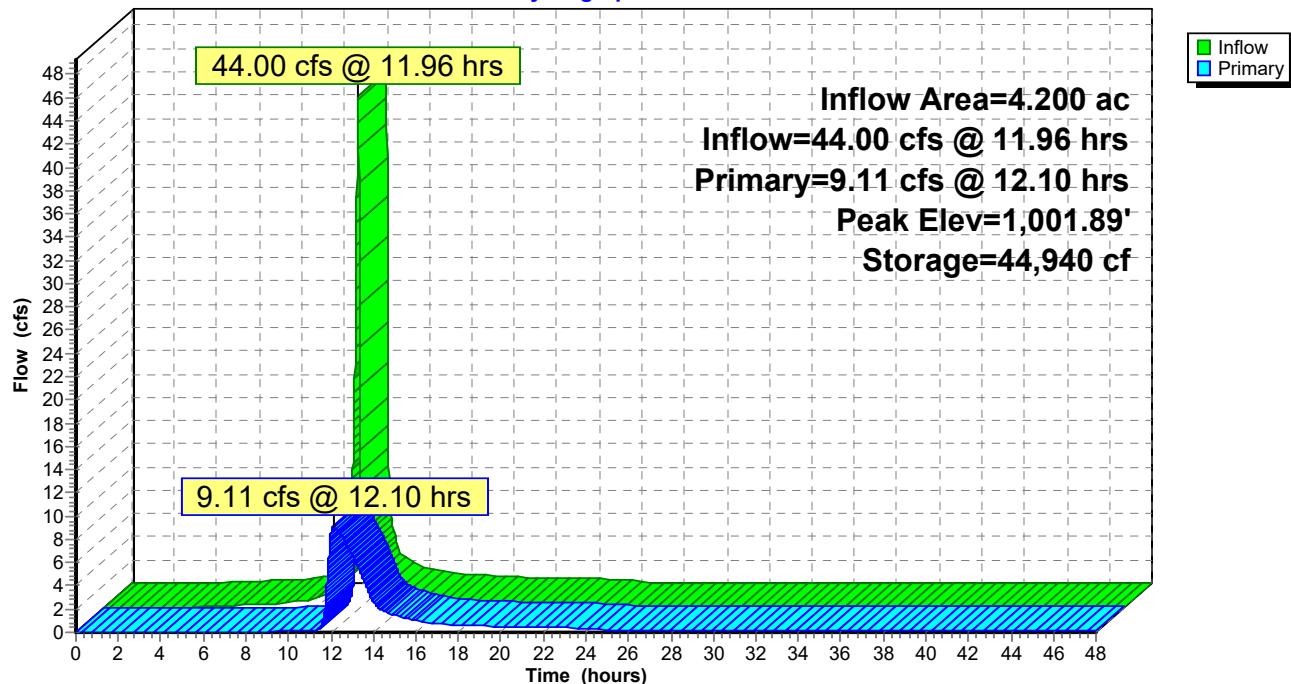
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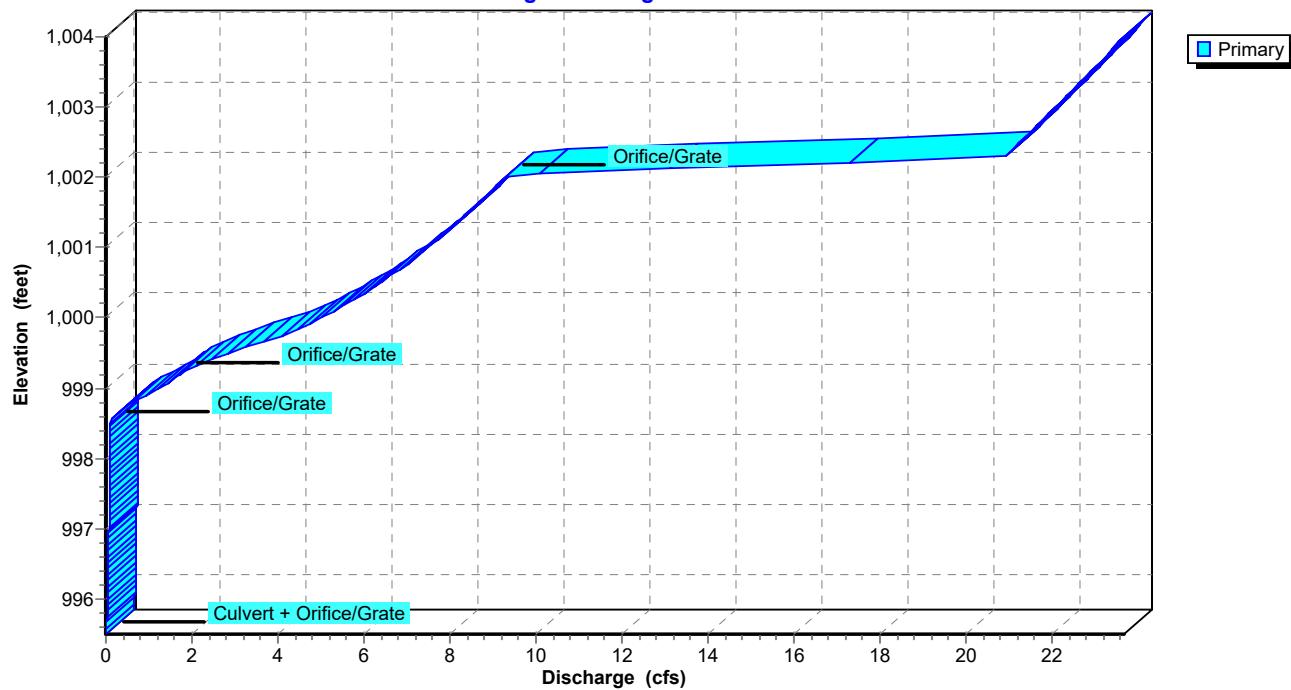
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Pond 1P: Proposed Detention

Hydrograph

**Pond 1P: Proposed Detention**

Stage-Discharge



Proposed

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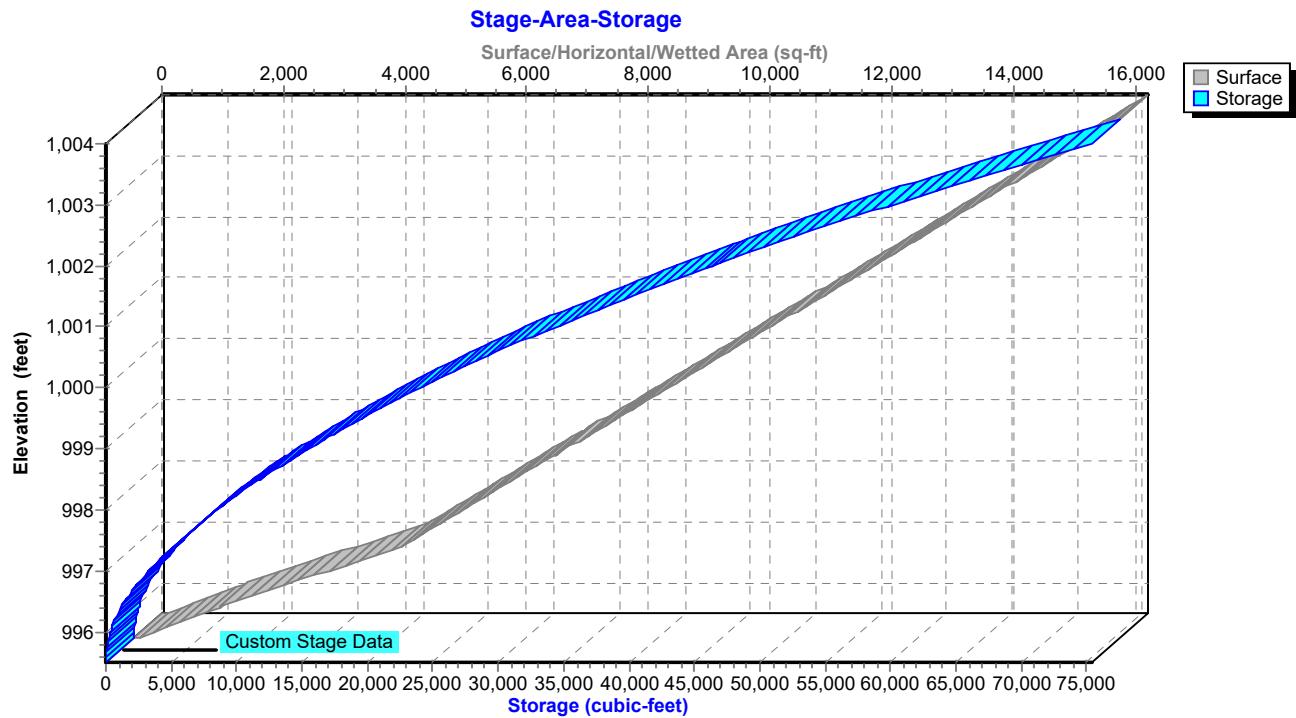
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Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Pond 1P: Proposed Detention



Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Hydrograph for Pond 1P: Proposed Detention

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
0.00	0.00	0	995.50	0.00
1.00	0.00	0	995.50	0.00
2.00	0.00	0	995.50	0.00
3.00	0.00	0	995.50	0.00
4.00	0.04	28	995.61	0.01
5.00	0.10	193	995.85	0.03
6.00	0.18	566	996.12	0.04
7.00	0.27	1,191	996.41	0.05
8.00	0.35	2,094	996.70	0.06
9.00	0.59	3,518	997.05	0.07
10.00	0.84	5,683	997.50	0.08
11.00	1.68	9,645	998.18	0.10
12.00	36.67	40,790	1,001.55	8.53
13.00	2.03	30,240	1,000.62	6.67
14.00	1.21	19,143	999.45	2.64
15.00	0.96	16,200	999.10	1.49
16.00	0.74	14,852	998.92	0.99
17.00	0.65	14,259	998.84	0.76
18.00	0.57	13,957	998.80	0.65
19.00	0.50	13,711	998.77	0.56
20.00	0.42	13,477	998.74	0.48
21.00	0.40	13,309	998.72	0.43
22.00	0.38	13,215	998.70	0.40
23.00	0.37	13,147	998.69	0.38
24.00	0.35	13,088	998.69	0.37
25.00	0.00	12,267	998.57	0.17
26.00	0.00	11,800	998.50	0.10
27.00	0.00	11,436	998.45	0.10
28.00	0.00	11,076	998.40	0.10
29.00	0.00	10,720	998.34	0.10
30.00	0.00	10,367	998.29	0.10
31.00	0.00	10,017	998.24	0.10
32.00	0.00	9,671	998.18	0.10
33.00	0.00	9,328	998.13	0.09
34.00	0.00	8,989	998.08	0.09
35.00	0.00	8,654	998.02	0.09
36.00	0.00	8,322	997.97	0.09
37.00	0.00	7,994	997.91	0.09
38.00	0.00	7,670	997.86	0.09
39.00	0.00	7,349	997.80	0.09
40.00	0.00	7,033	997.75	0.09
41.00	0.00	6,721	997.69	0.09
42.00	0.00	6,412	997.64	0.09
43.00	0.00	6,108	997.58	0.08
44.00	0.00	5,808	997.52	0.08
45.00	0.00	5,513	997.47	0.08
46.00	0.00	5,221	997.41	0.08
47.00	0.00	4,934	997.35	0.08
48.00	0.00	4,652	997.30	0.08

Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Stage-Discharge for Pond 1P: Proposed Detention

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
995.50	0.00	998.15	0.10	1,000.80	7.07	1,003.45	22.83
995.55	0.00	998.20	0.10	1,000.85	7.18	1,003.50	22.91
995.60	0.01	998.25	0.10	1,000.90	7.28	1,003.55	22.99
995.65	0.02	998.30	0.10	1,000.95	7.39	1,003.60	23.07
995.70	0.02	998.35	0.10	1,001.00	7.49	1,003.65	23.15
995.75	0.03	998.40	0.10	1,001.05	7.59	1,003.70	23.22
995.80	0.03	998.45	0.10	1,001.10	7.69	1,003.75	23.30
995.85	0.03	998.50	0.10	1,001.15	7.79	1,003.80	23.38
995.90	0.03	998.55	0.14	1,001.20	7.88	1,003.85	23.46
995.95	0.04	998.60	0.20	1,001.25	7.98	1,003.90	23.53
996.00	0.04	998.65	0.29	1,001.30	8.07	1,003.95	23.61
996.05	0.04	998.70	0.39	1,001.35	8.17	1,004.00	23.69
996.10	0.04	998.75	0.51	1,001.40	8.26		
996.15	0.05	998.80	0.63	1,001.45	8.35		
996.20	0.05	998.85	0.77	1,001.50	8.44		
996.25	0.05	998.90	0.92	1,001.55	8.53		
996.30	0.05	998.95	1.08	1,001.60	8.62		
996.35	0.05	999.00	1.24	1,001.65	8.71		
996.40	0.05	999.05	1.38	1,001.70	8.79		
996.45	0.06	999.10	1.50	1,001.75	8.88		
996.50	0.06	999.15	1.61	1,001.80	8.96		
996.55	0.06	999.20	1.71	1,001.85	9.05		
996.60	0.06	999.25	1.84	1,001.90	9.13		
996.65	0.06	999.30	2.01	1,001.95	9.21		
996.70	0.06	999.35	2.20	1,002.00	9.29		
996.75	0.06	999.40	2.40	1,002.05	10.23		
996.80	0.07	999.45	2.62	1,002.10	11.89		
996.85	0.07	999.50	2.85	1,002.15	14.01		
996.90	0.07	999.55	3.09	1,002.20	16.50		
996.95	0.07	999.60	3.35	1,002.25	19.32		
997.00	0.07	999.65	3.61	1,002.30	20.93		
997.05	0.07	999.70	3.88	1,002.35	21.02		
997.10	0.07	999.75	4.11	1,002.40	21.10		
997.15	0.07	999.80	4.32	1,002.45	21.19		
997.20	0.08	999.85	4.51	1,002.50	21.27		
997.25	0.08	999.90	4.69	1,002.55	21.36		
997.30	0.08	999.95	4.86	1,002.60	21.44		
997.35	0.08	1,000.00	5.02	1,002.65	21.53		
997.40	0.08	1,000.05	5.18	1,002.70	21.61		
997.45	0.08	1,000.10	5.33	1,002.75	21.69		
997.50	0.08	1,000.15	5.48	1,002.80	21.78		
997.55	0.08	1,000.20	5.62	1,002.85	21.86		
997.60	0.08	1,000.25	5.75	1,002.90	21.94		
997.65	0.09	1,000.30	5.89	1,002.95	22.02		
997.70	0.09	1,000.35	6.02	1,003.00	22.11		
997.75	0.09	1,000.40	6.14	1,003.05	22.19		
997.80	0.09	1,000.45	6.27	1,003.10	22.27		
997.85	0.09	1,000.50	6.39	1,003.15	22.35		
997.90	0.09	1,000.55	6.51	1,003.20	22.43		
997.95	0.09	1,000.60	6.63	1,003.25	22.51		
998.00	0.09	1,000.65	6.74	1,003.30	22.59		
998.05	0.09	1,000.70	6.85	1,003.35	22.67		
998.10	0.09	1,000.75	6.96	1,003.40	22.75		

Stage-Area-Storage for Pond 1P: Proposed Detention

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
995.50	100	0	1,000.80	10,811	32,176
995.60	360	23	1,000.90	10,980	33,266
995.70	620	72	1,001.00	11,149	34,372
995.80	880	147	1,001.10	11,317	35,495
995.90	1,140	248	1,001.20	11,486	36,636
996.00	1,400	375	1,001.30	11,655	37,793
996.10	1,700	530	1,001.40	11,823	38,967
996.20	2,000	715	1,001.50	11,992	40,157
996.30	2,300	930	1,001.60	12,161	41,365
996.40	2,600	1,175	1,001.70	12,330	42,589
996.50	2,900	1,450	1,001.80	12,498	43,831
996.60	3,200	1,755	1,001.90	12,667	45,089
996.70	3,500	2,090	1,002.00	12,836	46,364
996.80	3,800	2,455	1,002.10	13,004	47,656
996.90	4,100	2,850	1,002.20	13,173	48,965
997.00	4,400	3,275	1,002.30	13,342	50,291
997.10	4,569	3,723	1,002.40	13,511	51,634
997.20	4,737	4,189	1,002.50	13,679	52,993
997.30	4,906	4,671	1,002.60	13,848	54,369
997.40	5,075	5,170	1,002.70	14,017	55,763
997.50	5,244	5,686	1,002.80	14,185	57,173
997.60	5,412	6,219	1,002.90	14,354	58,600
997.70	5,581	6,768	1,003.00	14,523	60,044
997.80	5,750	7,335	1,003.10	14,692	61,504
997.90	5,918	7,918	1,003.20	14,860	62,982
998.00	6,087	8,519	1,003.30	15,029	64,476
998.10	6,256	9,136	1,003.40	15,198	65,988
998.20	6,425	9,770	1,003.50	15,366	67,516
998.30	6,593	10,421	1,003.60	15,535	69,061
998.40	6,762	11,088	1,003.70	15,704	70,623
998.50	6,931	11,773	1,003.80	15,873	72,202
998.60	7,099	12,475	1,003.90	16,041	73,797
998.70	7,268	13,193	1,004.00	16,210	75,410
998.80	7,437	13,928			
998.90	7,606	14,680			
999.00	7,774	15,449			
999.10	7,943	16,235			
999.20	8,112	17,038			
999.30	8,280	17,857			
999.40	8,449	18,694			
999.50	8,618	19,547			
999.60	8,787	20,418			
999.70	8,955	21,305			
999.80	9,124	22,209			
999.90	9,293	23,129			
1,000.00	9,461	24,067			
1,000.10	9,630	25,022			
1,000.20	9,799	25,993			
1,000.30	9,968	26,981			
1,000.40	10,136	27,987			
1,000.50	10,305	29,009			
1,000.60	10,474	30,048			
1,000.70	10,642	31,103			

Summary for Link 1L: Proposed Total

Inflow Area = 5.030 ac, 46.32% Impervious, Inflow Depth > 5.66" for Jackson - 100 YR event

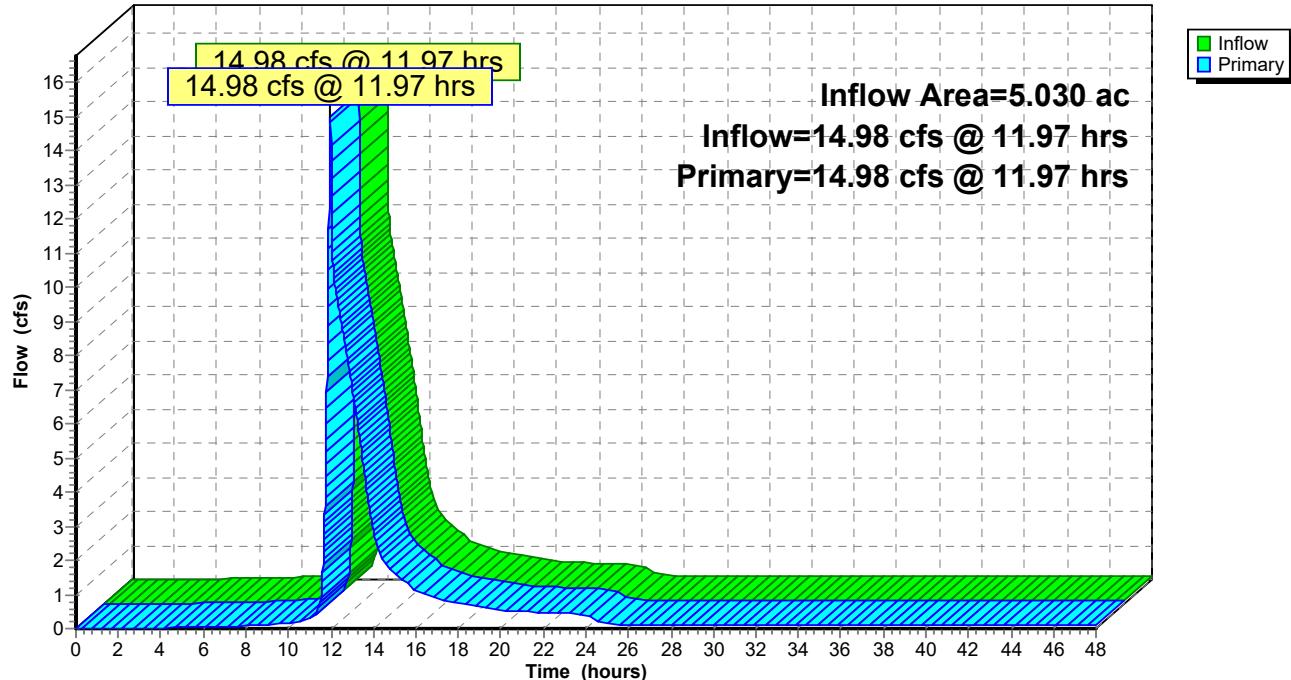
Inflow = 14.98 cfs @ 11.97 hrs, Volume= 2.371 af

Primary = 14.98 cfs @ 11.97 hrs, Volume= 2.371 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Link 1L: Proposed Total

Hydrograph



Proposed

Type II 24-hr Jackson - 100 YR Rainfall=7.70"

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Hydrograph for Link 1L: Proposed Total

Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)
0.00	0.00	0.00	0.00	26.50	0.10	0.00	0.10
0.50	0.00	0.00	0.00	27.00	0.10	0.00	0.10
1.00	0.00	0.00	0.00	27.50	0.10	0.00	0.10
1.50	0.00	0.00	0.00	28.00	0.10	0.00	0.10
2.00	0.00	0.00	0.00	28.50	0.10	0.00	0.10
2.50	0.00	0.00	0.00	29.00	0.10	0.00	0.10
3.00	0.00	0.00	0.00	29.50	0.10	0.00	0.10
3.50	0.00	0.00	0.00	30.00	0.10	0.00	0.10
4.00	0.01	0.00	0.01	30.50	0.10	0.00	0.10
4.50	0.02	0.00	0.02	31.00	0.10	0.00	0.10
5.00	0.03	0.00	0.03	31.50	0.10	0.00	0.10
5.50	0.04	0.00	0.04	32.00	0.10	0.00	0.10
6.00	0.04	0.00	0.04	32.50	0.10	0.00	0.10
6.50	0.05	0.00	0.05	33.00	0.09	0.00	0.09
7.00	0.06	0.00	0.06	33.50	0.09	0.00	0.09
7.50	0.07	0.00	0.07	34.00	0.09	0.00	0.09
8.00	0.08	0.00	0.08	34.50	0.09	0.00	0.09
8.50	0.09	0.00	0.09	35.00	0.09	0.00	0.09
9.00	0.11	0.00	0.11	35.50	0.09	0.00	0.09
9.50	0.13	0.00	0.13	36.00	0.09	0.00	0.09
10.00	0.16	0.00	0.16	36.50	0.09	0.00	0.09
10.50	0.20	0.00	0.20	37.00	0.09	0.00	0.09
11.00	0.28	0.00	0.28	37.50	0.09	0.00	0.09
11.50	0.81	0.00	0.81	38.00	0.09	0.00	0.09
12.00	14.52	0.00	14.52	38.50	0.09	0.00	0.09
12.50	8.87	0.00	8.87	39.00	0.09	0.00	0.09
13.00	7.02	0.00	7.02	39.50	0.09	0.00	0.09
13.50	4.96	0.00	4.96	40.00	0.09	0.00	0.09
14.00	2.85	0.00	2.85	40.50	0.09	0.00	0.09
14.50	1.98	0.00	1.98	41.00	0.09	0.00	0.09
15.00	1.66	0.00	1.66	41.50	0.09	0.00	0.09
15.50	1.37	0.00	1.37	42.00	0.09	0.00	0.09
16.00	1.12	0.00	1.12	42.50	0.08	0.00	0.08
16.50	0.97	0.00	0.97	43.00	0.08	0.00	0.08
17.00	0.87	0.00	0.87	43.50	0.08	0.00	0.08
17.50	0.80	0.00	0.80	44.00	0.08	0.00	0.08
18.00	0.75	0.00	0.75	44.50	0.08	0.00	0.08
18.50	0.70	0.00	0.70	45.00	0.08	0.00	0.08
19.00	0.65	0.00	0.65	45.50	0.08	0.00	0.08
19.50	0.60	0.00	0.60	46.00	0.08	0.00	0.08
20.00	0.56	0.00	0.56	46.50	0.08	0.00	0.08
20.50	0.52	0.00	0.52	47.00	0.08	0.00	0.08
21.00	0.50	0.00	0.50	47.50	0.08	0.00	0.08
21.50	0.48	0.00	0.48	48.00	0.08	0.00	0.08
22.00	0.47	0.00	0.47				
22.50	0.46	0.00	0.46				
23.00	0.45	0.00	0.45				
23.50	0.44	0.00	0.44				
24.00	0.43	0.00	0.43				
24.50	0.25	0.00	0.25				
25.00	0.17	0.00	0.17				
25.50	0.13	0.00	0.13				
26.00	0.10	0.00	0.10				

Proposed

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Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Proposed DetentionRunoff Area=4.200 ac 55.48% Impervious Runoff Depth=2.18"
Tc=5.0 min CN=87 Runoff=16.61 cfs 0.764 af**Subcatchment 2S: Proposed Bypass**Runoff Area=0.830 ac 0.00% Impervious Runoff Depth=1.24"
Tc=5.0 min CN=74 Runoff=1.91 cfs 0.086 af**Pond 1P: Proposed Detention**Peak Elev=999.20' Storage=17,018 cf Inflow=16.61 cfs 0.764 af
Outflow=1.70 cfs 0.663 af**Link 1L: Proposed Total**Inflow=2.46 cfs 0.749 af
Primary=2.46 cfs 0.749 af**Total Runoff Area = 5.030 ac Runoff Volume = 0.850 af Average Runoff Depth = 2.03"**
53.68% Pervious = 2.700 ac 46.32% Impervious = 2.330 ac

Proposed

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Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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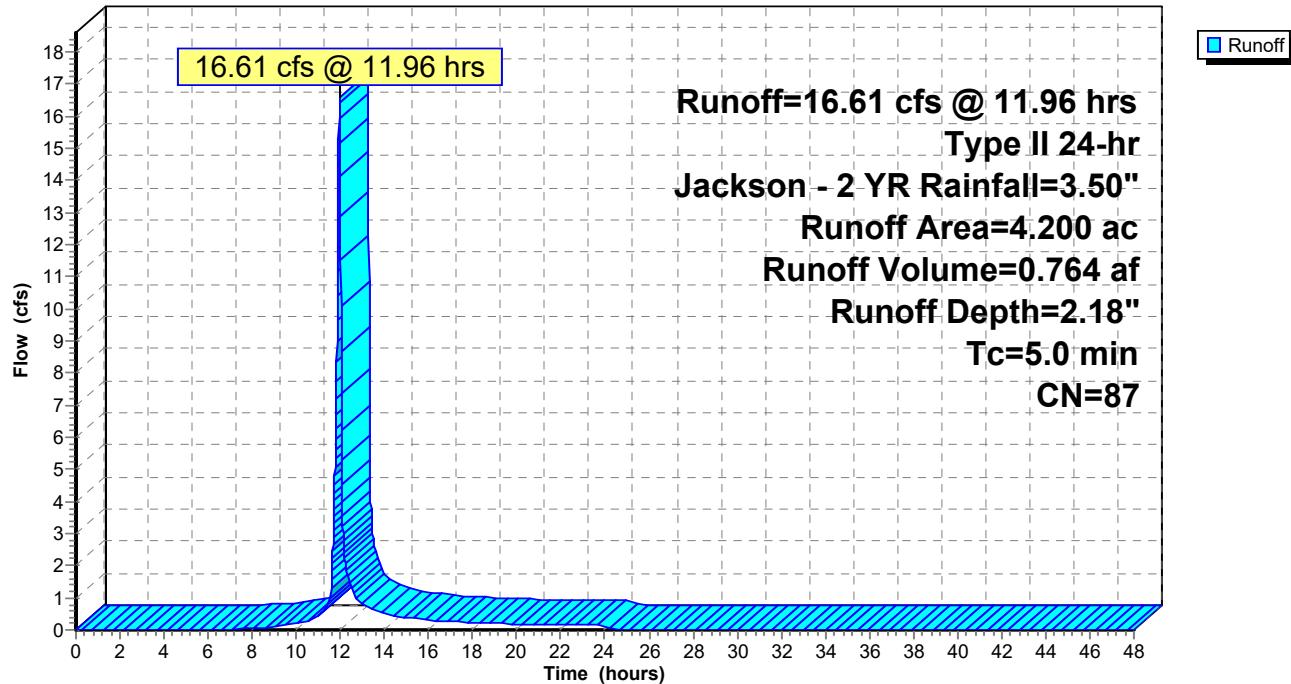
Summary for Subcatchment 1S: Proposed Detention

Runoff = 16.61 cfs @ 11.96 hrs, Volume= 0.764 af, Depth= 2.18"
Routed to Pond 1P : Proposed Detention

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
Type II 24-hr Jackson - 2 YR Rainfall=3.50"

Area (ac)	CN	Description
1.870	74	>75% Grass cover, Good, HSG C
2.330	98	Paved parking, HSG C
4.200	87	Weighted Average
1.870		44.52% Pervious Area
2.330		55.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 1S: Proposed Detention**Hydrograph**

Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Hydrograph for Subcatchment 1S: Proposed Detention

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	3.50	2.18	0.00
0.50	0.02	0.00	0.00	27.00	3.50	2.18	0.00
1.00	0.04	0.00	0.00	27.50	3.50	2.18	0.00
1.50	0.06	0.00	0.00	28.00	3.50	2.18	0.00
2.00	0.08	0.00	0.00	28.50	3.50	2.18	0.00
2.50	0.10	0.00	0.00	29.00	3.50	2.18	0.00
3.00	0.12	0.00	0.00	29.50	3.50	2.18	0.00
3.50	0.14	0.00	0.00	30.00	3.50	2.18	0.00
4.00	0.17	0.00	0.00	30.50	3.50	2.18	0.00
4.50	0.19	0.00	0.00	31.00	3.50	2.18	0.00
5.00	0.22	0.00	0.00	31.50	3.50	2.18	0.00
5.50	0.25	0.00	0.00	32.00	3.50	2.18	0.00
6.00	0.28	0.00	0.00	32.50	3.50	2.18	0.00
6.50	0.31	0.00	0.00	33.00	3.50	2.18	0.00
7.00	0.35	0.00	0.02	33.50	3.50	2.18	0.00
7.50	0.38	0.00	0.03	34.00	3.50	2.18	0.00
8.00	0.42	0.01	0.04	34.50	3.50	2.18	0.00
8.50	0.46	0.02	0.07	35.00	3.50	2.18	0.00
9.00	0.51	0.03	0.11	35.50	3.50	2.18	0.00
9.50	0.57	0.04	0.13	36.00	3.50	2.18	0.00
10.00	0.63	0.06	0.19	36.50	3.50	2.18	0.00
10.50	0.71	0.09	0.28	37.00	3.50	2.18	0.00
11.00	0.82	0.14	0.45	37.50	3.50	2.18	0.00
11.50	0.99	0.22	0.87	38.00	3.50	2.18	0.00
12.00	2.32	1.16	14.10	38.50	3.50	2.18	0.00
12.50	2.57	1.37	1.30	39.00	3.50	2.18	0.00
13.00	2.70	1.48	0.82	39.50	3.50	2.18	0.00
13.50	2.80	1.56	0.63	40.00	3.50	2.18	0.00
14.00	2.87	1.63	0.49	40.50	3.50	2.18	0.00
14.50	2.93	1.68	0.44	41.00	3.50	2.18	0.00
15.00	2.99	1.73	0.39	41.50	3.50	2.18	0.00
15.50	3.04	1.77	0.35	42.00	3.50	2.18	0.00
16.00	3.08	1.81	0.31	42.50	3.50	2.18	0.00
16.50	3.12	1.84	0.29	43.00	3.50	2.18	0.00
17.00	3.16	1.88	0.27	43.50	3.50	2.18	0.00
17.50	3.19	1.91	0.25	44.00	3.50	2.18	0.00
18.00	3.22	1.94	0.24	44.50	3.50	2.18	0.00
18.50	3.25	1.96	0.22	45.00	3.50	2.18	0.00
19.00	3.28	1.99	0.21	45.50	3.50	2.18	0.00
19.50	3.31	2.01	0.19	46.00	3.50	2.18	0.00
20.00	3.33	2.03	0.17	46.50	3.50	2.18	0.00
20.50	3.35	2.05	0.17	47.00	3.50	2.18	0.00
21.00	3.38	2.07	0.17	47.50	3.50	2.18	0.00
21.50	3.40	2.09	0.16	48.00	3.50	2.18	0.00
22.00	3.42	2.11	0.16				
22.50	3.44	2.13	0.16				
23.00	3.46	2.15	0.15				
23.50	3.48	2.16	0.15				
24.00	3.50	2.18	0.15				
24.50	3.50	2.18	0.00				
25.00	3.50	2.18	0.00				
25.50	3.50	2.18	0.00				
26.00	3.50	2.18	0.00				

Proposed

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Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Summary for Subcatchment 2S: Proposed Bypass

Runoff = 1.91 cfs @ 11.97 hrs, Volume= 0.086 af, Depth= 1.24"
Routed to Link 1L : Proposed Total

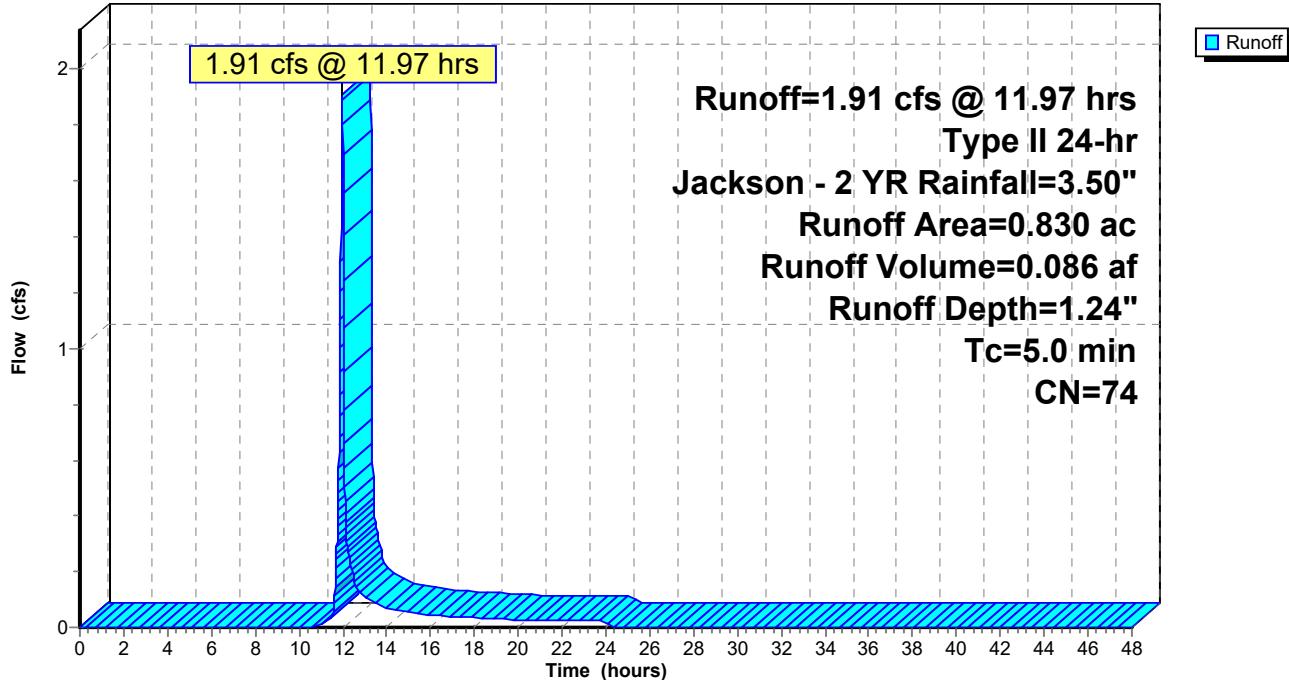
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
Type II 24-hr Jackson - 2 YR Rainfall=3.50"

Area (ac)	CN	Description
0.830	74	>75% Grass cover, Good, HSG C
0.000	98	Paved parking, HSG C
0.830	74	Weighted Average
0.830		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	Direct Entry,				

Subcatchment 2S: Proposed Bypass

Hydrograph



Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Hydrograph for Subcatchment 2S: Proposed Bypass

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
0.00	0.00	0.00	0.00	26.50	3.50	1.24	0.00
0.50	0.02	0.00	0.00	27.00	3.50	1.24	0.00
1.00	0.04	0.00	0.00	27.50	3.50	1.24	0.00
1.50	0.06	0.00	0.00	28.00	3.50	1.24	0.00
2.00	0.08	0.00	0.00	28.50	3.50	1.24	0.00
2.50	0.10	0.00	0.00	29.00	3.50	1.24	0.00
3.00	0.12	0.00	0.00	29.50	3.50	1.24	0.00
3.50	0.14	0.00	0.00	30.00	3.50	1.24	0.00
4.00	0.17	0.00	0.00	30.50	3.50	1.24	0.00
4.50	0.19	0.00	0.00	31.00	3.50	1.24	0.00
5.00	0.22	0.00	0.00	31.50	3.50	1.24	0.00
5.50	0.25	0.00	0.00	32.00	3.50	1.24	0.00
6.00	0.28	0.00	0.00	32.50	3.50	1.24	0.00
6.50	0.31	0.00	0.00	33.00	3.50	1.24	0.00
7.00	0.35	0.00	0.00	33.50	3.50	1.24	0.00
7.50	0.38	0.00	0.00	34.00	3.50	1.24	0.00
8.00	0.42	0.00	0.00	34.50	3.50	1.24	0.00
8.50	0.46	0.00	0.00	35.00	3.50	1.24	0.00
9.00	0.51	0.00	0.00	35.50	3.50	1.24	0.00
9.50	0.57	0.00	0.00	36.00	3.50	1.24	0.00
10.00	0.63	0.00	0.00	36.50	3.50	1.24	0.00
10.50	0.71	0.00	0.00	37.00	3.50	1.24	0.00
11.00	0.82	0.00	0.01	37.50	3.50	1.24	0.00
11.50	0.99	0.02	0.04	38.00	3.50	1.24	0.00
12.00	2.32	0.51	1.69	38.50	3.50	1.24	0.00
12.50	2.57	0.65	0.17	39.00	3.50	1.24	0.00
13.00	2.70	0.73	0.11	39.50	3.50	1.24	0.00
13.50	2.80	0.78	0.09	40.00	3.50	1.24	0.00
14.00	2.87	0.83	0.07	40.50	3.50	1.24	0.00
14.50	2.93	0.87	0.06	41.00	3.50	1.24	0.00
15.00	2.99	0.90	0.06	41.50	3.50	1.24	0.00
15.50	3.04	0.93	0.05	42.00	3.50	1.24	0.00
16.00	3.08	0.96	0.04	42.50	3.50	1.24	0.00
16.50	3.12	0.98	0.04	43.00	3.50	1.24	0.00
17.00	3.16	1.01	0.04	43.50	3.50	1.24	0.00
17.50	3.19	1.03	0.04	44.00	3.50	1.24	0.00
18.00	3.22	1.05	0.04	44.50	3.50	1.24	0.00
18.50	3.25	1.07	0.03	45.00	3.50	1.24	0.00
19.00	3.28	1.09	0.03	45.50	3.50	1.24	0.00
19.50	3.31	1.11	0.03	46.00	3.50	1.24	0.00
20.00	3.33	1.13	0.03	46.50	3.50	1.24	0.00
20.50	3.35	1.14	0.03	47.00	3.50	1.24	0.00
21.00	3.38	1.16	0.02	47.50	3.50	1.24	0.00
21.50	3.40	1.17	0.02	48.00	3.50	1.24	0.00
22.00	3.42	1.18	0.02				
22.50	3.44	1.20	0.02				
23.00	3.46	1.21	0.02				
23.50	3.48	1.23	0.02				
24.00	3.50	1.24	0.02				
24.50	3.50	1.24	0.00				
25.00	3.50	1.24	0.00				
25.50	3.50	1.24	0.00				
26.00	3.50	1.24	0.00				

Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Summary for Pond 1P: Proposed Detention

Inflow Area = 4.200 ac, 55.48% Impervious, Inflow Depth = 2.18" for Jackson - 2 YR event

Inflow = 16.61 cfs @ 11.96 hrs, Volume= 0.764 af

Outflow = 1.70 cfs @ 12.36 hrs, Volume= 0.663 af, Atten= 90%, Lag= 23.8 min

Primary = 1.70 cfs @ 12.36 hrs, Volume= 0.663 af

Routed to Link 1L : Proposed Total

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 999.20' @ 12.36 hrs Surf.Area= 8,108 sf Storage= 17,018 cf

Plug-Flow detention time= 494.7 min calculated for 0.663 af (87% of inflow)

Center-of-Mass det. time= 432.1 min (1,243.2 - 811.1)

Volume	Invert	Avail.Storage	Storage Description
#1	995.50'	75,410 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
995.50	100	0	0
996.00	1,400	375	375
997.00	4,400	2,900	3,275
1,004.00	16,210	72,135	75,410

Device	Routing	Invert	Outlet Devices
#1	Primary	995.50'	18.0" Round Culvert L= 48.3' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 995.50' / 995.00' S= 0.0104 '/' Cc= 0.900 n= 0.013, Flow Area= 1.77 sf
#2	Device 1	995.50'	1.5" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	998.50'	12.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	999.20'	15.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#5	Device 1	1,002.00'	288.0" W x 6.0" H Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=1.70 cfs @ 12.36 hrs HW=999.20' (Free Discharge)

- ↑1=Culvert (Passes 1.70 cfs of 14.61 cfs potential flow)
 ↑2=Orifice/Grate (Orifice Controls 0.11 cfs @ 9.18 fps)
 ↑3=Orifice/Grate (Orifice Controls 1.59 cfs @ 3.18 fps)
 ↑4=Orifice/Grate (Controls 0.00 cfs)
 ↑5=Orifice/Grate (Controls 0.00 cfs)

Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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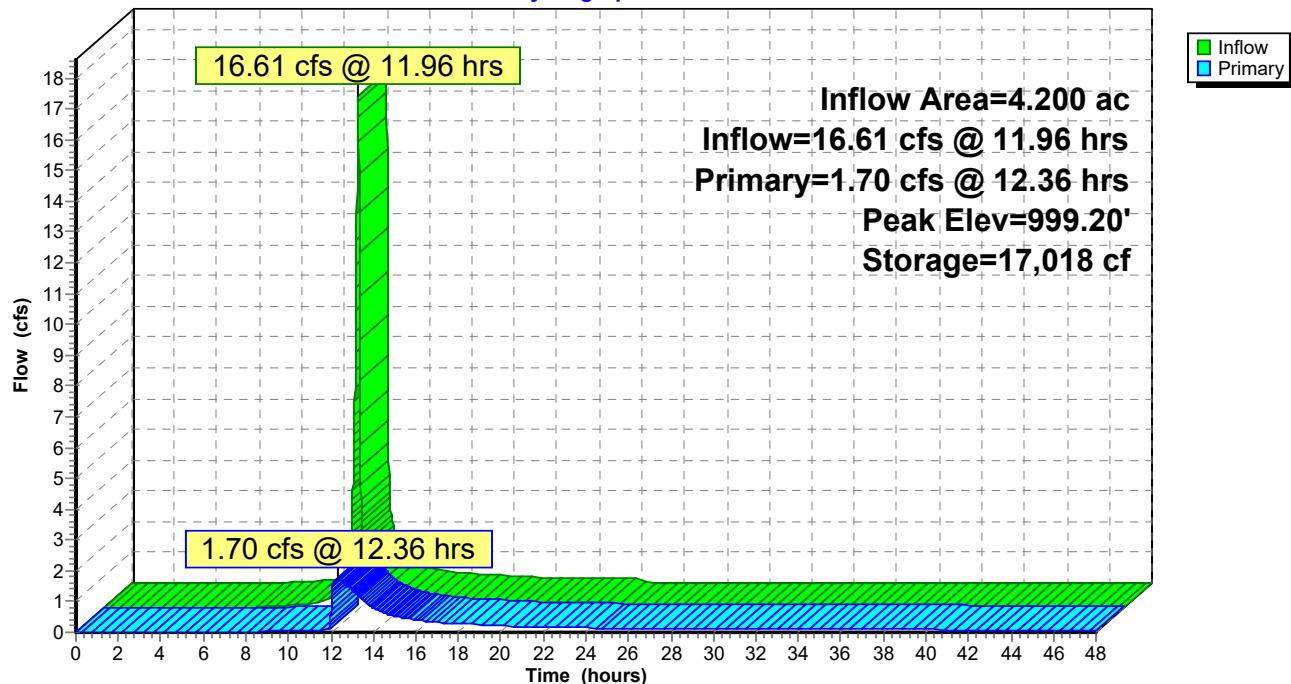
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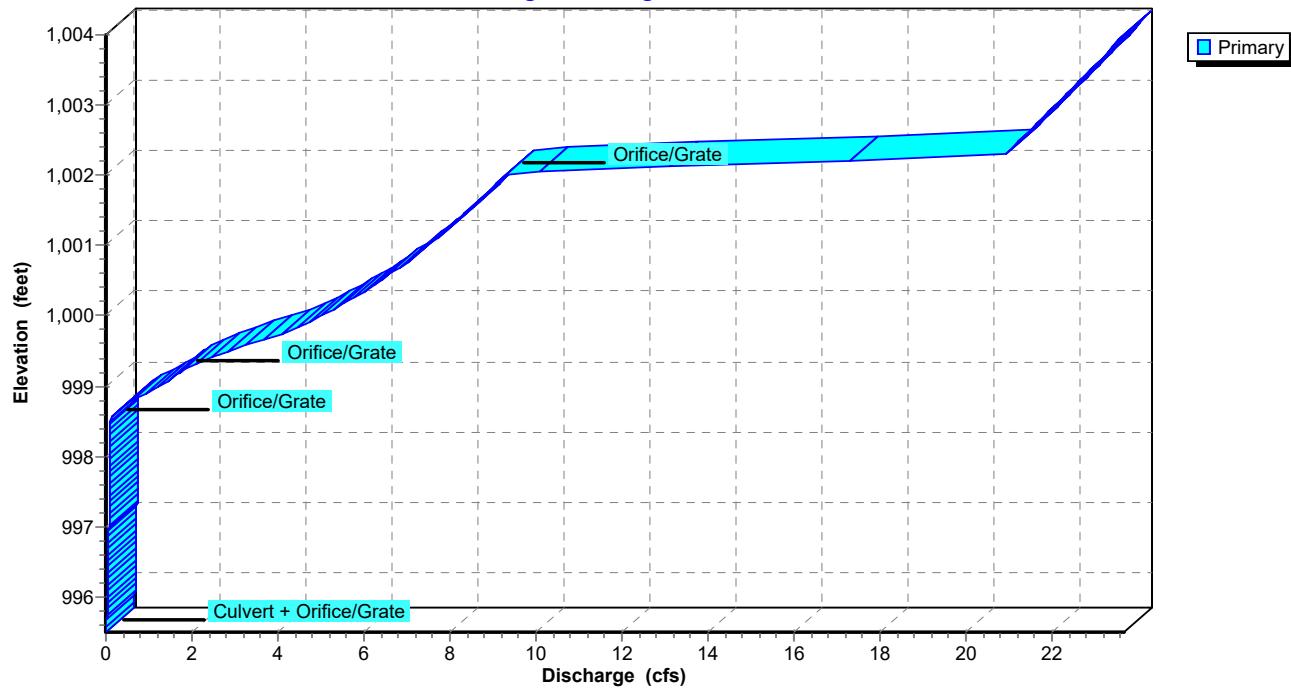
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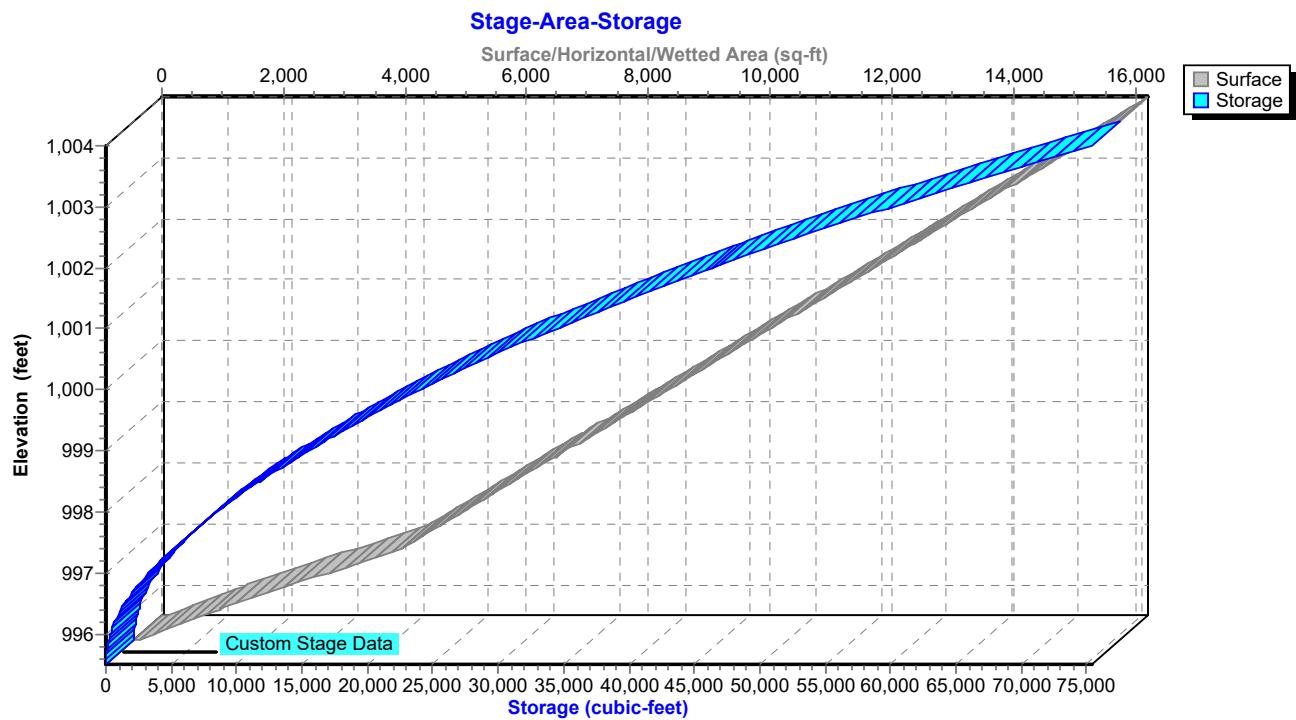
Pond 1P: Proposed Detention

Hydrograph

**Pond 1P: Proposed Detention**

Stage-Discharge



Pond 1P: Proposed Detention

Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Hydrograph for Pond 1P: Proposed Detention

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
0.00	0.00	0	995.50	0.00
1.00	0.00	0	995.50	0.00
2.00	0.00	0	995.50	0.00
3.00	0.00	0	995.50	0.00
4.00	0.00	0	995.50	0.00
5.00	0.00	0	995.50	0.00
6.00	0.00	0	995.50	0.00
7.00	0.02	13	995.56	0.01
8.00	0.04	70	995.69	0.02
9.00	0.11	231	995.88	0.03
10.00	0.19	586	996.13	0.04
11.00	0.45	1,466	996.51	0.06
12.00	14.10	14,143	998.83	0.71
13.00	0.82	15,918	999.06	1.40
14.00	0.49	14,356	998.86	0.80
15.00	0.39	13,624	998.76	0.53
16.00	0.31	13,223	998.70	0.40
17.00	0.27	12,952	998.67	0.33
18.00	0.24	12,786	998.64	0.28
19.00	0.21	12,641	998.62	0.25
20.00	0.17	12,494	998.60	0.22
21.00	0.17	12,378	998.59	0.19
22.00	0.16	12,309	998.58	0.18
23.00	0.15	12,262	998.57	0.16
24.00	0.15	12,225	998.56	0.16
25.00	0.00	11,800	998.50	0.10
26.00	0.00	11,436	998.45	0.10
27.00	0.00	11,076	998.40	0.10
28.00	0.00	10,720	998.34	0.10
29.00	0.00	10,367	998.29	0.10
30.00	0.00	10,017	998.24	0.10
31.00	0.00	9,671	998.18	0.10
32.00	0.00	9,328	998.13	0.09
33.00	0.00	8,989	998.08	0.09
34.00	0.00	8,654	998.02	0.09
35.00	0.00	8,322	997.97	0.09
36.00	0.00	7,994	997.91	0.09
37.00	0.00	7,670	997.86	0.09
38.00	0.00	7,350	997.80	0.09
39.00	0.00	7,033	997.75	0.09
40.00	0.00	6,721	997.69	0.09
41.00	0.00	6,412	997.64	0.09
42.00	0.00	6,108	997.58	0.08
43.00	0.00	5,808	997.52	0.08
44.00	0.00	5,513	997.47	0.08
45.00	0.00	5,221	997.41	0.08
46.00	0.00	4,934	997.35	0.08
47.00	0.00	4,652	997.30	0.08
48.00	0.00	4,374	997.24	0.08

Proposed

Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Stage-Discharge for Pond 1P: Proposed Detention

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
995.50	0.00	998.15	0.10	1,000.80	7.07	1,003.45	22.83
995.55	0.00	998.20	0.10	1,000.85	7.18	1,003.50	22.91
995.60	0.01	998.25	0.10	1,000.90	7.28	1,003.55	22.99
995.65	0.02	998.30	0.10	1,000.95	7.39	1,003.60	23.07
995.70	0.02	998.35	0.10	1,001.00	7.49	1,003.65	23.15
995.75	0.03	998.40	0.10	1,001.05	7.59	1,003.70	23.22
995.80	0.03	998.45	0.10	1,001.10	7.69	1,003.75	23.30
995.85	0.03	998.50	0.10	1,001.15	7.79	1,003.80	23.38
995.90	0.03	998.55	0.14	1,001.20	7.88	1,003.85	23.46
995.95	0.04	998.60	0.20	1,001.25	7.98	1,003.90	23.53
996.00	0.04	998.65	0.29	1,001.30	8.07	1,003.95	23.61
996.05	0.04	998.70	0.39	1,001.35	8.17	1,004.00	23.69
996.10	0.04	998.75	0.51	1,001.40	8.26		
996.15	0.05	998.80	0.63	1,001.45	8.35		
996.20	0.05	998.85	0.77	1,001.50	8.44		
996.25	0.05	998.90	0.92	1,001.55	8.53		
996.30	0.05	998.95	1.08	1,001.60	8.62		
996.35	0.05	999.00	1.24	1,001.65	8.71		
996.40	0.05	999.05	1.38	1,001.70	8.79		
996.45	0.06	999.10	1.50	1,001.75	8.88		
996.50	0.06	999.15	1.61	1,001.80	8.96		
996.55	0.06	999.20	1.71	1,001.85	9.05		
996.60	0.06	999.25	1.84	1,001.90	9.13		
996.65	0.06	999.30	2.01	1,001.95	9.21		
996.70	0.06	999.35	2.20	1,002.00	9.29		
996.75	0.06	999.40	2.40	1,002.05	10.23		
996.80	0.07	999.45	2.62	1,002.10	11.89		
996.85	0.07	999.50	2.85	1,002.15	14.01		
996.90	0.07	999.55	3.09	1,002.20	16.50		
996.95	0.07	999.60	3.35	1,002.25	19.32		
997.00	0.07	999.65	3.61	1,002.30	20.93		
997.05	0.07	999.70	3.88	1,002.35	21.02		
997.10	0.07	999.75	4.11	1,002.40	21.10		
997.15	0.07	999.80	4.32	1,002.45	21.19		
997.20	0.08	999.85	4.51	1,002.50	21.27		
997.25	0.08	999.90	4.69	1,002.55	21.36		
997.30	0.08	999.95	4.86	1,002.60	21.44		
997.35	0.08	1,000.00	5.02	1,002.65	21.53		
997.40	0.08	1,000.05	5.18	1,002.70	21.61		
997.45	0.08	1,000.10	5.33	1,002.75	21.69		
997.50	0.08	1,000.15	5.48	1,002.80	21.78		
997.55	0.08	1,000.20	5.62	1,002.85	21.86		
997.60	0.08	1,000.25	5.75	1,002.90	21.94		
997.65	0.09	1,000.30	5.89	1,002.95	22.02		
997.70	0.09	1,000.35	6.02	1,003.00	22.11		
997.75	0.09	1,000.40	6.14	1,003.05	22.19		
997.80	0.09	1,000.45	6.27	1,003.10	22.27		
997.85	0.09	1,000.50	6.39	1,003.15	22.35		
997.90	0.09	1,000.55	6.51	1,003.20	22.43		
997.95	0.09	1,000.60	6.63	1,003.25	22.51		
998.00	0.09	1,000.65	6.74	1,003.30	22.59		
998.05	0.09	1,000.70	6.85	1,003.35	22.67		
998.10	0.09	1,000.75	6.96	1,003.40	22.75		

Proposed

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Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Stage-Area-Storage for Pond 1P: Proposed Detention

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
995.50	100	0	1,000.80	10,811	32,176
995.60	360	23	1,000.90	10,980	33,266
995.70	620	72	1,001.00	11,149	34,372
995.80	880	147	1,001.10	11,317	35,495
995.90	1,140	248	1,001.20	11,486	36,636
996.00	1,400	375	1,001.30	11,655	37,793
996.10	1,700	530	1,001.40	11,823	38,967
996.20	2,000	715	1,001.50	11,992	40,157
996.30	2,300	930	1,001.60	12,161	41,365
996.40	2,600	1,175	1,001.70	12,330	42,589
996.50	2,900	1,450	1,001.80	12,498	43,831
996.60	3,200	1,755	1,001.90	12,667	45,089
996.70	3,500	2,090	1,002.00	12,836	46,364
996.80	3,800	2,455	1,002.10	13,004	47,656
996.90	4,100	2,850	1,002.20	13,173	48,965
997.00	4,400	3,275	1,002.30	13,342	50,291
997.10	4,569	3,723	1,002.40	13,511	51,634
997.20	4,737	4,189	1,002.50	13,679	52,993
997.30	4,906	4,671	1,002.60	13,848	54,369
997.40	5,075	5,170	1,002.70	14,017	55,763
997.50	5,244	5,686	1,002.80	14,185	57,173
997.60	5,412	6,219	1,002.90	14,354	58,600
997.70	5,581	6,768	1,003.00	14,523	60,044
997.80	5,750	7,335	1,003.10	14,692	61,504
997.90	5,918	7,918	1,003.20	14,860	62,982
998.00	6,087	8,519	1,003.30	15,029	64,476
998.10	6,256	9,136	1,003.40	15,198	65,988
998.20	6,425	9,770	1,003.50	15,366	67,516
998.30	6,593	10,421	1,003.60	15,535	69,061
998.40	6,762	11,088	1,003.70	15,704	70,623
998.50	6,931	11,773	1,003.80	15,873	72,202
998.60	7,099	12,475	1,003.90	16,041	73,797
998.70	7,268	13,193	1,004.00	16,210	75,410
998.80	7,437	13,928			
998.90	7,606	14,680			
999.00	7,774	15,449			
999.10	7,943	16,235			
999.20	8,112	17,038			
999.30	8,280	17,857			
999.40	8,449	18,694			
999.50	8,618	19,547			
999.60	8,787	20,418			
999.70	8,955	21,305			
999.80	9,124	22,209			
999.90	9,293	23,129			
1,000.00	9,461	24,067			
1,000.10	9,630	25,022			
1,000.20	9,799	25,993			
1,000.30	9,968	26,981			
1,000.40	10,136	27,987			
1,000.50	10,305	29,009			
1,000.60	10,474	30,048			
1,000.70	10,642	31,103			

Summary for Link 1L: Proposed Total

Inflow Area = 5.030 ac, 46.32% Impervious, Inflow Depth > 1.79" for Jackson - 2 YR event

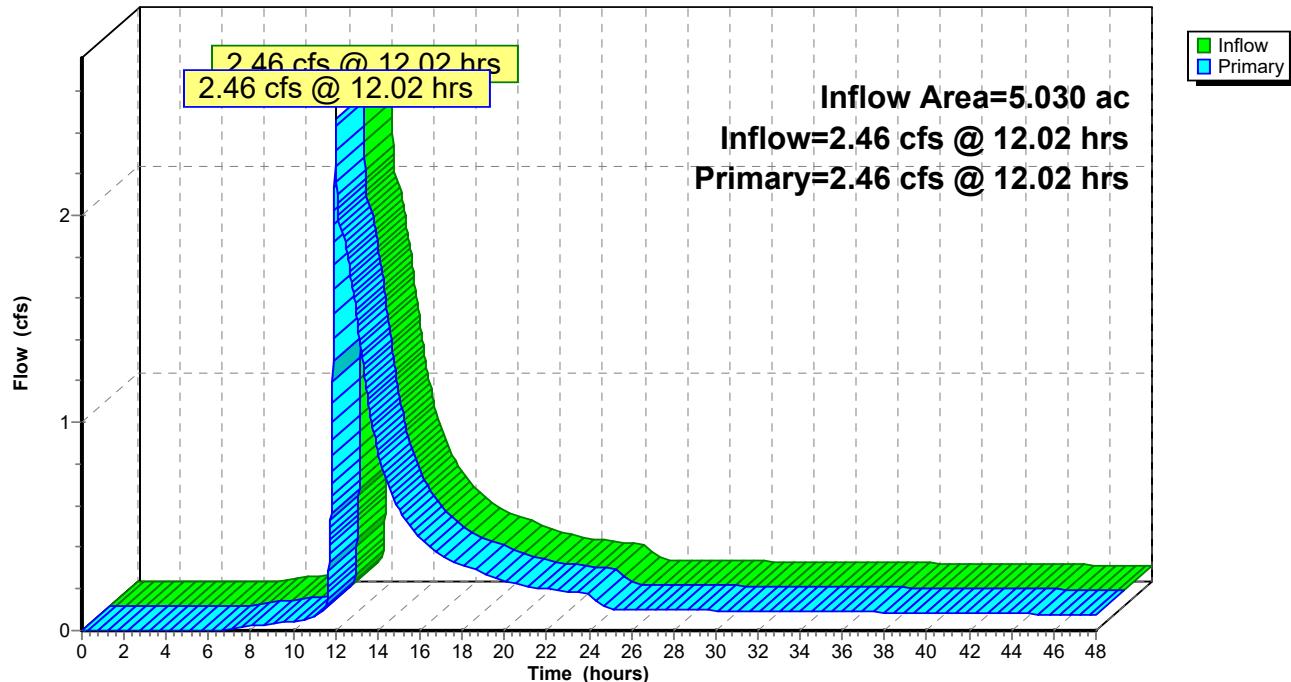
Inflow = 2.46 cfs @ 12.02 hrs, Volume= 0.749 af

Primary = 2.46 cfs @ 12.02 hrs, Volume= 0.749 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Link 1L: Proposed Total

Hydrograph



Proposed

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Type II 24-hr Jackson - 2 YR Rainfall=3.50"

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Hydrograph for Link 1L: Proposed Total

Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Primary (cfs)
0.00	0.00	0.00	0.00	26.50	0.10	0.00	0.10
0.50	0.00	0.00	0.00	27.00	0.10	0.00	0.10
1.00	0.00	0.00	0.00	27.50	0.10	0.00	0.10
1.50	0.00	0.00	0.00	28.00	0.10	0.00	0.10
2.00	0.00	0.00	0.00	28.50	0.10	0.00	0.10
2.50	0.00	0.00	0.00	29.00	0.10	0.00	0.10
3.00	0.00	0.00	0.00	29.50	0.10	0.00	0.10
3.50	0.00	0.00	0.00	30.00	0.10	0.00	0.10
4.00	0.00	0.00	0.00	30.50	0.10	0.00	0.10
4.50	0.00	0.00	0.00	31.00	0.10	0.00	0.10
5.00	0.00	0.00	0.00	31.50	0.10	0.00	0.10
5.50	0.00	0.00	0.00	32.00	0.09	0.00	0.09
6.00	0.00	0.00	0.00	32.50	0.09	0.00	0.09
6.50	0.00	0.00	0.00	33.00	0.09	0.00	0.09
7.00	0.01	0.00	0.01	33.50	0.09	0.00	0.09
7.50	0.01	0.00	0.01	34.00	0.09	0.00	0.09
8.00	0.02	0.00	0.02	34.50	0.09	0.00	0.09
8.50	0.03	0.00	0.03	35.00	0.09	0.00	0.09
9.00	0.03	0.00	0.03	35.50	0.09	0.00	0.09
9.50	0.04	0.00	0.04	36.00	0.09	0.00	0.09
10.00	0.04	0.00	0.04	36.50	0.09	0.00	0.09
10.50	0.05	0.00	0.05	37.00	0.09	0.00	0.09
11.00	0.07	0.00	0.07	37.50	0.09	0.00	0.09
11.50	0.11	0.00	0.11	38.00	0.09	0.00	0.09
12.00	2.41	0.00	2.41	38.50	0.09	0.00	0.09
12.50	1.85	0.00	1.85	39.00	0.09	0.00	0.09
13.00	1.52	0.00	1.52	39.50	0.09	0.00	0.09
13.50	1.14	0.00	1.14	40.00	0.09	0.00	0.09
14.00	0.86	0.00	0.86	40.50	0.09	0.00	0.09
14.50	0.69	0.00	0.69	41.00	0.09	0.00	0.09
15.00	0.59	0.00	0.59	41.50	0.08	0.00	0.08
15.50	0.51	0.00	0.51	42.00	0.08	0.00	0.08
16.00	0.45	0.00	0.45	42.50	0.08	0.00	0.08
16.50	0.40	0.00	0.40	43.00	0.08	0.00	0.08
17.00	0.37	0.00	0.37	43.50	0.08	0.00	0.08
17.50	0.34	0.00	0.34	44.00	0.08	0.00	0.08
18.00	0.31	0.00	0.31	44.50	0.08	0.00	0.08
18.50	0.30	0.00	0.30	45.00	0.08	0.00	0.08
19.00	0.28	0.00	0.28	45.50	0.08	0.00	0.08
19.50	0.26	0.00	0.26	46.00	0.08	0.00	0.08
20.00	0.24	0.00	0.24	46.50	0.08	0.00	0.08
20.50	0.23	0.00	0.23	47.00	0.08	0.00	0.08
21.00	0.21	0.00	0.21	47.50	0.08	0.00	0.08
21.50	0.21	0.00	0.21	48.00	0.08	0.00	0.08
22.00	0.20	0.00	0.20				
22.50	0.19	0.00	0.19				
23.00	0.19	0.00	0.19				
23.50	0.18	0.00	0.18				
24.00	0.18	0.00	0.18				
24.50	0.13	0.00	0.13				
25.00	0.10	0.00	0.10				
25.50	0.10	0.00	0.10				
26.00	0.10	0.00	0.10				

Proposed

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