

**STORM DRAINAGE CALCULATIONS**

**Whataburger**

1450 NE Douglas St.

Lee's Summit, MO 64086

BY

**ms consultants, inc.**  
COLUMBUS, OHIO

January 2021

## STORMWATER DRAINAGE SUMMARY

### **Whataburger**

Lee's Summit, MO

#### **CONTEXT**

The subject parcel is located in Lee's Summit, Missouri on the west side of NE Douglas St. just south of NE Mulberry St. The subject parcel is 1.39 acres and is currently an undeveloped lot. The site will be developed into a Whataburger restaurant. The proposed development will utilize an ADS Stormtech underground chamber system and outlet control structure for the site stormwater management and discharge into the existing storm structure at the northeast corner of the site following existing drainage patterns.

#### **TIME OF CONCENTRATION (T<sub>c</sub>)**

A minimum time of concentration of 5 minutes was used for both the existing and proposed time of concentration due to the minimal size of the lot and short travel time.

#### **WEIGHTED CURVE NUMBER**

Although not used due to detention requirements outlined below, the curve number for pre-development onsite conditions was determined to be 74.00 based on 1.39 acres of pasture, grassland, or range" in good condition per TR-55 method outlined in the APWA Design Criteria.

A weighted curve number was calculated for the proposed site conditions. A value of 98 was used for the impervious areas, which total 1.04 acres of the drainage area and a value of 74 was used for the areas with good grass cover which total 0.35 acres of the total drainage area. The watershed area drains via storm sewers into the proposed underground detention system and has a post development composite curve number of 92. The calculations for pre- and post-development runoff-coefficients are included in Appendix A.

#### **RAINFALL INTENSITY**

The rainfall depths and intensities were obtained from the NOAA rainfall atlas website. Rainfall intensities can be found in Appendix A.

#### **DETENTION REQUIREMENTS**

The development was designed to convey the peak discharge generated by the 1% storm per the Kansas City Metropolitan Chapter APWA Section 5600. Discharge from the developed site has been analyzed and released at rate less than 0.5 CFS per acre for the 2 year storm event, 2.0 CFS per acre for the 10 year storm, and 3.0 per acer for the 100 year.

The required detention volume generated by the overall development is contained in the proposed underground detention system. Calculations supporting the storm release and pond design can be found in Appendix B.

## UGS

Storm Event	Pre-Dev Flow (CFS)	Allowable Release Rate (CFS)	Post Dev Rate (CFS)	Pond Discharge (CFS)	Pond Surface Elevation
2-year	2.89	0.70	5.82	0.26	1009.17
10-year	6.09	2.78	9.50	1.76	1010.05
100-year	12.70	4.17	16.08	3.77	1012.97

## **STORM SEWER DESIGN**

The site consists of a proposed onsite stormwater pipe network that drains to an underground detention system, an outlet control structure, and a discharge pipe which outfalls to the existing storm system at the northeast corner of the parcel. The on-site storm sewer system has been designed using the rational method to convey the 25 year storm and checked to ensure that there will be no surcharging during a 25 year storm event. Catchment areas and drainage map can be found in Appendix C and storm sewer conveyance calculations are included in Appendix D.

## **OUTLET CONTROL STRUCTURE**

The water quality volume is controlled within the outlet control structure by a 1.4” circular orifice at elevation 1006.75. The 2 yr. - 100 yr. storm is controlled within the outlet control structure by two 6” orifices at elevation 1009.00 and a 4’ wide weir wall set within the structure at elevation 1013.00. The top of structure is elevation 1014.50 with the 100 yr. pond elevation at 1012.97. The outlet control structure can be found in the site civil plans in Appendix F.

## **WATER QUALITY**

On-site water quality requirements are being met through the use of the proposed isolator row in the UGS system and additional water quality storage volume within the underground storage systems and released through the outlet control structure. The water quality orifice on the outlet control structure has been designed to release the water quality volume over a period of 40 hours for the detention storage. The MARC/APWA BMP Manual requires a water quality volume based on the equation  $WQv = Rv \times P \times A / 12$ . The proposed site has provide 0.11 acre-feet of water quality volume at an elevation of 1008.14. The calculations are included in Appendix E.

## **SUMMARY**

As indicated above and shown within the attachments, stormwater calculations have been performed using PondPack and spreadsheets to meet the city of Lee’s Summit, Missouri Design Criteria including using 30% stone voids for the UGS instead of the industry standard of 40% and does not exceed the post development allowable release rates using comprehensive control.

APPENDIX A  
CURVE NUMBER VALUES,  
& RAINFALL DATA

**PondPack Pond Routing Input (UGS)**

**PROJECT:**

Whataburger

**Drainage Area:**

1.39 acres

**Existing Conditions: Analysis Boundary**

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN
Open Space - Meadow	C	60,461	1.39	74
Woods - Good Condition	-	0	0.00	77
Gravel	-	0	0.00	91
Impervious	-	0	0.00	98
<b>TOTAL:</b>		60,461	1.39	74

**Developed Conditions: Analysis Boundary**

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN
Open Space - Good Condition	C	15,307	0.35	74
Woods	-	0	0.00	77
Gravel	-	0	0.00	91
Impervious Area	C	45,145	1.04	98
<b>TOTAL</b>		60,452	1.39	92



**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Lees Summit, Missouri, USA\***  
**Latitude: 38.9425°, Longitude: -94.3752°**  
**Elevation: 999.68 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

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**PF tabular**

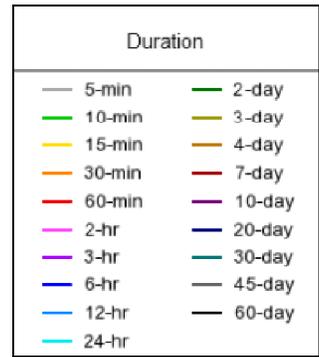
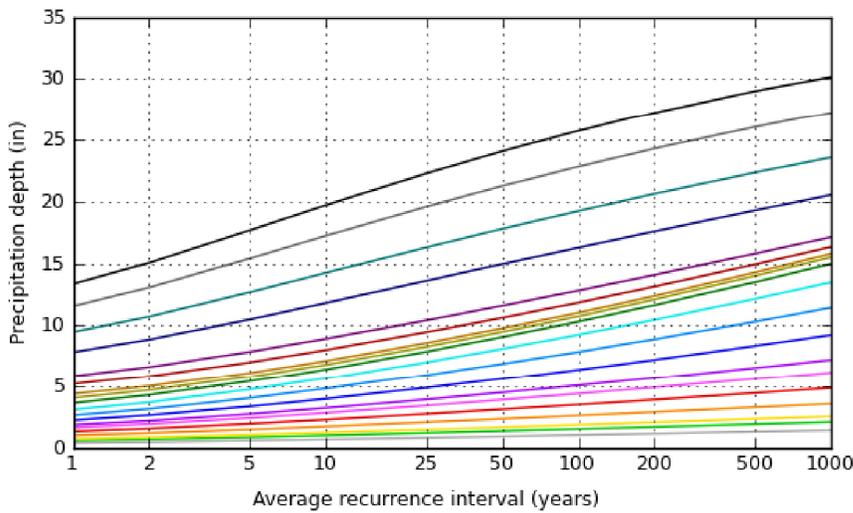
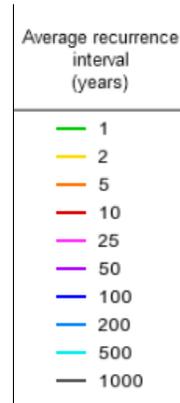
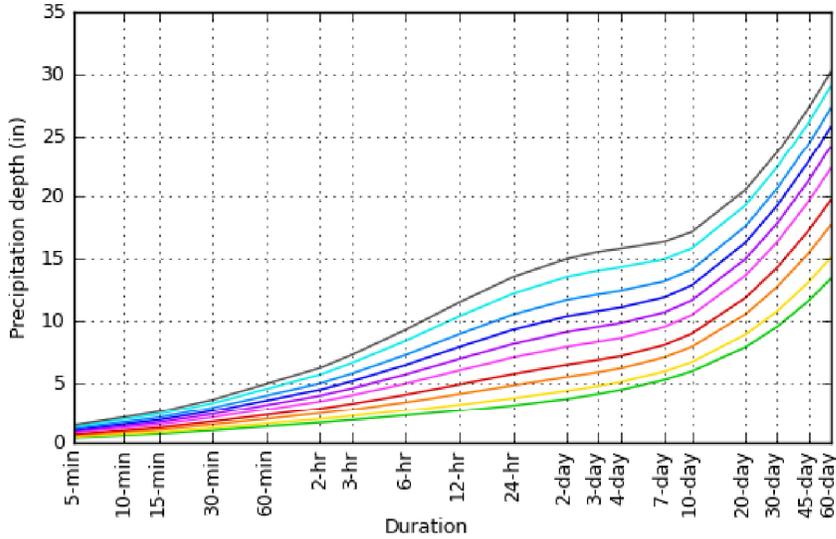
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.414</b> (0.330-0.516)	<b>0.483</b> (0.384-0.602)	<b>0.597</b> (0.474-0.746)	<b>0.694</b> (0.548-0.870)	<b>0.831</b> (0.636-1.07)	<b>0.939</b> (0.703-1.23)	<b>1.05</b> (0.761-1.40)	<b>1.16</b> (0.812-1.59)	<b>1.32</b> (0.887-1.85)	<b>1.44</b> (0.944-2.04)
<b>10-min</b>	<b>0.607</b> (0.483-0.756)	<b>0.707</b> (0.563-0.881)	<b>0.874</b> (0.694-1.09)	<b>1.02</b> (0.802-1.27)	<b>1.22</b> (0.932-1.57)	<b>1.38</b> (1.03-1.80)	<b>1.54</b> (1.12-2.05)	<b>1.70</b> (1.19-2.33)	<b>1.93</b> (1.30-2.71)	<b>2.10</b> (1.38-2.99)
<b>15-min</b>	<b>0.740</b> (0.589-0.921)	<b>0.862</b> (0.686-1.07)	<b>1.07</b> (0.846-1.33)	<b>1.24</b> (0.978-1.55)	<b>1.48</b> (1.14-1.92)	<b>1.68</b> (1.26-2.19)	<b>1.87</b> (1.36-2.50)	<b>2.08</b> (1.45-2.84)	<b>2.35</b> (1.59-3.30)	<b>2.57</b> (1.69-3.65)
<b>30-min</b>	<b>1.02</b> (0.817-1.28)	<b>1.20</b> (0.956-1.50)	<b>1.49</b> (1.18-1.87)	<b>1.74</b> (1.37-2.18)	<b>2.09</b> (1.60-2.69)	<b>2.36</b> (1.77-3.08)	<b>2.63</b> (1.91-3.52)	<b>2.92</b> (2.04-3.99)	<b>3.30</b> (2.22-4.63)	<b>3.60</b> (2.36-5.11)
<b>60-min</b>	<b>1.34</b> (1.07-1.67)	<b>1.57</b> (1.25-1.96)	<b>1.96</b> (1.56-2.45)	<b>2.29</b> (1.81-2.88)	<b>2.77</b> (2.12-3.58)	<b>3.14</b> (2.35-4.11)	<b>3.52</b> (2.56-4.71)	<b>3.92</b> (2.74-5.37)	<b>4.46</b> (3.01-6.26)	<b>4.89</b> (3.21-6.94)
<b>2-hr</b>	<b>1.65</b> (1.33-2.05)	<b>1.94</b> (1.56-2.40)	<b>2.43</b> (1.94-3.01)	<b>2.85</b> (2.26-3.55)	<b>3.44</b> (2.66-4.43)	<b>3.92</b> (2.96-5.10)	<b>4.41</b> (3.23-5.87)	<b>4.93</b> (3.47-6.71)	<b>5.63</b> (3.82-7.85)	<b>6.17</b> (4.08-8.71)
<b>3-hr</b>	<b>1.87</b> (1.50-2.30)	<b>2.20</b> (1.77-2.71)	<b>2.76</b> (2.21-3.41)	<b>3.24</b> (2.58-4.02)	<b>3.94</b> (3.06-5.06)	<b>4.51</b> (3.42-5.85)	<b>5.09</b> (3.74-6.75)	<b>5.71</b> (4.04-7.75)	<b>6.56</b> (4.47-9.12)	<b>7.22</b> (4.80-10.2)
<b>6-hr</b>	<b>2.25</b> (1.82-2.75)	<b>2.66</b> (2.15-3.26)	<b>3.37</b> (2.72-4.14)	<b>3.99</b> (3.20-4.92)	<b>4.90</b> (3.83-6.26)	<b>5.64</b> (4.30-7.28)	<b>6.40</b> (4.74-8.45)	<b>7.22</b> (5.14-9.75)	<b>8.35</b> (5.74-11.6)	<b>9.24</b> (6.18-12.9)
<b>12-hr</b>	<b>2.65</b> (2.16-3.22)	<b>3.17</b> (2.58-3.85)	<b>4.05</b> (3.29-4.94)	<b>4.83</b> (3.90-5.91)	<b>5.97</b> (4.70-7.58)	<b>6.90</b> (5.30-8.85)	<b>7.87</b> (5.86-10.3)	<b>8.90</b> (6.38-11.9)	<b>10.3</b> (7.14-14.2)	<b>11.5</b> (7.72-15.9)
<b>24-hr</b>	<b>3.11</b> (2.54-3.75)	<b>3.71</b> (3.04-4.48)	<b>4.76</b> (3.88-5.76)	<b>5.68</b> (4.61-6.90)	<b>7.02</b> (5.56-8.86)	<b>8.11</b> (6.28-10.3)	<b>9.26</b> (6.94-12.1)	<b>10.5</b> (7.56-14.0)	<b>12.2</b> (8.47-16.6)	<b>13.5</b> (9.16-18.6)
<b>2-day</b>	<b>3.66</b> (3.01-4.38)	<b>4.31</b> (3.55-5.16)	<b>5.44</b> (4.46-6.53)	<b>6.43</b> (5.25-7.76)	<b>7.89</b> (6.29-9.88)	<b>9.08</b> (7.07-11.5)	<b>10.3</b> (7.80-13.4)	<b>11.7</b> (8.48-15.4)	<b>13.5</b> (9.48-18.3)	<b>15.0</b> (10.2-20.5)
<b>3-day</b>	<b>4.06</b> (3.36-4.85)	<b>4.71</b> (3.89-5.62)	<b>5.83</b> (4.80-6.97)	<b>6.82</b> (5.59-8.19)	<b>8.29</b> (6.64-10.3)	<b>9.49</b> (7.43-12.0)	<b>10.8</b> (8.16-13.9)	<b>12.1</b> (8.85-16.0)	<b>14.0</b> (9.88-19.0)	<b>15.5</b> (10.7-21.2)
<b>4-day</b>	<b>4.40</b> (3.65-5.23)	<b>5.04</b> (4.17-5.99)	<b>6.15</b> (5.08-7.33)	<b>7.13</b> (5.86-8.54)	<b>8.59</b> (6.90-10.7)	<b>9.78</b> (7.68-12.3)	<b>11.0</b> (8.41-14.2)	<b>12.4</b> (9.09-16.3)	<b>14.3</b> (10.1-19.3)	<b>15.8</b> (10.9-21.5)
<b>7-day</b>	<b>5.21</b> (4.34-6.15)	<b>5.87</b> (4.89-6.95)	<b>7.02</b> (5.83-8.32)	<b>8.02</b> (6.63-9.55)	<b>9.47</b> (7.63-11.7)	<b>10.6</b> (8.39-13.3)	<b>11.9</b> (9.07-15.1)	<b>13.2</b> (9.69-17.2)	<b>14.9</b> (10.6-20.0)	<b>16.4</b> (11.3-22.1)
<b>10-day</b>	<b>5.89</b> (4.93-6.94)	<b>6.64</b> (5.55-7.82)	<b>7.88</b> (6.56-9.30)	<b>8.93</b> (7.41-10.6)	<b>10.4</b> (8.41-12.7)	<b>11.6</b> (9.17-14.4)	<b>12.8</b> (9.83-16.2)	<b>14.1</b> (10.4-18.3)	<b>15.8</b> (11.3-21.0)	<b>17.1</b> (11.9-23.1)
<b>20-day</b>	<b>7.85</b> (6.61-9.18)	<b>8.87</b> (7.46-10.4)	<b>10.5</b> (8.81-12.3)	<b>11.8</b> (9.87-13.9)	<b>13.6</b> (11.0-16.4)	<b>15.0</b> (11.9-18.3)	<b>16.3</b> (12.5-20.4)	<b>17.6</b> (13.0-22.6)	<b>19.3</b> (13.8-25.4)	<b>20.5</b> (14.4-27.5)
<b>30-day</b>	<b>9.49</b> (8.02-11.0)	<b>10.7</b> (9.06-12.5)	<b>12.7</b> (10.7-14.8)	<b>14.3</b> (11.9-16.7)	<b>16.3</b> (13.2-19.5)	<b>17.8</b> (14.1-21.6)	<b>19.2</b> (14.8-23.9)	<b>20.6</b> (15.3-26.3)	<b>22.4</b> (16.0-29.2)	<b>23.6</b> (16.6-31.5)
<b>45-day</b>	<b>11.6</b> (9.82-13.4)	<b>13.1</b> (11.1-15.2)	<b>15.4</b> (13.0-17.9)	<b>17.2</b> (14.5-20.1)	<b>19.6</b> (15.9-23.3)	<b>21.3</b> (16.9-25.7)	<b>22.8</b> (17.6-28.2)	<b>24.3</b> (18.1-30.7)	<b>26.1</b> (18.8-33.9)	<b>27.2</b> (19.2-36.2)
<b>60-day</b>	<b>13.4</b> (11.4-15.5)	<b>15.1</b> (12.8-17.4)	<b>17.7</b> (15.0-20.5)	<b>19.7</b> (16.6-22.9)	<b>22.3</b> (18.1-26.3)	<b>24.1</b> (19.2-28.9)	<b>25.7</b> (19.9-31.6)	<b>27.2</b> (20.3-34.3)	<b>29.0</b> (20.9-37.5)	<b>30.2</b> (21.4-40.0)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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### PF graphical

PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 38.9425°, Longitude: -94.3752°



### Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



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1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Lees Summit, Missouri, USA\***  
**Latitude: 38.9391°, Longitude: -94.3793°**  
**Elevation: 1017.4 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

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**PF tabular**

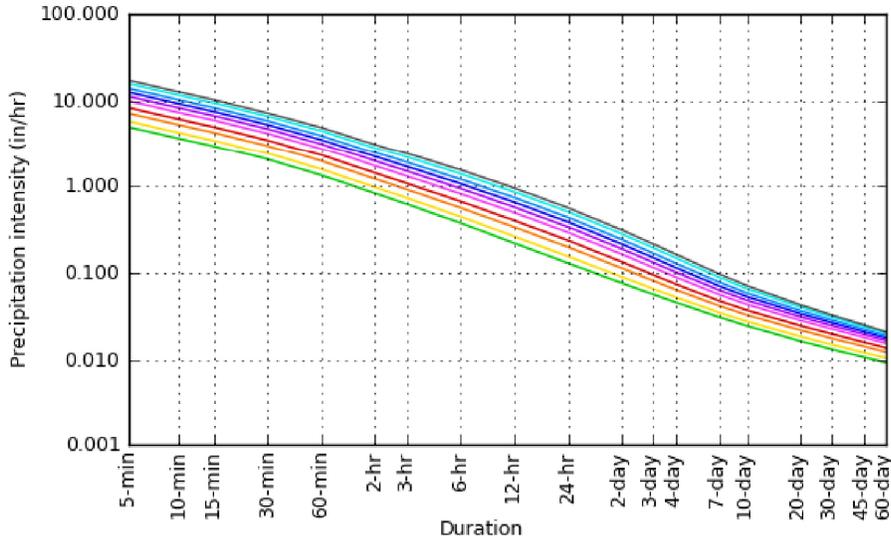
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>4.97</b> (4.00-6.13)	<b>5.80</b> (4.66-7.15)	<b>7.16</b> (5.74-8.86)	<b>8.33</b> (6.62-10.3)	<b>9.97</b> (7.69-12.8)	<b>11.3</b> (8.50-14.6)	<b>12.6</b> (9.19-16.7)	<b>14.0</b> (9.79-18.9)	<b>15.8</b> (10.7-22.0)	<b>17.3</b> (11.4-24.3)
<b>10-min</b>	<b>3.64</b> (2.93-4.49)	<b>4.24</b> (3.41-5.23)	<b>5.24</b> (4.20-6.49)	<b>6.10</b> (4.85-7.57)	<b>7.30</b> (5.63-9.34)	<b>8.25</b> (6.22-10.7)	<b>9.22</b> (6.73-12.2)	<b>10.2</b> (7.17-13.9)	<b>11.6</b> (7.83-16.1)	<b>12.6</b> (8.32-17.8)
<b>15-min</b>	<b>2.96</b> (2.38-3.65)	<b>3.45</b> (2.77-4.26)	<b>4.26</b> (3.41-5.28)	<b>4.96</b> (3.95-6.16)	<b>5.94</b> (4.58-7.60)	<b>6.71</b> (5.06-8.69)	<b>7.50</b> (5.47-9.92)	<b>8.31</b> (5.83-11.3)	<b>9.42</b> (6.36-13.1)	<b>10.3</b> (6.77-14.5)
<b>30-min</b>	<b>2.05</b> (1.65-2.53)	<b>2.40</b> (1.93-2.96)	<b>2.99</b> (2.39-3.69)	<b>3.48</b> (2.77-4.32)	<b>4.17</b> (3.22-5.34)	<b>4.71</b> (3.56-6.10)	<b>5.27</b> (3.84-6.97)	<b>5.84</b> (4.09-7.92)	<b>6.61</b> (4.46-9.18)	<b>7.20</b> (4.74-10.1)
<b>60-min</b>	<b>1.34</b> (1.08-1.65)	<b>1.57</b> (1.26-1.94)	<b>1.96</b> (1.57-2.42)	<b>2.29</b> (1.83-2.85)	<b>2.76</b> (2.13-3.54)	<b>3.14</b> (2.37-4.07)	<b>3.52</b> (2.57-4.67)	<b>3.92</b> (2.75-5.33)	<b>4.47</b> (3.02-6.22)	<b>4.89</b> (3.22-6.89)
<b>2-hr</b>	<b>0.826</b> (0.668-1.01)	<b>0.970</b> (0.784-1.19)	<b>1.21</b> (0.977-1.49)	<b>1.42</b> (1.14-1.76)	<b>1.72</b> (1.34-2.19)	<b>1.96</b> (1.49-2.53)	<b>2.21</b> (1.62-2.91)	<b>2.46</b> (1.74-3.33)	<b>2.82</b> (1.92-3.90)	<b>3.09</b> (2.05-4.33)
<b>3-hr</b>	<b>0.622</b> (0.504-0.759)	<b>0.731</b> (0.592-0.893)	<b>0.917</b> (0.741-1.12)	<b>1.08</b> (0.867-1.33)	<b>1.31</b> (1.02-1.67)	<b>1.50</b> (1.15-1.93)	<b>1.70</b> (1.25-2.23)	<b>1.90</b> (1.35-2.56)	<b>2.19</b> (1.49-3.01)	<b>2.41</b> (1.60-3.36)
<b>6-hr</b>	<b>0.376</b> (0.306-0.455)	<b>0.445</b> (0.362-0.539)	<b>0.563</b> (0.457-0.684)	<b>0.667</b> (0.539-0.814)	<b>0.818</b> (0.643-1.04)	<b>0.941</b> (0.723-1.20)	<b>1.07</b> (0.795-1.40)	<b>1.21</b> (0.862-1.62)	<b>1.40</b> (0.961-1.91)	<b>1.55</b> (1.03-2.14)
<b>12-hr</b>	<b>0.220</b> (0.180-0.265)	<b>0.263</b> (0.215-0.317)	<b>0.336</b> (0.275-0.406)	<b>0.401</b> (0.326-0.486)	<b>0.496</b> (0.392-0.624)	<b>0.572</b> (0.442-0.728)	<b>0.653</b> (0.488-0.849)	<b>0.738</b> (0.531-0.983)	<b>0.857</b> (0.594-1.17)	<b>0.951</b> (0.642-1.31)
<b>24-hr</b>	<b>0.129</b> (0.107-0.155)	<b>0.155</b> (0.127-0.185)	<b>0.198</b> (0.163-0.238)	<b>0.237</b> (0.193-0.285)	<b>0.292</b> (0.233-0.366)	<b>0.338</b> (0.263-0.427)	<b>0.386</b> (0.290-0.498)	<b>0.436</b> (0.316-0.577)	<b>0.506</b> (0.353-0.686)	<b>0.562</b> (0.382-0.768)
<b>2-day</b>	<b>0.076</b> (0.063-0.090)	<b>0.090</b> (0.074-0.107)	<b>0.113</b> (0.093-0.135)	<b>0.134</b> (0.110-0.160)	<b>0.164</b> (0.131-0.204)	<b>0.189</b> (0.148-0.237)	<b>0.215</b> (0.163-0.275)	<b>0.242</b> (0.177-0.318)	<b>0.281</b> (0.198-0.378)	<b>0.311</b> (0.213-0.423)
<b>3-day</b>	<b>0.056</b> (0.047-0.067)	<b>0.065</b> (0.054-0.077)	<b>0.081</b> (0.067-0.096)	<b>0.095</b> (0.078-0.113)	<b>0.115</b> (0.092-0.142)	<b>0.132</b> (0.103-0.165)	<b>0.149</b> (0.114-0.191)	<b>0.168</b> (0.123-0.220)	<b>0.194</b> (0.137-0.260)	<b>0.215</b> (0.148-0.291)
<b>4-day</b>	<b>0.046</b> (0.038-0.054)	<b>0.052</b> (0.044-0.062)	<b>0.064</b> (0.053-0.076)	<b>0.074</b> (0.061-0.088)	<b>0.089</b> (0.072-0.110)	<b>0.102</b> (0.080-0.127)	<b>0.115</b> (0.088-0.146)	<b>0.129</b> (0.095-0.168)	<b>0.149</b> (0.105-0.199)	<b>0.164</b> (0.113-0.222)
<b>7-day</b>	<b>0.031</b> (0.026-0.036)	<b>0.035</b> (0.029-0.041)	<b>0.042</b> (0.035-0.049)	<b>0.048</b> (0.040-0.056)	<b>0.056</b> (0.046-0.069)	<b>0.063</b> (0.050-0.078)	<b>0.070</b> (0.054-0.089)	<b>0.078</b> (0.058-0.101)	<b>0.089</b> (0.063-0.118)	<b>0.097</b> (0.067-0.130)
<b>10-day</b>	<b>0.025</b> (0.021-0.029)	<b>0.028</b> (0.023-0.032)	<b>0.033</b> (0.027-0.038)	<b>0.037</b> (0.031-0.044)	<b>0.043</b> (0.035-0.053)	<b>0.048</b> (0.038-0.059)	<b>0.053</b> (0.041-0.067)	<b>0.059</b> (0.043-0.075)	<b>0.066</b> (0.047-0.087)	<b>0.071</b> (0.050-0.095)
<b>20-day</b>	<b>0.016</b> (0.014-0.019)	<b>0.018</b> (0.016-0.021)	<b>0.022</b> (0.018-0.025)	<b>0.025</b> (0.021-0.029)	<b>0.028</b> (0.023-0.034)	<b>0.031</b> (0.025-0.038)	<b>0.034</b> (0.026-0.042)	<b>0.037</b> (0.027-0.047)	<b>0.040</b> (0.029-0.052)	<b>0.043</b> (0.030-0.057)
<b>30-day</b>	<b>0.013</b> (0.011-0.015)	<b>0.015</b> (0.013-0.017)	<b>0.018</b> (0.015-0.020)	<b>0.020</b> (0.017-0.023)	<b>0.023</b> (0.018-0.027)	<b>0.025</b> (0.020-0.030)	<b>0.027</b> (0.021-0.033)	<b>0.029</b> (0.021-0.036)	<b>0.031</b> (0.022-0.040)	<b>0.033</b> (0.023-0.043)
<b>45-day</b>	<b>0.011</b> (0.009-0.012)	<b>0.012</b> (0.010-0.014)	<b>0.014</b> (0.012-0.016)	<b>0.016</b> (0.013-0.018)	<b>0.018</b> (0.015-0.021)	<b>0.020</b> (0.016-0.024)	<b>0.021</b> (0.016-0.026)	<b>0.022</b> (0.017-0.028)	<b>0.024</b> (0.017-0.031)	<b>0.025</b> (0.018-0.033)
<b>60-day</b>	<b>0.009</b> (0.008-0.011)	<b>0.010</b> (0.009-0.012)	<b>0.012</b> (0.010-0.014)	<b>0.014</b> (0.012-0.016)	<b>0.015</b> (0.013-0.018)	<b>0.017</b> (0.013-0.020)	<b>0.018</b> (0.014-0.022)	<b>0.019</b> (0.014-0.024)	<b>0.020</b> (0.015-0.026)	<b>0.021</b> (0.015-0.028)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

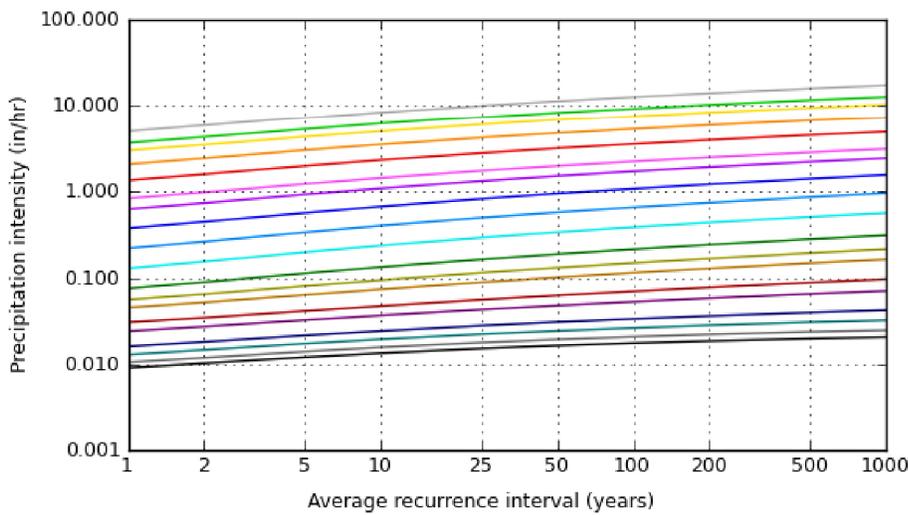
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### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
 Latitude: 38.9391°, Longitude: -94.3793°



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration	
5-min	2-day
10-min	3-day
15-min	4-day
30-min	7-day
60-min	10-day
2-hr	20-day
3-hr	30-day
6-hr	45-day
12-hr	60-day
24-hr	

### Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



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[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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Job Description: **Whataburger**

Job No: 62-40497

Computed By: JML

Date: 1/21/2021

Checked By:

Date:

**POST CONSTRUCTION STORMWATER MANAGEMENT SUMMARY**

**Lee's Summit NOAA - 24-Hour Rainfall Totals**

Return Period (yr)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
24-hr Depth (in)	3.70	X	5.70	X	X	9.30

**Project Peak Runoff Volume Mitigation Summary**

		UGS		
<b>Pre-Development</b>				
Project Drainage Area (ac)		1.39		
Curve Number (CN)		74		
Impervious Area (ac)		0.00		
<b>Post-Development</b>				
Project Drainage Area (ac)		1.39		
Curve Number (CN)		92		
Impervious Area (ac)		1.04		
Increase in Impervious Area (ac)		1.04		

**Project Peak Runoff Rate Mitigation Summary**

		UGS		
<b>Pre-Development</b>				
POI Drainage Area (ac)		1.39		
Curve Number (CN)		74		
Time of Concentration, $T_c$ (min.)		5.00		
<b>Post-Development</b>				
POI Drainage Area (ac)		1.39		
Curve Number (CN) to Pond		92		
Time of Concentration, $T_c$ , to Pond (mins)		5.00		

		Storm Frequency	UGS		
<b>2-yr</b>					
Pre-project Peak Runoff Rate to POI (cfs)			2.89		
Post-project Peak Runoff Rate to POI (cfs) - No Control			5.82		
Required Peak Runoff Release Rate (cfs)			0.70		
Post-project Peak Runoff Rate to POI (cfs) - Outlet Structure			0.26		
Net Change to Peak Runoff Rate to POI (cfs)			-2.63		
Release Rate Percentage at POI			9%		
<b>10-yr</b>					
Pre-project Peak Runoff Rate to POI (cfs)			6.09		
Post-project Peak Runoff Rate to POI (cfs) - No Control			9.50		
Required Peak Runoff Release Rate (cfs)			2.78		
Post-project Peak Runoff Rate to POI (cfs) - Outlet Structure			1.76		
Net Change to Peak Runoff Rate to POI (cfs)			-4.33		
Release Rate Percentage at POI			29%		
<b>100-yr</b>					
Pre-project Peak Runoff Rate to POI (cfs)			12.70		
Post-project Peak Runoff Rate to POI (cfs) - No Control			16.08		
Required Peak Runoff Release Rate (cfs)			4.17		
Post-project Peak Runoff Rate to POI (cfs) - Outlet Structure			3.77		
Net Change to Peak Runoff Rate to POI (cfs)			-8.93		
Release Rate Percentage at POI			30%		

APPENDIX B

POND DETENTION CALCULATIONS

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# Wataburger Lees Summit

Subsection: Master Network Summary

## Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft <sup>3</sup> /s)
CM-1	Pre 2 yr	2	0.160	11.950	2.89
CM-1	Post 2 yr	2	0.328	11.900	5.82
CM-1	Pre 10 yr	10	0.337	11.900	6.09
CM-1	Post 10 yr	10	0.550	11.900	9.50
CM-1	Pre 100 yr	100	0.701	11.900	12.70
CM-1	Post 100 yr	100	0.958	11.900	16.08

## Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft <sup>3</sup> /s)
O-1	Pre 2 yr	2	0.160	11.950	2.89
O-1	Post 2 yr	2	0.140	13.350	0.26
O-1	Pre 10 yr	10	0.337	11.900	6.09
O-1	Post 10 yr	10	0.355	12.150	1.76
O-1	Pre 100 yr	100	0.701	11.900	12.70
O-1	Post 100 yr	100	0.758	12.100	3.77

## Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft <sup>3</sup> /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
PO-1 (IN)	Post 2 yr	2	0.328	11.900	5.82	(N/A)	(N/A)
PO-1 (OUT)	Post 2 yr	2	0.140	13.350	0.26	1,009.17	0.210
PO-1 (IN)	Post 10 yr	10	0.550	11.900	9.50	(N/A)	(N/A)
PO-1 (OUT)	Post 10 yr	10	0.355	12.150	1.76	1,010.05	0.299
PO-1 (IN)	Post 100 yr	100	0.958	11.900	16.08	(N/A)	(N/A)
PO-1 (OUT)	Post 100 yr	100	0.758	12.100	3.77	1,012.97	0.499

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 2 years  
 Storm Event: 2 year

Storm Event	2 year
Return Event	2 years
Duration	24.000 hours
Depth	3.7 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.922 hours
Flow (Peak, Computed)	5.97 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.900 hours
Flow (Peak Interpolated Output)	5.82 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	92.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	0.9 in
Maximum Retention (Pervious, 20 percent)	0.2 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	2.8 in
Runoff Volume (Pervious)	0.328 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.328 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 2 years

Storm Event: 2 year

---

SCS Unit Hydrograph Parameters	
Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 2 years  
 Storm Event: 2 year

Storm Event	2 year
Return Event	2 years
Duration	24.000 hours
Depth	3.7 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.933 hours
Flow (Peak, Computed)	2.98 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.950 hours
Flow (Peak Interpolated Output)	2.89 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	74.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	3.5 in
Maximum Retention (Pervious, 20 percent)	0.7 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	1.4 in
Runoff Volume (Pervious)	0.160 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.160 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 2 years

Storm Event: 2 year

---

SCS Unit Hydrograph Parameters	
Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 10 years  
 Storm Event: 10 year

Storm Event	10 year
Return Event	10 years
Duration	24.000 hours
Depth	5.7 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.922 hours
Flow (Peak, Computed)	9.70 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.900 hours
Flow (Peak Interpolated Output)	9.50 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	92.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	0.9 in
Maximum Retention (Pervious, 20 percent)	0.2 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	4.8 in
Runoff Volume (Pervious)	0.550 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.550 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 10 years

Storm Event: 10 year

---

SCS Unit Hydrograph Parameters	
Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 10 years  
 Storm Event: 10 year

Storm Event	10 year
Return Event	10 years
Duration	24.000 hours
Depth	5.7 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.922 hours
Flow (Peak, Computed)	6.39 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.900 hours
Flow (Peak Interpolated Output)	6.09 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	74.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	3.5 in
Maximum Retention (Pervious, 20 percent)	0.7 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	2.9 in
Runoff Volume (Pervious)	0.337 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.337 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 10 years

Storm Event: 10 year

---

SCS Unit Hydrograph Parameters	
Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 100 years  
 Storm Event: 100 year

Storm Event	100 year
Return Event	100 years
Duration	24.000 hours
Depth	9.3 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.922 hours
Flow (Peak, Computed)	16.37 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.900 hours
Flow (Peak Interpolated Output)	16.08 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	92.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	0.9 in
Maximum Retention (Pervious, 20 percent)	0.2 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	8.3 in
Runoff Volume (Pervious)	0.959 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.958 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 100 years

Storm Event: 100 year

---

SCS Unit Hydrograph Parameters	
Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary  
 Label: CM-1

Return Event: 100 years  
 Storm Event: 100 year

Storm Event	100 year
Return Event	100 years
Duration	24.000 hours
Depth	9.3 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	1.388 acres
<hr/>	
Computational Time Increment	0.011 hours
Time to Peak (Computed)	11.922 hours
Flow (Peak, Computed)	13.13 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	11.900 hours
Flow (Peak Interpolated Output)	12.70 ft <sup>3</sup> /s
<hr/>	
<b>Drainage Area</b>	
SCS CN (Composite)	74.000
Area (User Defined)	1.388 acres
Maximum Retention (Pervious)	3.5 in
Maximum Retention (Pervious, 20 percent)	0.7 in
<hr/>	
<b>Cumulative Runoff</b>	
Cumulative Runoff Depth (Pervious)	6.1 in
Runoff Volume (Pervious)	0.702 ac-ft
<hr/>	
<b>Hydrograph Volume (Area under Hydrograph curve)</b>	
Volume	0.701 ac-ft
<hr/>	
<b>SCS Unit Hydrograph Parameters</b>	
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

## Wataburger Lees Summit

Subsection: Unit Hydrograph Summary

Label: CM-1

Return Event: 100 years

Storm Event: 100 year

---

### SCS Unit Hydrograph Parameters

---

Unit peak, qp	18.87 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

---

## Wataburger Lees Summit

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Return Event: 2 years

Storm Event: 2 year

Requested Pond Water Surface Elevations	
Minimum (Headwater)	1,006.75 ft
Increment (Headwater)	0.50 ft
Maximum (Headwater)	1,014.50 ft

### Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Orifice-Circular	Orifice - 1	Forward	Culvert - 1	1,006.75	1,014.50
Orifice-Circular	Orifice - 2	Forward	Culvert - 1	1,009.00	1,014.50
Rectangular Weir	Weir - 1	Forward	Culvert - 1	1,013.00	1,014.50
Culvert-Circular	Culvert - 1	Forward	TW	1,005.75	1,014.50
Tailwater Settings	Tailwater			(N/A)	(N/A)

## Wataburger Lees Summit

Subsection: Outlet Input Data

Return Event: 2 years

Label: Composite Outlet Structure - 1

Storm Event: 2 year

Structure ID: Orifice - 1	
Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	1,006.75 ft
Orifice Diameter	1.4 in
Orifice Coefficient	0.600
Structure ID: Orifice - 2	
Structure Type: Orifice-Circular	
Number of Openings	2
Elevation	1,009.00 ft
Orifice Diameter	6.0 in
Orifice Coefficient	0.600
Structure ID: Weir - 1	
Structure Type: Rectangular Weir	
Number of Openings	1
Elevation	1,013.00 ft
Weir Length	4.00 ft
Weir Coefficient	3.00 (ft <sup>0.5</sup> )/s
Structure ID: Culvert - 1	
Structure Type: Culvert-Circular	
Number of Barrels	1
Diameter	12.0 in
Length	53.70 ft
Length (Computed Barrel)	53.74 ft
Slope (Computed)	0.040 ft/ft
Outlet Control Data	
Manning's n	0.013
Ke	0.200
Kb	0.031
Kr	0.200
Convergence Tolerance	0.00 ft
Inlet Control Data	
Equation Form	Form 1
K	0.0045
M	2.0000
C	0.0317
Y	0.6900

## Wataburger Lees Summit

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Return Event: 2 years

Storm Event: 2 year

---

Inlet Control Data	
T1 ratio (HW/D)	1.075
T2 ratio (HW/D)	1.177
Slope Correction Factor	-0.500

---

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

---

T1 Elevation	1,006.83 ft	T1 Flow	2.75 ft <sup>3</sup> /s
T2 Elevation	1,006.93 ft	T2 Flow	3.14 ft <sup>3</sup> /s

---

## Wataburger Lees Summit

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Return Event: 2 years

Storm Event: 2 year

Structure ID: TW	
Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall
Convergence Tolerances	
Maximum Iterations	30
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft
Flow Tolerance (Minimum)	0.001 ft <sup>3</sup> /s
Flow Tolerance (Maximum)	10.000 ft <sup>3</sup> /s

## Wataburger Lees Summit

Subsection: Level Pool Pond Routing Summary  
 Label: PO-1 (IN)

Return Event: 100 years  
 Storm Event: 100 year

Infiltration			
Infiltration Method (Computed)	No Infiltration		
Initial Conditions			
Elevation (Water Surface, Initial)	1,006.75 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft <sup>3</sup> /s		
Flow (Initial Infiltration)	0.00 ft <sup>3</sup> /s		
Flow (Initial, Total)	0.00 ft <sup>3</sup> /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	16.08 ft <sup>3</sup> /s	Time to Peak (Flow, In)	11.900 hours
Flow (Peak Outlet)	3.77 ft <sup>3</sup> /s	Time to Peak (Flow, Outlet)	12.100 hours
Peak Conditions			
Elevation (Water Surface, Peak)	1,012.97 ft		
Volume (Peak)	0.499 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.958 ac-ft		
Volume (Total Infiltration)	0.000 ac-ft		
Volume (Total Outlet Outflow)	0.758 ac-ft		
Volume (Retained)	0.199 ac-ft		
Volume (Unrouted)	-0.001 ac-ft		
Error (Mass Balance)	0.1 %		

# Wataburger Lees Summit

Subsection: Pond Inflow Summary

Label: PO-1 (IN)

Return Event: 2 years

Storm Event: 2 year

## Summary for Hydrograph Addition at 'PO-1'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	CM-1

## Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (hours)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	CM-1	0.328	11.900	5.82
Flow (In)	PO-1	0.328	11.900	5.82

# Wataburger Lees Summit

Subsection: Pond Inflow Summary

Label: PO-1 (IN)

Return Event: 10 years

Storm Event: 10 year

## Summary for Hydrograph Addition at 'PO-1'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	CM-1

## Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (hours)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	CM-1	0.550	11.900	9.50
Flow (In)	PO-1	0.550	11.900	9.50

# Wataburger Lees Summit

Subsection: Pond Inflow Summary

Label: PO-1 (IN)

Return Event: 100 years

Storm Event: 100 year

## Summary for Hydrograph Addition at 'PO-1'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	CM-1

## Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (hours)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	CM-1	0.958	11.900	16.08
Flow (In)	PO-1	0.958	11.900	16.08

# Wataburger Lees Summit

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APPENDIX C  
CATCHMENT AREAS  
& DRAINAGE MAP

**Catchment Areas**

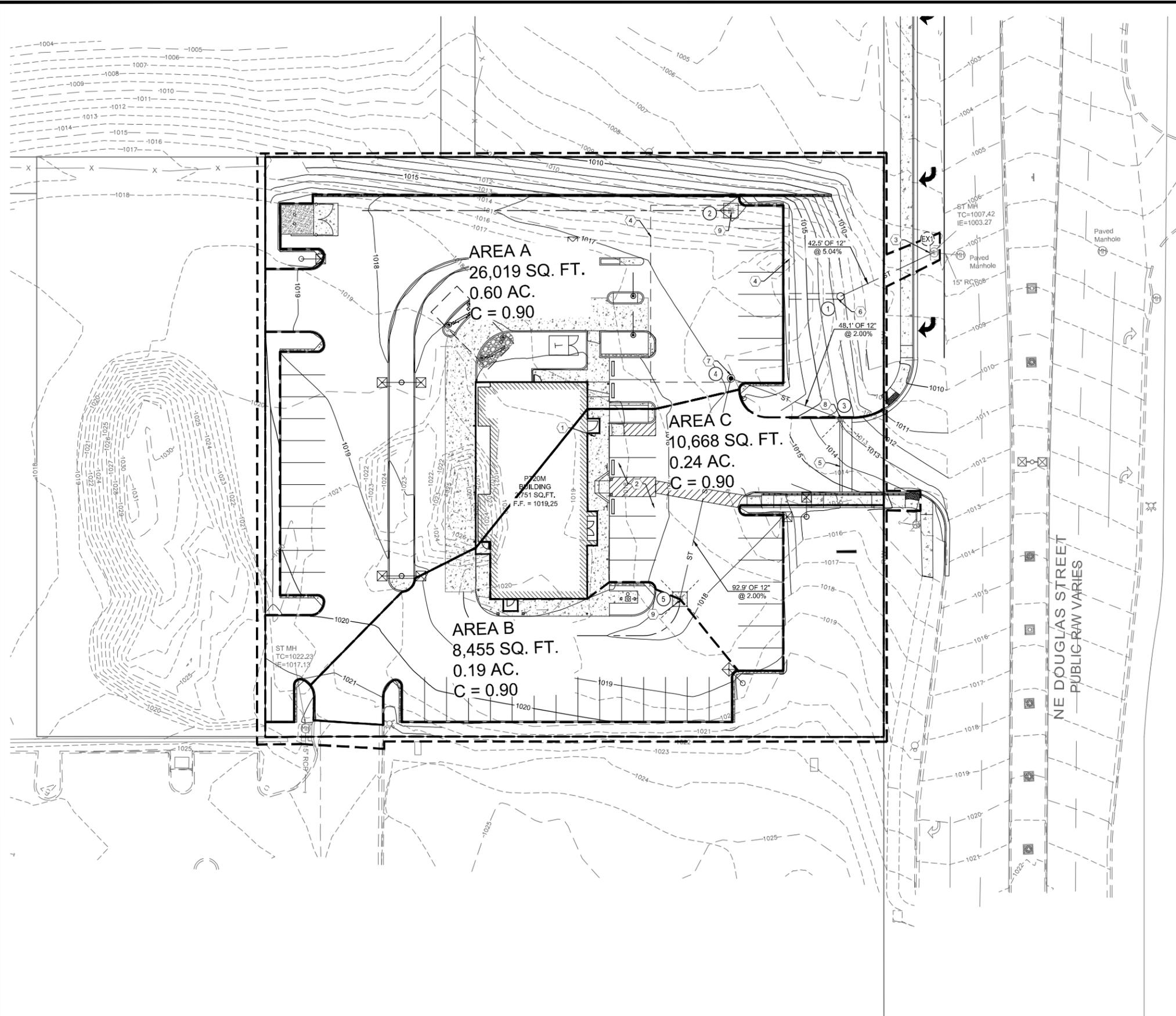
**Project Name: WB Lees Summit**

**Project Number: 62-40497**

**Date: 10/16/2020**

<b>Catchment Areas</b>			
	<b>sq.ft.</b>	<b>Ac.</b>	<b>c</b>
<b>A</b>			
Impervious	26,019	0.60	0.90
Gravel	0	0.00	0.50
Grass	0	0.00	0.30
Total	26,019	0.60	0.90
<b>B</b>			
Impervious	8,455	0.19	0.90
Gravel	0	0.00	0.50
Grass	0	0.00	0.30
Total	8,455	0.19	0.90
<b>C</b>			
Impervious	10,668	0.24	0.90
Gravel	0	0.00	0.50
Grass	0	0.00	0.30
Total	10,668	0.24	0.90

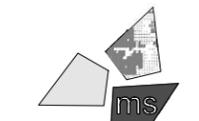
N:\03\62140497\01-Lees Summit, MO\Docs\Catcs\Civil\Storm\Catchment Areas.dwg, 12/16/2020 4:26 PM, lee\_jesse



REVISION/DATE/DESCRIPTION

60% Plan Set	10/20/20
90% Plan Set	11/17/20
100% Plan Set	12/16/20

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**ms consultants, inc.**  
 engineers, architects, planners  
 2221 Schrock Road  
 Columbus, Ohio 43229-1547  
 phone 614.898.7100  
 fax 614.898.7570

**PROJECT**  
 WHATABURGER  
 PT20M BUILDING  
 1450 NE DOUGLAS ST.  
 LEE'S SUMMIT, MO  
 64086

**SHEET TITLE**  
 CATCHMENT  
 AREA PLAN



The Missouri One Call System is a communications system which was established to help prevent damage to underground facilities and to promote safety. Missouri One Call operators are on duty 24 hours a day, seven days a week. Missouri One Call provides a telephone number for contractors and the general public to call for notification of their intent to use equipment for excavation, grading, blasting, boring, demolition or other types of similar work.

1-800-DIG-RITE or 811

MAKE THE CALL...IT'S THE LAW

DRAWN BY: LLL/AMA

CHECKED BY: KEA

PROJECT NO: 40497-01

DRAWING

CA

APPENDIX D  
STORM CONVEYANCE  
CALCULATIONS

# Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID	
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)		
1	End	92.9	0.19	0.19	0.90	0.17	0.17	5.0	5.0	9.9	1.69	5.46	4.06	12	2.00	1010.00	1011.86	1010.50	1012.41	1016.85	1017.70	5 to 4	
WB Lees Area B																Number of lines: 1				Run Date: 12/16/2020			
NOTES: Intensity = 37.95 / (Inlet time + 3.40) ^ 0.63; Return period = Yrs. 25 ; c = cir e = ellip b = box																							

# Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID	
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)		
1	End	48.0	0.24	0.24	0.90	0.22	0.22	5.0	5.0	9.9	2.14	5.46	4.13	12	2.00	1010.00	1010.96	1010.63	1011.59	1016.85	1013.00	3 to 4	
WB Lees Area C																Number of lines: 1				Run Date: 3/3/2021			
NOTES: Intensity = $37.95 / (\text{Inlet time} + 3.40)^{0.63}$ ; Return period = Yrs. 25 ; c = cir e = ellip b = box																							

APPENDIX E  
WATER QUALITY CALCULATION

**WATER QUALITY VOLUME CALCULATIONS- Drainage Area into Pond**

**Project Name:** WB Lees Summit

**Project Number:** 62-40497

**Date:** 10/16/2020

**UGS 1**

**$WQ_v = R_v * P * A / 12$**

Post Construction			
Total Area	60,452 SF	1.39	acres
Impervious Area	45,145 SF	1.04	acres
Gravel Area	0.0 SF	0.00	acres
i =	0.75		

**$R_v = 0.05 + 0.9i$**

Rv= 0.72 Volumetric Runoff Coefficient

P = 0.90 inch precipitation depth

A = Area draining into the BMP in acres

P =	1.37		
A =	1.39		
WQ <sub>v</sub> =	0.11 ac-feet	4,983.73	ft <sup>3</sup>

**WATER QUALITY VOLUME CALCULATIONS- Drainage Area into Pond**

Project Name: WB Lees Summit  
 Project Number: 62-40497  
 Date: 1/21/2021

UGS

**VOLUMETRIC STAGE STORAGE**

STAGE	TOT VOL (ft^3)	TOT VOL (ac-ft)
1006.75	0.00	0.000
1007.00	437.00	0.010
1008.00	3,727.00	0.086
1009.00	8,420.00	0.193
1010.00	12,821.00	0.294
1011.00	16,764.00	0.385
1013.50	22,668.00	0.520

WQv = 4,983.73 cf

WQelev = 1008.14

**WQv- Orifice #1:**

PIPE DIA.	1.4	in	0.117	ft			
total PIPE A	1.539	in^2	0.011	ft^2			
C	0.6						
INV.	1006.75						
STAGE	Q1 (CFS)	Q2 (CFS)	Q (CFS)	Q AVG (CFS)	INC VOL (CFT)	INC DRAW (HR)	TOT DRAW (HR)
1006.75	0.000	0	0				
				0.03	4738	44.4	
1008.14	0.059	0.000	0.06				44.4

APPENDIX F  
COMPLETE SITE CIVIL PLANS