



**KAW
VALLEY**
ENGINEERING

**MASTER DRAINAGE PLAN
LEE'S SUMMIT HIGH SCHOOL
ADDITIONS & RENOVATIONS & ATHLETICS
400 SE BLUE PARKWAY
LEE'S SUMMIT, MISSOURI 64063
SECTION 8, TOWNSHIP 47 N, RANGE 31 W**

Prepared for:

LEE SUMMIT SCHOOL DISTRICT
502 SE Transport Drive
Lee's Summit, Missouri 64081

Prepared by:

KAW VALLEY ENGINEERING, INC.
14700 West 114th Terrace
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October 9, 2020

Revised: November 20, 2020

Revised: December 14, 2020

Kaw Valley Engineering Project No. **C20D0496**

MASTER DRAINAGE PLAN

LEE'S SUMMIT HIGH SCHOOL ADDITIONS & RENOVATIONS
LEE'S SUMMIT HIGH SCHOOL ATHLETICS
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EXHIBITS

- Exhibit A – FEMA Firmette, Existing Conditions & Soils Map
- Exhibit B – Proposed Grading Plan
- Exhibit C – Drainage Area Map & Calculations, Storm Sewer Plan and Profiles,
BMP Plan, EDDB Calculations
- Exhibit D – PondPack Analysis

REVISIONS

Revision 0 – October 9, 2020	Initial Issue
Revision 1 – November 20, 2020	Per City Comments
Revision 2 – December 14, 2020	Per City Comments

INTRODUCTION

The Lee's Summit School District is proposing extensive building additions and ancillary improvements across the Lee's Summit High School (LSHS) at 400 SE Blue Parkway in Lee's Summit, Missouri. With authorization from the Lee Summit School District, Inc., Kaw Valley Engineering, Inc. has completed a study of the existing and proposed storm drainage conditions associated with the project.

PURPOSE OF STUDY

The purpose of this study is to analyze the changes in storm water drainage conditions and flows associated with the proposed project. Furthermore, the study will show that the proposed drainage system for this project will comply with the adopted City of Lee's Summit, Missouri storm water guidelines.

CITY STORMWATER MANAGEMENT REQUIREMENTS

Based upon the Storm Water Management Guidelines as described in the KC Metropolitan Chapter of APWA as adopted by the City of Lee's Summit, the redevelopment on this property would be subject to the following requirements:

- The post development storm water peak runoff control is required for the 1%, 10% and 50% annual chance storm events as defined under Comprehensive Protection strategy outlined in APWA Section 5601.5 A4.a as modified in the City of Lee's Summit Design and Construction Manual. This project is an additions and renovations project on a fully developed site. The comprehensive Protection Strategy is applied to the increase in impervious coverage in acreage on the LSHS Campus.
- Volumetric and/or extended detention control of the 90% mean annual event (Water Quality Event or 1.37") is proposed to be provided to mitigate the proposed increase in impervious coverage associated with this project as well.

EXISTING CONDITIONS

The project site is located on the north side of the Blue Parkway, west of Missouri Highway 291. The address is 400 SE Blue Parkway as located on the general vicinity map.



The Lee's Summit High School property consists of approximately 45.53 acres. However, a project area of 17.48 acres has been defined since part of the site will remain undisturbed and is not part of the scope of this project. The project site currently consists of a school building, concrete hardscape, parking areas and driveways, athletics spaces, and green space. Table 1 details the existing land cover of the project area. Storm water runoff from the existing project area generally drains by overland flow and storm sewer to the northwest corner of the LSHS Campus. Runoff is conveyed in an open channel along the north property line of the LSHS campus that discharges into an unnamed tributary upstream of Prairie Lee Lake. This site is in Zone "X" on the revised flood insurance rate map for Lee's Summit (community panel No. 29095C0436G & 29095C0438G) dated January 20, 2017. A copy of the Flood Panel (Firmette) is included in Exhibit A for reference. The existing site topography (demolition plan) is also included in Exhibit A.

Table 1 - Existing Land Cover in the Project Area							
Description	Area (Sq. Ft)	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
Existing	761,400	17.48	565,150	12.97	74%	0.75	92

A soils map has been provided for the site. The soils were identified according to the soil survey maps in the *NRCS Web Soil Survey*. The map indicates that the following soils exist on the site and included the following engineering characteristics and soil and water features information.

- **10082- Arisburg-Urban Land Complex, 1 to 5 percent slopes.** The surface water runoff class is medium. The water table is at a depth of about 18 to 36 inches. This somewhat poorly drained soil is not hydric and is classed in Hydrologic Group C. No seasonal water table is present.

- **10180- Udarents-Urban Land – Sampsel Complex, 2 to 5 percent slopes.** The surface water runoff class is very high. The water table is at a depth is more than 80 inches. This somewhat poorly drained soil is not hydric and is classed in Hydrologic Group C and C/D.

DESCRIPTION OF PROPOSED IMPROVEMENTS

As stated above, the proposed improvements at Lee’s Summit High School will include a building addition, improvements to the stadium, improvement to pedestrian access and flow, reconstruction of the building services area, extension of the emergency access drive and expansion of the existing parking lots to offset the loss in existing parking spaces. The proposed improvements will encompass 17.48 acres of land which includes the disturbance and development within the Prairie Lee Lake watershed. Current plans propose an increase of approximately 16,000 SF of Impervious coverage or 2.1% within the defined project area. Most of the additional impervious coverage is proposed to be constructed on the north side of the property due to the expansion of the existing parking lot and future construction of a weight room. To mitigate the increase in impervious coverage specifically on the north side of campus, an extended dry detention basin is proposed to be constructed in the northwest corner of the site to collect and treat runoff from portions of the aforementioned north parking expansion area. The proposed improvements will preserve the general drainage patterns on the Campus. Storm Sewers will be extended and resized to address onsite capacity issues. Table 2 details the proposed land cover of the property within the project area. See Exhibit B Proposed Grading Plan.

Table 2 - Proposed Land Cover in the Project Area

Description	Area (Sq. Ft)	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
Proposed Undetained	727,600	16.70	550,900	12.65	76%	0.75	92
Proposed Detained (STF)	33,800	0.78	30,250	0.69	89%	0.84	95
Proposed	761,400	17.48	581,150	13.34	76%	0.76	92

DRAINAGE ANALYSIS

The storm runoff for the project site was analyzed for the WQv (90%), 2-year (50%), 10-year (10%), and 100 (1%)-year events for the existing and proposed conditions.

The Curve Number (CN) for the drainage areas to be used in the calculations are identified in Tables 1 and 2. This number was based upon the percentage of impervious and pervious surfaces as specified in section 5600 of APWA. It was assumed that pervious surfaces CN value of 74 and impervious surfaces have a CN value of 98.

Time of concentration (Tc) for the proposed conditions was calculated using methods outlined in APWA 5600. The time of concentration (Tc) was calculated for each project area for the existing and proposed conditions using the Urban Hydrology for Small Watersheds TR-55 manual.

Runoff for storm sewer design was calculated using the Rational Method as described in The KC Metropolitan Chapter of APWA Section 5600. Runoff for detention and routing was calculated using the SCS method as described in TR-55.

STORM SEWER ANALYSIS

The existing private storm sewer system will be modified, and new structures and pipes will be installed as part of this project. During review of the existing infrastructure, it was noted that contributions from the Lee’s Summit High School exceeded the capacity of the existing public storm sewer on Browning Street for a 10-year event. As part of this project, a substantial portion of the south half of the Lee’s Summit High School Campus will be redirected via a new storm extension between the existing school and tennis courts. Refer to Exhibit C for the drainage area map, storm sewer calculations and storm sewer plan and profiles.

RELEASE RATE REQUIREMENTS

Under the comprehensive protection method, the City of Lee’s Summit Design and Construction Manual stipulates that the post development release rate is to be detained to a defined cfs/acre rate of runoff. As indicated in Tables 1 and 2 of the report, the impervious surfaces within the project limits will increase by approximately 16,000 SF. Table 3 is a calculation of the existing discharge rates from the defined project area on the LSHS campus.

Table 3 - Existing Release Rates								
Description	Area (ac)	Curve Number	Tc (min)	WQv Year Storm		2 Year Storm	10 Year Storm	100 Year Storm
				Q (cfs)	Volume (ac-ft)	Q (cfs)	Q (cfs)	Q (cfs)
						Q (cfs)	Q (cfs)	Q (cfs)
Existing	17.48	91.8	10.10	16.5	1.001	59.9	100.6	142.7

Table 4 is calculation of the allowable increase in release rates from the LSHS campus in accordance with the comprehensive control strategy for the 2-year, 10-year and 100-year storm events.

Table 4 - Comprehensive Control Strategy (CCS)					
Allowable Site Discharge from Additional Impervious Coverage					
Description	SF	AC	2-year Storm 50% (0.5 cfs/acre)	10-year Storm 10% (2 cfs/acre)	100-year Storm 1% (3 cfs/acre)
CCS - Change in Impervious Coverage	16,000.00	0.37	0.18	0.73	1.10

Table 5 specifies the allowable site discharge from the campus. Table 5 also shows the comparison of the existing + allowable and proposed release rates without mitigation. The proposed condition was subdivided to document the unmitigated release rates in both the detained (proposed as part of this project) and undetained drainage areas.

Table 5 - Comparative Analysis of Project Area								
Description	Area (ac)	Curve Number	Tc (min)	WQv Year Storm		2 Year Storm	10 Year Storm	100 Year Storm
				Q (cfs)	Volume (ac-ft)	Q (cfs)	Q (cfs)	Q (cfs)
Existing + Allowable	17.48			16.5	1.001	60.1	101.3	143.8
<i>Proposed Undetained</i>	<i>16.70</i>	<i>92.2</i>	<i>10.10</i>	<i>1.1</i>	<i>0.058</i>	<i>3.3</i>	<i>5.3</i>	<i>7.5</i>
<i>Proposed Detained (STF)</i>	<i>0.78</i>	<i>95.5</i>	<i>5.00</i>	<i>15.8</i>	<i>0.962</i>	<i>57.3</i>	<i>96.2</i>	<i>136.4</i>
Proposed	17.48	92.3		16.9	1.020	60.6	101.5	143.9
Target Reduction from STF				0.4	0.019	0.5	0.2	0.1

To account for this increase of storm water runoff associated with the proposed project and meet the target reductions, Kaw Valley Engineering recommends that the Lee Summit School District constructs an on-site extended dry detention basin to reduce the peak discharge outflow from the site for all storm events analyzed and reduce volumetric increases for the WQv event.

DETENTION BASIN & ANALYSIS RESULTS

The extended dry detention basin (STF) will be located in the northwest corner of the site and is designed in general accordance with APWA 5600 standards. The detention basin will treat runoff from an adjacent parking lot. The detention basin will consist of an above ground detention pond and underground chamber system. The surface pond will have a bottom elevation of 1010.0, top elevation of 1012.0, and maximum side slopes of 3:1 for ease of maintenance. The basin floor will be constructed with a highly permeable Loamy Sand and rip rap floor that will infiltrate surface water into an underground gravel bed and chamber system. The chamber system will be equipped with inspection ports, an overflow drain and capped underdrain routed to the primary outlet structure. The underdrain will be equipped with a secured cleanout cap and 1" orifice. The cap can be removed for underdrain maintenance and inspection. Table 6 provides the drainage area and impervious coverage of the runoff entering the detention basin (STF).

Table 6 – Extended Dry Detention Basin (STF)						
Description	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
EEDB (STF)	0.78	30,250	0.69	89%	0.83	95

The detention basin will receive stormwater from overland flow via a flume from the adjacent parking to the south. The outflow will be regulated by an 8" drain tied to the chamber system beneath the basin floor. This 8" drain is designed to limit the discharge from the WQv (1-year event) storm through the basin underdrain system. The gravel bed and chamber system allow for the storage of runoff for extended periods of time. Both the underdrain and 8" chamber connector drain will connect to a 4' by 4' yard inlet with a 6" x 4' opening on the west face of the box. This outlet is designed to detain the 2-year, 10-year and 100-year events. The structure will be located on the east side of the basin and will also serve as the emergency outlet structure. The flow from

the outlet structure will be conveyed through a 15-inch HDPE storm pipe and discharge to the east into an existing drainage channel. If consecutive 100-year storm events are realized, the detention basin berm will be overtopped on the north and east sides of pond and runoff will drain by overland flow into the existing channel on the north side of the Lee’s Summit High School property. Rip rap will be installed at the discharge point of the 15” HDPE storm line. The rip rap apron is to be at least 20’ long and consist of 12” to 15” (D50) stone based on the pipe size and discharge velocity. The Drainage Area Map, BMP Plan, and EDDB Calculations are included in Exhibit C of the report.

As documented in Table 7 below, the proposed extended dry detention basin will effectively limit the post construction runoff to the less than the existing rates for the WQv, and the existing + allowable rates for the 2-year, 10-year and 100-year storm events. The requisite increase in volume associated with the WQv is also addressed. The Pondpack Analysis for the existing and proposed conditions is included in Exhibit D of the report.

Table 7 - Proposed Condition with Infiltration Basin Routing Summary				
1-year (WQv) Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow From Project Area
Inflow (cfs)	1.1	15.8	Proposed Inflow (cfs)	16.9
Outflow (cfs)	0.04	15.8	Proposed Outflow (cfs)*	15.8
Storage (ac-ft)	0.031		Existing Flow (cfs)	16.5
Max WS Elev.	1077.88		Reduction in Flow (cfs)	1.1
			Calculated Volume Reduction	0.020
			Prescribed Volume Reduction	0.019
2-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow From Project Area
Inflow (cfs)	3.3	57.3	Proposed Inflow (cfs)	60.6
Outflow (cfs)	2.7	57.3	Proposed Outflow (cfs)*	60.0
Storage (ac-ft)	0.047		Existing Flow (cfs) + CCS	60.1
Max WS Elev.	1011.03		Reduction in Flow (cfs)	0.6
10-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow From Project Area
Inflow (cfs)	5.3	96.2	Proposed Inflow (cfs)	101.5
Outflow (cfs)	3.5	96.2	Proposed Outflow (cfs)*	99.6
Storage (ac-ft)	0.07		Existing Flow (cfs) + CCS	101.3
Max WS Elev.	1011.62		Reduction in Flow (cfs)	1.9
100-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow From Project Area
Inflow (cfs)	7.5	136.4	Proposed Inflow (cfs)	143.9
Outflow (cfs)	6.4	136.4	Proposed Outflow (cfs)*	142.8
Storage (ac-ft)	0.082		Existing Flow (cfs) + CCS	143.8
Max WS Elev.	1011.91		Reduction in Flow (cfs)	1.1

*Note: Summation of Hydrographs vary from Peak Outflow due to offsetting peaks.

Based on these findings, it is the opinion of Kaw Valley Engineering, Inc. that the increases in runoff for the WQv, 2-year, 10-year and 100-year storm events and increase in volume and runoff for the WQv event related to the planned improvements associated with the LSHS Additions and

Renovations and LSHS Athletics projects can be effectively mitigated with the proposed Detention Strategy. A 1” difference between the planned 100-year WSE and emergency overflow berm is proposed to limit the potential for temporary ponding in the adjacent parking lot that could occur with consecutive 100-year storm events.

Respectfully submitted,
Kaw Valley Engineering, Inc.

David D. Wood, P.E.
Project Manager

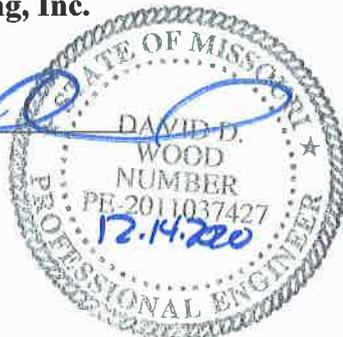


Exhibit A
FEMA Firmette
Existing Conditions Plan
Soils Map

National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone X
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		Cross Sections with 1% Annual Chance Water Surface Elevation
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **4/28/2020 at 2:17:12 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

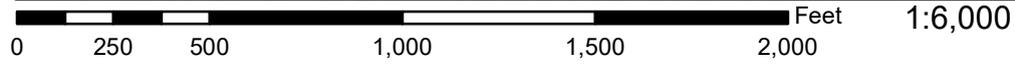
38°54'32.47"N

94°22'16.18"W



94°21'38.73"W

USGS The National Map: Orthoimagery. Data refreshed April, 2019.



38°54'4.47"N





Lee's Summit High School

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Lee's Summit, MO 64063

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David Wood
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REVISONS		
Number	DESCRIPTION	DATE

PROJECT NO: 0119-0100
DATE: November 20, 2020

EXISTING CONDITIONS

C400

Final Development Plan

DESCRIPTIONS: (PER TITLE COMMITMENT)

TRACT 1: (MISSOURI WARRANTY DEED, BOOK 923, AT PAGE 743)(DEED 1A)
ALL OF THE SOUTHWEST QUARTER OF THE NORTHEAST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, EXCEPT THAT PART CONVEYED TO THE STATE OF MISSOURI BY WARRANTY DEED RECORDED IN BOOK 856 AT PAGE 111 (DEED 1B), AND ALSO EXCEPT THAT PART THEREOF CONVEYED TO THE STATE OF MISSOURI BY WARRANTY DEED RECORDED IN BOOK 661 AT PAGE 166 (DEED 1C).

ALSO EXCEPT THAT PART THEREOF CONVEYED TO ARTHUR B. MCLENNAN AND PAULINE P. MCLENNAN, HUSBAND AND WIFE BY WARRANTY DEED RECORDED IN BOOK 883 AT PAGE 51 (DEED 1D), AND ALSO EXCEPT A TRACT OF LAND IN SAID SOUTHWEST QUARTER OF THE NORTHEAST QUARTER, SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, MORE PARTICULARLY DESCRIBED AS FOLLOWS:
BEGINNING AT A POINT 651.69 FEET NORTH OF THE SOUTHWEST CORNER OF THE SAID QUARTER SECTION, THENCE WEST 491.69 FEET; THENCE NORTH 63 FEET; THENCE EAST 491.69 FEET TO THE QUARTER SECTION LINE; THENCE SOUTH 63 FEET TO POINT OF BEGINNING.

TRACT 2: (MISSOURI WARRANTY DEED, BOOK 1243, AT PAGE 716)(DEED 2)
ALL OF THE WEST 327 FEET OF THE NORTH 2 ACRES OF THE SOUTHWEST QUARTER OF THE NORTHEAST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, MORE PARTICULARLY DESCRIBED AS FOLLOWS:
BEGINNING AT A POINT 198 FEET NORTH OF THE SOUTHWEST CORNER OF THE SOUTHWEST QUARTER OF THE NORTHEAST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN JACKSON COUNTY, MISSOURI, AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 132 FEET; THENCE WEST 327 FEET; THENCE SOUTH 132 FEET TO POINT OF BEGINNING.

TRACT 3: (MISSOURI WARRANTY DEED, BOOK 1277, AT PAGE 325)(DEED 3)
THE SOUTH 4 ACRES OF THE NORTHWEST 1/4 OF THE NORTHEAST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

TRACT 4: (REPORT OF COMMISSIONERS, BOOK 1484, AT PAGE 306)(DEED 4)
ALL OF THE WEST 327 FEET OF THE SOUTH 3 ACRES OF THAT PART OF THE NORTHWEST QUARTER OF THE NORTHEAST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, DESCRIBED AS FOLLOWS:
BEGINNING AT THE SOUTHWEST CORNER OF THE SOUTHWEST QUARTER OF THE NORTHEAST QUARTER AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 198 FEET; THENCE WEST 327 FEET; THENCE SOUTH 198 FEET TO THE POINT OF BEGINNING.

TRACT 5: (MISSOURI WARRANTY DEED, BOOK 1491, AT PAGE 140)(DEED 5)
ALL THAT PART OF THE EAST HALF OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI DESCRIBED AS FOLLOWS:
BEGINNING AT THE NORTHEAST CORNER OF THE INTERSECTION OF 7TH STREET AND BROWNING AVENUE; THENCE SOUTH ALONG THE EAST LINE OF BROWNING AVENUE A DISTANCE OF 478.52 FEET TO THE NORTH LINE OF 8TH STREET; THENCE EAST ALONG THE NORTH LINE OF 8TH STREET A DISTANCE OF 133 FEET TO THE EAST LINE OF SAID QUARTER SECTION; THENCE NORTH ALONG THE EAST LINE OF SAID QUARTER SECTION A DISTANCE OF 478.52 FEET TO THE NORTH LINE OF 7TH STREET EXTENDED; THENCE WEST ALONG THE NORTH LINE OF 7TH STREET EXTENDED A DISTANCE OF 133.77 FEET TO THE POINT OF BEGINNING.

TRACT 6: (MISSOURI WARRANTY DEED, BOOK 1536, AT PAGE 205)(DEED 6)
ALL THAT PART OF THE SOUTHWEST 1/4 OF THE NORTHEAST 1/4 OF SECTION 8, TOWNSHIP 47 RANGE 31, DESCRIBED AS FOLLOWS:
BEGINNING AT A POINT 556.69 FEET NORTH OF THE SOUTHWEST CORNER OF 1/4 OF 1/4 SECTION. THENCE WEST 491.69 FEET; THENCE NORTH 158 FEET; THENCE EAST 491.69 FEET; THENCE SOUTH 158 FEET TO THE POINT OF BEGINNING. ALL IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

EXCEPT THAT PART CONTAINED IN THE REPORT OF COMMISSIONERS RECORDED AS DOCUMENT NO 131081 IN BOOK 889 AT PAGE 465, DESCRIBED AS FOLLOWS:
ALL THAT PART OF THE SW 1/4 OF THE NE 1/4 OF SECTION 8, T47N, R31W, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI DESCRIBED AS FOLLOWS: BEGINNING AT A POINT 714.69 FEET NORTH AND 57 FEET WEST OF THE SOUTHWEST CORNER OF THE SW 1/4 OF THE NE 1/4 OF SAID SECTION 8, SAID POINT BEING 70 FEET WESTERLY OF THE CENTERLINE OF STATE HIGHWAY DESIGNATED ROUTE 00 (71 BY-PASS), AS MEASURED AT RIGHT ANGLES THERETO; THENCE SOUTH 3 DEGREES 14 MINUTES 23 SECONDS WEST PARALLEL TO SAID HIGHWAY CENTERLINE, 158 FEET; THENCE WEST PARALLEL TO THE SOUTH LINE OF SAID 1/4 1/4 SECTION, A DISTANCE OF 432 FEET; THENCE NORTH PARALLEL TO THE EAST LINE OF SAID 1/4 1/4 SECTION, A DISTANCE OF 75 FEET; THENCE NORTHEASTERLY ALONG A STRAIGHT LINE TO THE POINT OF BEGINNING.

TRACT 7: (MISSOURI WARRANTY DEED, BOOK 1869, AT PAGE 312)(DEED 7)
BEGINNING AT A POINT 1320.0 FEET NORTH OF THE EAST 1/2 CENTER LINE OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, AND ON THE EAST LINE OF THE EAST 1/2 OF THE NORTHEAST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31, THENCE WEST 186.3, THENCE NORTH 100 FEET; THENCE EAST 186.3 FEET TO A POINT ON THE EAST LINE; THENCE SOUTH ON SAID EAST LINE 100.0 FEET TO THE POINT OF BEGINNING, EXCEPTING THEREFROM THAT PART SITUATED IN US HIGHWAY 71 BY-PASS.

TRACT 8: (MISSOURI WARRANTY DEED, BOOK 1869, AT PAGE 313)(DEED 8)
ALL OF THE SOUTH 3 ACRES OF THE EAST 1/2 OF THE NORTHWEST 1/4 OF THE NORTHEAST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT JACKSON COUNTY, MISSOURI, EXCEPT THE WEST 327 FEET THEREOF AND ALSO EXCEPT THE SOUTH 100 FEET OF THE EAST 186.3 FEET THEREOF.

TRACT 9: (MISSOURI WARRANTY DEED, BOOK 1-79, AT PAGE 635)(DEED 9)
THE EAST 88.5 FEET OF THAT PART OF LOT 1, MUCKEY ADDITION, A SUBDIVISION IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, LYING SOUTH OF THE SOUTH LINE OF 8TH STREET, AS SAID STREET IS DESCRIBED IN DEED RECORDED IN BOOK 1039 AT PAGE 122, EXCEPT THE NORTH 155 FEET OF SAID EAST 88.5 FEET.

TRACT 10: (MISSOURI WARRANTY DEED, BOOK 551, AT PAGE 135)(DEED 10)
ALL OF THE NORTH 2 ACRES OF THE SOUTH 5 ACRES OF THE SOUTHWEST 1/4 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31, EXCEPT ALL THE WEST 327 FEET THEREOF MORE PARTICULARLY DESCRIBED AS FOLLOWS: BEGINNING AT A POINT 198 FEET NORTH OF THE SOUTHWEST CORNER OF THE SOUTHWEST 1/4 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31 AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 132 FEET; THENCE WEST 327 FEET TO POINT OF BEGINNING. ALL IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

TRACT 11: (MISSOURI WARRANTY DEED, BOOK 623, AT PAGE 833)(DEED 11)
THE SOUTH 220 FEET OF THE WEST 88.5 FEET OF LOT 1, MUCKEY ADDITION, A SUBDIVISION IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

DESCRIPTION: (PER TITLE COMMITMENT)

TRACT 1: (MISSOURI WARRANTY DEED, Bk. 1-80, Pg. 1904)
ALL THAT PART OF LOT 3, MUCKEY ADDITION, A SUBDIVISION OF LAND IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI ACCORDING TO THE RECORDED PLAT THEREOF, LYING SOUTH OF THE SOUTH LINE OF 6TH STREET IN LEE'S SUMMIT, AS SAID STREET IS DESCRIBED IN THE DEED RECORDED IN BOOK 1039 AT PAGE 122.

HORIZONTAL AND VERTICAL DATUM:

UNLESS OTHERWISE NOTED THE COORDINATES SHOWN HEREON ARE GROUND COORDINATES BASED ON THE MISSOURI STATE PLANE (1983) WEST ZONE (NAD 1983) (NAD 1983).
CAF: 0.9999978
NAD 83 TO NAD 83 U.S. SURVEY FEET
SCALED AROUND 0.0
NAD 83 TO NAD 83 U.S. SURVEY FEET
SCALED AROUND 0.0
NAD 83 TO NAD 83 U.S. SURVEY FEET
SCALED AROUND 0.0

PROJECT CONTROL:

CP #200	1/2" REBAR W/ ORANGE KVE CAP	996470.24 (GRID)	282149.83 (GRID)
CP #201	1/2" REBAR W/ ORANGE KVE CAP	996468.55 (GRID)	282676.55 (GRID)
CP #202	1/2" REBAR W/ ORANGE KVE CAP	996467.41 (GRID)	282640.11 (GRID)
CP #203	1/2" REBAR W/ ORANGE KVE CAP	996467.41 (GRID)	282640.11 (GRID)
CP #204	1/2" REBAR W/ ORANGE KVE CAP	997295.43 (GRID)	282639.70 (GRID)
CP #205	1/2" REBAR W/ ORANGE KVE CAP	997301.59 (GRID)	282620.67 (GRID)
CP #206	1/2" REBAR W/ ORANGE KVE CAP	997883.94 (GRID)	282627.18 (GRID)
CP #207	1/2" REBAR W/ ORANGE KVE CAP	997868.66 (GRID)	282671.70 (GRID)

SITE BENCHMARKS:

BM-50	FOUND CUT SQUARE AT THE WEST NORTHWEST CONCRETE HEADWALL ON THE WEST SIDE OF THE EAST ENTRY DRIVE TO LEE'S SUMMIT HIGH SCHOOL.	ELEVATION= 1042.70
BM-61	CUT SQUARE WITH PUNCH IN THE SOUTHWEST EDGE ON A CONCRETE LIGHT BASE ON THE NORTH SIDE OF THE DRIVE LANE AT THE HIGH SCHOOL ADMINISTRATION CENTER ENTRY.	ELEVATION= 1042.74
BM-62	SET CUT SQUARE AT THE NORTHEAST CORNER OF THE FIRST STEP UP OF A CONCRETE WALK ON THE NORTH SIDE OF THE EAST MAIN WING.	ELEVATION= 1040.51
BM-63	SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF A CONCRETE PATIO WITH COVERED TABLES ON THE EAST SIDE OF BUILDING "B".	ELEVATION= 1015.74
BM-64	SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF STEPS TO THE NORTH ENTRY TO BUILDING "B" ON THE WEST SIDE.	ELEVATION= 1015.34

FLOOD STATEMENT:

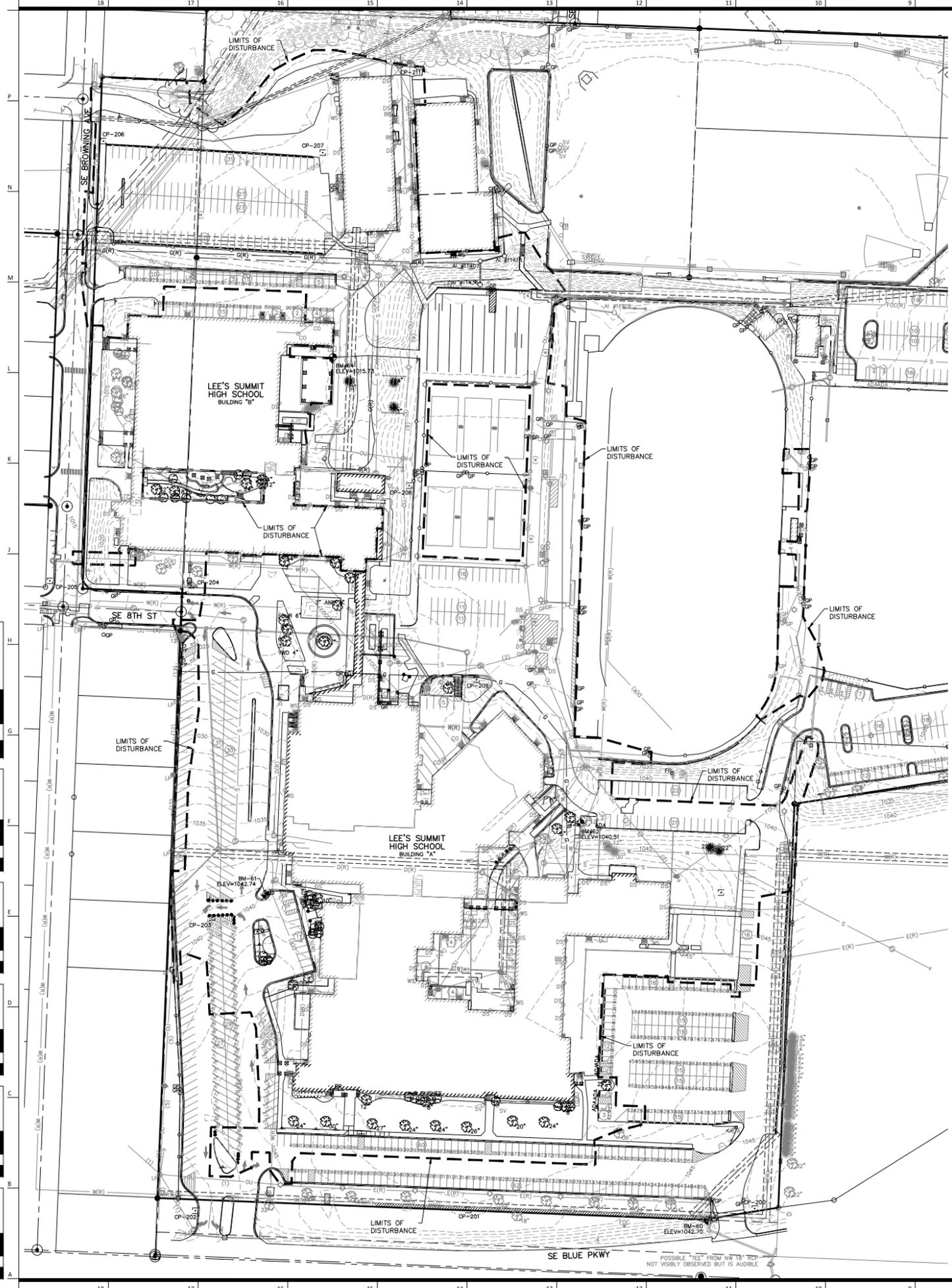
THE SURVEYED PARCEL LIES WITHIN ZONE "X" (AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN) AS DETERMINED BY FEMA FLOOD INSURANCE RATE MAP NUMBER 29095C04380, MAP REVISED JANUARY 20, 2017, AND BY MAP NUMBER 29095C04380, REVISED JANUARY 20, 2017 LEE'S SUMMIT, JACKSON COUNTY, MISSOURI. LOCATION DETERMINED BY A SCALED GRAPHICAL PLOT OF THE FLOOD INSURANCE RATE MAP.

UNDERGROUND UTILITY STATEMENT:

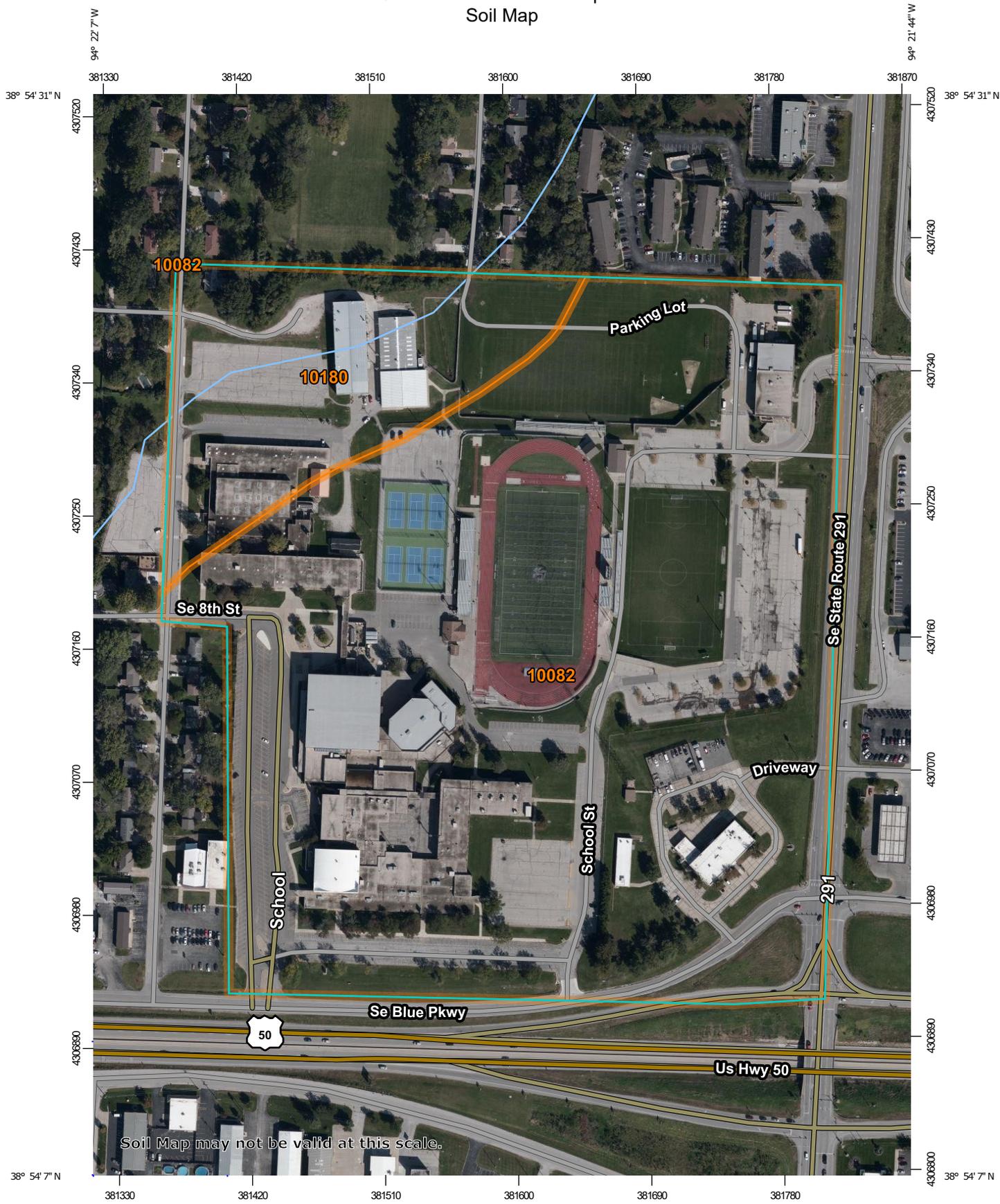
THE UNDERGROUND UTILITIES SHOWN HEREON ARE DEPICTED FROM FIELD SURVEY INFORMATION OF ONE-CALL LOCATED UTILITIES AND/OR THE SCALING AND PLOTTING OF EXISTING UTILITY MAPS AND DRAWINGS MADE AVAILABLE TO THE SURVEYOR AT THE TIME OF SURVEY. THE SURVEYOR DOES NOT CERTIFY THAT THE UNDERGROUND UTILITIES SHOWN COMPRISE ALL UNDERGROUND UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. FURTHERMORE, THE SURVEYOR DOES NOT CERTIFY THAT THE UNDERGROUND UTILITIES SHOWN ARE IN THE EXACT LOCATION DEPICTED ALTHOUGH HE DOES CERTIFY THAT THEY ARE DEPICTED AS POSSIBLE FROM INFORMATION MADE AVAILABLE TO THE SURVEYOR AT THE TIME OF SURVEY. THE SURVEYOR HAS NOT PHYSICALLY LOCATED THE UNDERGROUND UTILITIES SHOWN HEREON BY EXCAVATION UNLESS OTHERWISE NOTED ON THIS SURVEY.
MISSOURI ONE CALL TICKET NUMBER: #200431409, 200431440, 200431475, 200440745.

LEGEND:

- CONTROL POINT
- BENCHMARK
- STREET/TRAFFIC SIGN
- PAINTED DIRECTIONAL ARROW
- TURN LANE DIRECTION
- HANDICAP SYMBOL
- PARKING STALL COUNT
- WHEEL STOP
- UNDERGROUND FIBER OPTIC CABLE
- UNDERGROUND FIBER OPTIC (FROM RECORDS)
- TELEPHONE PEDESTAL
- SANITARY SEWER MANHOLE
- STORM SEWER MANHOLE
- AREA INLET
- CURB INLET
- SANITARY SEWER CLEAN OUT
- FLOOR DRAIN
- FLARED END SECTION
- SANITARY SEWER LINE
- STORM SEWER LINE
- CORRUGATED METAL PIPE
- REINFORCED CONCRETE PIPE
- VITRIFIED CLAY PIPE
- DUCTILE IRON PIPE
- HDPPE
- HIGH DENSITY POLYETHYLENE
- WALL MOUNTED LIGHT
- WALL MOUNTED CAMERA
- UNDERGROUND ELECTRIC
- OVERHEAD UTILITY LINE (# OF LINES)
- PULL BOX
- LIGHT POLE
- UTILITY POLE
- UTILITY POLE W/ LIGHT
- UTILITY POLE W/ TRANSFORMER
- GUY ANCHOR
- WATER LINE PER RECORD
- UNDERGROUND ELECTRIC PER RECORD
- WALL MOUNTED ELECTRICAL OUTLET
- BACK TO BACK OF CURB MEASUREMENT
- UNDERGROUND ELECTRIC PEDESTAL
- UNDERGROUND GAS PER RECORD
- SANITARY SEWER LINE PER RECORD
- STORM SEWER LINE PER RECORD
- AIR CONDITIONER
- UNDERGROUND GAS
- GAS METER
- GAS VALVE
- GAS RISER
- GAS LINE SIGN
- EXISTING SPOT ELEVATION
- EXISTING GRADE 5' CONTOUR
- DOOR ELEVATION
- AT THRESHOLD
- FF FINISH FLOOR ELEVATION
- BHE BUILDING HEIGHT/ELEVATION
- E/E EDGE TO EDGE OF ASPHALT
- WATER SPOUT
- WATER LINE
- WATER METER
- WATER LINE GATE VALVE
- FIRE HYDRANT
- SPRINKLER CONTROL BOX
- WATER MANHOLE
- SPRINKLER VALVE
- SHAMESE FIRE CONNECTOR
- CANOPY SUPPORT
- MAIL BOX
- CONCRETE JOINT/CUT LINE
- BUSH
- DECIDUOUS TREE
- CONIFEROUS TREE
- TREE LINE
- FLAG POLE
- T/E TRASH ENCLOSURE
- L/S LANDSCAPING AREA
- CONC CONCRETE
- LW LOWEST WIRE HEIGHT
- ELECTRIC METER
- SPEAKER BOX
- BREAKER BOX
- HANDICAP SIGN
- HRMP HANDICAP RAMP
- GATE POST
- CHAIN LINK FENCE
- WOOD FENCE
- BOLLARD



Custom Soil Resource Report Soil Map



Map Scale: 1:3,560 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 15N WGS84

Exhibit B
Proposed Grading Plan

Lee's Summit High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4200 Pennsylvania Avenue
Kansas City, MO 64111
816.931.6655 voice
www.goulddevans.com

structural engineer:
Bob D. Campbell & Company, Inc.
4338 Belleview
Kansas City, MO 64111
816.531.4144

civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
913.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.463.8700

NOTE:

- CONTRACTOR SHALL REFER TO ARCHITECTURAL PLANS FOR EXACT LOCATIONS AND DIMENSIONS OF ENTRANCE, SLOPED PAVING, EXIT PORCHES, RAMPS, TRUCK DOCKS, PRECISE BUILDING DIMENSIONS AND EXACT BUILDING UTILITY ENTRANCE LOCATIONS.
- THESE PLANS HAVE NOT BEEN VERIFIED WITH FINAL ARCHITECTURAL CONTRACT DRAWINGS. CONTRACTOR SHALL VERIFY AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES. CONTRACTOR IS FULLY RESPONSIBLE FOR REVIEW AND COORDINATION OF ALL DRAWINGS AND CONTRACTOR DOCUMENTS.
- ALL DIMENSIONS ARE TO BACK OF CURB UNLESS NOTED OTHERWISE.
- ALL DIMENSIONS ARE PERPENDICULAR TO PROPERTY LINE.

WARRANTY / DISCLAIMER
THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN OR DO WARRANT THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR
THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS. THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

SAFETY NOTICE TO CONTRACTOR
IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

HORIZONTAL AND VERTICAL DATUM:
UNLESS OTHERWISE NOTED THE COORDINATES SHOWN HEREON ARE GROUND COORDINATES BASED ON THE MISSOURI STATE PLANE (1983) WEST ZONE (NAD 1983) (NAD 1983)
CAP: 0.9999978
SCALED AROUND 0.0

UA-25 (PID: 095024)
NORTHING: 303646.030 (GRID/METERS) 996313.829 (GROUND/FEET)
EASTING: 860950.475 (GRID/METERS) 2824923.692 (GROUND/FEET)
ELEVATION: 321.8 (METERS) 1055.77 (FEET)

PROJECT CONTROL:

CP #202	1/2" REBAR W/ ORANGE KVE CAP	996470.24 (GRID)
	NORTHING: 996572.06 (GROUND)	2827149.83 (GRID)
	EASTING: 2827436.76 (GROUND)	
	ELEV = 1049.49	

SITE BENCHMARKS:

BM-60
FOUND OUT SQUARE AT THE WEST NORTHWEST CONCRETE HEADWALL ON THE WEST SIDE OF THE EAST ENTRY DRIVE TO LEE'S SUMMIT HIGH SCHOOL
ELEVATION= 1042.70

CP #201	1/2" REBAR W/ ORANGE KVE CAP	996468.55 (GRID)
	NORTHING: 996570.39 (GROUND)	2826766.55 (GRID)
	EASTING: 2827055.45 (GROUND)	
	ELEV = 1048.24	

BM-61
SET CUT SQUARE WITH PUNCH IN THE SOUTHWEST EDGE ON A CONCRETE LIGHT BASE ON THE NORTH SIDE OF THE DRIVE LANE AT THE HIGH SCHOOL ADMINISTRATION CENTER ENTRY.
ELEVATION= 1042.74

CP #203	MAG NAIL	996655.74 (GRID)
	NORTHING: 996957.62 (GROUND)	2826423.62 (GRID)
	EASTING: 2826712.48 (GROUND)	
	ELEV = 1039.43	

BM-62
SET CUT SQUARE AT THE NORTHEAST CORNER OF THE FIRST STEP UP OF A CONCRETE WALK ON THE NORTH SIDE OF THE EAST MAIN WING.
ELEVATION= 1040.51

CP #204	1/2" REBAR W/ ORANGE KVE CAP	997295.43 (GRID)
	NORTHING: 997397.36 (GROUND)	2826395.70 (GRID)
	EASTING: 2826684.55 (GROUND)	
	ELEV = 1023.04	

BM-63
SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF A CONCRETE PATIO WITH COVERED TABLES ON THE EAST SIDE OF BUILDING "B".
ELEVATION= 1040.51

CP #205	1/2" REBAR W/ ORANGE KVE CAP	997301.59 (GRID)
	NORTHING: 997403.51 (GROUND)	2826206.47 (GRID)
	EASTING: 2826495.31 (GROUND)	
	ELEV = 1018.15	

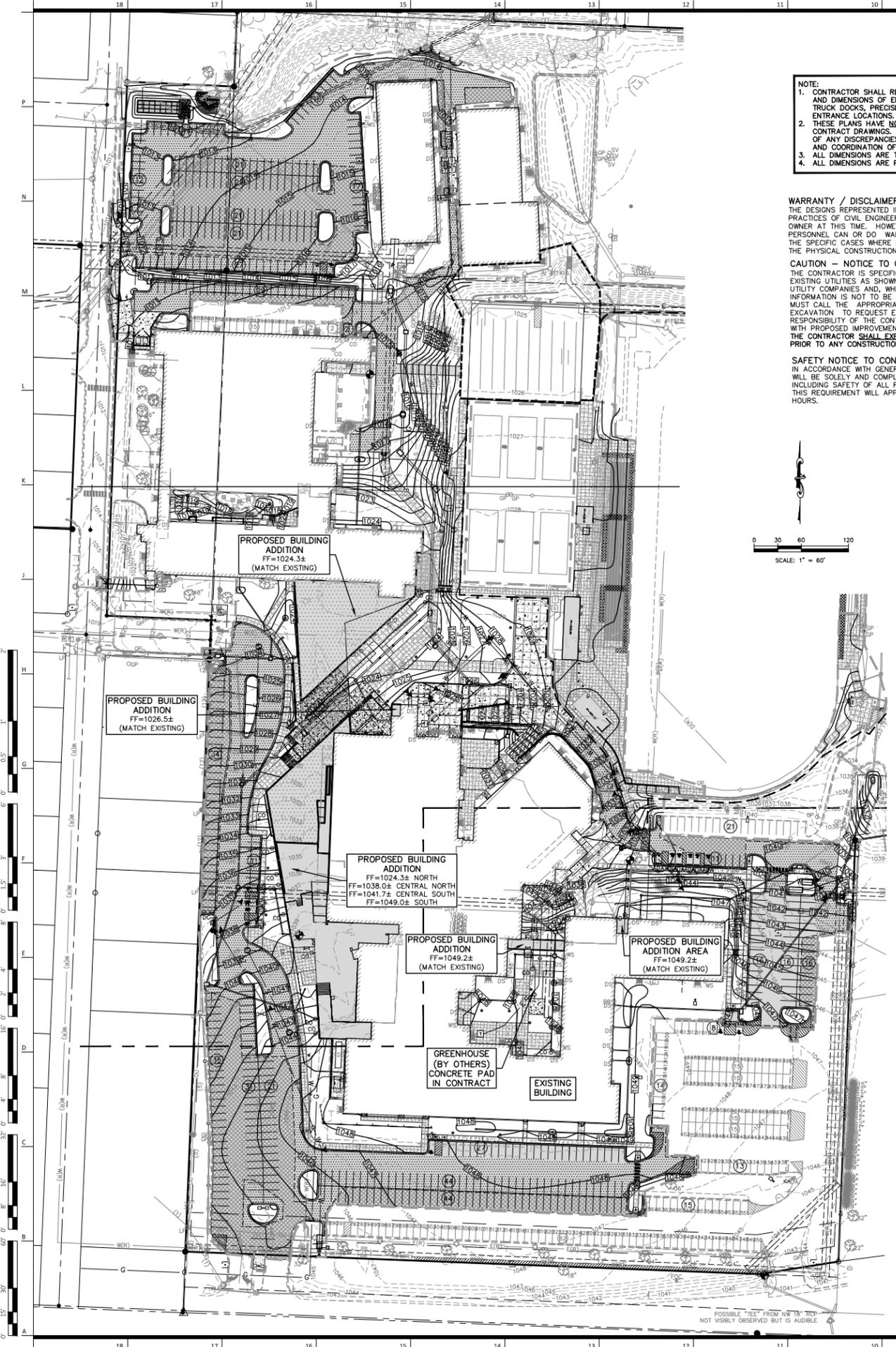
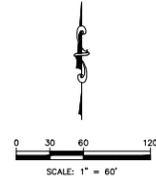
BM-64
SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF STEPS TO THE NORTH ENTRY TO BUILDING "B" ON THE WEST SIDE.
ELEVATION= 1015.34

CP #206	1/2" REBAR W/ ORANGE KVE CAP	997883.94 (GRID)
	NORTHING: 997985.93 (GROUND)	2826395.70 (GRID)
	EASTING: 2826567.03 (GROUND)	
	ELEV = 1012.56	

CP #207	1/2" REBAR W/ ORANGE KVE CAP	997868.66 (GRID)
	NORTHING: 997970.64 (GROUND)	2826571.70 (GRID)
	EASTING: 2826860.58 (GROUND)	
	ELEV = 1014.79	

GRADING NOTES:

- THE CONSTRUCTION AREA SHALL BE CLEARED, GRUBBED, AND STRIPPED OF TOPSOIL AND ORGANIC MATTER FROM ALL AREAS TO BE OCCUPIED BY BUILDING AND PAVING. TOPSOIL FOR REPLACEMENT ON SLOPES MAY BE STOCKPILED ON SITE. EXCESS TOPSOIL MAY BE WASTED IN FILL SLOPES PROVIDED THAT NO TOPSOIL WILL BE WASTED WITHIN 10 FEET OF THE EDGE OF THE BUILDING OR PARKING AREA. BURNING OF TIMBER WILL NOT BE PERMITTED UNLESS APPROVAL IS OBTAINED FROM GOVERNING OFFICIALS. STRIPPING EXISTING TOPSOIL AND ORGANIC MATTER SHALL BE TO A MINIMUM DEPTH OF 6 INCHES. CONSTRUCTION MANAGER SHALL DESIGNATE LOCATION OF STOCKPILE AREAS DURING CONSTRUCTION. ANY UNAUTHORIZED STOCKPILE SHALL BE REMOVE/RELOCATED AT THE CONTRACTOR'S EXPENSE.
- AREAS TO RECEIVE FILL SHALL BE SCARIFIED AND THE TOP 12-INCH DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698 WITH A MOISTURE CONTENT OF +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT OF LESS THAN 40 AND 0 TO +4% FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40. ANY UNSUITABLE AREAS SHALL BE UNDERCUT AND REPLACED WITH SUITABLE MATERIAL BEFORE ANY FILL MATERIAL CAN BE APPLIED.
- OFF-SITE SOIL MATERIAL FOR USE UNDER BUILDING AND PAVED AREAS SHALL HAVE A PLASTICITY INDEX OF 25 OR LESS, A LIQUID LIMIT OF 45 OR LESS AND CONTAIN NO ROCK LARGER THAN THREE INCHES. OFF-SITE FILL MATERIAL SHALL BE APPROVED BY THE OWNER'S TESTING AGENCY PRIOR TO BRINGING ON SITE.
- EARTHWORK UNDER THE BUILDING, PAVING AND LIGHTLY LOADED STRUCTURAL FEATURES SHALL COMPLY WITH THE CONTRACT DOCUMENTS AND PROJECT GEOTECHNICAL REPORT. THE BUILDING PAD SHALL BE EXCAVATED AS REQUIRED TO ALLOW THE PLACEMENT OF LOW VOLUME CHANGE MATERIAL. REFER TO GEOTECHNICAL REPORT FOR PREPARING BUILDING PAD AND LOW VOLUME CHANGE THICKNESS REQUIREMENTS. OTHER FILL MATERIAL SHALL BE MADE IN LIFTS NOT TO EXCEED EIGHT INCHES DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698. LVC SOILS SHALL BE COMPACTED AT A MOISTURE CONTENT OF 0 TO +4% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40 AND +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT LESS THAN 40. NO ROCK LARGER THAN THREE INCHES IN ANY DIMENSION NOR ANY SHALE SHALL BE PLACED IN THE TOP 24 INCHES OF EMBANKMENT.
- ON-SITE HIGH PLASTICITY CLAYS MAY BE TREATED WITH 5% TYPE 1/2 PORTLAND CEMENT BY WEIGHT. REFER TO PROJECT GEOTECHNICAL REPORT FOR REQUIREMENTS.
- AREAS THAT ARE TO BE CUT TO SUBGRADE LEVELS SHALL BE PROOF ROLLED WITH A LOADED DUMP TRUCK OR SIMILAR APPROVED CONSTRUCTION EQUIPMENT TO DETECT UNSUITABLE SOIL CONDITIONS.
- IN ALL AREAS OF EXCAVATION, IF UNSUITABLE SOIL CONDITIONS ARE ENCOUNTERED, THE OWNER'S ENGINEER SHALL RECOMMEND TO THE OWNER THE METHODS OF UNDERCUTTING AND REPLACEMENT OF PROPERLY COMPACTED, APPROVED FILL MATERIAL. ALL PROOFROLLING AND UNDERCUTTING SHOULD BE PERFORMED DURING A PERIOD OF DRY WEATHER.
- ALL EXCAVATIONS SHALL BE CONSIDERED AS UNCLASSIFIED. REFER TO PROJECT GEOTECHNICAL REPORT.
- ALL DISTURBED SLOPES ARE TO BE 3:1 OR FLATTER.
- DETENTION BASIN AND ALL SLOPES DISTURBED EXCEEDING 4:1 SHALL BE HYDROSEEDED, SODDED OR PROTECTED BY EROSION CONTROL BLANKETS THAT WILL PREVENT EROSION AND PLACED SUCH THAT THE SURFACE IS FLUSH WITH SURROUNDING GROUND AND SHAPED TO CHANNEL WATER IN DIRECTIONS INDICATED. SEE GENERAL NOTES ON THIS SHEETS.
- ALL SLOPES AND AREAS DISTURBED BY CONSTRUCTION SHALL BE GRADED SMOOTH AND A MINIMUM OF FOUR INCHES OF TOPSOIL APPLIED. IF ADEQUATE TOPSOIL IS NOT AVAILABLE ON-SITE, THE CONTRACTOR SHALL PROVIDE TOPSOIL, APPROVED BY THE OWNER, AS NEEDED. THE AREA SHALL THEN BE SODDED OR SEEDED, FERTILIZED, MULCHED, WATERED AND MAINTAINED UNTIL HARDY GRASS GROWTH IS ESTABLISHED IN ALL AREAS. ANY AREAS DISTURBED FOR ANY REASON SHALL BE CORRECTED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER PRIOR TO FINAL ACCEPTANCE OF THE PROJECT. REFER TO THE NOTES ON THIS SHEET FOR TEMPORARY SEEDING SPECIFICATIONS. REFER TO PROJECT SITE PLAN FOR FINAL STABILIZATION TREATMENTS.
- CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS.
- THE CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO AVOID PROPERTY DAMAGE TO ADJACENT PROPERTIES DURING THE CONSTRUCTION PHASES OF THIS PROJECT. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR ANY DAMAGES TO THE ADJACENT PROPERTIES OCCURRING DURING THE CONSTRUCTION PHASES OF THIS PROJECT.
- IT IS NOT THE DUTY OF THE ENGINEER OR THE OWNER TO REVIEW THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES, IN, ON OR NEAR THE CONSTRUCTION SITE AT ANY TIME DURING CONSTRUCTION.
- IF ANY OF THESE NOTES CONFLICT WITH THE PROJECT GEOTECHNICAL REPORT (CFS PROJECT 20-1075) AND ALL ADDENDUMS PREPARED BY CFS ENGINEERS DATED JUNE 12, 2020, RECOMMENDATIONS IN GEOTECHNICAL REPORT SHALL GOVERN.
- GRADE AT ALL STOOPS SHALL BE 1/2" BELOW FINISH FLOOR ELEVATION AND SLOPE AWAY FROM THE BUILDING AT 1/4"/FT. (2.0%).



UNLESS A PROFESSIONAL SEAL WITH SIGNATURE AND DATE IS AFFIXED, THIS DOCUMENT IS PRELIMINARY AND IS NOT INTENDED FOR CONSTRUCTION RECORDING PURPOSES OR IMPLEMENTATION

NUMBER	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
2	PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

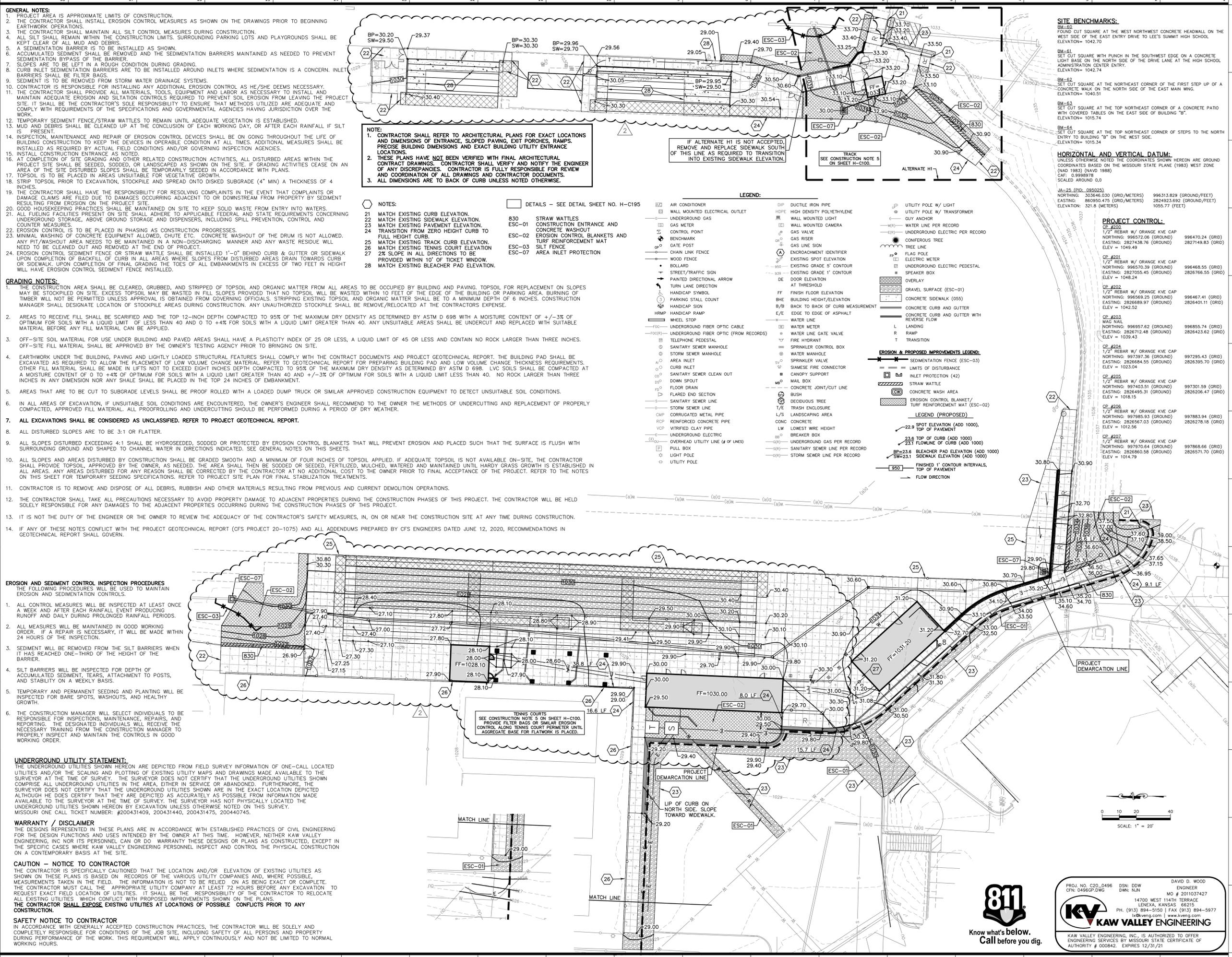
OVERALL GRADING PLAN
C300
Final Development Plan

PROJ. NO. C20_0496 DSN: DDW DAVID D. WOOD ENGINEER
CPR: 0496CPR.DWG DWN: N/JN MO # 2011037427
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
PH. (913) 894-5150 | FAX (913) 894-5977
kd@kveeng.com | www.kveeng.com

KV KAW VALLEY ENGINEERING

KAW VALLEY ENGINEERING, INC. IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000842. EXPIRES 12/31/21





GENERAL NOTES:
1. PROJECT AREA IS APPROXIMATE LIMITS OF CONSTRUCTION.
2. THE CONTRACTOR SHALL INSTALL EROSION CONTROL MEASURES AS SHOWN ON THE DRAWINGS PRIOR TO BEGINNING EARTHWORK OPERATIONS.
3. THE CONTRACTOR SHALL MAINTAIN ALL SILT CONTROL MEASURES DURING CONSTRUCTION.
4. ALL SILT SHALL REMAIN WITHIN THE CONSTRUCTION LIMITS. SURROUNDING PARKING LOTS AND PLAYGROUNDS SHALL BE KEPT CLEAR OF ALL MUD AND DEBRIS.
5. A SEDIMENTATION BARRIER IS TO BE INSTALLED AS SHOWN.
6. ACCUMULATED SEDIMENT SHALL BE REMOVED AND THE SEDIMENTATION BARRIERS MAINTAINED AS NEEDED TO PREVENT SEDIMENTATION BYPASS OF THE BARRIERS.
7. SLOPES ARE TO BE LEFT IN A ROUGH CONDITION DURING GRADING.
8. CURB INLET SEDIMENTATION BARRIERS ARE TO BE INSTALLED AROUND INLETS WHERE SEDIMENTATION IS A CONCERN. INLET BARRIERS SHALL BE FILTER BAGS.
9. SEDIMENT IS TO BE REMOVED FROM STORM WATER DRAINAGE SYSTEMS.
10. CONTRACTOR IS RESPONSIBLE FOR INSTALLING ANY ADDITIONAL EROSION CONTROL AS HE/SHE DEEMS NECESSARY.
11. THE CONTRACTOR SHALL PROVIDE ALL MATERIALS, TOOLS, EQUIPMENT AND LABOR AS NECESSARY TO INSTALL AND MAINTAIN ADEQUATE EROSION AND SEDIMENTATION CONTROLS REQUIRED TO PREVENT SOIL EROSION FROM LEAVING THE PROJECT SITE. IT SHALL BE THE CONTRACTOR'S SOLE RESPONSIBILITY TO ENSURE THAT METHODS UTILIZED ARE ADEQUATE AND COMPLY WITH REQUIREMENTS OF THE SPECIFICATIONS AND GOVERNMENTAL AGENCIES HAVING JURISDICTION OVER THE WORK.
12. TEMPORARY SEDIMENT FENCE/STRAW WATTLES TO REMAIN UNTIL ADEQUATE VEGETATION IS ESTABLISHED.
13. MUD AND DEBRIS SHALL BE CLEANED UP AT THE CONCLUSION OF EACH WORKING DAY, OR AFTER EACH RAINFALL IF SILT IS PRESENT.
14. INSPECTION, MAINTENANCE AND REPAIR OF EROSION CONTROL DEVICES SHALL BE ON GOING THROUGHOUT THE LIFE OF BUILDING CONSTRUCTION TO KEEP THE DEVICES IN OPERABLE CONDITION AT ALL TIMES. ADDITIONAL MEASURES SHALL BE INSTALLED AS REQUIRED BY ACTUAL FIELD CONDITIONS AND/OR GOVERNING INSPECTION AGENCIES.
15. INSTALL CONSTRUCTION ENTRANCE AS NOTED.
16. AT COMPLETION OF SITE GRADING AND OTHER RELATED CONSTRUCTION ACTIVITIES, ALL DISTURBED AREAS WITHIN THE PROJECT SITE SHALL BE SEEDED, SODDED, OR LANDSCAPED AS SHOWN ON THE SITE. IF GRADING ACTIVITIES CEASE ON AN AREA OF THE SITE DISTURBED SLOPES SHALL BE TEMPORARILY SEEDED IN ACCORDANCE WITH PLANS.
17. TOPSOIL IS TO BE PLACED IN AREAS UNSUITABLE FOR VEGETATIVE GROWTH.
18. STRIP TOPSOIL PRIOR TO EXCAVATION, STOCKPILE AND SPREAD ONTO DISKED SUBGRADE (4" MIN) A THICKNESS OF 4 INCHES.
19. THE CONTRACTOR SHALL HAVE THE RESPONSIBILITY FOR RESOLVING COMPLAINTS IN THE EVENT THAT COMPLAINTS OR DAMAGE CLAIMS ARE FILED DUE TO DAMAGES OCCURRING ADJACENT TO OR DOWNSTREAM FROM PROPERTY BY SEDIMENT RESULTING FROM EROSION ON THE PROJECT SITE.
20. GOOD HOUSEKEEPING PRACTICES SHALL BE MAINTAINED ON SITE TO KEEP SOIL WASTE FROM ENTRY INTO WATERS.
21. ALL FUELING FACILITIES PRESENT ON SITE SHALL ADHERE TO APPLICABLE FEDERAL AND STATE REQUIREMENTS CONCERNING UNDERGROUND STORAGE, ABOVE GROUND STORAGE AND DISPENSERS, INCLUDING SPILL PREVENTION, CONTROL AND COUNTER MEASURES.
22. EROSION CONTROL IS TO BE PLACED IN PHASING AS CONSTRUCTION PROGRESSES.
23. MINIMAL WASHING OF CONCRETE EQUIPMENT ALLOWED, CHUTE ETC. CONCRETE WASHOUT OF THE DRUM IS NOT ALLOWED. ANY PIT/WASHOUT AREA NEEDS TO BE MAINTAINED IN A NON-DISCHARGING MANNER AND ANY WASTE RESIDUE WILL NEED TO BE CLEANED OUT AND REMOVED AT THE END OF PROJECT.
24. EROSION CONTROL SEDIMENT FENCE OR STRAW WATTLE SHALL BE INSTALLED 1'-0" BEHIND CURB & GUTTER OR SIDEWALK UPON COMPLETION OF BACKFILL OF CURB IN ALL AREAS WHERE SLOPES FROM DISTURBED AREAS DRAIN TOWARDS CURB OR SIDEWALK. UPON COMPLETION OF FINAL GRADING, THE TOES OF ALL EMBANKMENTS IN EXCESS OF TWO FEET IN HEIGHT WILL HAVE EROSION CONTROL SEDIMENT FENCE INSTALLED.

GRADING NOTES:
1. THE CONSTRUCTION AREA SHALL BE CLEARED, GRUBBED, AND STRIPPED OF TOPSOIL AND ORGANIC MATTER FROM ALL AREAS TO BE OCCUPIED BY BUILDING AND PAVING. TOPSOIL FOR REPLACEMENT ON SLOPES MAY BE STOCKPILED ON SITE. EXCESS TOPSOIL MAY BE WASTED IN FILL SLOPES PROVIDED THAT NO TOPSOIL WILL BE WASTED WITHIN 10 FEET OF THE EDGE OF THE BUILDING OR PARKING AREA. BURNING OF TIMBER WILL NOT BE PERMITTED UNLESS APPROVAL IS OBTAINED FROM GOVERNING OFFICIALS. STRIPPING EXISTING TOPSOIL AND ORGANIC MATTER SHALL BE TO A MINIMUM DEPTH OF 6 INCHES. CONSTRUCTION MANAGER SHALL DESIGNATE LOCATION OF STOCKPILE AREAS DURING CONSTRUCTION. ANY UNAUTHORIZED STOCKPILE SHALL BE REMOVE/RELOCATED AT THE CONTRACTORS EXPENSE.
2. AREAS TO RECEIVE FILL SHALL BE SCARIFIED AND THE TOP 12-INCH DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698 WITH A MOISTURE CONTENT OF +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT OF LESS THAN 40 AND 0 TO +4% FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40. ANY UNSUITABLE AREAS SHALL BE UNDERCUT AND REPLACED WITH SUITABLE MATERIAL BEFORE ANY FILL MATERIAL CAN BE APPLIED.
3. OFF-SITE SOIL MATERIAL FOR USE UNDER BUILDING AND PAVED AREAS SHALL HAVE A PLASTICITY INDEX OF 25 OR LESS, A LIQUID LIMIT OF 45 OR LESS AND CONTAIN NO ROCK LARGER THAN THREE INCHES. OFF-SITE FILL MATERIAL SHALL BE APPROVED BY THE OWNER'S TESTING AGENCY PRIOR TO BRINGING ON SITE.
4. EARTHWORK UNDER THE BUILDING, PAVING AND LIGHTLY LOADED STRUCTURAL FEATURES SHALL COMPLY WITH THE CONTRACT DOCUMENTS AND PROJECT GEOTECHNICAL REPORT. THE BUILDING PAD SHALL BE EXCAVATED AS REQUIRED TO ALLOW THE PLACEMENT OF LOW VOLUME CHANGE MATERIAL. REFER TO GEOTECHNICAL REPORT FOR PREPARING BUILDING PAD AND LOW VOLUME CHANGE THICKNESS REQUIREMENTS. OTHER FILL MATERIAL SHALL BE MADE IN LIFTS NOT TO EXCEED EIGHT INCHES DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698. LVC SOILS SHALL BE COMPACTED AT A MOISTURE CONTENT OF 0 TO +4% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40 AND +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT LESS THAN 40. NO ROCK LARGER THAN THREE INCHES IN ANY DIMENSION NOR ANY SHALE SHALL BE PLACED IN THE TOP 24 INCHES OF EMBANKMENT.
5. AREAS THAT ARE TO BE CUT TO SUBGRADE LEVELS SHALL BE PROOF ROLLED WITH A LOADED DUMP TRUCK OR SIMILAR APPROVED CONSTRUCTION EQUIPMENT TO DETECT UNSUITABLE SOIL CONDITIONS.
6. IN ALL AREAS OF EXCAVATION, IF UNSUITABLE SOIL CONDITIONS ARE ENCOUNTERED, THE OWNER'S ENGINEER SHALL RECOMMEND TO THE OWNER THE METHODS OF UNDERCUTTING AND REPLACEMENT OF PROPERLY COMPACTED, APPROVED FILL MATERIAL. ALL PROOFROLLING AND UNDERCUTTING SHOULD BE PERFORMED DURING A PERIOD OF DRY WEATHER.
7. ALL EXCAVATIONS SHALL BE CONSIDERED AS UNCLASSIFIED. REFER TO PROJECT GEOTECHNICAL REPORT.
8. ALL DISTURBED SLOPES ARE TO BE 3:1 OR FLATTER.
9. ALL SLOPES DISTURBED EXCEEDING 4:1 SHALL BE HYDROSEEDDED, SODDED OR PROTECTED BY EROSION CONTROL BLANKETS THAT WILL PREVENT EROSION AND PLACED SUCH THAT THE SURFACE IS FLUSH WITH SURROUNDING GROUND AND SHAPED TO CHANNEL WATER IN DIRECTIONS INDICATED. SEE GENERAL NOTES ON THIS SHEETS.
10. ALL SLOPES AND AREAS DISTURBED BY CONSTRUCTION SHALL BE GRADED SMOOTH AND A MINIMUM OF FOUR INCHES OF TOPSOIL APPLIED. IF ADEQUATE TOPSOIL IS NOT AVAILABLE ON-SITE, THE CONTRACTOR SHALL PROVIDE TOPSOIL, APPROVED BY THE OWNER, AS NEEDED. THE AREA SHALL THEN BE SODDED OR SEEDED, FERTILIZED, MULCHED, WATERED AND MAINTAINED UNTIL HARDY GRASS GROWTH IS ESTABLISHED IN ALL AREAS. ANY AREAS DISTURBED FOR ANY REASON SHALL BE CORRECTED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER PRIOR TO FINAL ACCEPTANCE OF THE PROJECT. REFER TO THE NOTES ON THIS SHEET FOR TEMPORARY SEEDING SPECIFICATIONS. REFER TO PROJECT SITE PLAN FOR FINAL STABILIZATION TREATMENTS.
11. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS.
12. THE CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO AVOID PROPERTY DAMAGE TO ADJACENT PROPERTIES DURING THE CONSTRUCTION PHASES OF THIS PROJECT. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR ANY DAMAGES TO THE ADJACENT PROPERTIES OCCURRING DURING THE CONSTRUCTION PHASES OF THIS PROJECT.
13. IT IS NOT THE DUTY OF THE ENGINEER OR THE OWNER TO REVIEW THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES, IN, ON OR NEAR THE CONSTRUCTION SITE AT ANY TIME DURING CONSTRUCTION.
14. IF ANY OF THESE NOTES CONFLICT WITH THE PROJECT GEOTECHNICAL REPORT (CFS PROJECT 20-1075) AND ALL ADDENDUMS PREPARED BY CFS ENGINEERS DATED JUNE 12, 2020, RECOMMENDATIONS IN GEOTECHNICAL REPORT SHALL GOVERN.

EROSION AND SEDIMENT CONTROL INSPECTION PROCEDURES
THE FOLLOWING PROCEDURES WILL BE USED TO MAINTAIN EROSION AND SEDIMENTATION CONTROLS.
1. ALL CONTROL MEASURES WILL BE INSPECTED AT LEAST ONCE A WEEK AND AFTER EACH RAINFALL EVENT PRODUCING RUNOFF AND DAILY DURING PROLONGED RAINFALL PERIODS.
2. ALL MEASURES WILL BE MAINTAINED IN GOOD WORKING ORDER. IF A REPAIR IS NECESSARY, IT WILL BE MADE WITHIN 24 HOURS OF THE INSPECTION.
3. SEDIMENT WILL BE REMOVED FROM THE SILT BARRIERS WHEN IT HAS REACHED ONE-THIRD OF THE HEIGHT OF THE BARRIER.
4. SILT BARRIERS WILL BE INSPECTED FOR DEPTH OF ACCUMULATED SEDIMENT, TEARS, ATTACHMENT TO POSTS, AND STABILITY ON A WEEKLY BASIS.
5. TEMPORARY AND PERMANENT SEEDING AND PLANTING WILL BE INSPECTED FOR BARE SPOTS, WASHOUTS, AND HEALTHY GROWTH.
6. THE CONSTRUCTION MANAGER WILL SELECT INDIVIDUALS TO BE RESPONSIBLE FOR INSPECTIONS, MAINTENANCE, REPAIRS, AND REPORTING. THE DESIGNATED INDIVIDUALS WILL RECEIVE THE NECESSARY TRAINING FROM THE CONSTRUCTION MANAGER TO PROPERLY INSPECT AND MAINTAIN THE CONTROLS IN GOOD WORKING ORDER.

UNDERGROUND UTILITY STATEMENT:
THE UNDERGROUND UTILITIES SHOWN HEREON ARE DEPICTED FROM FIELD SURVEY INFORMATION OF ONE-CALL LOCATED UTILITIES AND/OR THE SCALING AND PLOTTING OF EXISTING UTILITY MAPS AND DRAWINGS MADE AVAILABLE TO THE SURVEYOR AT THE TIME OF SURVEY. THE SURVEYOR DOES NOT CERTIFY THAT THE UNDERGROUND UTILITIES SHOWN COMPRISE ALL UNDERGROUND UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. FURTHERMORE, THE SURVEYOR DOES NOT CERTIFY THAT THE UNDERGROUND UTILITIES SHOWN ARE IN THE EXACT LOCATION DEPICTED ALTHOUGH HE DOES CERTIFY THAT THEY ARE DEPICTED AS ACCURATELY AS POSSIBLE FROM INFORMATION MADE AVAILABLE TO THE SURVEYOR AT THE TIME OF SURVEY. THE SURVEYOR HAS NOT PHYSICALLY LOCATED THE UNDERGROUND UTILITIES SHOWN HEREON BY EXCAVATION UNLESS OTHERWISE NOTED ON THIS SURVEY. MISSOURI ONE CALL TICKET NUMBER: #200431409, 200431440, 200431475, 200440745.

WARRANTY / DISCLAIMER
THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN DO WARRANTY THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR
THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS.
THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

SAFETY NOTICE TO CONTRACTOR
IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

NOTE:
1. CONTRACTOR SHALL REFER TO ARCHITECTURAL PLANS FOR EXACT LOCATIONS AND DIMENSIONS OF ENTRANCE, SLOPED PAVING, EXIT PORCHES, RAMPS, PRECISE BUILDING DIMENSIONS AND EXACT BUILDING UTILITY ENTRANCE LOCATIONS.
2. THESE PLANS HAVE NOT BEEN VERIFIED WITH FINAL ARCHITECTURAL CONTRACT DRAWINGS. CONTRACTOR SHALL VERIFY AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES. CONTRACTOR IS FULLY RESPONSIBLE FOR REVIEW AND COORDINATION OF ALL DRAWINGS AND CONTRACTOR DOCUMENTS.
3. ALL DIMENSIONS ARE TO BACK OF CURB UNLESS NOTED OTHERWISE.

NOTES:
21 MATCH EXISTING CURB ELEVATION.
22 MATCH EXISTING SIDEWALK ELEVATION.
23 MATCH EXISTING PAVEMENT ELEVATION.
24 TRANSITION FROM ZERO HEIGHT CURB TO FULL HEIGHT CURB.
25 MATCH EXISTING TRACK CURB ELEVATION.
26 MATCH EXISTING TENNIS COURT ELEVATION.
27 2% SLOPE IN ALL DIRECTIONS TO BE PROVIDED WITHIN 10' OF TICKET WINDOW.
28 MATCH EXISTING BLEACHER PAD ELEVATION.

DETAILS - SEE DETAIL SHEET NO. H-C195
830 STRAW WATTLES
ESC-01 CONSTRUCTION ENTRANCE AND CONCRETE WASHOUT
ESC-02 EROSION CONTROL BLANKETS AND TURF REINFORCEMENT MAT
ESC-03 SILT FENCE
ESC-07 AREA INLET PROTECTION

LEGEND:
AIR CONDITIONER
WALL MOUNTED ELECTRICAL OUTLET
UNDERGROUND GAS
GAS METER
CONTROL POINT
BENCHMARK
GATE POST
CHAIN LINK FENCE
WOOD FENCE
BOLLARD
PAINTED DIRECTIONAL ARROW
TURN LANE DIRECTION
HANDICAP SYMBOL
PARKING STALL COUNT
HANDICAP SIGN
HRMP
WHEEL STOP
UNDERGROUND FIBER OPTIC CABLE
UNDERGROUND FIBER OPTIC (FROM RECORDS)
TELEPHONE PEDESTAL
SANITARY SEWER MANHOLE
STORM SEWER MANHOLE
AREA INLET
CURB INLET
SANITARY SEWER CLEAN OUT
DOWN SPOUT
FLOOR DRAIN
FLARED END SECTION
SANITARY SEWER LINE
STORM SEWER LINE
CORRUGATED METAL PIPE
REINFORCED CONCRETE PIPE
WIRIIFIED CLAY PIPE
OVERHEAD ELECTRIC
UNDERGROUND UTILITY LINE (# OF LINES)
FULL BOX
LIGHT POLE
UTILITY POLE
DUCTILE IRON PIPE
HIGH DENSITY POLYETHYLENE
WALL MOUNTED LIGHT
WALL MOUNTED CAMERA
GAS VALVE
GAS RISER
GAS LINE SIGN
ENCROACHMENT IDENTIFIER
EXISTING SPOT ELEVATION
EXISTING GRADE 1' CONTOUR
EXISTING GRADE 1' CONTOUR
DOOR ELEVATION
AT THRESHOLD
FINISH FLOOR ELEVATION
BUILDING HEIGHT/ELEVATION
BACK TO BACK OF CURB MEASUREMENT
HANDICAP SIGN
EDGE TO EDGE OF ASPHALT
WATER LINE
WATER METER
WATER LINE GATE VALVE
FIRE HYDRANT
SPRINKLER CONTROL BOX
WATER MANHOLE
SPRINKLER VALVE
SIAMSE FIRE CONNECTOR
CANOPY SUPPORT
MAIL BOX
CONCRETE JOINT/CUT LINE
BUSH
DECIDUOUS TREE
TRASH ENCLOSURE
LANDSCAPING AREA
CONC
CONCRETE
LW LOWEST WIRE HEIGHT
BREAKER BOX
UNDERGROUND GAS PER RECORD
SANITARY SEWER LINE PER RECORD
WATER LINE PER RECORD
STORM SEWER LINE PER RECORD

EROSION & PROPOSED IMPROVEMENTS LEGEND:
SEDIMENTATION FENCE (ESC-03)
LIMITS OF DISTURBANCE
INLET PROTECTION (42)
STRAW WATTLE
CONCRETE WASH AREA
EROSION CONTROL BLANKET/ TURF REINFORCEMENT MAT (ESC-02)
LEGEND (PROPOSED)
22.9 SPOT ELEVATION (ADD 1000), TOP OF PAVEMENT
23.6 TOP OF CURB (ADD 1000)
23.1 FLOWLINE OF CURB (ADD 1000)
23.6 BLEACHER PAD ELEVATION (ADD 1000)
23.1 SIDEWALK ELEVATION (ADD 1000)
830 FINISHED 1' CONTOUR INTERVALS, TOP OF PAVEMENT
FLOW DIRECTION

LEGEND (PROPOSED)
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FLOW DIRECTION

SITE BENCHMARKS:
BM-60 FOUND CUT SQUARE AT THE WEST NORTHWEST CORNER OF THE WEST SIDE OF THE EAST ENTRY DRIVE TO LEE'S SUMMIT HIGH SCHOOL. ELEVATION= 1042.70
BM-61 SET CUT SQUARE WITH PUNCH IN THE SOUTHWEST EDGE ON A CONCRETE LIGHT BASE ON THE NORTH SIDE OF THE DRIVE LANE AT THE HIGH SCHOOL ADMINISTRATION CENTER ENTRY. ELEVATION= 1042.74
BM-62 SET CUT SQUARE AT THE NORTHEAST CORNER OF THE FIRST STEP UP OF A CONCRETE WALK ON THE NORTH SIDE OF THE EAST MAIN WING. ELEVATION= 1040.51
BM-63 SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF A CONCRETE PATIO WITH COVERED TABLES ON THE EAST SIDE OF BUILDING "B". ELEVATION= 1015.74
BM-64 SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF STEPS TO THE NORTH ENTRY TO BUILDING "B" ON THE WEST SIDE. ELEVATION= 1015.54

HORIZONTAL AND VERTICAL DATUM:
UNLESS OTHERWISE NOTED THE COORDINATES SHOWN HEREON ARE GROUND COORDINATES BASED ON THE MISSOURI STATE PLANE (1983) WEST ZONE (NAD 1983) (NAVD 1988)
GAF: 0.9989878
SCALED AROUND 0.0
JA-25 (PID: 095025)
NORTHING: 303646.030 (GRID/METERS) 996313.829 (GROUND/FEET)
EASTING: 860950.475 (GRID/METERS) 2824923.692 (GROUND/FEET)
ELEVATION: 321.8 (METERS) 1055.77 (FEET)

PROJECT CONTROL:
CP-220 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996572.06 (GROUND) 996470.24 (GRID)
EASTING: 2827438.76 (GROUND) 2827149.83 (GRID)
ELEV = 1049.49
CP-201 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996570.39 (GROUND) 996468.55 (GRID)
EASTING: 2827055.45 (GROUND) 2826766.55 (GRID)
ELEV = 1048.24
CP-202 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996569.25 (GROUND) 996467.41 (GRID)
EASTING: 2826689.97 (GROUND) 2826401.11 (GRID)
ELEV = 1042.52
CP-203 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996557.62 (GROUND) 996855.74 (GRID)
EASTING: 2826712.48 (GROUND) 2826423.62 (GRID)
ELEV = 1039.43
CP-204 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997397.36 (GROUND) 997295.43 (GRID)
EASTING: 2826684.55 (GROUND) 2826395.70 (GRID)
ELEV = 1023.04
CP-205 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997433.51 (GROUND) 997301.59 (GRID)
EASTING: 2826495.31 (GROUND) 2826206.47 (GRID)
ELEV = 1018.15
CP-206 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997885.83 (GROUND) 997883.94 (GRID)
EASTING: 2826567.03 (GROUND) 2826278.18 (GRID)
ELEV = 1012.56
CP-207 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997970.64 (GROUND) 997868.66 (GRID)
EASTING: 2826680.58 (GROUND) 2826571.70 (GRID)
ELEV = 1014.79

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830 FINISHED 1' CONTOUR INTERVALS, TOP OF PAVEMENT
FLOW DIRECTION

LEGEND (PROPOSED)
22.9 SPOT ELEVATION (ADD 1000), TOP OF PAVEMENT
23.6 TOP OF CURB (ADD 1000)
23.1 FLOWLINE OF CURB (ADD 1000)
23.6 BLEACHER PAD ELEVATION (ADD 1000)
23.1 SIDEWALK ELEVATION (ADD 1000)
830 FINISHED 1' CONTOUR INTERVALS, TOP OF PAVEMENT
FLOW DIRECTION

LEGEND (PROPOSED)
22.9 SPOT ELEVATION (ADD 1000), TOP OF PAVEMENT
23.6 TOP OF CURB (ADD 1000)
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23.1 SIDEWALK ELEVATION (ADD 1000)
830 FINISHED 1' CONTOUR INTERVALS, TOP OF PAVEMENT
FLOW DIRECTION

LEGEND (PROPOSED)<

Exhibit C
Drainage Area Map & Calculations
Storm Sewer Plan and Profiles
BMP Plan
EDDB Calculations

Lee's Summit High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
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Kaw Valley Engineering, Inc.
Missouri Certificate of Authority: 000842
David Wood Date: 12/15/2020
Engineer License No. PE-2011037427

REVISIONS

Number	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
2	PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

DRAINAGE AREA MAP

C600

Final Development Plan

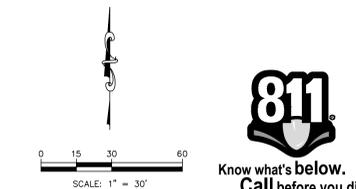
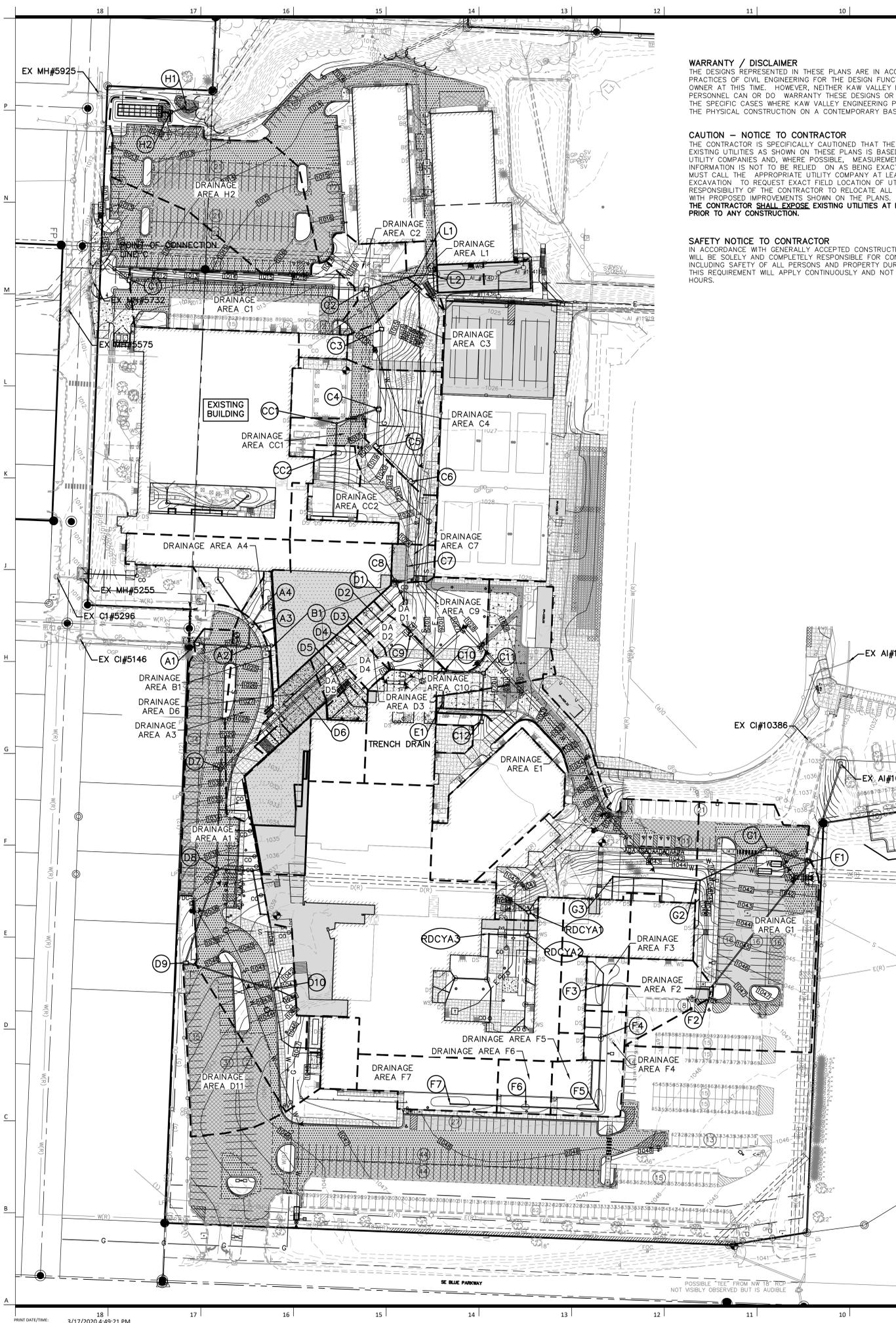
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CAUTION - NOTICE TO CONTRACTOR
THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS.
THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

SAFETY NOTICE TO CONTRACTOR
IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

Tc Calculations 11-13-2020
e's Summit High School Addition and Renovation
KVE Project # C20D0496

Structure	Pipe	Design Storm (years)	Time of Concentration										Notes
			Tributary Area A (ft ²)	Impervious Area	Runoff Coefficient, C	Total Distance	D1	Slope	Inlet Time (min)	D2	Travel Time (min)	Time of Concentration (min)	
A4	A4 - A3	10-year	0.04	0.01	0.45	30	30	2.5	4.7	0	0.0	4.7	5 Min Minimum
A3	A3 - A2	10-year	0.27	0.22	0.79	195	100	5.0	3.3	95	0.2	3.4	5 Min Minimum
A2	A2 - A1 #6375	10-year											
A1 #6375	A1 #6375 - A1	10-year											
A1	A1 - C1 #5146	10-year	1.12	0.89	0.78	625	100	5.0	3.4	525	0.9	4.3	5 Min Minimum
B1	B1 - A1	10-year											
C12	C12 - C11	10-year											
C11	C11 - C10	10-year											
C10	C10 - C9	10-year	0.60	0.57	0.87	180	100	2.0	3.3	80	0.1	3.4	5 Min Minimum
C9	C9 - C8	10-year	0.00	0.00	#DIV/0!	90	90	8.0	#DIV/0!	0	0.0	#DIV/0!	
C8	C8 - C7	10-year											
C7	C7 - C6	10-year	0.06	0.06	0.90	50	50	1.0	2.5	0	0.0	2.5	5 Min Minimum
C6	C6 - C5	10-year											
C5	C5 - C4	10-year											
C4	C4 - C3	10-year	0.46	0.16	0.51	120	100	15.0	4.3	20	0.0	4.3	5 Min Minimum
C3	C3 - C2	10-year	0.22	0.08	0.52	80	80	15.0	3.8	0	0.0	3.8	5 Min Minimum
C2	C2 - C1	10-year	0.20	0.11	0.63	80	80	6.0	2.0	0	0.0	2.0	5 Min Minimum
C1	C1 - INSERTA TEE 60" RCP	10-year	0.55	0.45	0.79	270	100	1.5	4.9	170	0.3	5.1	
CC2	CC2 - CC1	10-year											
CC1	CC1 - C4	10-year											
D10	D10 - D9	10-year											
D9	D9 - D8	10-year	0.37	0.37	0.90	220	100	6.0	3.0	120	0.2	3.2	5 Min Minimum
D8	D8 - D7	10-year											
D7	D7 - D6	10-year											
D6	D6 - D5	10-year	0.10	0.10	0.90	50	50	6.0	1.4	0	0.0	1.4	5 Min Minimum
D5	D5 - D4	10-year	0.06	0.05	0.80	50	50	6.0	2.1	0	0.0	2.1	5 Min Minimum
D4	D4 - D3	10-year	0.06	0.03	0.60	50	50	6.0	3.5	0	0.0	3.5	5 Min Minimum
D3	D3 - D2	10-year	0.05	0.02	0.54	50	50	6.0	3.9	0	0.0	3.9	5 Min Minimum
D2	D2 - D1	10-year	0.10	0.05	0.60	50	50	6.0	3.5	0	0.0	3.5	5 Min Minimum
D1	D1 - C9	10-year	0.29	0.07	0.44	50	50	6.0	4.6	0	0.0	4.6	5 Min Minimum
E1 (Dock Trench Drain)	E1 (Dock Trench Drain) - C11	10-year	1.15	0.89	0.66	460	100	5.0	4.6	360	0.6	5.2	
F7	F7 - F6	10-year	0.26	0.20	0.76	60	60	2.0	3.7	0	0.0	3.7	5 Min Minimum
F6	F6 - F5	10-year	0.11	0.08	0.74	30	30	2.0	2.8	0	0.0	2.8	5 Min Minimum
F5	F5 - F4	10-year	0.15	0.06	0.54	60	60	2.0	6.2	0	0.0	6.2	
F4	F4 - F3	10-year	0.08	0.00	0.30	30	30	2.0	6.3	0	0.0	6.3	
F3	F3 - F2	10-year	0.09	0.00	0.30	30	30	2.0	6.3	0	0.0	6.3	
F2	F2 - F1	10-year	0.19	0.09	0.58	100	100	2.0	7.4	0	0.0	7.4	
F1	F1 - A1 #10447	10-year											
G3	G3 - G2	10-year											
G2	G2 - G1	10-year											
G1	G1 - F1	10-year	1.14	1.00	0.83	340	100	4.0	3.1	240	0.4	3.5	5 Min Minimum



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Storm Sewer Calculations 11-15-2020
Lee's Summit School District - Lee's Summit High School Addition and Renovation
KVE Project # C20D0496

Lee's Summit School D



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phoenix • san francisco

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Lee's Summit High School

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Lee's Summit, MO 64063

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Lee's Summit R-7 School District
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Lee's Summit, MO 64086

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Kaw Valley Engineering, Inc.
Missouri Certificate of Authority: 000842
David Wood Date: 12/15/2020
Engineer License No. PE-2011037427

REVISIONS		
Number	DESCRIPTION	DATE
1	ADDENDUM #1 PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	11-19-2020
2		12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

STORM SEWER CALCULATIONS

C605

Final Development Plan

KVE	Design Storm (years)	Overland Flow										System Flow					Node	Pipe Design																		
		Structure	Downstream Structure	Pipe	Tributary Area, A (ac)	Impervious Area (ac)	Rainfall Coefficient	Antecedent Precipitation (in)	A-C (in)	Time of Concentration, Tc (min)	Rainfall Intensity (in/hr)	Tributary Runoff (cfs)	Total Area, A (ac)	Summation of Inlet & V.C. (ac)	Antecedent Precipitation (in)	System Tc (min)		System Rainfall Intensity (in/hr)	System Discharge (cfs)	Node Condition	Pipe Material	Pipe Shape	Pipe Size, D (in)	Manning's Coefficient	Upstream Invert (ft)	Downstream Invert (ft)	Length (ft)	Pipe Slope	Design Flow (cfs)	Full Flow Capacity (cfs)	Full Flow Velocity (fps)	Flow Time (sec)	Upstream Crown Elevation	Downstream Crown Elevation	Upstream Depth of Cover	Downstream Depth of Cover
Lee's Summit High School Addition and Renovation Private Storm Sewer	10-year	A4	A3	A4 - A3	0.04	0.01	0.45	1	0.02	5.0	7.4	0.1	0.04	0.02	1	5.0	7.4	0.1	PVC Drain Basin	HDPE	Circular	15	0.012	1019.20	1018.90	28.2	1.06%	0.1	7.2	5.9	4.8	1020.5	1020.2	2.4	3.6	1,022.90
	100-year	A4	A3	A4 - A3	0.04	0.01	0.45	1.25	0.02	5.0	10.3	0.2	0.04	0.02	1.25	5.0	10.3	0.2	Non Setback Curb Inlet	HDPE	Circular	15	0.012	1018.80	1018.30	27.9	1.08%	0.2	6.7	5.5	5.1	1019.9	1019.6	2.9	4.5	1,023.80
	10-year	A2	A1	A2 - A1	0.27	0.22	0.79	1	0.21	5.0	7.4	1.6	0.61	0.44	1	5.1	7.3	3.2	Junction Box	HDPE	Circular	15	0.013	1017.80	1017.42	43.1	1.58%	3.2	6.7	5.6	6.5	1019.1	1018.4	5.0	5.5	1,024.10
	100-year	A2	A1	A2 - A1	0.27	0.22	0.79	1.25	0.21	5.0	10.3	2.7	0.61	0.44	1.25	5.1	10.3	5.6	Junction Box	HDPE	Circular	15	0.013	1017.80	1017.42	43.1	1.58%	5.6	6.7	5.6	6.5	1019.1	1018.4	5.0	5.5	1,024.10
	10-year	A1	A1	A1 - A1	1.12	0.89	0.78	1	0.87	5.0	7.4	6.4	0.61	0.45	1	5.3	10.2	5.7	Non Setback Curb Inlet	RCP	Circular	15	0.013	1016.63	1013.55	151.2	2.04%	5.7	9.2	7.5	20.1	1017.9	1014.8	5.4	4.9	1,023.30
	100-year	A1	A1	A1 - A1	1.12	0.89	0.78	1.25	0.87	5.0	10.3	11.2	0.61	0.45	1.25	5.3	10.2	5.7	Non Setback Curb Inlet	RCP	Circular	15	0.013	1016.63	1013.55	151.2	2.04%	5.7	9.2	7.5	20.1	1017.9	1014.8	5.4	4.9	1,023.30
	10-year	B1	A1	B1 - A1				1							1				Cleanout/Trench Drain Outlet	PVC	Circular	6	0.013	1023.10	1018.60	43.5	10.34%	0.1	1.8	9.2	4.7	1023.6	1019.1	0.4	0.0	1,024.00
	100-year	B1	A1	B1 - A1				1.25							1.25				Cleanout/Trench Drain Outlet	PVC	Circular	6	0.013	1023.10	1018.60	43.5	10.34%	0.2	1.8	9.2	4.7	1023.6	1019.1	0.4	0.0	1,024.00
	10-year	C12	C11	C12 - C11				1							1				Junction Box	HDPE	Circular	15	0.012	1019.80	1018.80	63.9	1.56%	3.3	8.8	7.1	9.0	1021.1	1020.1	14.6	6.3	1,035.60
	100-year	C12	C11	C12 - C11				1.25							1.25				Junction Box	HDPE	Circular	15	0.012	1019.80	1018.80	63.9	1.56%	3.3	8.8	7.1	9.0	1021.1	1020.1	14.6	6.3	1,035.60
	10-year	C11	C10	C11 - C10				1							1				Junction Box	HDPE	Circular	15	0.012	1018.50	1018.00	51.1	0.98%	3.3	6.9	5.6	9.1	1019.8	1019.3	6.5	6.7	1,026.30
	100-year	C11	C10	C11 - C10				1.25							1.25				Junction Box	HDPE	Circular	15	0.012	1018.50	1018.00	51.1	0.98%	3.3	6.9	5.6	9.1	1019.8	1019.3	6.5	6.7	1,026.30
	10-year	C10	C9	C10 - C9	0.60	0.57	0.87	1	0.52	5.0	7.4	3.8	2.25	1.73	1	5.3	7.3	12.6	Non Setback Curb Inlet	HDPE	Circular	18	0.012	1017.70	1016.60	64.2	1.71%	12.6	14.9	8.4	7.6	1019.2	1018.1	6.7	5.0	1,025.90
	100-year	C10	C9	C10 - C9	0.60	0.57	0.87	1.25	0.52	5.0	10.3	6.7	2.25	1.73	1.25	5.3	10.2	22.1	Non Setback Curb Inlet	HDPE	Circular	18	0.012	1017.70	1016.60	64.2	1.71%	12.6	14.9	8.4	7.6	1019.2	1018.1	6.7	5.0	1,025.90
	10-year	C9	C8	C9 - C8				1							1				Junction Box	HDPE	Circular	24	0.012	1016.10	1015.80	42.4	0.71%	22.0	20.6	6.6	6.5	1018.1	1017.8	5.0	5.8	1,023.10
	100-year	C9	C8	C9 - C8				1.25							1.25				Junction Box	HDPE	Circular	24	0.012	1016.10	1015.80	42.4	0.71%	22.0	20.6	6.6	6.5	1018.1	1017.8	5.0	5.8	1,023.10
	10-year	C8	C7	C8 - C7				1							1				Junction Box	HDPE	Circular	30	0.012	1015.30	1014.80	48.4	1.03%	30.5	45.2	9.2	5.3	1017.8	1017.3	5.8	6.7	1,023.60
	100-year	C8	C7	C8 - C7				1.25							1.25				Junction Box	HDPE	Circular	30	0.012	1015.30	1014.80	48.4	1.03%	30.5	45.2	9.2	5.3	1017.8	1017.3	5.8	6.7	1,023.60
	10-year	C7	C6	C7 - C6	0.06	0.06	0.90	1	0.05	5.0	7.4	0.4	6.12	4.91	1	9.2	6.2	30.7	Area Inlet	HDPE	Circular	30	0.012	1014.80	1013.70	109.3	1.01%	30.7	44.6	9.1	12.0	1017.3	1016.2	6.7	8.3	1,024.00
	100-year	C7	C6	C7 - C6	0.06	0.06	0.90	1.25	0.05	5.0	10.3	0.7	6.12	4.91	1.25	9.2	6.2	30.5	Area Inlet	HDPE	Circular	30	0.012	1014.80	1013.70	109.3	1.01%	30.7	44.6	9.1	12.0	1017.3	1016.2	6.7	8.3	1,024.00
	10-year	C6	C5	C6 - C5				1							1				Junction Box	HDPE	Circular	30	0.012	1013.50	1012.90	64.8	0.93%	30.5	42.8	8.7	7.4	1016.0	1015.4	8.5	3.1	1,024.50
	100-year	C6	C5	C6 - C5				1.25							1.25				Junction Box	HDPE	Circular	30	0.012	1013.50	1012.90	64.8	0.93%	30.5	42.8	8.7	7.4	1016.0	1015.4	8.5	3.1	1,024.50
	10-year	C5	C4	C5 - C4				1							1				Junction Box	HDPE	Circular	30	0.012	1009.50	1009.00	48.8	1.02%	30.4	45.0	9.2	5.3	1012.0	1011.5	6.5	3.3	1,018.50
	100-year	C5	C4	C5 - C4				1.25							1.25				Junction Box	HDPE	Circular	30	0.012	1009.50	1009.00	48.8	1.02%	30.4	45.0	9.2	5.3	1012.0	1011.5	6.5	3.3	1,018.50
	10-year	C4	C3	C4 - C3	0.46	0.16	0.51	1	0.23	5.0	7.4	1.7	7.11	5.45	1	9.6	6.2	33.6	Grate Inlet	HDPE	Circular	30	0.012	1008.80	1007.70	104.7	1.05%	33.6	45.5	9.3	11.3	1011.3	1010.2	3.5	4.0	1,014.80
	100-year	C4	C3	C4 - C3	0.46	0.16	0.51	1.25	0.23	5.0	10.3	3.0	7.11	5.45	1.25	9.6	6.2	33.6	Grate Inlet	HDPE	Circular	30	0.012	1008.80	1007.70	104.7	1.05%	33.6	45.5	9.3	11.3	1011.3	1010.2	3.5	4.0	1,014.80
	10-year	C3	C2	C3 - C2	0.22	0.08	0.52	1	0.11	5.0	7.4	0.8	7.33	5.57	1	9.7	6.1	34.1	Grate Inlet	HDPE	Circular	30	0.012	1007.50	1006.90	55.7	1.08%	34.1	46.1	9.4	5.9	1010.0	1009.4	4.2	4.3	1,014.20
	100-year	C3	C2	C3 - C2	0.22	0.08	0.52	1.25	0.11	5.0	10.3	1.5	7.33	5.57	1.25	9.7	6.1	34.1	Grate Inlet	HDPE	Circular	30	0.012	1007.50	1006.90	55.7	1.08%	34.1	46.1	9.4	5.9	1010.0	1009.4	4.2	4.3	1,014.20
	10-year	C2	C1	C2 - C1	0.20	0.11	0.63	1	0.13	5.0	7.4	0.9	7.64	5.79	1	10.3	6.0	34.8	Grate Inlet	HDPE	Circular	30	0.012	1006.70	1003.60	307.5	1.01%	34.8	44.6	9.1	33.8	1009.2	1006.1	4.5	4.5	1,013.70
	100-year	C2	C1	C2 - C1	0.20	0.11	0.63	1.25	0.13	5.0	10.3	1.6	7.64	5.79	1.25	10.3	6.0	34.8	Grate Inlet	HDPE	Circular	30	0.012	1006.70	1003.60	307.5	1.01%	34.8	44.6	9.1	33.8	1009.2	1006.1	4.5	4.5	1,013.70
	10-year	C1	INSERTA TEE 60" RCP	C1 - INSERTA TEE 60" RCP	0.55	0.45	0.79	1	0.44	5.1	7.4	3.2	8.19	6.23	1	10.3	6.0	37.4	Non Setback Curb Inlet/Yard Inlet	HDPE	Circular	30	0.012	1003.40	1002.90	36.7	1.36%	37.4	51.9	10.6	3.5	1005.9	1005.4	4.7	5.6	1,010.60
	100-year	C1	INSERTA TEE 60" RCP	C1 - INSERTA TEE 60" RCP	0.55	0.45	0.79	1.25	0.44	5.1	10.3	5.6	8.19	6.23	1.25																					

Lee's Summit High School

400 SE Blue Pkwy
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David Wood
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Engineer License No. PE-2011037427

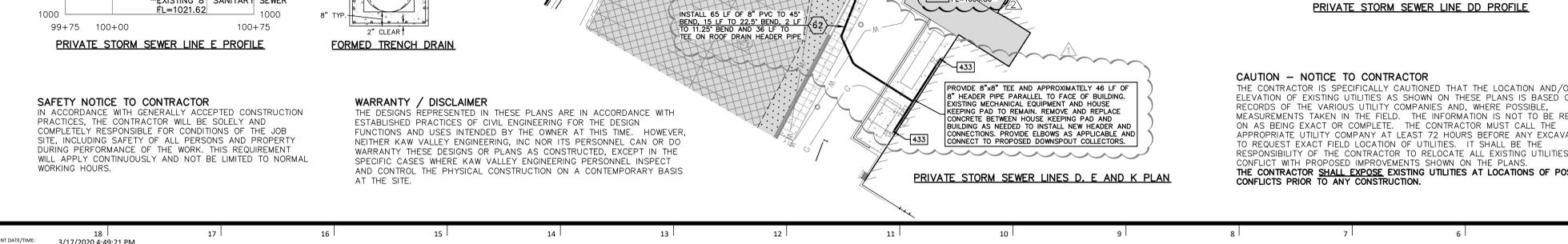
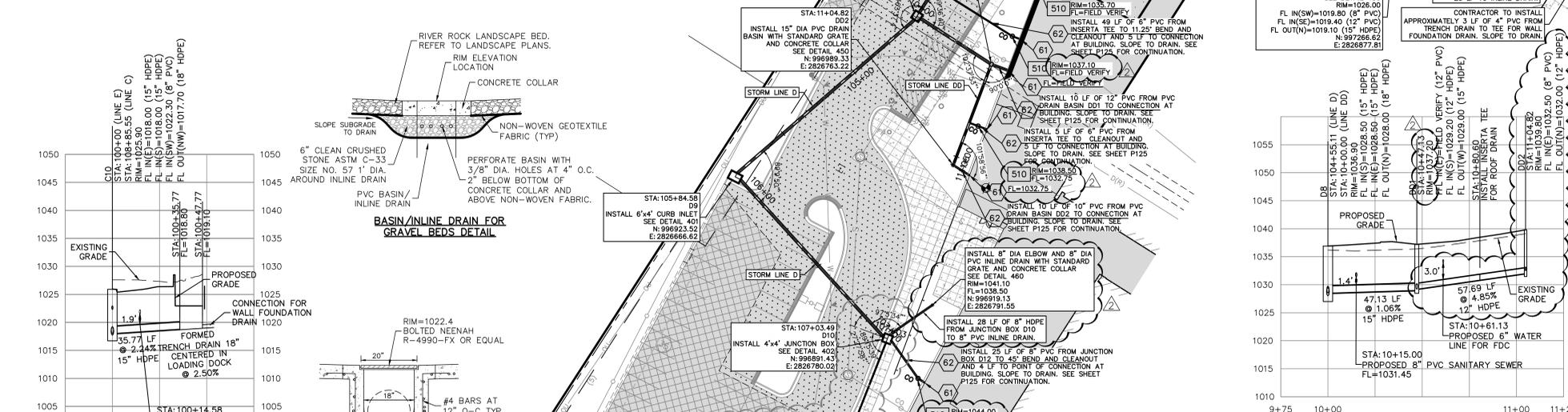
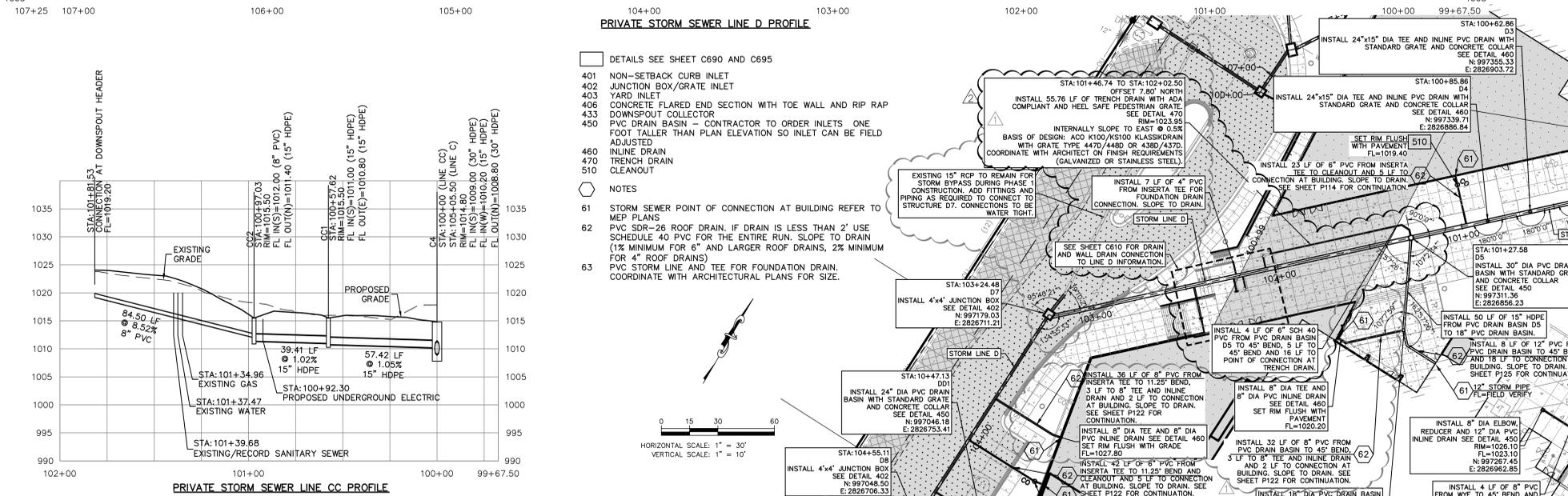
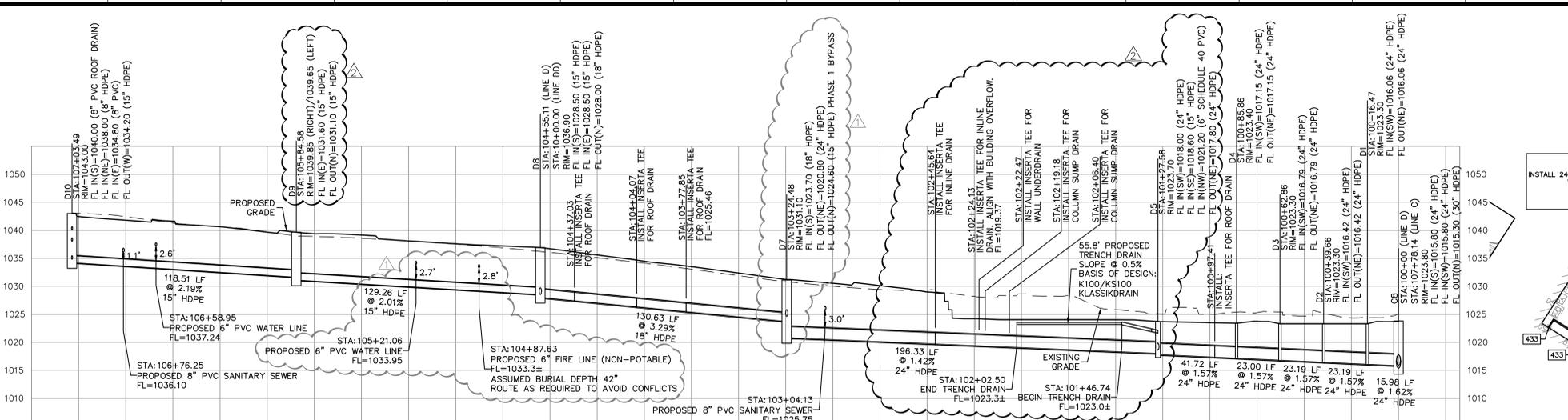
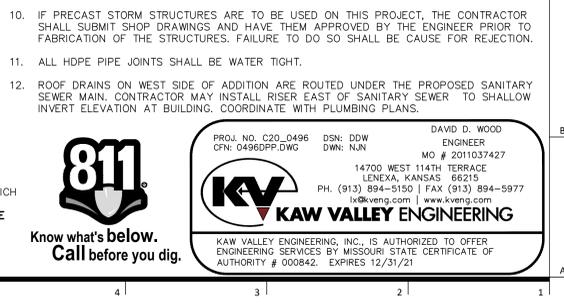
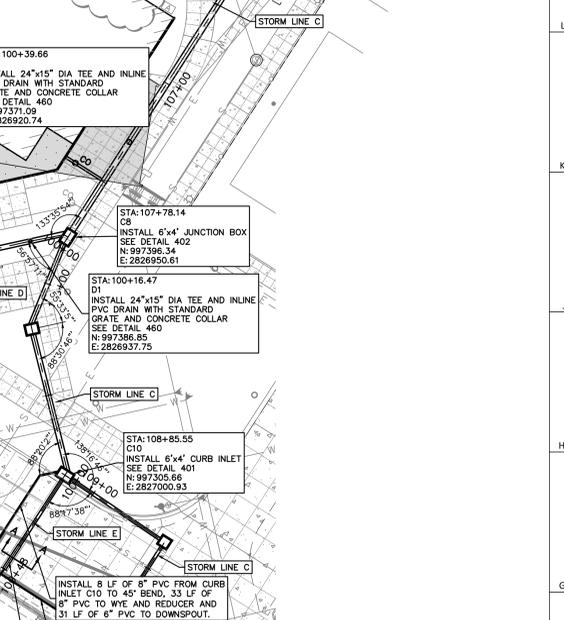
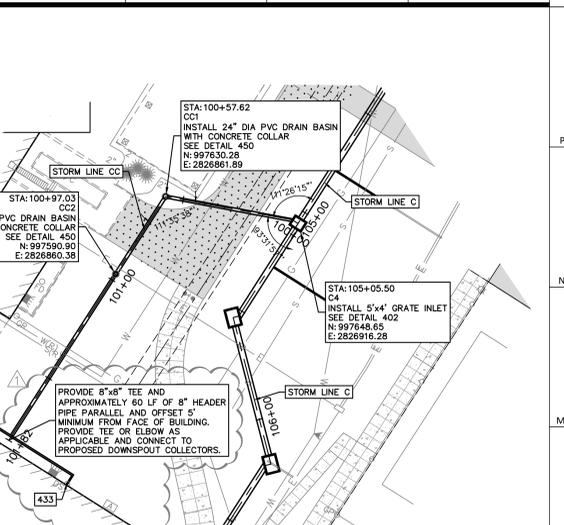
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Number	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
2	PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

PRIVATE STORM SEWER PLAN AND PROFILE

C630

Final Development Plan



PRINT DATE/TIME: 3/17/2020 4:49:21 PM

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11. ALL HDPE PIPE JOINTS SHALL BE WATER TIGHT.
12. ROOF DRAINS ON WEST SIDE OF ADDITION ARE ROUTED UNDER THE PROPOSED SANITARY SEWER MAIN. CONTRACTOR MAY INSTALL RISER EAST OF SANITARY SEWER TO ALLOW INVERT ELEVATION AT BUILDING. COORDINATE WITH PLUMBING PLANS.

PROJ. NO. C20_0496 DSK: DWN ENGINEER
CFN: 0496DD.DWG DWN: NJW MO # 2011037427
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LENEXA, KANSAS 66215
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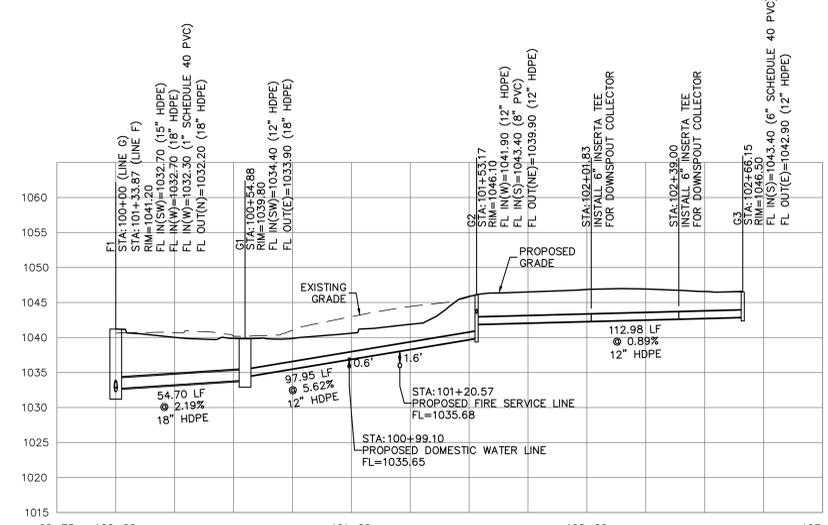
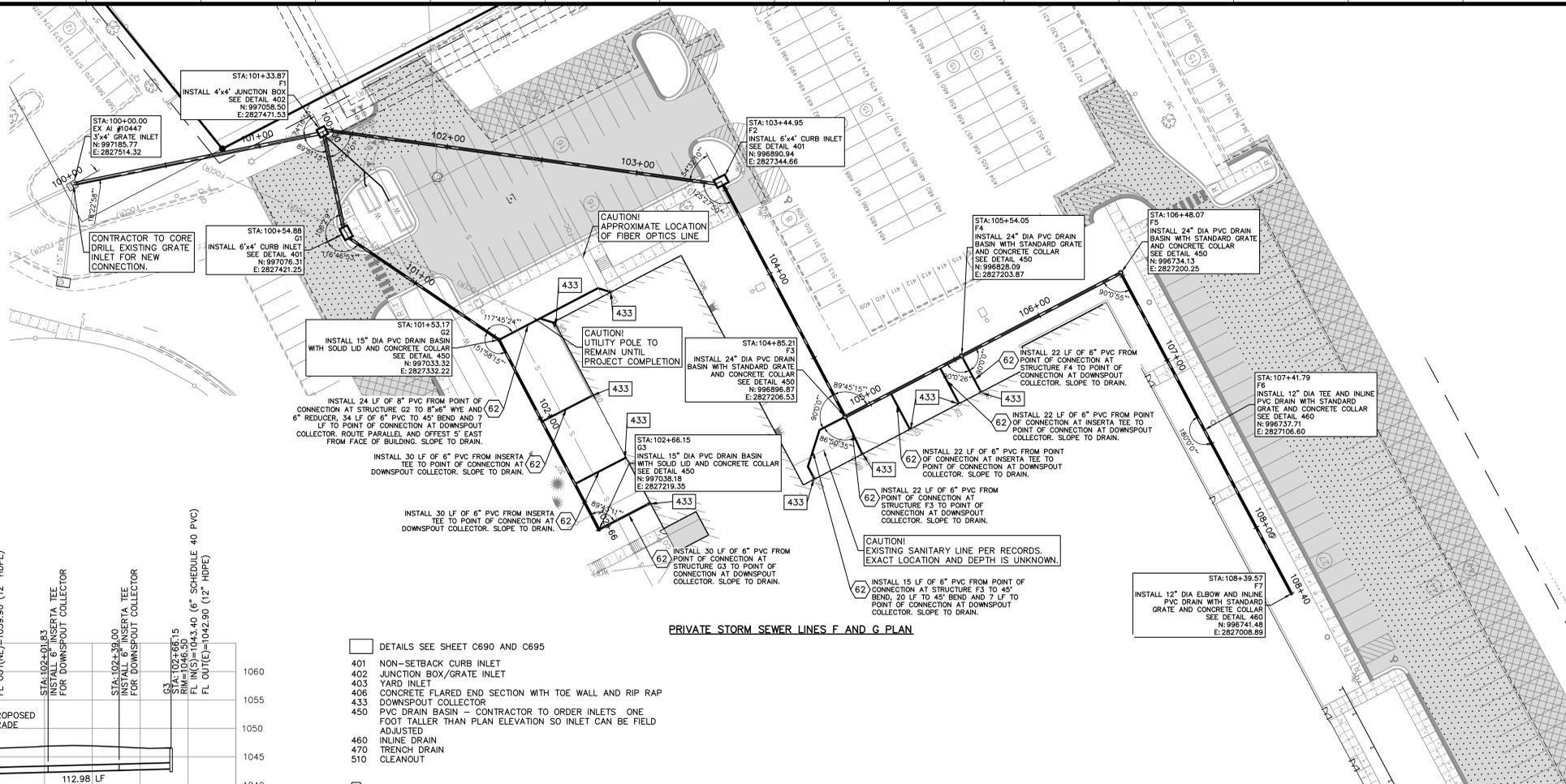
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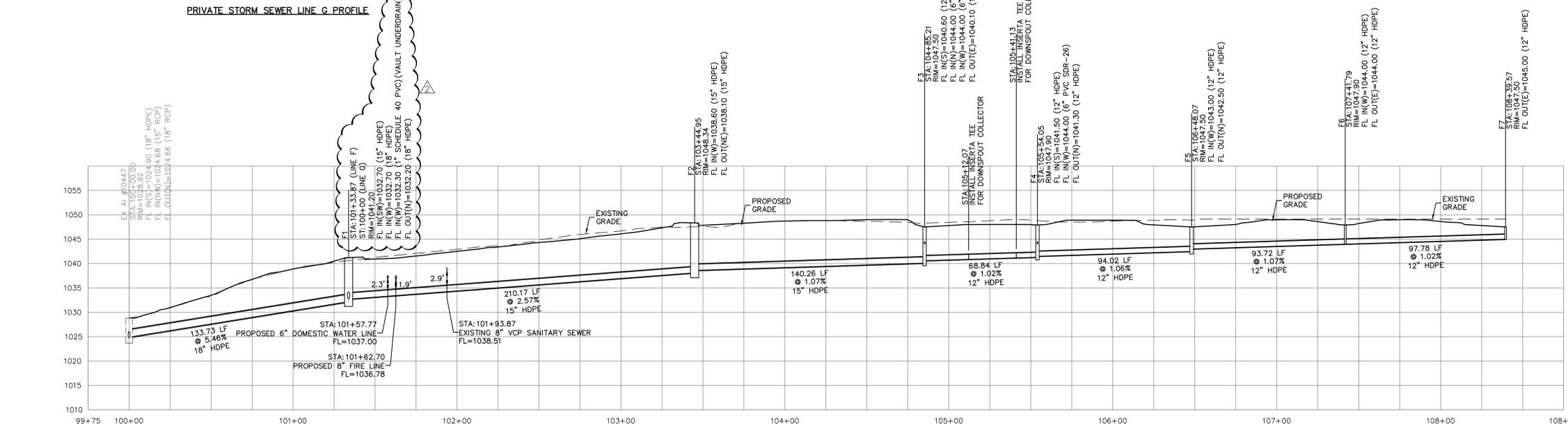
mechanical/electrical engineer:
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- 401 NON-SETBACK CURB INLET
 - 402 JUNCTION BOX/GRATE INLET
 - 403 YARD INLET
 - 406 CONCRETE FLARED END SECTION WITH TOE WALL AND RIP RAP
 - 433 DOWNSPOUT COLLECTOR
 - 450 PVC DRAIN BASIN - CONTRACTOR TO ORDER INLETS ONE FOOT TALLER THAN PLAN ELEVATION SO INLET CAN BE FIELD ADJUSTED
 - 460 INLINE DRAIN
 - 470 TRENCH DRAIN
 - 510 CLEANOUT
- NOTES
- 61 STORM SEWER POINT OF CONNECTION AT BUILDING REFER TO MEP PLANS
 - 62 PVC SDR-26 ROOF DRAIN, IF DRAIN IS LESS THAN 2' USE SCHEDULE 40 PVC FOR THE ENTIRE RUN. SLOPE TO DRAIN (1% MINIMUM FOR 6\"/>



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PROJ. NO. C20_0496 DSN: DWG DAVID D. WOOD
CFN: 0496DPP.DWG DWN: NUN MO # 2011037427

KV KAW VALLEY ENGINEERING
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
PH. (913) 894-5150 | FAX (913) 894-5977
kv@kveng.com | www.kveng.com

KAW VALLEY ENGINEERING, INC. IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000842. EXPIRES 12/31/21

PRIVATE STORM SEWER PLAN AND PROFILE

C640

Final Development Plan

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Kaw Valley Engineering, Inc.
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David Wood Date: 12/15/2020
Engineer License No. PE-2011037427

Number	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
2	PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

Lee's Summit High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

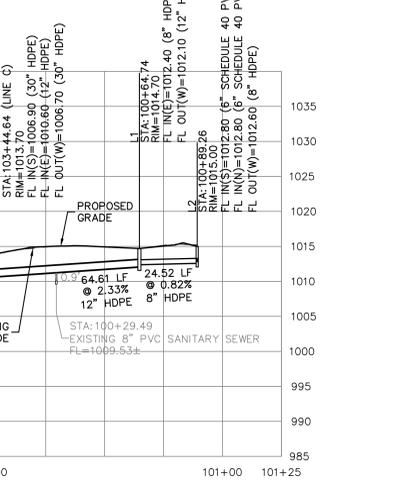
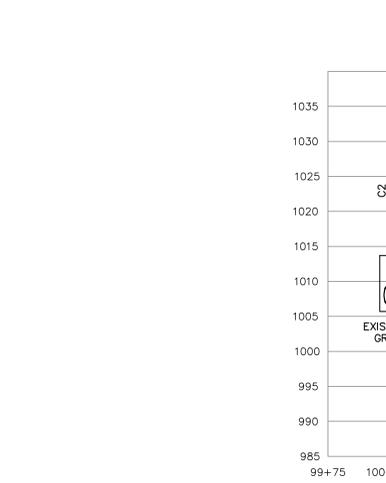
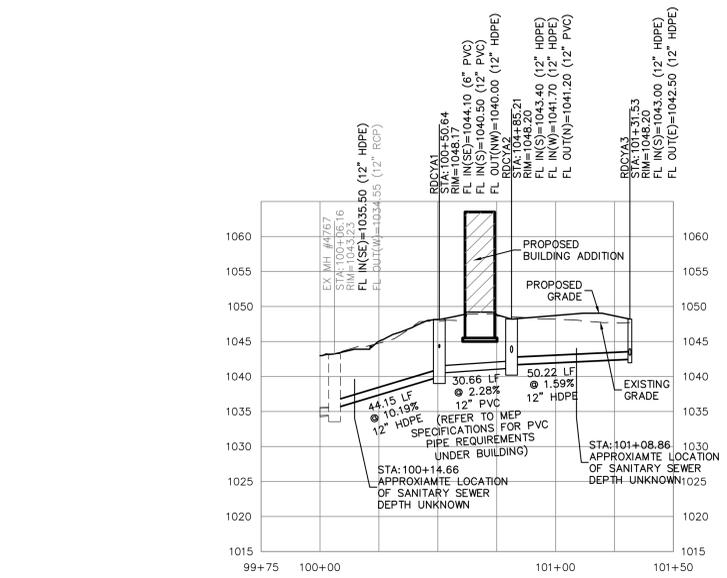
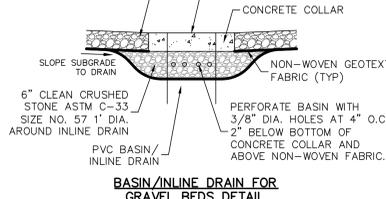
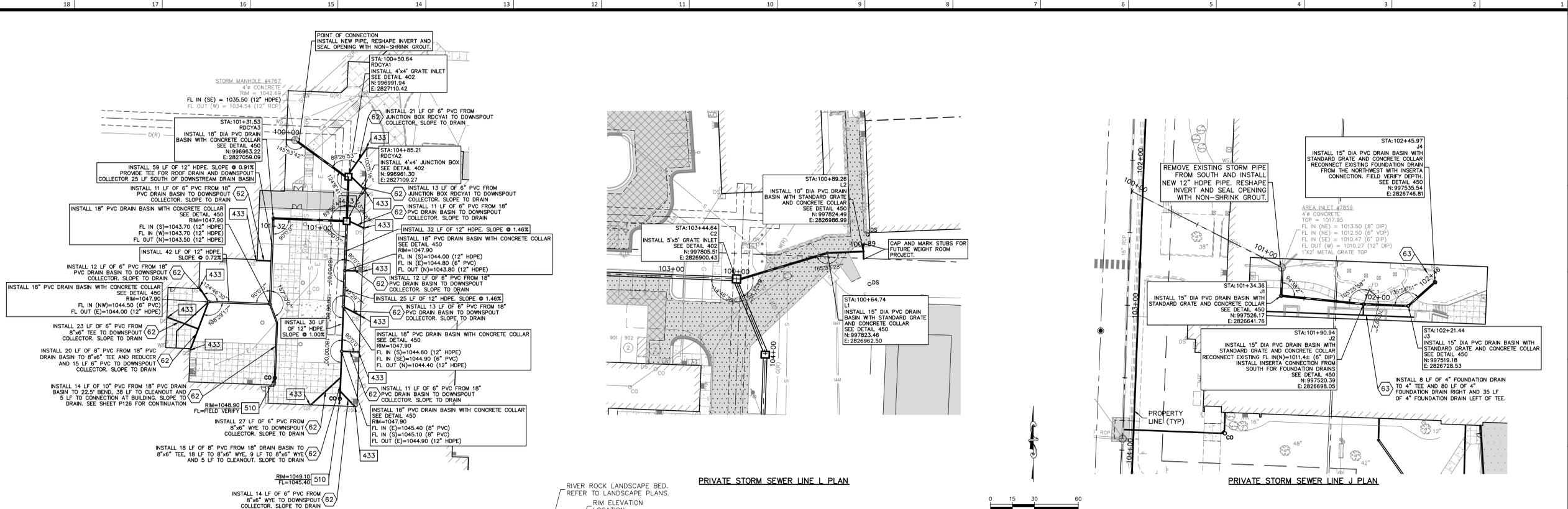
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- | | |
|---|---|
| <ul style="list-style-type: none"> 401 NON-SETBACK CURB INLET 402 JUNCTION BOX/GRATE INLET 403 YARD INLET 406 CONCRETE FLARED END SECTION WITH TOE WALL AND RIP RAP 433 DOWNSPOUT COLLECTOR 450 PVC DRAIN BASIN - CONTRACTOR TO ORDER INLETS ONE FOOT TALLER THAN PLAN ELEVATION SO INLET CAN BE FIELD ADJUSTED 460 INLINE DRAIN 470 TRENCH DRAIN 510 CLEANOUT | <ul style="list-style-type: none"> 61 STORM SEWER POINT OF CONNECTION AT BUILDING REFER TO MEP PLANS 62 PVC SDR-26 ROOF DRAIN, IF DRAIN IS LESS THAN 2' USE SCHEDULE 40 PVC FOR THE ENTIRE RUN. SLOPE TO DRAIN (1% MINIMUM FOR 6" AND LARGER ROOF DRAINS, 2% MINIMUM FOR 4" ROOF DRAINS) 63 PVC STORM LINE AND TEE FOR FOUNDATION DRAIN. COORDINATE WITH ARCHITECTURAL PLANS FOR SIZE. |
|---|---|

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PROJECT NO: 0119-0100
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PRIVATE STORM SEWER PLAN AND PROFILE

C650

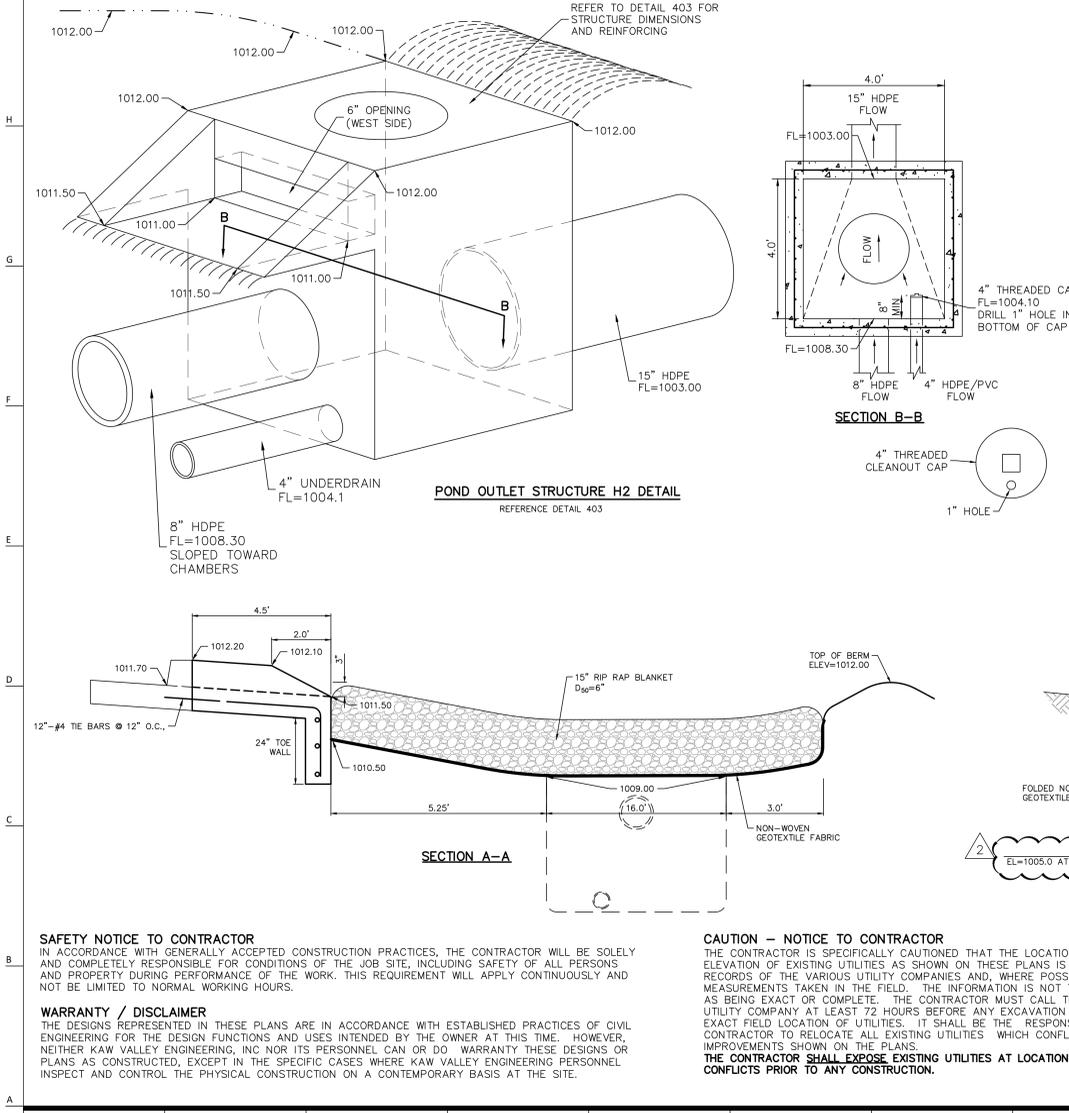
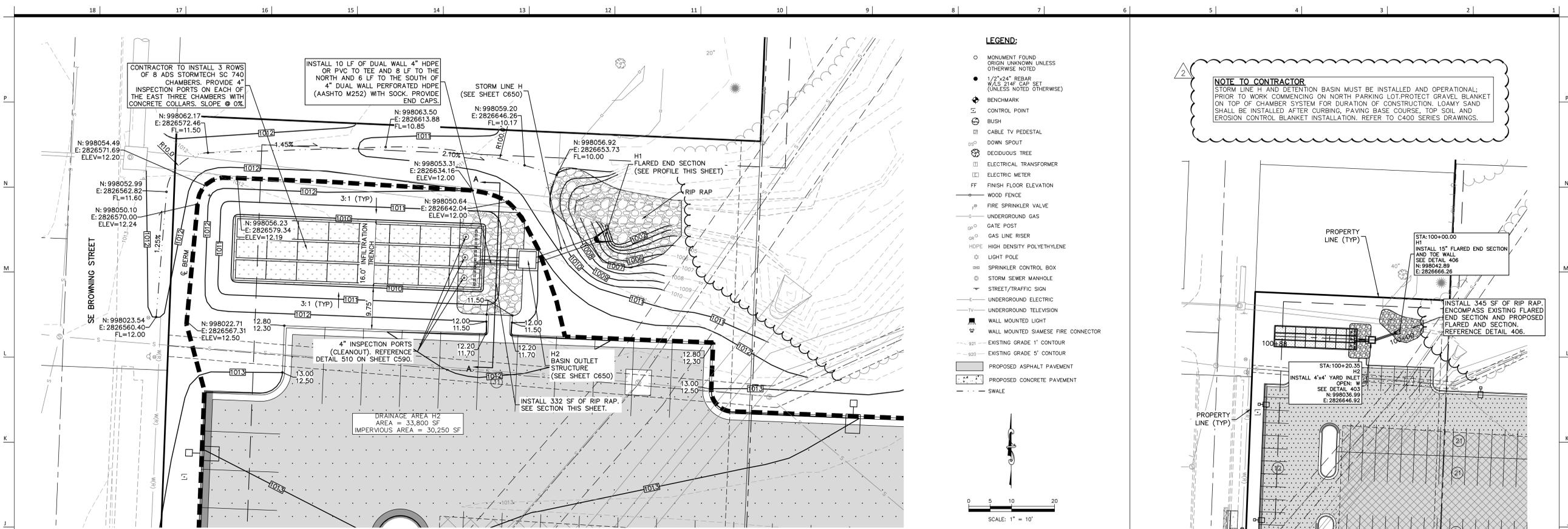
Final Development Plan



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Pond Volume			Detention Pond		
Elevation	Cum CF	ac-ft	Elevation	Surface Area (sf)	Surface Area (ac)
1005.5	0	0	1010	940	0.022
1006	141	0.003	1011	1430	0.033
1007	841	0.019	1011.5	1700	0.039
1008	1429	0.033	1011.7	1900	0.044
1009	1759	0.040			
1010	1759	0.040			
1011	2004	0.046			
1012	3704	0.085			

PLANTING SCHEDULE		
QTY.	BOTANICAL NAME	COMMON NAME
940 SF COVERAGE	ANDROPOGON GERARDII	BIG BLUE STEM (CENTER)
2' O.C.	PANICUM VIRGATUM	SWITCH GRASS (CENTER)
	SCHIZACHYRIUM SCOPARIUM	LITTLE BLUE STEM (PERIMETER)

LOCAL SOURCE
APPLIED ECOLOGIST SOLUTIONS
1269 N 222 ROAD
BALDWIN CITY, KS 66006
PH: 785-594-2245

NATIVE GRASSES (PLUGS 24" ON CENTER AT ELEVATION 1010.50 AND BELOW)
NOTE: SLOPES SHALL BE STABILIZED PRIOR TO PLANTING PERMANENT VEGETATION. UPSTREAM EROSION CONTROL SHALL REMAIN IN PLACE UNTIL VEGETATION IN BASIN IS ESTABLISHED.

SAFETY NOTICE TO CONTRACTOR
IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

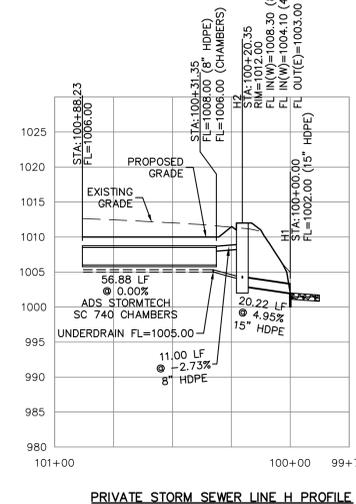
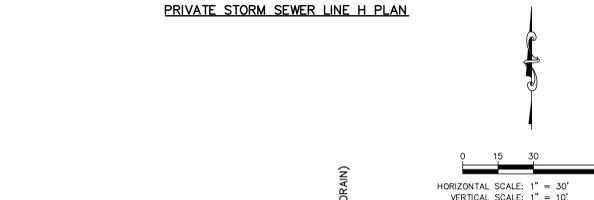
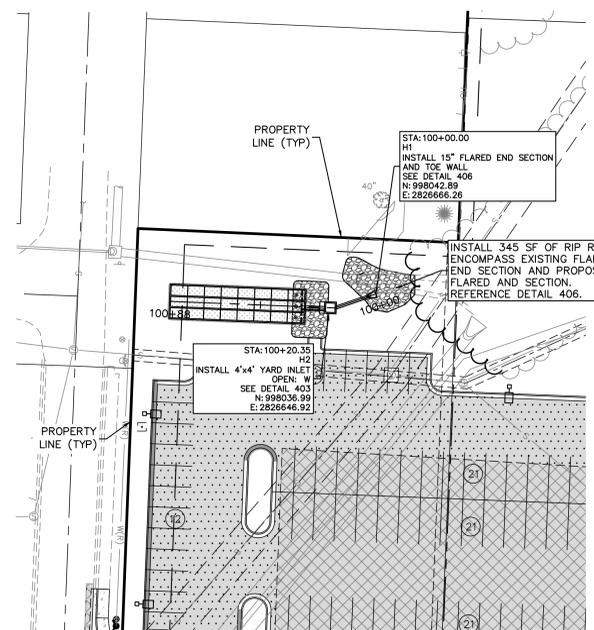
WARRANTY / DISCLAIMER
THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN OR DO WARRANTY THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR
THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS.
THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

INFILTRATION TRENCH
MINIMUM SURFACE ELEVATION = 940 SF
VOLUMETRIC STORAGE FOR INFILTRATION = 1320 CF

NOTE:
SIDES AND BOTTOM OF INFILTRATION TRENCH MUST BE LINED WITH GEOTEXTILE FABRIC (FILTER FABRIC)

NOTE TO CONTRACTOR
STORM LINE H AND DETENTION BASIN MUST BE INSTALLED AND OPERATIONAL PRIOR TO WORK COMMENCING ON NORTH PARKING LOT. PROTECT GRAVEL BLANKET ON TOP OF CHAMBER SYSTEM FOR DURATION OF CONSTRUCTION. LOAMY SAND SHALL BE INSTALLED AFTER CURBING, PAVING BASE COURSE, TOP SOIL AND EROSION CONTROL BLANKET INSTALLATION. REFER TO C400 SERIES DRAWINGS.



PRIVATE STORM SEWER LINE H PROFILE



PROJ. NO. C20_0496 DSN: DDW ENGINEER
 CFN: 0496BMP.DWG DWN: NJN MO # 201037427
 14700 WEST 124TH TERRACE
 LENEXA, KANSAS 66215
 PH. (913) 894-5150 | FAX (913) 894-5977
 kv@kve.com | www.kve.com

KAW VALLEY ENGINEERING

KAW VALLEY ENGINEERING, INC. IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000842. EXPIRES 12/31/21

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phoenix • san francisco

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Lee's Summit High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4200 Pennsylvania Avenue
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structural engineer:
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14700 West 124th Terrace
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mechanical/electrical engineer:
Henderson Engineering
1801 Main St
Kansas City, MO 64108
816.663.3700

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Kaw Valley Engineering, Inc.
Missouri Certificate of Authority: 000842
David Wood Date: 12/15/2020
Engineer License No. PE-2011037427

REVISIONS

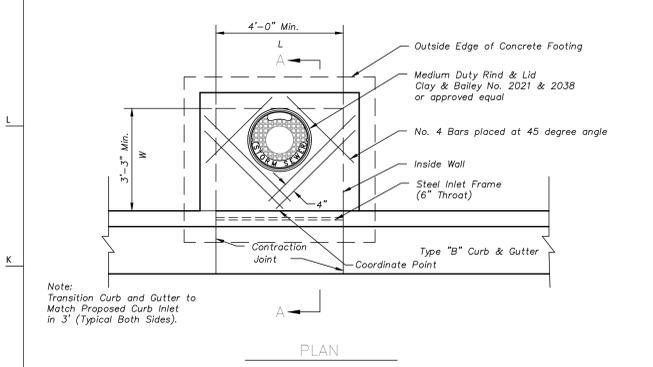
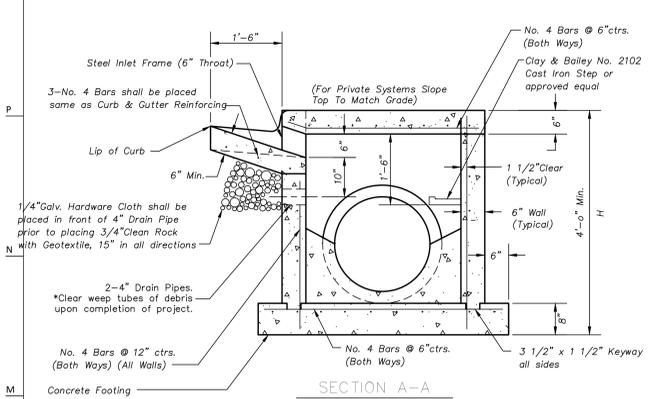
Number	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
2	PER CITY COMMENTS AND COORDINATION WITH PACKAGE 2	12-15-2020

PROJECT NO: 0119-0100
DATE: November 20, 2020

BMP PLAN

C660

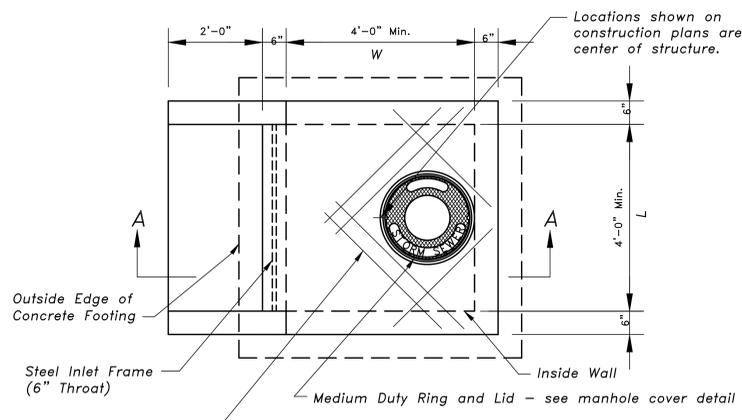
Final Development Plan



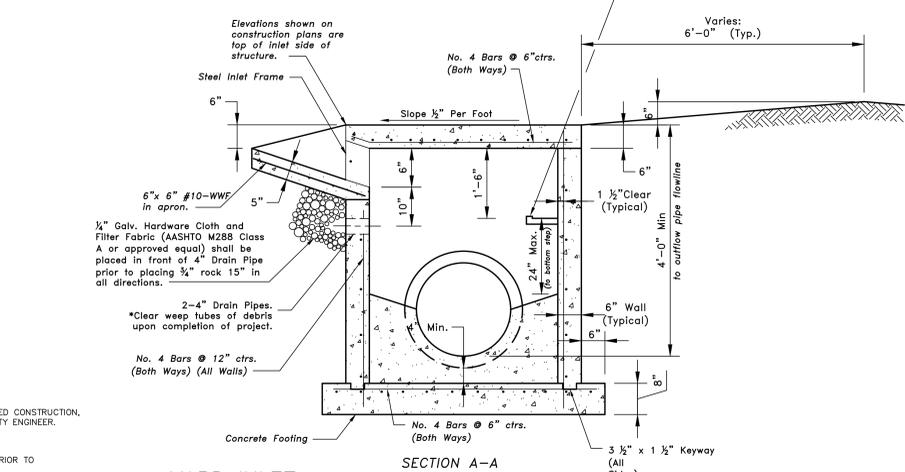
NON-SETBACK CURB INLET
 USE STEEL INLET FRAME WITH 6" THROAT
 PARKING LOTS ONLY

JUNCTION BOX YARD INLETS AND CURB INLET NOTES

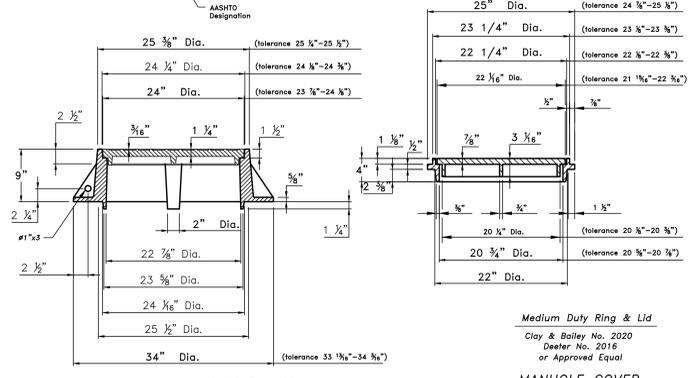
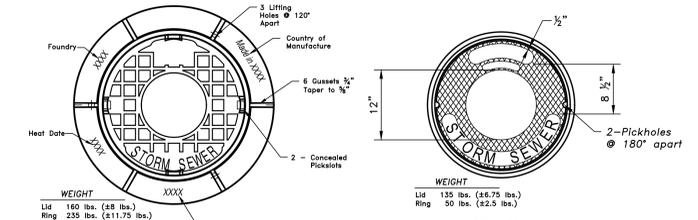
- GENERAL**
- ALL STORM SEWER STRUCTURES SHALL BE PRE-CAST OR POURED IN PLACE. IF PRE-CAST STRUCTURES ARE USED FOR PUBLICLY FINANCED, MAINTAINED OR ADMINISTERED CONSTRUCTION, THE TOPS SHALL BE POURED IN PLACE AND THE WALL STEEL SHALL BE LEFT EXPOSED TO A HEIGHT 2" BELOW THE FINISH TOP ELEVATION, OR AS DIRECTED BY THE CITY ENGINEER.
 - PRE-CAST SHOP DRAWINGS ARE TO BE APPROVED BY THE ENGINEER.
 - DO NOT SCALE THESE DRAWINGS FOR DIMENSIONS OR CLEARANCES. ANY QUESTIONS REGARDING DIMENSIONS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO CONSTRUCTION.
 - THE FIRST DIMENSION LISTED IN THE CONSTRUCTION NOTES IS THE "L" DIMENSION, THE SECOND DIMENSION IS THE "W" DIMENSION. THE CONCRETE THICKNESS AND REINFORCEMENT SHOWN IS FOR BOXES WITH ("L"+"H") AND ("W"+"H") LESS THEN OR EQUAL TO 20. FOR BOXES WITH EITHER OF THESE CALCULATIONS GREATER THAN 20, A SPECIAL DESIGN IS REQUIRED. PRECASTER SHALL PROVIDE DESIGN CALCULATIONS FOR DEEP STRUCTURES TO ENGINEER PRIOR TO CONSTRUCTING BOX.
- CONCRETE**
- CONCRETE USED IN THIS WORK SHALL BE CLASS "A" CONCRETE (AE) THROUGHOUT, AND SHALL MEET THE REQUIREMENTS OF THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.
 - CONCRETE CONSTRUCTION SHALL MEET THE APPLICABLE REQUIREMENTS OF STANDARD SPECIFICATIONS FOR MCB, LATEST EDITION, EXCEPT AS MODIFIED IN THE APWA TECHNICAL SPECIFICATIONS.
 - INLET FLOORS SHALL BE SHAPED WITH NON-REINFORCED CONCRETE INVERTS TO PROVIDE SMOOTH FLOW.
 - BEVEL ALL EXPOSED EDGES WITH 3/4" TRIANGULAR MOLDING.
 - 8" SOLID CONCRETE BLOCK OR BRICK MAY BE USED IN WALLS IN LIEU OF POURED CONCRETE WHERE NEITHER "H"+"L" NOR "H"+"W" (IN FEET) EXCEED FOURTEEN. BLOCK OR BRICK MAY BE USED IN ANY BOX WHERE "H" IS 5' OR LESS.
 - ALL CRUSHED STONE USED AS AGGREGATE FOR CONCRETE CONSTRUCTION SHALL BE OBTAINED FROM QUARRIES AND BEDS DESIGNATED BY THE MISSOURI DEPARTMENT OF TRANSPORTATION AS MEETING DURABILITY REQUIREMENTS OF KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.
- REINFORCING STEEL**
- REINFORCING STEEL SHALL BE NEW BILLET, MINIMUM GRADE 60 AS PER ASTM A615, AND SHALL BE BENT COLD.
 - ALL DIMENSIONS RELATIVE TO REINFORCING STEEL ARE TO CENTERLINE OF BARS. 2" CLEARANCE SHALL BE PROVIDED THROUGHOUT UNLESS NOTED OTHERWISE. TOLERANCE OF +/- 1/8" SHALL BE PERMITTED.
 - ALL LAP SPLICES NOT SHOWN SHALL BE A MINIMUM OF 40 BAR DIAMETERS IN LENGTH.
 - ALL REINFORCING STEEL SHALL BE SUPPORTED ON FABRICATED STEEL BAR SUPPORTS @ 3'-0" MAXIMUM SPACING.
 - ALL DOWELS SHALL BE ACCURATELY PLACED AND SECURELY TIED IN PLACE PRIOR TO PLACEMENT OF BOTTOM SLAB CONCRETE. STOKING OF DOWELS INTO FRESH OR PARTIALLY HARDENED CONCRETE WILL NOT BE ACCEPTABLE.
- CONSTRUCTION**
- THE BOTTOM SLAB SHALL BE AT LEAST 24 HOURS OLD BEFORE PLACING SIDEWALL CONCRETE. ALL SIDEWALL FORMS SHALL REMAIN IN PLACE A MINIMUM OF 24 HOURS AFTER SIDEWALLS ARE POURED BEFORE REMOVAL, AND AFTER REMOVAL SHALL BE IMMEDIATELY TREATED WITH MEMBRANE CURING COMPOUND.
 - PIPE CONNECTIONS TO PRE-CAST STRUCTURES SHALL HAVE A MINIMUM OF 6" OF CONCRETE AROUND THE ENTIRE PIPE WITHIN 2' OF THE STRUCTURE.
 - MATERIAL SELECTION AND COMPACTION REQUIREMENTS FOR BACKFILL AROUND STRUCTURES SHALL BE AS SPECIFIED IN THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.



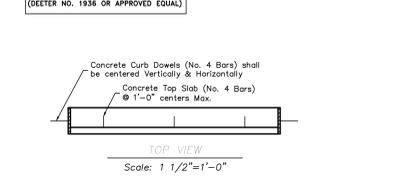
YARD INLET
 Scale: 1/2"=1'-0"



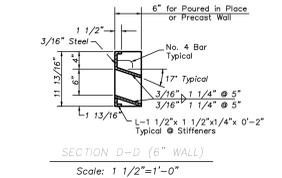
SECTION A-A
 Scale: 3/4"=1'-0"



MANHOLE COVER
 (Public Systems Only)
 SCALE: 1/2"=1'-0"
 1/200, Feb. 2005



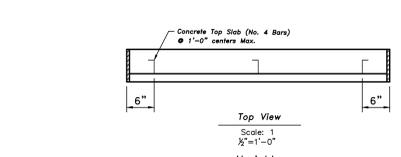
HEAVY DUTY RING & LID
 Scale: 1 1/2"=1'-0"



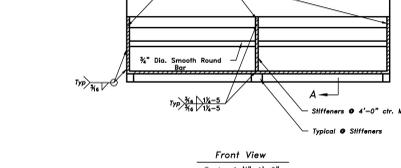
SECTION D-D (6" WALL)
 Scale: 1 1/2"=1'-0"

- Notes: 1. All Welds shall be performed in accordance with appropriate AWS Specifications & Procedures.
 2. All Welds on Exposed Surfaces shall be dressed so as to provide a pleasing finished appearance.
 3. The Entire Frame shall be Hot Dip Zinc in Accordance ASTM A-123

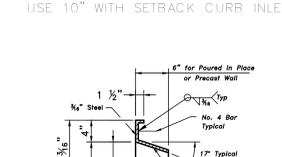
STEEL INLET FRAME (6" AND 10" THROAT)
 USE 6" WITH NON-SETBACK CURB INLET/AREA INLET
 USE 10" WITH SETBACK CURB INLET



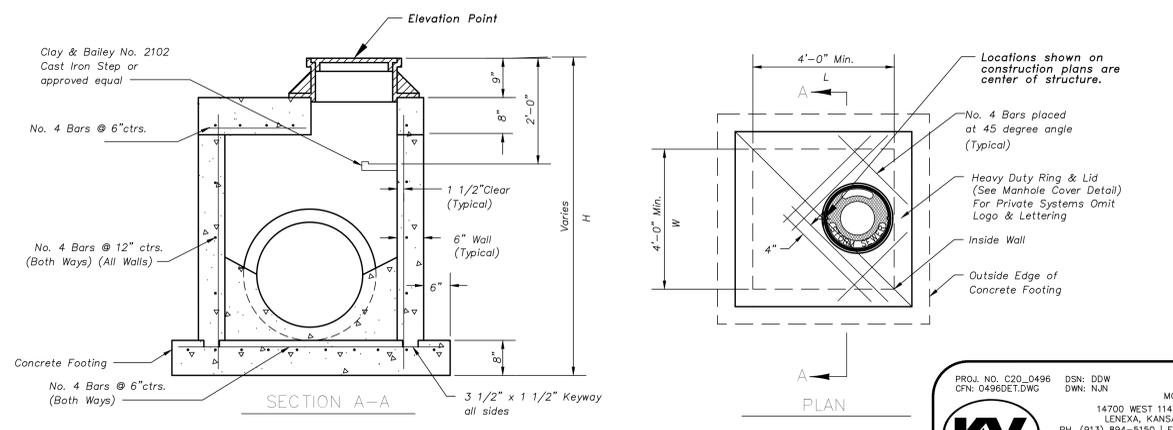
Top View
 Scale: 1 1/2"=1'-0"



Front View
 Scale: 1 1/2"=1'-0"



SECTION A-A
 Scale: 1 1/2"=1'-0"



JUNCTION BOX/GRATE INLET
 Scale: 1/2"=1'-0"

FOR JUNCTION BOX WITH GRATE, USE CATCH BASIN INLET GRATE AND FRAME (DEETER NO. 1936 OR APPROVED EQUAL)

PROJ. NO. C20_0496 DSN: DDW DAVID D. WOOD
 CFN: 0496DET.DWG DWN: NJN ENGINEER
 MO # 201037427
 14700 WEST 114TH TERRACE
 LENEXA, KANSAS 66215
 PH. (913) 894-5150 | FAX (913) 894-5977
 kv@kve.com | www.kve.com

KV KAW VALLEY ENGINEERING

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Lee's Summit High School

400 SE Blue Pkwy
 Lee's Summit, MO 64063
 owner:
 Lee's Summit R-7 School District
 301 NE Tudor Road
 Lee's Summit, MO 64086

architect:
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 4338 Bellevue
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mechanical/electrical engineer:
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Kaw Valley Engineering, Inc.
 Missouri Certificate of Authority: 000842
 David Wood Date: 12/15/2020
 Engineer License No. PE-2011037427

REVISIONS

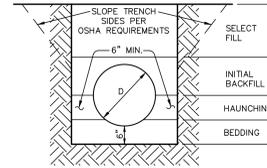
Number	DESCRIPTION	DATE
1	ADDENDUM #1	11-19-2020
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PROJECT NO: 0119-0100
 DATE: November 20, 2020

STORM SEWER DETAILS

C690

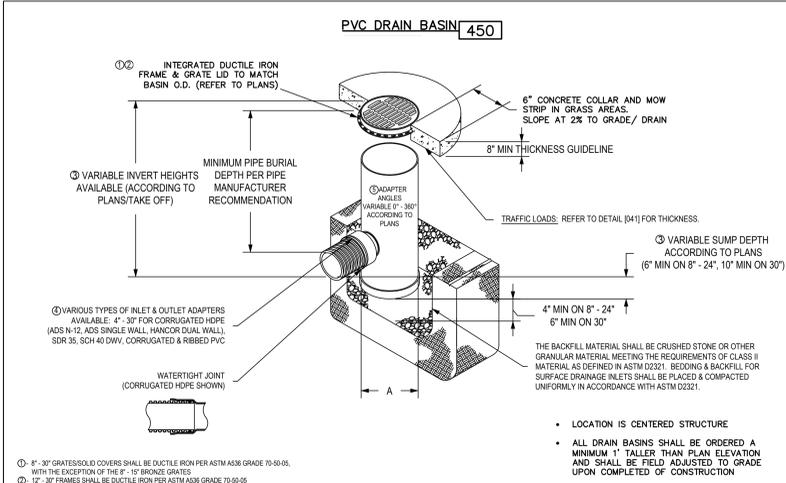
Final Development Plan



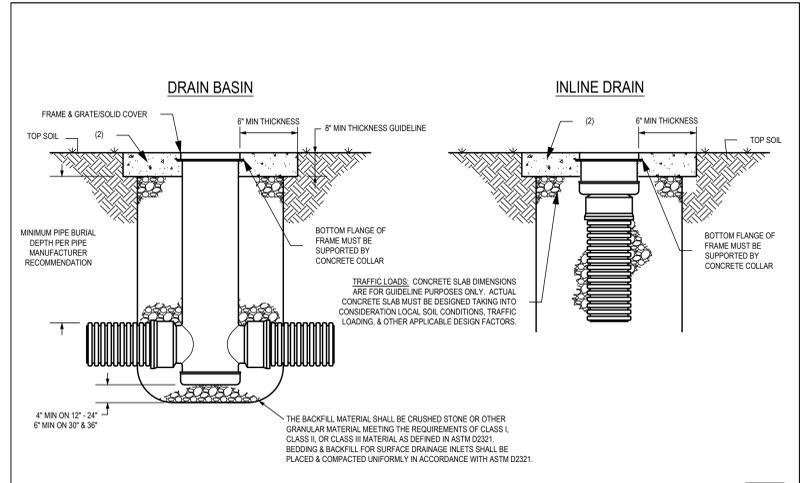
FLEXIBLE PIPE: INCLUDES CORRUGATED METAL PIPE, CORRUGATED POLYETHYLENE PIPE AND/OR POLYVINYL CHLORIDE PIPE.

- 1. BEDDING SHALL BE COMPACTED CRUSHED STONE AND SHALL BE SHAPED TO THE BOTTOM OF THE PIPE.
2. HAUNCHING AND INITIAL BACKFILL MATERIAL SHALL BE CLASS I OR II (REF. ASTM D2321) GRANULAR MATERIAL AND SHALL BE COMPACTED TO 95% STANDARD PROCTOR.

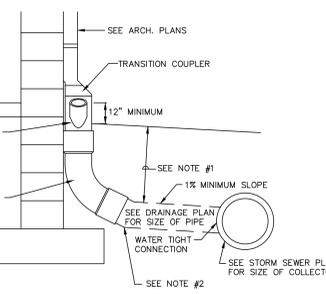
TRENCH AND BEDDING DETAILS
REFER TO KANSAS CITY METROPOLITAN CHAPTER OF APWA SPECIFICATIONS SECTION 2102.4



NYLOPLAST BASIN IS THE BASIS OF DESIGN
DRAIN BY EBC MATERIAL: 375 VERONA AVE, BUFORD, GA 30518
DATE: 1-23-06
APPROVED BY: GJA PROJECT NO: NAME
DATE: 1-23-06

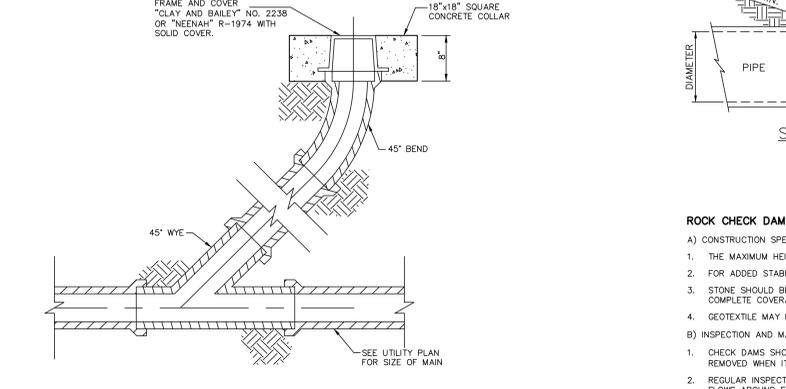


1. GRATESOLID COVERS SHALL MEET H-20 LOAD RATING FOR 30\"/>

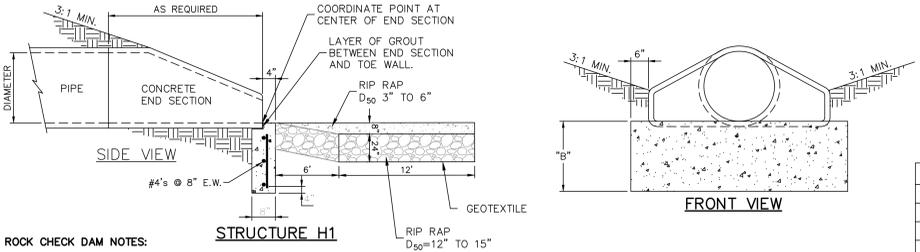


- NOTES:
1) FOR ALL DEPTHS OF COVER LESS THAN TWO (2) FEET, PIPE MUST BE SCHEDULE 40 PVC. FOR DEPTHS OF COVER GREATER THAN TWO (2) FEET, FLEXIBLE PIPE MAY BE USED. REFER TO SPECIFICATIONS FOR ALLOWABLE PIPE TYPES.
2) A WATER TIGHT CONNECTION SHALL BE MAINTAINED WITH ANY TRANSITION FROM SCHEDULE 40 PVC PIPE TO ANY OTHER PIPE TYPE.

DOWNSPOUT COLLECTOR 433



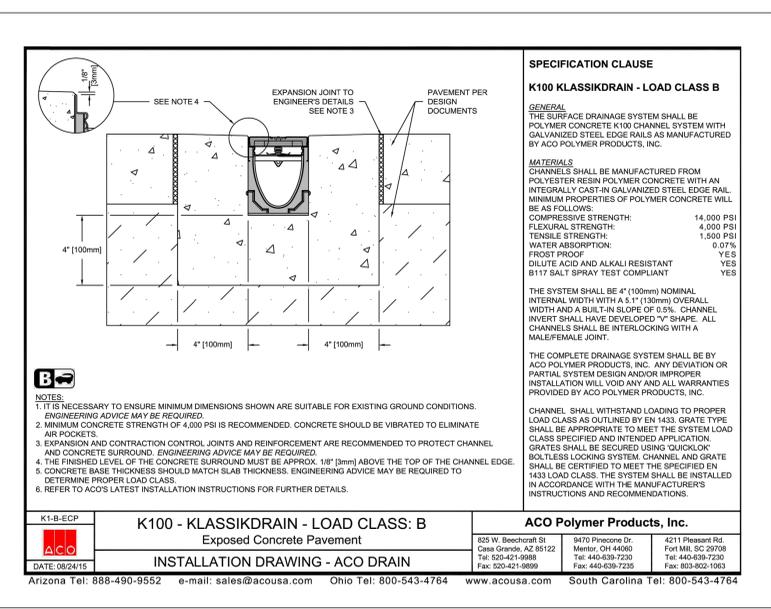
CLEAN-OUT 510



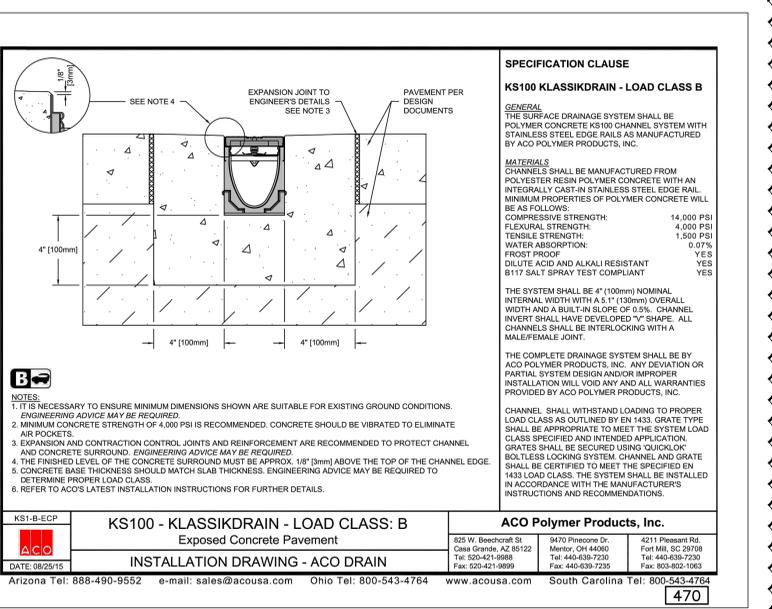
- ROCK CHECK DAM NOTES:
A) CONSTRUCTION SPECIFICATIONS & INSTALLATION:
1. THE MAXIMUM HEIGHT OF THE DAM SHALL BE 1 FEET. THE CENTER OF THE CHECK DAM IS AT THE SAME ELEVATION OF THE OUTER EDGES.
2. FOR ADDED STABILITY, THE BASE OF THE CHECK DAM SHALL BE KEVED INTO THE SOIL APPROXIMATELY 6 INCHES.
3. STONE SHOULD BE PLACED ACCORDING TO THE CONFIGURATION ABOVE. HAND OR MECHANICAL PLACEMENT WILL BE NECESSARY TO ACHIEVE COMPLETE COVERAGE OF THE DITCH OR SWALE AND TO INSURE THAT THE CENTER OF THE DAM IS LOWER THEN THE EDGES.
4. GEOTEXTILE MAY BE USED UNDER THE STONE TO PROVIDE A STABLE FOUNDATION AND TO FACILITATE REMOVAL OF THE STONE.
B) INSPECTION AND MAINTENANCE:
1. CHECK DAMS SHOULD BE CHECKED FOR SEDIMENT ACCUMULATION AFTER EACH STORM EVENT OF 1/2\"/>

TABLE
TOE WALL DEPTH
PIPE DIAMETER \"B\"
12\" - 21\" 24\"
24\" - 48\" 30\"
54\" - 66\" 36\"

CONCRETE FLARED END SECTION W/ TOE WALL AND RIP RAP STILLING BASIN 406
NOTES:
1. THE DEPTH OF THE TOE WALL SHALL BE PER TABLE. IF BEDROCK IS ENCOUNTERED A MINIMUM OF 12\"/>



K100 - KLASSIKDRAIN - LOAD CLASS B
Exposed Concrete Pavement
INSTALLATION DRAWING - ACO DRAIN
ACO Polymer Products, Inc.
825 W. Beechcraft St., Mesa, AZ 85202
4211 Pleasant Rd., Fort Mill, SC 29708



KS100 - KLASSIKDRAIN - LOAD CLASS B
Exposed Concrete Pavement
INSTALLATION DRAWING - ACO DRAIN
ACO Polymer Products, Inc.
825 W. Beechcraft St., Mesa, AZ 85202
4211 Pleasant Rd., Fort Mill, SC 29708

PROJECT NO: 0119-0100
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DAVID D. WOOD ENGINEER
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
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Lee's Summit High School
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mechanical/electrical engineer: Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.3700
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DATE: 12-15-2020
STORM SEWER DETAILS
C695
Final Development Plan

Lee's Summit R7 District
Athletics Facilities

Lee's Summit High School
400 SE Blue Parkway
Lee's Summit, MO 64063

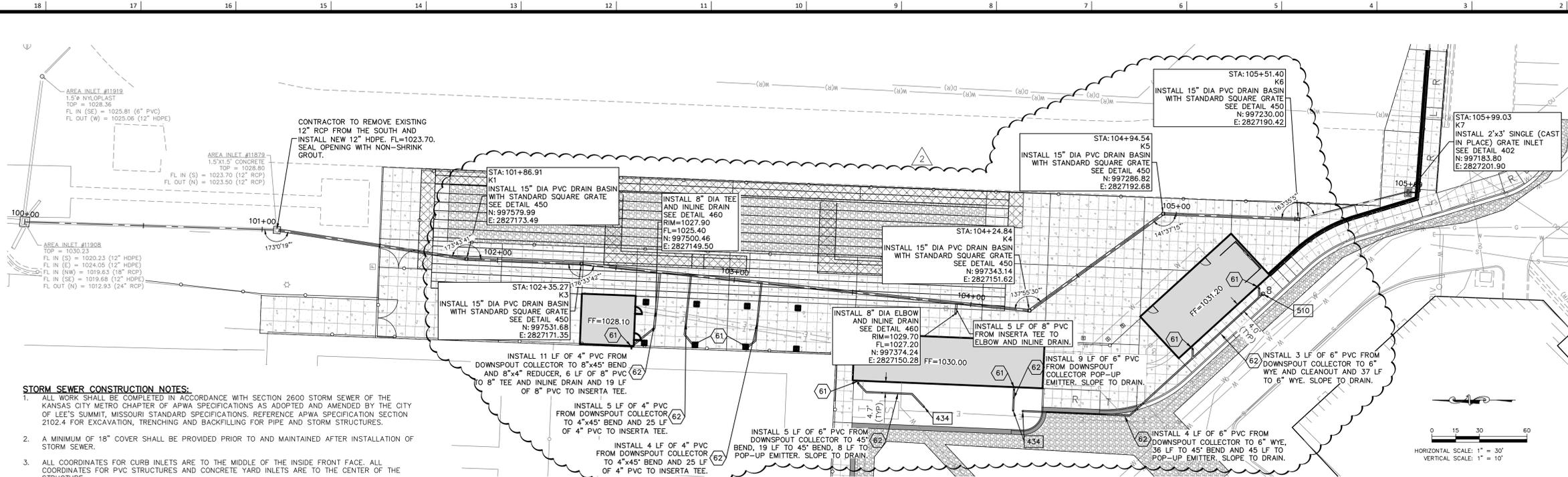
owner:
Lee's Summit R7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4200 Pennsylvania Avenue
Kansas City, MO 64111
816.931.6655 voice
www.goulddevans.com

structural engineer:
Bob D. Campbell & Company, Inc.
4338 Bellview
Kansas City, MO 64111
816.931.4344

civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
913.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700



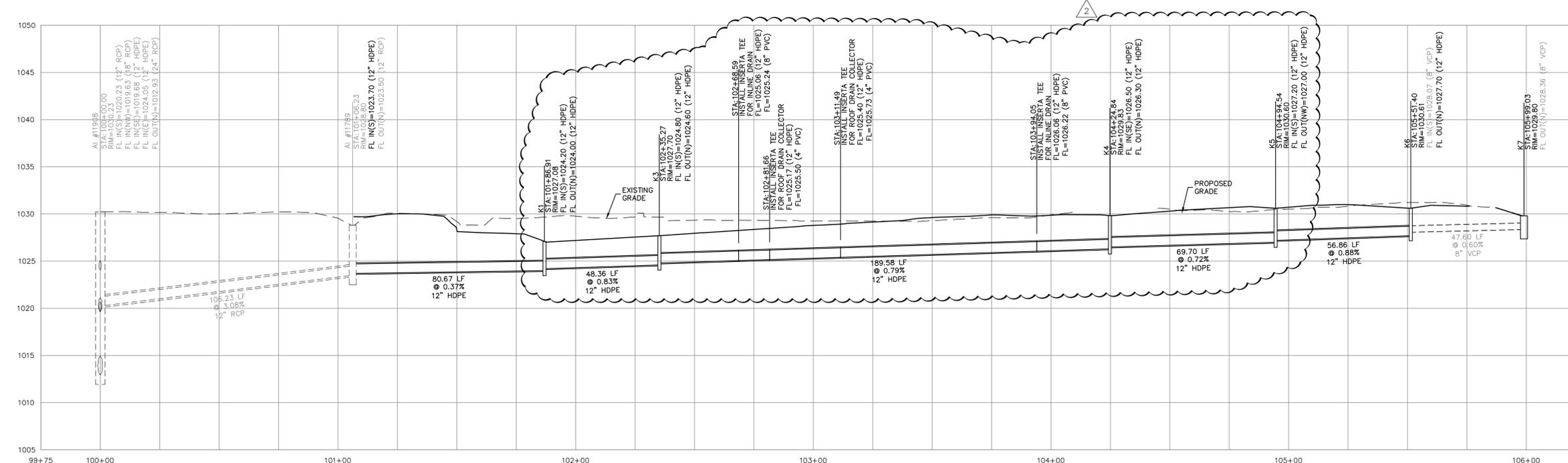
STORM SEWER CONSTRUCTION NOTES:

- ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH SECTION 2600 STORM SEWER OF THE KANSAS CITY METRO CHAPTER OF APWA SPECIFICATIONS AS ADOPTED AND AMENDED BY THE CITY OF LEE'S SUMMIT, MISSOURI STANDARD SPECIFICATIONS, REFERENCE APWA SPECIFICATION SECTION 2102.4 FOR EXCAVATION, TRENCHING AND BACKFILLING FOR PIPE AND STORM STRUCTURES.
- A MINIMUM OF 18" COVER SHALL BE PROVIDED PRIOR TO AND MAINTAINED AFTER INSTALLATION OF STORM SEWER.
- ALL COORDINATES FOR CURB INLETS ARE TO THE MIDDLE OF THE INSIDE FRONT FACE. ALL COORDINATES FOR PVC STRUCTURES AND CONCRETE YARD INLETS ARE TO THE CENTER OF THE STRUCTURE.
- ALL JUNCTION BOXES/AREA INLETS HAVE ONE COORDINATE PROVIDED AT THE CENTER OF STRUCTURE. SEE PLAN FOR CLARIFICATION. ORIENT STRUCTURES PARALLEL TO ADJACENT CURB, BUILDING OR WALL FACE, UNLESS NOTED OTHERWISE.
- RIM ELEVATION IS PROVIDED AT COORDINATE, UNLESS NOTED OTHERWISE. CONTRACTOR TO ADJUST ELEVATION OF RIM AS REQUIRED TO MATCH SLOPE OF ADJACENT CURB LINE. REFER TO GRADING PLAN (C300 SERIES SHEETS).
- ALL EXISTING UTILITIES INDICATED ON THE DRAWING ARE ACCORDING TO THE BEST INFORMATION AVAILABLE TO THE ENGINEER. HOWEVER, ALL UTILITIES ACTUALLY EXISTING MAY NOT BE SHOWN. UTILITIES DAMAGED THROUGH THE NEGLIGENCE OF THE CONTRACTOR TO OBTAIN THE LOCATION OF SAME SHALL BE REPAIRED OR REPLACED BY THE CONTRACTOR AT THEIR EXPENSE.
- ALL BACKFILL SHALL BE COMPACTED TO 95 PERCENT STANDARD DENSITY AT OPTIMUM MOISTURE.
- ALL EXCAVATION BENEATH THE STREETS AND PARKING LOTS FOR DRAINAGE PIPE LESS THAN 4'-0" IN DIAMETER SHALL BE BACKFILLED WITH AGGREGATE TO FOUR FEET (4') PAST BACK OF CURB IN ACCORDANCE WITH APWA SPECIFICATIONS SECTION 2102.4J.
- RELOCATION OF ANY WATER LINE, SEWER LINE OR SERVICE LINE THEREOF REQUIRED FOR THE CONSTRUCTION OF THIS PROJECT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR AND SHALL BE AT THEIR EXPENSE.
- IF PRECAST STORM STRUCTURES ARE TO BE USED ON THIS PROJECT, THE CONTRACTOR SHALL SUBMIT SHOP DRAWINGS AND HAVE THEM APPROVED BY THE ENGINEER PRIOR TO FABRICATION OF THE STRUCTURES. FAILURE TO DO SO SHALL BE CAUSE FOR REJECTION.
- ALL HDPE PIPE JOINTS SHALL BE WATER TIGHT.

PRIVATE STORM SEWER LINE K PLAN

- DETAILS SEE SHEET C690 AND C691
- 402 SINGLE GRATE INLET
- 433 DOWNSPOUT COLLECTOR
- 434 POP-UP EMITTER
- 450 PVC DRAIN BASIN - CONTRACTOR TO ORDER INLETS. ONE FOOT TALLER THAN PLAN ELEVATION SO INLET CAN BE FIELD ADJUSTED
- 460 INLINE DRAIN
- 510 CLEANOUT

- NOTES
- 61 DOWNSPOUT COLLECTOR (SEE DETAIL 433 ON SHEET W-C901)
- 62 PVC SCH-40 ROOF DRAIN SLOPE TO DRAIN (1% MINIMUM FOR 6" ROOF DRAINS, 2% MINIMUM FOR 4" ROOF DRAINS)



PRIVATE STORM SEWER LINE K PROFILE

SAFETY NOTICE TO CONTRACTOR
IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

WARRANTY / DISCLAIMER
THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH THE ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN OR DO WARRANTY THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTINUING BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR
THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS. THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.



PROJ. NO. C20_0496 DSN: DDW DAVID D. WOOD
 CTN: 0496PPP.Dwg DWN: NJM ENGINEER
 MO # 2011037427
 14700 WEST 114TH TERRACE
 LENEXA, KANSAS 66215
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KAW VALLEY ENGINEERING

KAW VALLEY ENGINEERING, INC. IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000842. EXPIRES 12/31/21

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Kaw Valley Engineering, Inc.
 Missouri Certificate of Authority: 000842
 David Wood
 License No. PE-2011037427

REVISIONS		
Number	DESCRIPTION	DATE
1	Addendum 1	10/13/20
2	Addendum 3	10/23/20

PROJECT NO: 0119-0100
 DATE: SEPTEMBER 28, 2020

**STORM SEWER
PLAN AND PROFILE**

H-C600

BID SET

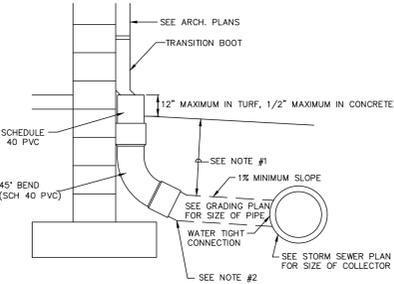
Lee's Summit R7 District
Athletics Facility

Lee's Summit High School
400 SE Blue Parkway
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 N Tudor Road
Lee's Summit, MO 64086

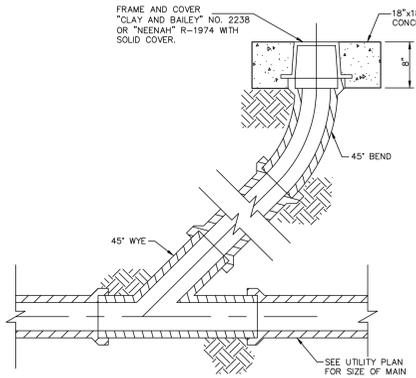
architect:
Gould Evans
4200 Pennsylvania Avenue
Kansas City, MO 64111
816.931.6655 voice
www.goulddevans.com
structural engineer:
Bob D. Campbell & Company, Inc.
4338 Bellevue
Kansas City, MO 64111
816.531.4144
civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
913.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700



- NOTES:
- FOR ALL DEPTHS OF COVER LESS THAN TWO (2) FEET, PIPE MUST BE SCHEDULE 40 PVC. FOR DEPTHS OF COVER GREATER THAN TWO (2) FEET, FLEXIBLE PIPE MAY BE USED. REFER TO SPECIFICATIONS FOR ALLOWABLE PIPE TYPES.
 - A WATERTIGHT CONNECTION SHALL BE MAINTAINED WITH ANY TRANSITION FROM SCHEDULE 40 PVC PIPE TO ANY OTHER PIPE TYPE.
 - THE DOWNSPOUT COLLECTOR DRAIN SHALL BE INSTALLED BEFORE THE DOWNSPOUTS ARE INSTALLED ON THE BUILDING. SITEWORK CONTRACTOR SHALL BE RESPONSIBLE FOR ALL WORK TO AND INCLUDING THE ROBERT SCREEN. BUILDING CONTRACTOR SHALL BE RESPONSIBLE FOR THE CONNECTION AT THE POINT OF THE ROBERT SCREEN.

DOWNSPOUT COLLECTOR 433



CLEAN-OUT 510

PVC DRAIN BASIN 450

INTEGRATED DUCTILE IRON FRAME & GRATE LID TO MATCH BASIN O.D. (REFER TO PLANS)

6" CONCRETE COLLAR AND MOW STRIP IN GRASS AREAS. SLOPE AT 2% TO GRADE/ DRAIN

8" MIN THICKNESS GUIDELINE

TRAFFIC LOADS: REFER TO DETAIL [041] FOR THICKNESS

MINIMUM PIPE BURIAL DEPTH PER PIPE MANUFACTURER RECOMMENDATION

ADAPTER ANGLES VARIABLE 0°-30° ACCORDING TO PLANS

VARIABLE INVERT HEIGHTS AVAILABLE (ACCORDING TO PLANS/TAKE OFF)

VARIABLE SUMP DEPTH ACCORDING TO PLANS (6" MIN ON 6"-24", 10" MIN ON 30")

4" MIN ON 8"-24" 6" MIN ON 30"

THE BACKFILL MATERIAL SHALL BE CRUSHED STONE OR OTHER GRANULAR MATERIAL MEETING THE REQUIREMENTS OF CLASS II MATERIAL AS DEFINED IN ASTM D2321. BEDDING & BACKFILL FOR SURFACE DRAINAGE INLETS SHALL BE PLACED & COMPACTED UNIFORMLY IN ACCORDANCE WITH ASTM D2321.

LOCATION IS CENTERED STRUCTURE

ALL DRAIN BASINS SHALL BE ORDERED A MINIMUM 1" TALLER THAN PLAN ELEVATION AND SHALL BE FIELD ADJUSTED TO GRADE UPON COMPLETION OF CONSTRUCTION

NYLOPLAST BASIN IS THE BASIS OF DESIGN

DRAWN BY: ERG	MATERIAL:	3130 VERONA AVE BURLINGAME, CA 94010 PHN (770) 932-3443 FAX (770) 932-2489 www.nyloplast.com
DATE: 1-23-04	PROJECT NO./NAME:	TITLE: DRAIN BASIN WITH STANDARD GRATE QUICK SPEC INSTALLATION DETAIL
APP'D BY: CJA	DATE: 1-23-04	DWG NO.: 7001-110-144 REV. D
DWG SIZE: A	SCALE: 1/4" = 1'-0"	SHEET: 1 OF 1

DRAIN BASIN

INLINE DRAIN

TRAFFIC LOADS: CONCRETE SLAB DIMENSIONS ARE FOR GUIDELINE PURPOSES ONLY. ACTUAL CONCRETE SLAB MUST BE DESIGNED TAKING INTO CONSIDERATION LOCAL SOIL CONDITIONS, TRAFFIC LOADING, & OTHER APPLICABLE DESIGN FACTORS.

THE BACKFILL MATERIAL SHALL BE CRUSHED STONE OR OTHER GRANULAR MATERIAL MEETING THE REQUIREMENTS OF CLASS I, CLASS II, OR CLASS III MATERIAL AS DEFINED IN ASTM D2321. BEDDING & BACKFILL FOR SURFACE DRAINAGE INLETS SHALL BE PLACED & COMPACTED UNIFORMLY IN ACCORDANCE WITH ASTM D2321.

THIS PRINT DISCLOSES SUBJECT MATTER IN WHICH NYLOPLAST HAS PROPRIETARY RIGHTS. THE RECEIPT OR POSSESSION OF THIS PRINT DOES NOT CONFER TRANSFER OR LICENSE THE USE OF THE DESIGN OR TECHNICAL INFORMATION SHOWN HEREIN. REPRODUCTION OF THIS PRINT OR ANY INFORMATION CONTAINED HEREIN, OR MANUFACTURE OF ANY ARTICLE HEREFROM, FOR THE DISCLOSURE TO OTHERS IS FORBIDDEN, EXCEPT BY SPECIFIC WRITTEN PERMISSION FROM NYLOPLAST.

DRAWN BY: ERG	MATERIAL:	3130 VERONA AVE BURLINGAME, CA 94010 PHN (770) 932-3443 FAX (770) 932-2489 www.nyloplast.com
DATE: 01-05-09	PROJECT NO./NAME:	TITLE: DRAIN BASIN & INLINE DRAIN TUBE TRAFFIC INSTALLATION
REVIS'D BY: NMH	DATE: 06-12-16	DWG NO.: 7001-110-340 REV. G
DWG SIZE: A	SCALE: 1/2" = 1'-0"	SHEET: 1 OF 1

DOUBLE GRATE INLET DETAILS

SINGLE GRATE INLET DETAILS

NOTE:

- Location point at center of inlet.
- A separate top slab may be utilized.
- Not recommended for use in areas with bicycle traffic.
- * East Jordan is an approved manufacturer for castings.

AMERICAN PUBLIC WORKS ASSOCIATION
KANSAS CITY METROPOLITAN CHAPTER
STANDARD DRAWING NUMBER: G-1
ADOPTED: APRIL 17, 1996

INLET NOTES

GENERAL

- ALL STORM SEWER STRUCTURES SHALL BE POURED IN PLACE.
- DO NOT SCALE THESE DRAWINGS FOR DIMENSIONS OR CLEARANCES. ANY QUESTIONS REGARDING DIMENSIONS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO CONSTRUCTION.
- THE FIRST DIMENSION LISTED IN THE CONSTRUCTION NOTES IS THE "L" DIMENSION, THE SECOND DIMENSION IS THE "W" DIMENSION, THE CONCRETE THICKNESS AND REINFORCEMENT SHOWN IS FOR BOXES WITH ("L" > "W") AND ("W" > "L") LESS THEN OR EQUAL TO 20. FOR BOXES WITH EITHER OF THESE CALCULATIONS GREATER THAN 20, A SPECIAL DESIGN IS REQUIRED. PRECASTER SHALL PROVIDE DESIGN CALCULATIONS FOR DEEP STRUCTURES TO ENGINEER PRIOR TO CONSTRUCTING BOX.

CONCRETE

- CONCRETE USED IN THIS WORK SHALL BE CLASS "A" CONCRETE (AE) THROUGHOUT, AND SHALL MEET THE REQUIREMENTS OF THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.
- CONCRETE CONSTRUCTION SHALL MEET THE APPLICABLE REQUIREMENTS OF STANDARD SPECIFICATIONS FOR MCB, LATEST EDITION, EXCEPT AS MODIFIED IN THE APWA TECHNICAL SPECIFICATIONS.
- INLET FLOORS SHALL BE SHAPED WITH NON-REINFORCED CONCRETE INVERTS TO PROVIDE SMOOTH FLOW.
- BEVEL ALL EXPOSED EDGES WITH 3/8" TRIANGULAR MOLDING.
- 8" SOLID CONCRETE BLOCK OR BRICK MAY BE USED IN WALLS IN LIEU OF POURED CONCRETE WHERE NEITHER "H" > "L" NOR "H" > "W" (IN FEET) EXCEED FOURTEEN. BLOCK OR BRICK MAY BE USED IN ANY BOX WHERE "H" IS 5' OR LESS.
- ALL CRUSHED STONE USED AS AGGREGATE FOR CONCRETE CONSTRUCTION SHALL BE OBTAINED FROM QUARRIES AND BEDS DESIGNATED BY THE MISSOURI DEPARTMENT OF TRANSPORTATION AS MEETING DURABILITY REQUIREMENTS OF KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.

REINFORCING STEEL

- REINFORCING STEEL SHALL BE NEW BILLET, MINIMUM GRADE 60 AS PER ASTM A615, AND SHALL BE BENT COLD.
- ALL DIMENSIONS RELATIVE TO REINFORCING STEEL ARE TO CENTERLINE OF BARS. 2" CLEARANCE SHALL BE PROVIDED THROUGHOUT UNLESS NOTED OTHERWISE. TOLERANCE OF +/- 1/8" SHALL BE PERMITTED.
- ALL LAP SPLICES NOT SHOWN SHALL BE A MINIMUM OF 40 BAR DIAMETERS IN LENGTH.
- ALL REINFORCING STEEL SHALL BE SUPPORTED ON FABRICATED TIE BAR SUPPORTS @ 3"-0" MAXIMUM SPACING.
- ALL DOWELS SHALL BE ACCURATELY PLACED AND SECURELY TIED IN PLACE PRIOR TO PLACEMENT OF BOTTOM SLAB CONCRETE. STICKING OF DOWELS INTO FRESH OR PARTIALLY HARDENED CONCRETE WILL NOT BE ACCEPTABLE.

CONSTRUCTION

- THE BOTTOM SLAB SHALL BE AT LEAST 24 HOURS OLD BEFORE PLACING SIDEWALL CONCRETE. ALL SIDEWALL FORMS SHALL REMAIN IN PLACE A MINIMUM OF 24 HOURS AFTER SIDEWALLS ARE POURED BEFORE REMOVAL, AND AFTER REMOVAL SHALL BE IMMEDIATELY TREATED WITH MEMBRANE CURING COMPOUND.
- MATERIAL SELECTION AND COMPACTION REQUIREMENTS FOR BACKFILL AROUND STRUCTURES SHALL BE AS SPECIFIED IN THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.

NDS
We put water in its place

NDS, INC.
851 NORTH HARVARD AVE.
LINDSAY, CA 93247
TOLL FREE: 1-800-726-1994
PHONE: (559) 562-9888
FAX: (559) 562-4488
www.ndspro.com

NOTES:

- INSTALLATION TO BE COMPLETED IN ACCORDANCE WITH MANUFACTURER'S SPECIFICATIONS.
- DO NOT SCALE DRAWING.
- THIS DRAWING IS INTENDED FOR USE BY ARCHITECTS, ENGINEERS, CONTRACTORS, CONSULTANTS AND DESIGN PROFESSIONALS FOR PLANNING PURPOSES ONLY.
- ALL INFORMATION CONTAINED HEREIN WAS CURRENT AT THE TIME OF DEVELOPMENT BUT MUST BE REVIEWED AND APPROVED BY THE PRODUCT MANUFACTURER TO BE CONSIDERED ACCURATE.

ROUND SPEED BASINS

ROUND GRATE WITH SPEED-BASIN

NDS
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TECHNICAL SPECIFICATIONS

6" Pop Up Emitter with 6" Basin

Part #: 625 - Center Spring Loaded
Material: High Density Polypropylene (HDPE)
Colors: Pop Up (Green) Basin (Black)
Fits: 3" and 4" sewer, drain, triple wall, corrugated and sch. 40 pipe
Spring: Stainless Steel Grade 302
Opening Pressure: 1 PSI
Open Surface Area: 28.8 Sq. Inches
Flow Rate
1" Head: 124.60 GPM
0.5" Head: 88.10 GPM
Basin: 6" NDS Speed-D Basin
Weight Per Each: 2.14 lbs.
UV inhibitor

Load Recommendation Guide

Class A

- Loads of 140 psi.
- Recommended for pedestrians, bicycles and wheel chair traffic.

851 N. Harvard Avenue
Lindsay, CA 93247
800-726-1994

Visit ndspro.com for specs, detail drawings, and case studies

NDS
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TRENCH AND BEDDING DETAILS

FLEXIBLE PIPE: INCLUDES CORRUGATED METAL PIPE, CORRUGATED POLYETHYLENE PIPE AND/OR POLYVINYL CHLORIDE PIPE.

- BEDDING SHALL BE COMPACTED CRUSHED STONE AND SHALL BE SHAPED TO THE BOTTOM OF THE PIPE.
- HAUNCHING AND INITIAL BACKFILL MATERIAL SHALL BE CLASS I OR II (REF. ASTM D2321) GRANULAR MATERIAL AND SHALL BE COMPACTED TO 95% STANDARD PROCTOR.

POP-UP EMITTER 434

PROJ. NO. C20_0496 DSN: DDW DAVID D. WOOD
CTN: 0496DET.DWG DWN: NJM ENGINEER MO # 2011037427

14700 WEST 114TH TERRACE
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KV KAW VALLEY ENGINEERING

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UNLESS A PROFESSIONAL SEAL WITH SIGNATURE AND DATE IS AFFIXED, THIS DOCUMENT IS PRELIMINARY AND IS NOT INTENDED FOR CONSTRUCTION, RECORDING PURPOSES OR IMPLEMENTATION

DAVID D. WOOD
Professional Engineer
Missouri License No. PE-2011037427

Kaw Valley Engineering, Inc.
Missouri Certificate of Authority: 000842
David Wood Date: 09/28/2020
Engineer License No. PE-2011037427

REVISIONS

Number	DESCRIPTION	DATE
1	Addendum 1	10/13/20
2	Addendum 3	10/23/20

PROJECT NO: 0119-0100
DATE: SEPTEMBER 28, 2020

STORM DETAILS

H-C690

BID SET

Extended Dry Detention Basin Design			
Tributary Area	0.78 AC	0.78 Acres	
Impervious Area	0.69 AC	84 CN	
Pervious Area	0.09 AC	12%	
Treatment Volume (from PondPack) 3180 ft ³			
WQV Storage Elevation	1008		
Basin Bottom Elevation Above Sediment Deposition	N/A		
Water Quality Outlet, Perforated Riser Pipe/Underlain (24-hour draw down)			
Depth of WQV at outlet:	3.9 ft		
Average Head of WQV over invert of orifice:	1.95 ft		
Average WQV outflow rate:	0.0367 cfs		
Utilize 1" Orifice in Screw in Cap			

I. Basin Water Quality Storage Volume			
Step 1	Tributary Area to EDOB, A _t (ac)	A _t (ac)=	0.78
Step 2	Calculate WQ _v using methodology in Section 6	WQ _v (ac-ft)=	0.0730 3,179.88 CF
Step 3	Add 20 percent to account for silt and sediment deposition	W _{total} (ac-ft)=	0.0876 3,815.86 CF

III. Flood Control
Refer to APWA Specifications Section 5608
Notes:

IV. Trash Racks			
Step 1	Total outlet area, A _{tr} (in ²)	A _{tr} (in ²)=	N/A
Step 2	Required trash rack open area, A' _{tr} (in ²)	A' _{tr} (in ²)=	N/A
--not applicable for perforated riser--			

V. Basin Shape			
Step 1	Length to width ratio should be at least 3:1 (L/W) wherever practicable	(L/W)=	3:1
Step 2	Low flow channel side lining (Concrete, Soil/Riprap, None, or Specify)	Lining Type=	Soil/Riprap
Step 3	Top stage floor drainage slope (toward low flow channel), S ₁ (%)	S ₁ (%)=	2
	Top stage depth, D ₁ (ft)	D ₁ (ft)=	4.5
Step 4	Bottom stage volume, V _{bc} (ac-ft)	V _{bc} (ac-ft)=	-

VI. Forebay (Optional)			
Step 1	Volume should be greater than 10% of WQ _v	Min V _{fb} (ac-ft)=	0.0073
Step 2	Forebay depth, Z _{fb} (ft)	Z _{fb} (ft)=	0.5
Step 3	Forebay surface area, A _{fb} (ac)	Min A _{fb} (ac)=	0.0146
Step 4	Paved/hard bottom and sides?	Yes or No	No

VII. Basin Side Slopes			
Step 1	Basin side slopes should be at least 4:1 (H:V)	Basin SS (H:V)=	3:1 Max

VIII. Dam Embankment Side Slopes			
Step 1	Dam embankment slopes should be at least 3:1 (H:V)	Dam Emb. SS (H:V)=	3:1

IX. Vegetation			
Step 1	Native Grass, Irrigated Turf Grass, Specify	Vegetation Type=	Native

X. Inlet Protection			
Step 1	Indicate method of inlet protection/energy dissipation at EDOB inlet	Inlet Protection=	Riprap

XI. Access			
Step 1	Indicate that access has been provided for maintenance vehicles	Is Access Provided=	Yes

Orifice size (in)	WQV release rate (cfs)		# of holes (ft ²)	# of holes req'd (ft ²)	# holes used	Total discharge (cfs)	Time to empty (hrs)	Orifice Flow - Circular				HwD			
	Q (cfs)	Q (ft ³ /min)						A (ft ²)	V (ft/s)	H (ft)	Q (ft ³ /min)				
1/32	0.0000	24664.33	1027.68	616.63	0.0000	#DIV/0!		1/32	0.0313	0.000	0.0008	0.6	1.95	0.000	748.80
1/16	0.0001	6166.08	256.92	154.15	0.0000	#DIV/0!		1/16	0.0625	0.000	0.0031	0.6	1.95	0.000	374.40
3/32	0.0003	2740.48	114.19	68.51	0.0000	#DIV/0!		3/32	0.0938	0.000	0.0069	0.6	1.95	0.000	249.60
1/8	0.0006	1541.52	64.23	38.54	0.0000	#DIV/0!		1/8	0.1250	0.000	0.0123	0.6	1.95	0.001	187.20
5/32	0.0009	986.57	41.11	24.86	0.0000	#DIV/0!		5/32	0.1563	0.000	0.0192	0.6	1.95	0.001	149.76
3/16	0.0013	686.12	38.55	17.13	0.0000	#DIV/0!		3/16	0.1875	0.000	0.0276	0.6	1.95	0.001	124.80
7/32	0.0018	503.35	20.97	12.58	0.0000	#DIV/0!		7/32	0.2188	0.000	0.0376	0.6	1.95	0.002	106.97
1/4	0.0023	385.38	16.06	9.63	0.0000	#DIV/0!		1/4	0.2500	0.000	0.0491	0.6	1.95	0.002	93.60
9/32	0.0029	304.50	12.69	7.61	0.0000	#DIV/0!		9/32	0.2813	0.000	0.0621	0.6	1.95	0.003	83.20
5/16	0.0036	246.64	10.28	6.17	0.0000	#DIV/0!		5/16	0.3125	0.001	0.0767	0.6	1.95	0.004	74.88
11/32	0.0043	203.84	8.49	5.10	0.0000	#DIV/0!		11/32	0.3438	0.001	0.0928	0.6	1.95	0.004	68.07
3/8	0.0052	171.28	7.14	4.28	0.0000	#DIV/0!		3/8	0.3750	0.001	0.1104	0.6	1.95	0.005	62.40
13/32	0.0061	145.84	6.08	3.65	0.0000	#DIV/0!		13/32	0.4063	0.001	0.1296	0.6	1.95	0.006	57.60
7/16	0.0070	125.84	5.24	3.15	0.0000	#DIV/0!		7/16	0.4375	0.001	0.1503	0.6	1.95	0.007	53.49
15/32	0.0081	109.62	4.57	2.74	0.0000	#DIV/0!		15/32	0.4688	0.001	0.1726	0.6	1.95	0.008	49.92
1/2	0.0092	96.36	4.03	2.41	0.0000	#DIV/0!		1/2	0.5000	0.001	0.1963	0.6	1.95	0.009	46.80
17/32	0.0103	85.34	3.56	2.13	0.0000	#DIV/0!		17/32	0.5313	0.002	0.2217	0.6	1.95	0.010	44.00
9/16	0.0116	76.12	3.17	1.90	0.0000	#DIV/0!		9/16	0.5625	0.002	0.2485	0.6	1.95	0.012	41.65
19/32	0.0129	68.32	2.85	1.71	0.0000	#DIV/0!		19/32	0.5938	0.002	0.2769	0.6	1.95	0.013	39.41
5/8	0.0143	61.86	2.57	1.54	0.0000	#DIV/0!		5/8	0.6250	0.002	0.3068	0.6	1.95	0.014	37.44
21/32	0.0158	56.93	2.33	1.40	0.0000	#DIV/0!		21/32	0.6563	0.002	0.3382	0.6	1.95	0.015	35.66
11/16	0.0173	50.96	2.12	1.27	0.0000	#DIV/0!		11/16	0.6875	0.003	0.3712	0.6	1.95	0.017	34.04
23/32	0.0189	46.62	1.94	1.17	0.0000	#DIV/0!		23/32	0.7188	0.003	0.4057	0.6	1.95	0.019	32.56
3/4	0.0206	42.82	1.78	1.07	0.0000	#DIV/0!		3/4	0.7500	0.003	0.4418	0.6	1.95	0.021	31.20
25/32	0.0224	39.46	1.64	0.99	0.0000	#DIV/0!		25/32	0.7813	0.003	0.4794	0.6	1.95	0.022	29.95
13/16	0.0242	36.49	1.52	0.91	0.0000	#DIV/0!		13/16	0.8125	0.004	0.5185	0.6	1.95	0.024	28.80
27/32	0.0261	33.83	1.41	0.85	0.0000	#DIV/0!		27/32	0.8438	0.004	0.5591	0.6	1.95	0.026	27.73
7/8	0.0281	31.46	1.31	0.79	0.0000	#DIV/0!		7/8	0.8750	0.004	0.6013	0.6	1.95	0.028	26.74
29/32	0.0301	29.33	1.22	0.73	0.0000	#DIV/0!		29/32	0.9063	0.004	0.6450	0.6	1.95	0.030	25.82
15/16	0.0322	27.40	1.14	0.69	0.0000	#DIV/0!		15/16	0.9375	0.005	0.6903	0.6	1.95	0.032	24.96
31/32	0.0344	25.67	1.07	0.64	0.0000	#DIV/0!		31/32	0.9688	0.005	0.7371	0.6	1.95	0.034	24.15
1	0.0367	24.09	1.00	0.60	1	0.0367	24.09	1	1.0000	0.005	0.7854	0.6	1.95	0.037	23.40
1 1/32	0.0390	22.65	0.94	0.57	0.0000	#DIV/0!		1 1/32	1.0313	0.006	0.8353	0.6	1.95	0.039	22.69
1 1/16	0.0414	21.34	0.89	0.53	0.0000	#DIV/0!		1 1/16	1.0625	0.006	0.8866	0.6	1.95	0.041	22.02
1 3/32	0.0439	20.13	0.84	0.50	0.0000	#DIV/0!		1 3/32	1.0938	0.007	0.9396	0.6	1.95	0.044	21.39
1 1/8	0.0464	19.03	0.79	0.48	0.0000	#DIV/0!		1 1/8	1.1250	0.007	0.9940	0.6	1.95	0.046	20.80
1 5/32	0.0490	18.02	0.75	0.45	0.0000	#DIV/0!		1 5/32	1.1563	0.007	1.0500	0.6	1.95	0.049	20.24
1 3/16	0.0517	17.08	0.71	0.43	0.0000	#DIV/0!		1 3/16	1.1875	0.008	1.1075	0.6	1.95	0.052	19.71
1 7/32	0.0545	16.22	0.68	0.41	0.0000	#DIV/0!		1 7/32	1.2188	0.008	1.1666	0.6	1.95	0.054	19.20
1 1/4	0.0573	15.42	0.64	0.39	0.0000	#DIV/0!		1 1/4	1.2500	0.009	1.2272	0.6	1.95	0.057	18.72
1 9/32	0.0602	14.67	0.61	0.37	0.0000	#DIV/0!		1 9/32	1.2813	0.009	1.2893	0.6	1.95	0.060	18.26
1 5/16	0.0632	13.98	0.58	0.35	0.0000	#DIV/0!		1 5/16	1.3125	0.009	1.3530	0.6	1.95	0.063	17.83
1 11/32	0.0662	13.34	0.56	0.33	0.0000	#DIV/0!		1 11/32	1.3438	0.010	1.4182	0.6	1.95	0.066	17.41
1 3/8	0.0693	12.74	0.53	0.32	0.0000	#DIV/0!		1 3/8	1.3750	0.010	1.4849	0.6	1.95	0.069	17.02
1 13/32	0.0725	12.18	0.51	0.30	0.0000	#DIV/0!		1 13/32	1.4063	0.011	1.5532	0.6	1.95	0.073	16.64
1 7/16	0.0758	11.66	0.49	0.29	0.0000	#DIV/0!		1 7/16	1.4375	0.011	1.6230	0.6	1.95	0.076	16.28
1 15/32	0.0791	11.17	0.47	0.28	0.0000	#DIV/0!		1 15/32	1.4688	0.012	1.6943	0.6	1.95	0.079	15.93
1 1/2	0.0825	10.71	0.45	0.27	0.0000	#DIV/0!		1 1/2	1.5000	0.012	1.7671	0.6	1.95	0.083	15.60
1 17/32	0.0860	10.27	0.43	0.26	0.0000	#DIV/0!		1 17/32	1.5313	0.013	1.8415	0.6	1.95	0.086	15.28
1 9/16	0.0895	9.87	0.41	0.25	0.0000	#DIV/0!		1 9/16	1.5625	0.013	1.9175	0.6	1.95	0.090	14.98
1 19/32	0.0931	9.48	0.40	0.24	0.0000	#DIV/0!		1 19/32	1.5938	0.014	1.9949	0.6	1.95	0.093	14.68
1 5/8	0.0968	9.12	0.38	0.23	0.0000	#DIV/0!		1 5/8	1.6250	0.014	2.0739	0.6	1.95	0.097	14.40
1 21/32	0.1006	8.78	0.37	0.22	0.0000	#DIV/0!		1 21/32	1.6563	0.015	2.1545	0.6	1.95	0.101	14.13
1 11/16	0.1044	8.46	0.35	0.21	0.0000	#DIV/0!		1 11/16	1.6875	0.016	2.2365	0.6	1.95	0.104	13.87
1 23/32	0.1083	8.15	0.34	0.20	0.0000	#DIV/0!		1 23/32	1.7188	0.016	2.3201	0.6	1.95	0.108	13.61
1 3/4	0.1123	7.86	0.33	0.20	0.0000	#DIV/0!		1 3/4	1.7500	0.017	2.4053	0.6	1.95	0.112	13.37
1 25/32	0.1164	7.59	0.32	0.19	0.0000	#DIV/0!		1 25/32	1.7813	0.017	2.4920	0.6	1.95	0.116	13.14
1 13/16	0.1206	7.33	0.31	0.18	0.0000	#DIV/0!		1 13/16	1.8125	0.018	2.5802	0.6	1.95	0.120	12.91
1 27/32	0.1247	7.09	0.30	0.18	0.0000	#DIV/0!		1 27/32	1.8438	0.019	2.6699	0.6	1.95	0.125	12.69
1 7/8	0.1289	6.86	0.29	0.17	0.0000	#DIV/0!		1 7/8	1.8750	0.019	2.7612	0.6	1.95	0.129	12.48
1 29/32	0.1333	6.63	0.28	0.17	0.0000	#DIV/0!		1 29/32	1.9063	0.020	2.8540	0.6	1.95	0.133	12.28
1 15/16	0.1377	6.42	0.27	0.16	0.0000	#DIV/0!		1 15/16							

Exhibit D
PondPack Analysis

Lee's Summit High School - Network Layout

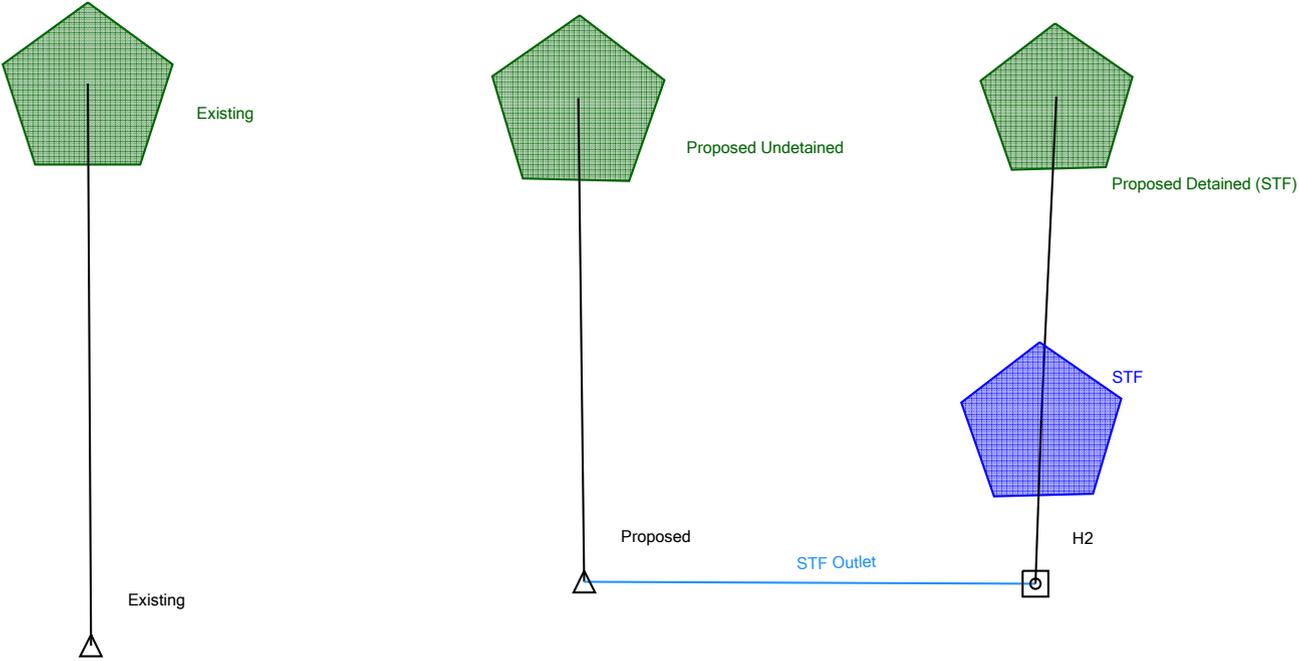


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Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Proposed Detained (STF)	WQv	1	0.058	11.900	1.05
Proposed Detained (STF)	2-year	2	0.190	11.900	3.28
Proposed Detained (STF)	10-YEAR	10	0.318	11.900	5.33
Proposed Detained (STF)	100-YEAR	100	0.452	11.900	7.47
Existing	WQv	1	0.955	12.000	15.66
Existing	2-year	2	3.637	12.000	56.87
Existing	10-YEAR	10	6.315	12.000	95.45
Existing	100-YEAR	100	9.170	12.000	135.41
Proposed Undetained	WQv	1	0.910	12.000	14.93
Proposed Undetained	2-year	2	3.466	12.000	54.21
Proposed Undetained	10-YEAR	10	6.020	12.000	90.98
Proposed Undetained	100-YEAR	100	8.741	12.000	129.08

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Existing	WQv	1	0.955	12.000	15.66
Existing	2-year	2	3.637	12.000	56.87
Existing	10-YEAR	10	6.315	12.000	95.45
Existing	100-YEAR	100	9.170	12.000	135.41
Proposed	WQv	1	0.948	12.000	14.96
Proposed	2-year	2	3.617	12.000	56.91
Proposed	10-YEAR	10	6.292	12.000	94.44
Proposed	100-YEAR	100	9.147	12.000	135.44

Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
STF (IN)	WQv	1	0.058	11.900	1.05	(N/A)	(N/A)
STF (OUT)	WQv	1	0.038	13.500	0.04	1,007.88	0.031
STF (IN)	2-year	2	0.190	11.900	3.28	(N/A)	(N/A)
STF (OUT)	2-year	2	0.151	12.000	2.70	1,011.03	0.047
STF (IN)	10-YEAR	10	0.318	11.900	5.33	(N/A)	(N/A)
STF (OUT)	10-YEAR	10	0.272	12.050	3.51	1,011.62	0.070
STF (IN)	100-YEAR	100	0.452	11.900	7.47	(N/A)	(N/A)
STF (OUT)	100-YEAR	100	0.406	12.000	6.37	1,011.91	0.082

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

Time-Depth Curve: 100-yr

Label	100-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	100 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.1	0.1	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.2
2.000	0.2	0.2	0.2	0.2	0.2
2.500	0.2	0.2	0.2	0.2	0.3
3.000	0.3	0.3	0.3	0.3	0.3
3.500	0.3	0.3	0.3	0.3	0.4
4.000	0.4	0.4	0.4	0.4	0.4
4.500	0.4	0.4	0.4	0.5	0.5
5.000	0.5	0.5	0.5	0.5	0.5
5.500	0.5	0.6	0.6	0.6	0.6
6.000	0.6	0.6	0.6	0.6	0.7
6.500	0.7	0.7	0.7	0.7	0.7
7.000	0.8	0.8	0.8	0.8	0.8
7.500	0.8	0.8	0.9	0.9	0.9
8.000	0.9	0.9	0.9	1.0	1.0
8.500	1.0	1.0	1.0	1.1	1.1
9.000	1.1	1.1	1.2	1.2	1.2
9.500	1.2	1.3	1.3	1.3	1.3
10.000	1.4	1.4	1.4	1.5	1.5
10.500	1.6	1.6	1.6	1.7	1.7
11.000	1.8	1.8	1.9	2.0	2.1
11.500	2.2	2.3	2.7	3.3	4.3
12.000	5.0	5.2	5.3	5.4	5.5
12.500	5.6	5.7	5.7	5.8	5.8
13.000	5.9	5.9	6.0	6.0	6.0
13.500	6.1	6.1	6.1	6.2	6.2
14.000	6.2	6.3	6.3	6.3	6.3
14.500	6.4	6.4	6.4	6.4	6.5
15.000	6.5	6.5	6.5	6.6	6.6
15.500	6.6	6.6	6.6	6.7	6.7
16.000	6.7	6.7	6.7	6.7	6.8
16.500	6.8	6.8	6.8	6.8	6.8
17.000	6.9	6.9	6.9	6.9	6.9

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	6.9	6.9	7.0	7.0	7.0
18.000	7.0	7.0	7.0	7.0	7.1
18.500	7.1	7.1	7.1	7.1	7.1
19.000	7.1	7.1	7.2	7.2	7.2
19.500	7.2	7.2	7.2	7.2	7.2
20.000	7.2	7.2	7.3	7.3	7.3
20.500	7.3	7.3	7.3	7.3	7.3
21.000	7.3	7.3	7.4	7.4	7.4
21.500	7.4	7.4	7.4	7.4	7.4
22.000	7.4	7.4	7.4	7.5	7.5
22.500	7.5	7.5	7.5	7.5	7.5
23.000	7.5	7.5	7.5	7.5	7.5
23.500	7.6	7.6	7.6	7.6	7.6
24.000	7.6	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Time-Depth Curve: 10-yr

Label	10-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	10 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.2	0.2	0.2	0.2	0.2
3.000	0.2	0.2	0.2	0.2	0.2
3.500	0.2	0.2	0.2	0.2	0.3
4.000	0.3	0.3	0.3	0.3	0.3
4.500	0.3	0.3	0.3	0.3	0.3
5.000	0.3	0.4	0.4	0.4	0.4
5.500	0.4	0.4	0.4	0.4	0.4
6.000	0.4	0.4	0.5	0.5	0.5
6.500	0.5	0.5	0.5	0.5	0.5
7.000	0.5	0.6	0.6	0.6	0.6
7.500	0.6	0.6	0.6	0.6	0.6
8.000	0.7	0.7	0.7	0.7	0.7
8.500	0.7	0.7	0.8	0.8	0.8
9.000	0.8	0.8	0.8	0.9	0.9
9.500	0.9	0.9	0.9	1.0	1.0
10.000	1.0	1.0	1.0	1.1	1.1
10.500	1.1	1.2	1.2	1.2	1.3
11.000	1.3	1.3	1.4	1.4	1.5
11.500	1.6	1.7	1.9	2.4	3.1
12.000	3.6	3.8	3.8	3.9	4.0
12.500	4.0	4.1	4.1	4.2	4.2
13.000	4.2	4.3	4.3	4.3	4.4
13.500	4.4	4.4	4.4	4.5	4.5
14.000	4.5	4.5	4.5	4.6	4.6
14.500	4.6	4.6	4.6	4.7	4.7
15.000	4.7	4.7	4.7	4.7	4.8
15.500	4.8	4.8	4.8	4.8	4.8
16.000	4.8	4.9	4.9	4.9	4.9
16.500	4.9	4.9	4.9	4.9	4.9
17.000	5.0	5.0	5.0	5.0	5.0

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	5.0	5.0	5.0	5.0	5.1
18.000	5.1	5.1	5.1	5.1	5.1
18.500	5.1	5.1	5.1	5.1	5.1
19.000	5.2	5.2	5.2	5.2	5.2
19.500	5.2	5.2	5.2	5.2	5.2
20.000	5.2	5.2	5.3	5.3	5.3
20.500	5.3	5.3	5.3	5.3	5.3
21.000	5.3	5.3	5.3	5.3	5.3
21.500	5.3	5.3	5.4	5.4	5.4
22.000	5.4	5.4	5.4	5.4	5.4
22.500	5.4	5.4	5.4	5.4	5.4
23.000	5.4	5.4	5.5	5.5	5.5
23.500	5.5	5.5	5.5	5.5	5.5
24.000	5.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

Time-Depth Curve: 2-yr

Label	2-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	2 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.1	0.1	0.1	0.1	0.1
3.000	0.1	0.1	0.1	0.1	0.1
3.500	0.1	0.1	0.2	0.2	0.2
4.000	0.2	0.2	0.2	0.2	0.2
4.500	0.2	0.2	0.2	0.2	0.2
5.000	0.2	0.2	0.2	0.2	0.2
5.500	0.2	0.3	0.3	0.3	0.3
6.000	0.3	0.3	0.3	0.3	0.3
6.500	0.3	0.3	0.3	0.3	0.3
7.000	0.3	0.4	0.4	0.4	0.4
7.500	0.4	0.4	0.4	0.4	0.4
8.000	0.4	0.4	0.4	0.4	0.5
8.500	0.5	0.5	0.5	0.5	0.5
9.000	0.5	0.5	0.5	0.5	0.6
9.500	0.6	0.6	0.6	0.6	0.6
10.000	0.6	0.6	0.7	0.7	0.7
10.500	0.7	0.7	0.8	0.8	0.8
11.000	0.8	0.8	0.9	0.9	1.0
11.500	1.0	1.1	1.2	1.5	2.0
12.000	2.3	2.4	2.4	2.5	2.5
12.500	2.6	2.6	2.6	2.7	2.7
13.000	2.7	2.7	2.7	2.8	2.8
13.500	2.8	2.8	2.8	2.8	2.9
14.000	2.9	2.9	2.9	2.9	2.9
14.500	2.9	2.9	3.0	3.0	3.0
15.000	3.0	3.0	3.0	3.0	3.0
15.500	3.0	3.0	3.1	3.1	3.1
16.000	3.1	3.1	3.1	3.1	3.1
16.500	3.1	3.1	3.1	3.1	3.1
17.000	3.2	3.2	3.2	3.2	3.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	3.2	3.2	3.2	3.2	3.2
18.000	3.2	3.2	3.2	3.2	3.2
18.500	3.3	3.3	3.3	3.3	3.3
19.000	3.3	3.3	3.3	3.3	3.3
19.500	3.3	3.3	3.3	3.3	3.3
20.000	3.3	3.3	3.3	3.3	3.4
20.500	3.4	3.4	3.4	3.4	3.4
21.000	3.4	3.4	3.4	3.4	3.4
21.500	3.4	3.4	3.4	3.4	3.4
22.000	3.4	3.4	3.4	3.4	3.4
22.500	3.4	3.4	3.4	3.5	3.5
23.000	3.5	3.5	3.5	3.5	3.5
23.500	3.5	3.5	3.5	3.5	3.5
24.000	3.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Time-Depth Curve: WQ

Label	WQ
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	1 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.0
1.500	0.0	0.0	0.0	0.0	0.0
2.000	0.0	0.0	0.0	0.0	0.0
2.500	0.0	0.0	0.0	0.0	0.0
3.000	0.0	0.0	0.1	0.1	0.1
3.500	0.1	0.1	0.1	0.1	0.1
4.000	0.1	0.1	0.1	0.1	0.1
4.500	0.1	0.1	0.1	0.1	0.1
5.000	0.1	0.1	0.1	0.1	0.1
5.500	0.1	0.1	0.1	0.1	0.1
6.000	0.1	0.1	0.1	0.1	0.1
6.500	0.1	0.1	0.1	0.1	0.1
7.000	0.1	0.1	0.1	0.1	0.1
7.500	0.1	0.2	0.2	0.2	0.2
8.000	0.2	0.2	0.2	0.2	0.2
8.500	0.2	0.2	0.2	0.2	0.2
9.000	0.2	0.2	0.2	0.2	0.2
9.500	0.2	0.2	0.2	0.2	0.2
10.000	0.2	0.3	0.3	0.3	0.3
10.500	0.3	0.3	0.3	0.3	0.3
11.000	0.3	0.3	0.3	0.4	0.4
11.500	0.4	0.4	0.5	0.6	0.8
12.000	0.9	0.9	1.0	1.0	1.0
12.500	1.0	1.0	1.0	1.0	1.0
13.000	1.1	1.1	1.1	1.1	1.1
13.500	1.1	1.1	1.1	1.1	1.1
14.000	1.1	1.1	1.1	1.1	1.1
14.500	1.1	1.2	1.2	1.2	1.2
15.000	1.2	1.2	1.2	1.2	1.2
15.500	1.2	1.2	1.2	1.2	1.2
16.000	1.2	1.2	1.2	1.2	1.2
16.500	1.2	1.2	1.2	1.2	1.2
17.000	1.2	1.2	1.2	1.2	1.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	1.2	1.3	1.3	1.3	1.3
18.000	1.3	1.3	1.3	1.3	1.3
18.500	1.3	1.3	1.3	1.3	1.3
19.000	1.3	1.3	1.3	1.3	1.3
19.500	1.3	1.3	1.3	1.3	1.3
20.000	1.3	1.3	1.3	1.3	1.3
20.500	1.3	1.3	1.3	1.3	1.3
21.000	1.3	1.3	1.3	1.3	1.3
21.500	1.3	1.3	1.3	1.3	1.3
22.000	1.3	1.3	1.3	1.3	1.3
22.500	1.3	1.3	1.3	1.4	1.4
23.000	1.4	1.4	1.4	1.4	1.4
23.500	1.4	1.4	1.4	1.4	1.4
24.000	1.4	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Elevation-Volume-Flow Table (Pond)
 Label: STF
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Infiltration	
Infiltration Method (Computed)	Constant
Infiltration Rate (Constant)	0.01 ft ³ /s

Initial Conditions	
Elevation (Water Surface, Initial)	1,005.50 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft ³ /s
Flow (Initial Infiltration)	0.00 ft ³ /s
Flow (Initial, Total)	0.00 ft ³ /s
Time Increment	0.050 hours

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,005.50	0.00	0.000	0.000	0.00	0.00	0.00
1,005.60	0.01	0.001	0.000	0.01	0.01	0.30
1,005.70	0.01	0.001	0.000	0.01	0.02	0.60
1,005.80	0.01	0.002	0.000	0.01	0.02	0.89
1,005.90	0.02	0.002	0.000	0.01	0.02	1.18
1,006.00	0.02	0.003	0.000	0.01	0.02	1.48
1,006.10	0.02	0.005	0.000	0.01	0.03	2.25
1,006.20	0.02	0.006	0.000	0.01	0.03	3.03
1,006.30	0.02	0.008	0.000	0.01	0.03	3.80
1,006.40	0.02	0.009	0.000	0.01	0.03	4.58
1,006.50	0.03	0.011	0.000	0.01	0.03	5.36
1,006.60	0.03	0.013	0.000	0.01	0.03	6.13
1,006.70	0.03	0.014	0.000	0.01	0.03	6.91
1,006.80	0.03	0.016	0.000	0.01	0.04	7.68
1,006.90	0.03	0.017	0.000	0.01	0.04	8.46
1,007.00	0.03	0.019	0.000	0.01	0.04	9.23
1,007.10	0.03	0.020	0.000	0.01	0.04	9.91
1,007.20	0.03	0.022	0.000	0.01	0.04	10.59
1,007.30	0.03	0.023	0.000	0.01	0.04	11.27
1,007.40	0.04	0.025	0.000	0.01	0.04	11.95
1,007.50	0.04	0.026	0.000	0.01	0.04	12.63
1,007.60	0.04	0.027	0.000	0.01	0.04	13.31
1,007.70	0.04	0.029	0.000	0.01	0.04	13.98
1,007.80	0.04	0.030	0.000	0.01	0.05	14.66
1,007.90	0.04	0.032	0.000	0.01	0.05	15.34
1,008.00	0.04	0.033	0.000	0.01	0.05	16.02
1,008.10	0.04	0.034	0.000	0.01	0.05	16.36
1,008.20	0.04	0.034	0.000	0.01	0.05	16.70
1,008.30	0.04	0.035	0.000	0.01	0.05	17.04

Subsection: Elevation-Volume-Flow Table (Pond)
 Label: STF
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,008.40	0.07	0.036	0.000	0.01	0.08	17.40
1,008.50	0.15	0.037	0.000	0.01	0.16	17.82
1,008.60	0.27	0.037	0.000	0.01	0.28	18.28
1,008.70	0.44	0.038	0.000	0.01	0.44	18.79
1,008.80	0.63	0.039	0.000	0.01	0.63	19.31
1,008.90	0.84	0.039	0.000	0.01	0.84	19.86
1,009.00	1.08	0.040	0.000	0.01	1.09	20.45
1,009.10	1.22	0.040	0.000	0.01	1.22	20.58
1,009.20	1.34	0.040	0.000	0.01	1.34	20.70
1,009.30	1.45	0.040	0.000	0.01	1.45	20.81
1,009.40	1.55	0.040	0.000	0.01	1.55	20.91
1,009.50	1.64	0.040	0.000	0.01	1.65	21.01
1,009.60	1.73	0.040	0.000	0.01	1.74	21.10
1,009.70	1.82	0.040	0.000	0.01	1.82	21.18
1,009.80	1.90	0.040	0.000	0.01	1.91	21.27
1,009.90	1.98	0.040	0.000	0.01	1.98	21.34
1,010.00	2.05	0.040	0.000	0.01	2.06	21.42
1,010.10	2.12	0.041	0.000	0.01	2.13	21.78
1,010.20	2.19	0.041	0.000	0.01	2.20	22.14
1,010.30	2.26	0.042	0.000	0.01	2.27	22.50
1,010.40	2.33	0.042	0.000	0.01	2.33	22.86
1,010.50	2.39	0.043	0.000	0.01	2.40	23.21
1,010.60	2.45	0.044	0.000	0.01	2.46	23.56
1,010.70	2.52	0.044	0.000	0.01	2.52	23.91
1,010.80	2.57	0.045	0.000	0.01	2.58	24.26
1,010.90	2.63	0.045	0.000	0.01	2.64	24.61
1,011.00	2.69	0.046	0.000	0.01	2.70	24.96
1,011.10	2.74	0.050	0.000	0.01	2.75	26.90
1,011.20	2.80	0.054	0.000	0.01	2.80	28.84
1,011.30	2.85	0.058	0.000	0.01	2.86	30.79
1,011.40	2.90	0.062	0.000	0.01	2.91	32.73
1,011.50	2.96	0.066	0.000	0.01	2.96	34.66
1,011.60	3.39	0.069	0.000	0.01	3.39	36.98
1,011.70	4.13	0.073	0.000	0.01	4.13	39.61
1,011.80	5.08	0.077	0.000	0.01	5.08	42.45
1,011.90	6.19	0.081	0.000	0.01	6.19	45.45
1,012.00	7.44	0.085	0.000	0.01	7.45	48.59

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	1.05 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	10.150 hours
Flow (Peak Outlet)	0.04 ft ³ /s	Time to Peak (Flow, Outlet)	13.500 hours
Elevation (Water Surface, Peak)	1,007.88 ft		
Volume (Peak)	0.031 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.058 ac-ft		
Volume (Total Infiltration)	0.008 ac-ft		
Volume (Total Outlet Outflow)	0.038 ac-ft		
Volume (Retained)	0.012 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.2 %		

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	3.28 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	5.350 hours
Flow (Peak Outlet)	2.70 ft ³ /s	Time to Peak (Flow, Outlet)	12.000 hours
Elevation (Water Surface, Peak)	1,011.03 ft		
Volume (Peak)	0.047 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.190 ac-ft		
Volume (Total Infiltration)	0.010 ac-ft		
Volume (Total Outlet Outflow)	0.151 ac-ft		
Volume (Retained)	0.029 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.1 %		

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	5.33 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	3.450 hours
Flow (Peak Outlet)	3.51 ft ³ /s	Time to Peak (Flow, Outlet)	12.050 hours
Elevation (Water Surface, Peak)	1,011.62 ft		
Volume (Peak)	0.070 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.318 ac-ft		
Volume (Total Infiltration)	0.011 ac-ft		
Volume (Total Outlet Outflow)	0.272 ac-ft		
Volume (Retained)	0.035 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.1 %		

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	7.47 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	2.500 hours
Flow (Peak Outlet)	6.37 ft ³ /s	Time to Peak (Flow, Outlet)	12.000 hours
Elevation (Water Surface, Peak)	1,011.91 ft		
Volume (Peak)	0.082 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.452 ac-ft		
Volume (Total Infiltration)	0.011 ac-ft		
Volume (Total Outlet Outflow)	0.406 ac-ft		
Volume (Retained)	0.035 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.1 %		

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Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Proposed Detained (STF)	WQv	1	0.058	11.900	1.05
Proposed Detained (STF)	2-year	2	0.190	11.900	3.28
Proposed Detained (STF)	10-YEAR	10	0.318	11.900	5.33
Proposed Detained (STF)	100-YEAR	100	0.452	11.900	7.47
Existing	WQv	1	1.006	12.000	16.51
Existing	2-year	2	3.833	12.000	59.94
Existing	10-YEAR	10	6.657	12.000	100.62
Existing	100-YEAR	100	9.666	12.000	142.74
Proposed Undetained	WQv	1	0.962	12.000	15.77
Proposed Undetained	2-year	2	3.663	12.000	57.28
Proposed Undetained	10-YEAR	10	6.362	12.000	96.15
Proposed Undetained	100-YEAR	100	9.237	12.000	136.41

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Existing	WQv	1	1.006	12.000	16.51
Existing	2-year	2	3.833	12.000	59.94
Existing	10-YEAR	10	6.657	12.000	100.62
Existing	100-YEAR	100	9.666	12.000	142.74
Proposed	WQv	1	0.999	12.000	15.81
Proposed	2-year	2	3.814	12.000	59.99
Proposed	10-YEAR	10	6.634	12.000	99.60
Proposed	100-YEAR	100	9.643	12.000	142.77

Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
STF (IN)	WQv	1	0.058	11.900	1.05	(N/A)	(N/A)
STF (OUT)	WQv	1	0.038	13.500	0.04	1,007.88	0.031
STF (IN)	2-year	2	0.190	11.900	3.28	(N/A)	(N/A)
STF (OUT)	2-year	2	0.151	12.000	2.70	1,011.03	0.047
STF (IN)	10-YEAR	10	0.318	11.900	5.33	(N/A)	(N/A)
STF (OUT)	10-YEAR	10	0.272	12.050	3.51	1,011.62	0.070
STF (IN)	100-YEAR	100	0.452	11.900	7.47	(N/A)	(N/A)
STF (OUT)	100-YEAR	100	0.406	12.000	6.37	1,011.91	0.082

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

Time-Depth Curve: 100-yr

Label	100-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	100 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.1	0.1	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.2
2.000	0.2	0.2	0.2	0.2	0.2
2.500	0.2	0.2	0.2	0.2	0.3
3.000	0.3	0.3	0.3	0.3	0.3
3.500	0.3	0.3	0.3	0.3	0.4
4.000	0.4	0.4	0.4	0.4	0.4
4.500	0.4	0.4	0.4	0.5	0.5
5.000	0.5	0.5	0.5	0.5	0.5
5.500	0.5	0.6	0.6	0.6	0.6
6.000	0.6	0.6	0.6	0.6	0.7
6.500	0.7	0.7	0.7	0.7	0.7
7.000	0.8	0.8	0.8	0.8	0.8
7.500	0.8	0.8	0.9	0.9	0.9
8.000	0.9	0.9	0.9	1.0	1.0
8.500	1.0	1.0	1.0	1.1	1.1
9.000	1.1	1.1	1.2	1.2	1.2
9.500	1.2	1.3	1.3	1.3	1.3
10.000	1.4	1.4	1.4	1.5	1.5
10.500	1.6	1.6	1.6	1.7	1.7
11.000	1.8	1.8	1.9	2.0	2.1
11.500	2.2	2.3	2.7	3.3	4.3
12.000	5.0	5.2	5.3	5.4	5.5
12.500	5.6	5.7	5.7	5.8	5.8
13.000	5.9	5.9	6.0	6.0	6.0
13.500	6.1	6.1	6.1	6.2	6.2
14.000	6.2	6.3	6.3	6.3	6.3
14.500	6.4	6.4	6.4	6.4	6.5
15.000	6.5	6.5	6.5	6.6	6.6
15.500	6.6	6.6	6.6	6.7	6.7
16.000	6.7	6.7	6.7	6.7	6.8
16.500	6.8	6.8	6.8	6.8	6.8
17.000	6.9	6.9	6.9	6.9	6.9

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	6.9	6.9	7.0	7.0	7.0
18.000	7.0	7.0	7.0	7.0	7.1
18.500	7.1	7.1	7.1	7.1	7.1
19.000	7.1	7.1	7.2	7.2	7.2
19.500	7.2	7.2	7.2	7.2	7.2
20.000	7.2	7.2	7.3	7.3	7.3
20.500	7.3	7.3	7.3	7.3	7.3
21.000	7.3	7.3	7.4	7.4	7.4
21.500	7.4	7.4	7.4	7.4	7.4
22.000	7.4	7.4	7.4	7.5	7.5
22.500	7.5	7.5	7.5	7.5	7.5
23.000	7.5	7.5	7.5	7.5	7.5
23.500	7.6	7.6	7.6	7.6	7.6
24.000	7.6	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Time-Depth Curve: 10-yr

Label	10-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	10 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.2	0.2	0.2	0.2	0.2
3.000	0.2	0.2	0.2	0.2	0.2
3.500	0.2	0.2	0.2	0.2	0.3
4.000	0.3	0.3	0.3	0.3	0.3
4.500	0.3	0.3	0.3	0.3	0.3
5.000	0.3	0.4	0.4	0.4	0.4
5.500	0.4	0.4	0.4	0.4	0.4
6.000	0.4	0.4	0.5	0.5	0.5
6.500	0.5	0.5	0.5	0.5	0.5
7.000	0.5	0.6	0.6	0.6	0.6
7.500	0.6	0.6	0.6	0.6	0.6
8.000	0.7	0.7	0.7	0.7	0.7
8.500	0.7	0.7	0.8	0.8	0.8
9.000	0.8	0.8	0.8	0.9	0.9
9.500	0.9	0.9	0.9	1.0	1.0
10.000	1.0	1.0	1.0	1.1	1.1
10.500	1.1	1.2	1.2	1.2	1.3
11.000	1.3	1.3	1.4	1.4	1.5
11.500	1.6	1.7	1.9	2.4	3.1
12.000	3.6	3.8	3.8	3.9	4.0
12.500	4.0	4.1	4.1	4.2	4.2
13.000	4.2	4.3	4.3	4.3	4.4
13.500	4.4	4.4	4.4	4.5	4.5
14.000	4.5	4.5	4.5	4.6	4.6
14.500	4.6	4.6	4.6	4.7	4.7
15.000	4.7	4.7	4.7	4.7	4.8
15.500	4.8	4.8	4.8	4.8	4.8
16.000	4.8	4.9	4.9	4.9	4.9
16.500	4.9	4.9	4.9	4.9	4.9
17.000	5.0	5.0	5.0	5.0	5.0

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	5.0	5.0	5.0	5.0	5.1
18.000	5.1	5.1	5.1	5.1	5.1
18.500	5.1	5.1	5.1	5.1	5.1
19.000	5.2	5.2	5.2	5.2	5.2
19.500	5.2	5.2	5.2	5.2	5.2
20.000	5.2	5.2	5.3	5.3	5.3
20.500	5.3	5.3	5.3	5.3	5.3
21.000	5.3	5.3	5.3	5.3	5.3
21.500	5.3	5.3	5.4	5.4	5.4
22.000	5.4	5.4	5.4	5.4	5.4
22.500	5.4	5.4	5.4	5.4	5.4
23.000	5.4	5.4	5.5	5.5	5.5
23.500	5.5	5.5	5.5	5.5	5.5
24.000	5.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

Time-Depth Curve: 2-yr

Label	2-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	2 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.1	0.1	0.1	0.1	0.1
3.000	0.1	0.1	0.1	0.1	0.1
3.500	0.1	0.1	0.2	0.2	0.2
4.000	0.2	0.2	0.2	0.2	0.2
4.500	0.2	0.2	0.2	0.2	0.2
5.000	0.2	0.2	0.2	0.2	0.2
5.500	0.2	0.3	0.3	0.3	0.3
6.000	0.3	0.3	0.3	0.3	0.3
6.500	0.3	0.3	0.3	0.3	0.3
7.000	0.3	0.4	0.4	0.4	0.4
7.500	0.4	0.4	0.4	0.4	0.4
8.000	0.4	0.4	0.4	0.4	0.5
8.500	0.5	0.5	0.5	0.5	0.5
9.000	0.5	0.5	0.5	0.5	0.6
9.500	0.6	0.6	0.6	0.6	0.6
10.000	0.6	0.6	0.7	0.7	0.7
10.500	0.7	0.7	0.8	0.8	0.8
11.000	0.8	0.8	0.9	0.9	1.0
11.500	1.0	1.1	1.2	1.5	2.0
12.000	2.3	2.4	2.4	2.5	2.5
12.500	2.6	2.6	2.6	2.7	2.7
13.000	2.7	2.7	2.7	2.8	2.8
13.500	2.8	2.8	2.8	2.8	2.9
14.000	2.9	2.9	2.9	2.9	2.9
14.500	2.9	2.9	3.0	3.0	3.0
15.000	3.0	3.0	3.0	3.0	3.0
15.500	3.0	3.0	3.1	3.1	3.1
16.000	3.1	3.1	3.1	3.1	3.1
16.500	3.1	3.1	3.1	3.1	3.1
17.000	3.2	3.2	3.2	3.2	3.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	3.2	3.2	3.2	3.2	3.2
18.000	3.2	3.2	3.2	3.2	3.2
18.500	3.3	3.3	3.3	3.3	3.3
19.000	3.3	3.3	3.3	3.3	3.3
19.500	3.3	3.3	3.3	3.3	3.3
20.000	3.3	3.3	3.3	3.3	3.4
20.500	3.4	3.4	3.4	3.4	3.4
21.000	3.4	3.4	3.4	3.4	3.4
21.500	3.4	3.4	3.4	3.4	3.4
22.000	3.4	3.4	3.4	3.4	3.4
22.500	3.4	3.4	3.4	3.5	3.5
23.000	3.5	3.5	3.5	3.5	3.5
23.500	3.5	3.5	3.5	3.5	3.5
24.000	3.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Time-Depth Curve: WQ

Label	WQ
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	1 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.0
1.500	0.0	0.0	0.0	0.0	0.0
2.000	0.0	0.0	0.0	0.0	0.0
2.500	0.0	0.0	0.0	0.0	0.0
3.000	0.0	0.0	0.1	0.1	0.1
3.500	0.1	0.1	0.1	0.1	0.1
4.000	0.1	0.1	0.1	0.1	0.1
4.500	0.1	0.1	0.1	0.1	0.1
5.000	0.1	0.1	0.1	0.1	0.1
5.500	0.1	0.1	0.1	0.1	0.1
6.000	0.1	0.1	0.1	0.1	0.1
6.500	0.1	0.1	0.1	0.1	0.1
7.000	0.1	0.1	0.1	0.1	0.1
7.500	0.1	0.2	0.2	0.2	0.2
8.000	0.2	0.2	0.2	0.2	0.2
8.500	0.2	0.2	0.2	0.2	0.2
9.000	0.2	0.2	0.2	0.2	0.2
9.500	0.2	0.2	0.2	0.2	0.2
10.000	0.2	0.3	0.3	0.3	0.3
10.500	0.3	0.3	0.3	0.3	0.3
11.000	0.3	0.3	0.3	0.4	0.4
11.500	0.4	0.4	0.5	0.6	0.8
12.000	0.9	0.9	1.0	1.0	1.0
12.500	1.0	1.0	1.0	1.0	1.0
13.000	1.1	1.1	1.1	1.1	1.1
13.500	1.1	1.1	1.1	1.1	1.1
14.000	1.1	1.1	1.1	1.1	1.1
14.500	1.1	1.2	1.2	1.2	1.2
15.000	1.2	1.2	1.2	1.2	1.2
15.500	1.2	1.2	1.2	1.2	1.2
16.000	1.2	1.2	1.2	1.2	1.2
16.500	1.2	1.2	1.2	1.2	1.2
17.000	1.2	1.2	1.2	1.2	1.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)				
17.500	1.2	1.3	1.3	1.3	1.3
18.000	1.3	1.3	1.3	1.3	1.3
18.500	1.3	1.3	1.3	1.3	1.3
19.000	1.3	1.3	1.3	1.3	1.3
19.500	1.3	1.3	1.3	1.3	1.3
20.000	1.3	1.3	1.3	1.3	1.3
20.500	1.3	1.3	1.3	1.3	1.3
21.000	1.3	1.3	1.3	1.3	1.3
21.500	1.3	1.3	1.3	1.3	1.3
22.000	1.3	1.3	1.3	1.3	1.3
22.500	1.3	1.3	1.3	1.4	1.4
23.000	1.4	1.4	1.4	1.4	1.4
23.500	1.4	1.4	1.4	1.4	1.4
24.000	1.4	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Elevation-Volume-Flow Table (Pond)
 Label: STF
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Infiltration	
Infiltration Method (Computed)	Constant
Infiltration Rate (Constant)	0.01 ft ³ /s

Initial Conditions	
Elevation (Water Surface, Initial)	1,005.50 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft ³ /s
Flow (Initial Infiltration)	0.00 ft ³ /s
Flow (Initial, Total)	0.00 ft ³ /s
Time Increment	0.050 hours

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,005.50	0.00	0.000	0.000	0.00	0.00	0.00
1,005.60	0.01	0.001	0.000	0.01	0.01	0.30
1,005.70	0.01	0.001	0.000	0.01	0.02	0.60
1,005.80	0.01	0.002	0.000	0.01	0.02	0.89
1,005.90	0.02	0.002	0.000	0.01	0.02	1.18
1,006.00	0.02	0.003	0.000	0.01	0.02	1.48
1,006.10	0.02	0.005	0.000	0.01	0.03	2.25
1,006.20	0.02	0.006	0.000	0.01	0.03	3.03
1,006.30	0.02	0.008	0.000	0.01	0.03	3.80
1,006.40	0.02	0.009	0.000	0.01	0.03	4.58
1,006.50	0.03	0.011	0.000	0.01	0.03	5.36
1,006.60	0.03	0.013	0.000	0.01	0.03	6.13
1,006.70	0.03	0.014	0.000	0.01	0.03	6.91
1,006.80	0.03	0.016	0.000	0.01	0.04	7.68
1,006.90	0.03	0.017	0.000	0.01	0.04	8.46
1,007.00	0.03	0.019	0.000	0.01	0.04	9.23
1,007.10	0.03	0.020	0.000	0.01	0.04	9.91
1,007.20	0.03	0.022	0.000	0.01	0.04	10.59
1,007.30	0.03	0.023	0.000	0.01	0.04	11.27
1,007.40	0.04	0.025	0.000	0.01	0.04	11.95
1,007.50	0.04	0.026	0.000	0.01	0.04	12.63
1,007.60	0.04	0.027	0.000	0.01	0.04	13.31
1,007.70	0.04	0.029	0.000	0.01	0.04	13.98
1,007.80	0.04	0.030	0.000	0.01	0.05	14.66
1,007.90	0.04	0.032	0.000	0.01	0.05	15.34
1,008.00	0.04	0.033	0.000	0.01	0.05	16.02
1,008.10	0.04	0.034	0.000	0.01	0.05	16.36
1,008.20	0.04	0.034	0.000	0.01	0.05	16.70
1,008.30	0.04	0.035	0.000	0.01	0.05	17.04

Subsection: Elevation-Volume-Flow Table (Pond)
 Label: STF
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,008.40	0.07	0.036	0.000	0.01	0.08	17.40
1,008.50	0.15	0.037	0.000	0.01	0.16	17.82
1,008.60	0.27	0.037	0.000	0.01	0.28	18.28
1,008.70	0.44	0.038	0.000	0.01	0.44	18.79
1,008.80	0.63	0.039	0.000	0.01	0.63	19.31
1,008.90	0.84	0.039	0.000	0.01	0.84	19.86
1,009.00	1.08	0.040	0.000	0.01	1.09	20.45
1,009.10	1.22	0.040	0.000	0.01	1.22	20.58
1,009.20	1.34	0.040	0.000	0.01	1.34	20.70
1,009.30	1.45	0.040	0.000	0.01	1.45	20.81
1,009.40	1.55	0.040	0.000	0.01	1.55	20.91
1,009.50	1.64	0.040	0.000	0.01	1.65	21.01
1,009.60	1.73	0.040	0.000	0.01	1.74	21.10
1,009.70	1.82	0.040	0.000	0.01	1.82	21.18
1,009.80	1.90	0.040	0.000	0.01	1.91	21.27
1,009.90	1.98	0.040	0.000	0.01	1.98	21.34
1,010.00	2.05	0.040	0.000	0.01	2.06	21.42
1,010.10	2.12	0.041	0.000	0.01	2.13	21.78
1,010.20	2.19	0.041	0.000	0.01	2.20	22.14
1,010.30	2.26	0.042	0.000	0.01	2.27	22.50
1,010.40	2.33	0.042	0.000	0.01	2.33	22.86
1,010.50	2.39	0.043	0.000	0.01	2.40	23.21
1,010.60	2.45	0.044	0.000	0.01	2.46	23.56
1,010.70	2.52	0.044	0.000	0.01	2.52	23.91
1,010.80	2.57	0.045	0.000	0.01	2.58	24.26
1,010.90	2.63	0.045	0.000	0.01	2.64	24.61
1,011.00	2.69	0.046	0.000	0.01	2.70	24.96
1,011.10	2.74	0.050	0.000	0.01	2.75	26.90
1,011.20	2.80	0.054	0.000	0.01	2.80	28.84
1,011.30	2.85	0.058	0.000	0.01	2.86	30.79
1,011.40	2.90	0.062	0.000	0.01	2.91	32.73
1,011.50	2.96	0.066	0.000	0.01	2.96	34.66
1,011.60	3.39	0.069	0.000	0.01	3.39	36.98
1,011.70	4.13	0.073	0.000	0.01	4.13	39.61
1,011.80	5.08	0.077	0.000	0.01	5.08	42.45
1,011.90	6.19	0.081	0.000	0.01	6.19	45.45
1,012.00	7.44	0.085	0.000	0.01	7.45	48.59

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Infiltration	
Infiltration Method (Computed)	Constant
Infiltration Rate (Constant)	0.01 ft ³ /s

Initial Conditions	
Elevation (Water Surface, Initial)	1,005.50 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft ³ /s
Flow (Initial Infiltration)	0.00 ft ³ /s
Flow (Initial, Total)	0.00 ft ³ /s
Time Increment	0.050 hours

Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	1.05 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	10.150 hours
Flow (Peak Outlet)	0.04 ft ³ /s	Time to Peak (Flow, Outlet)	13.500 hours

Elevation (Water Surface, Peak)	1,007.88 ft
Volume (Peak)	0.031 ac-ft

Mass Balance (ac-ft)	
Volume (Initial)	0.000 ac-ft
Volume (Total Inflow)	0.058 ac-ft
Volume (Total Infiltration)	0.008 ac-ft
Volume (Total Outlet Outflow)	0.038 ac-ft
Volume (Retained)	0.012 ac-ft
Volume (Unrouted)	0.000 ac-ft
Error (Mass Balance)	0.2 %

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	3.28 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	5.350 hours
Flow (Peak Outlet)	2.70 ft ³ /s	Time to Peak (Flow, Outlet)	12.000 hours
Elevation (Water Surface, Peak)	1,011.03 ft		
Volume (Peak)	0.047 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.190 ac-ft		
Volume (Total Infiltration)	0.010 ac-ft		
Volume (Total Outlet Outflow)	0.151 ac-ft		
Volume (Retained)	0.029 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.1 %		

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Infiltration			
Infiltration Method (Computed)	Constant		
Infiltration Rate (Constant)	0.01 ft ³ /s		
Initial Conditions			
Elevation (Water Surface, Initial)	1,005.50 ft		
Volume (Initial)	0.000 ac-ft		
Flow (Initial Outlet)	0.00 ft ³ /s		
Flow (Initial Infiltration)	0.00 ft ³ /s		
Flow (Initial, Total)	0.00 ft ³ /s		
Time Increment	0.050 hours		
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	5.33 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	3.450 hours
Flow (Peak Outlet)	3.51 ft ³ /s	Time to Peak (Flow, Outlet)	12.050 hours
Elevation (Water Surface, Peak)	1,011.62 ft		
Volume (Peak)	0.070 ac-ft		
Mass Balance (ac-ft)			
Volume (Initial)	0.000 ac-ft		
Volume (Total Inflow)	0.318 ac-ft		
Volume (Total Infiltration)	0.011 ac-ft		
Volume (Total Outlet Outflow)	0.272 ac-ft		
Volume (Retained)	0.035 ac-ft		
Volume (Unrouted)	0.000 ac-ft		
Error (Mass Balance)	0.1 %		

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

Infiltration	
Infiltration Method (Computed)	Constant
Infiltration Rate (Constant)	0.01 ft ³ /s

Initial Conditions	
Elevation (Water Surface, Initial)	1,005.50 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft ³ /s
Flow (Initial Infiltration)	0.00 ft ³ /s
Flow (Initial, Total)	0.00 ft ³ /s
Time Increment	0.050 hours

Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	7.47 ft ³ /s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)	0.01 ft ³ /s	Time to Peak (Infiltration)	2.500 hours
Flow (Peak Outlet)	6.37 ft ³ /s	Time to Peak (Flow, Outlet)	12.000 hours

Elevation (Water Surface, Peak)	1,011.91 ft
Volume (Peak)	0.082 ac-ft

Mass Balance (ac-ft)	
Volume (Initial)	0.000 ac-ft
Volume (Total Inflow)	0.452 ac-ft
Volume (Total Infiltration)	0.011 ac-ft
Volume (Total Outlet Outflow)	0.406 ac-ft
Volume (Retained)	0.035 ac-ft
Volume (Unrouted)	0.000 ac-ft
Error (Mass Balance)	0.1 %

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SCS Type II (Time-Depth Curve, 2 years (2-year))...6, 7

STF (Elevation-Volume-Flow Table (Pond), 1 years (WQv))...10, 11

STF (IN) (Level Pool Pond Routing Summary, 1 years (WQv))...12

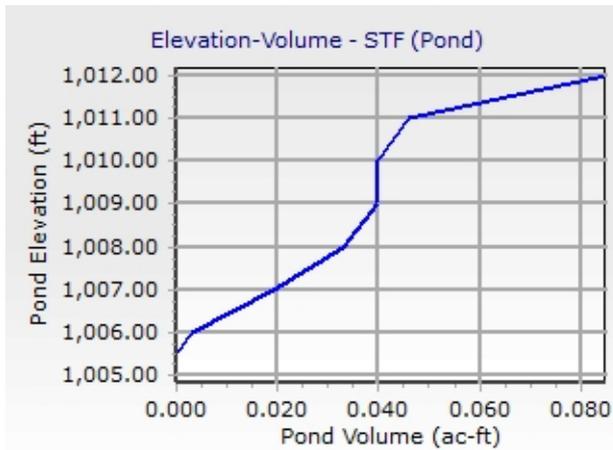
STF (IN) (Level Pool Pond Routing Summary, 10 years (10-YEAR))...14

STF (IN) (Level Pool Pond Routing Summary, 100 years (100-YEAR))...15

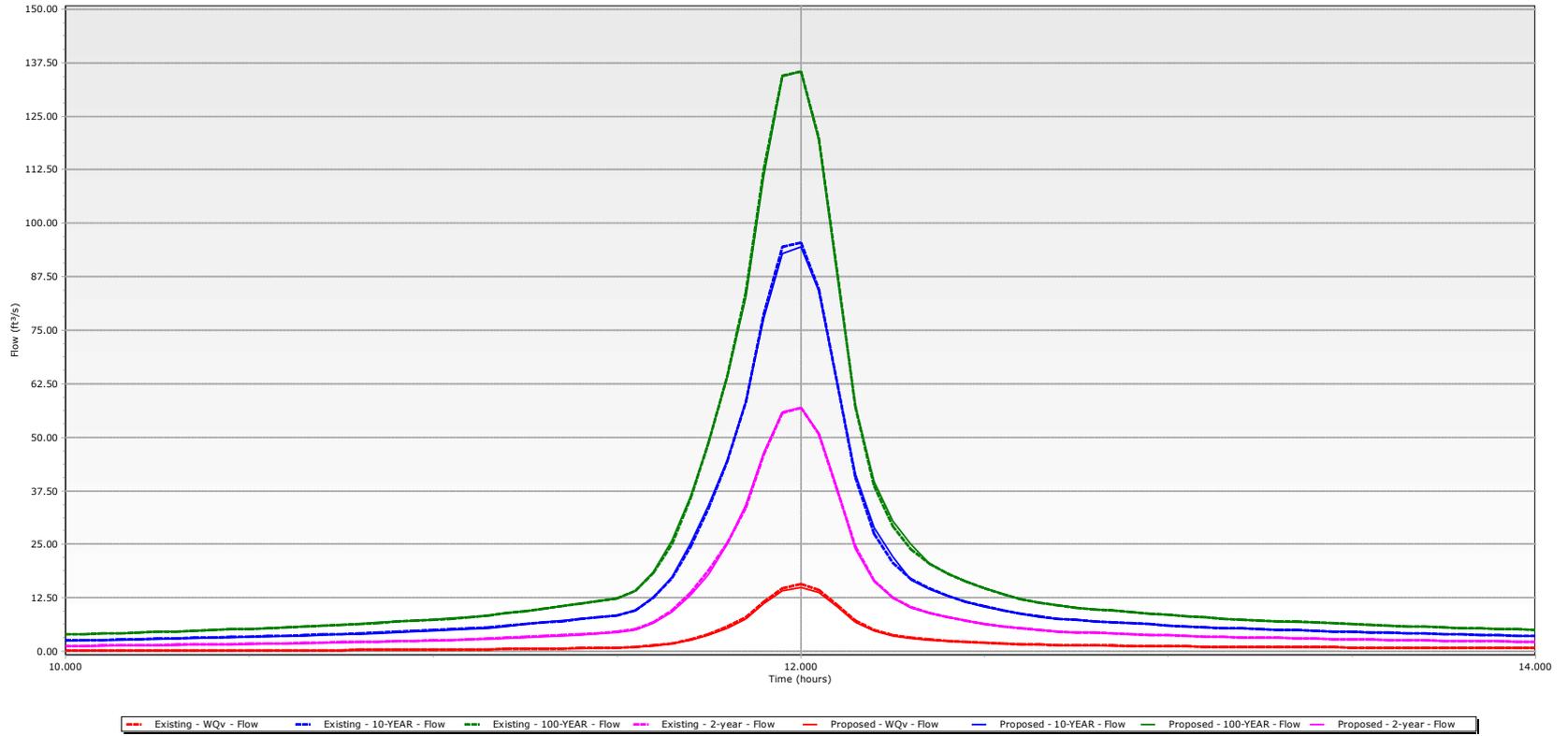
STF (IN) (Level Pool Pond Routing Summary, 2 years (2-year))...13

Elevation-Volume - STF (Pond)

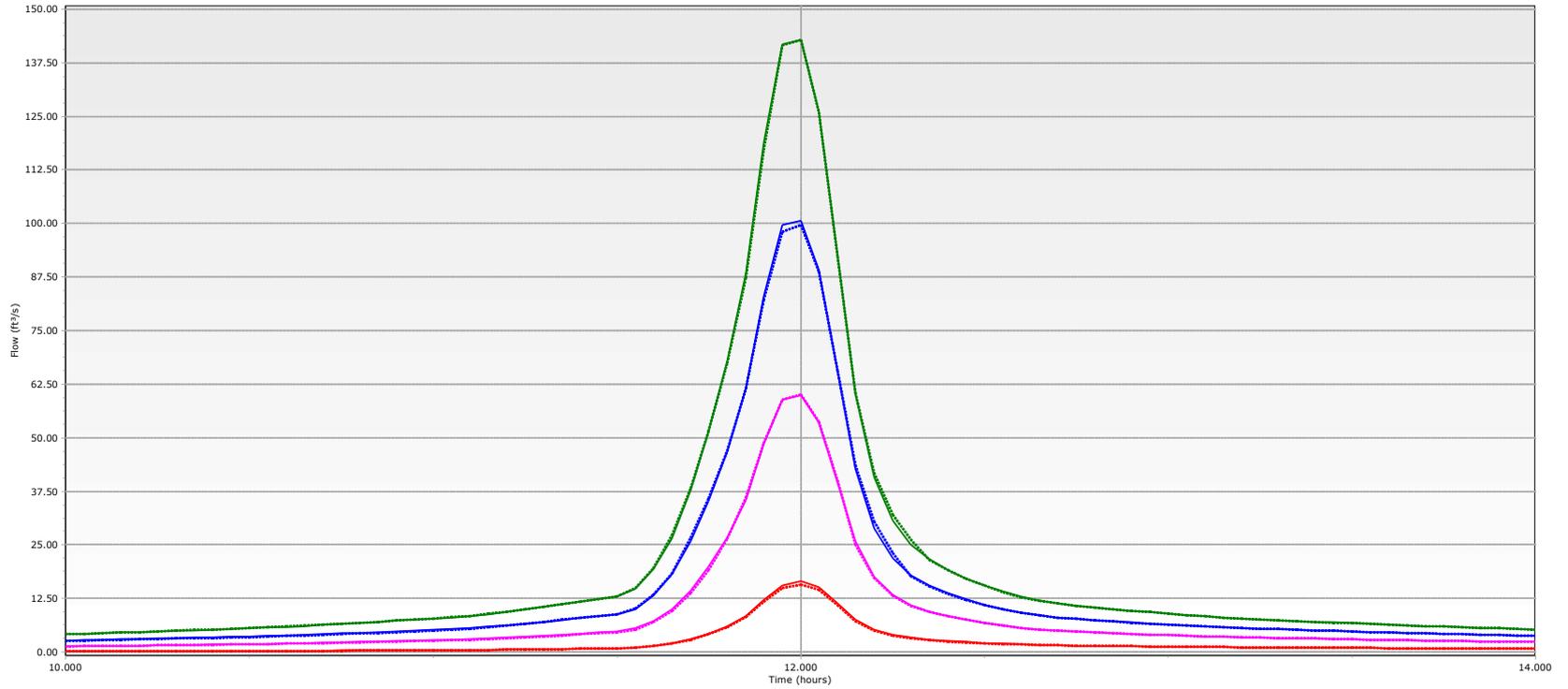
Pond Elevation (ft)	Pond Volume (ac-ft)
1,005.50	0.000
1,006.00	0.003
1,007.00	0.019
1,008.00	0.033
1,009.00	0.040
1,010.00	0.040
1,011.00	0.046
1,012.00	0.085



Existing Vs. Proposed Hydrograph



Existing vs Proposed Hydrograph



Existing - 10-YEAR - Flow Existing - WQv - Flow Existing - 100-YEAR - Flow Existing - 2-year - Flow Proposed - 10-YEAR - Flow Proposed - WQv - Flow Proposed - 100-YEAR - Flow Proposed - 2-year - Flow