

# **FINAL STORMWATER STUDY**

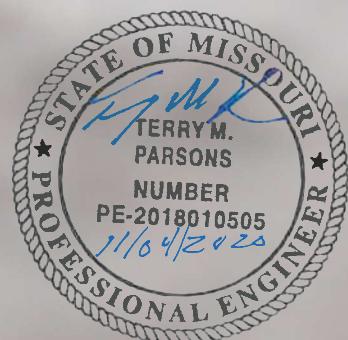
LS MIDDLE SCHOOL #4  
Lee's Summit, Jackson County, Missouri

**Prepared for:**

Lee's Summit School District  
Lee's Summit, Missouri

**Prepared By**

Olsson  
7301 W. 133<sup>rd</sup> Street, Suite 200  
Overland Park, Kansas 66213



August 2020  
(Revised November 2020)  
Olsson Project No. 020-0103

**olsson**

# TABLE OF CONTENTS

Summary .....	1
1. Introduction .....	1
1.1. Project Location and Description .....	1
1.2. Study Purpose.....	1
2. Methodology .....	1
2.1. General Criteria and References .....	1
2.2. Soils Description.....	2
3. Hydrologic/Hydraulic Analyses .....	2
3.1. Existing Conditions .....	2
3.2. Proposed Conditions Analysis .....	3
3.3. Stormwater Detention .....	5
4. Storm water treatment requirements .....	9
5. Clean Water Act Section 404 Permitting Requirements.....	9
6. FEMA/DWR Permit Requirements .....	<b>Error! Bookmark not defined.</b>
7. Conclusions and Recommendations .....	10
Appendix A Drainage Maps.....	11
Appendix B Accompanying Documents .....	12
Appendix C BMP Calculations and Information .....	13

## **APPENDICES**

Appendix A Drainage Maps

Appendix B Accompanying Documents

Appendix C BMP Calculations and Information

## SUMMARY

This storm drainage study is being submitted on behalf of the Lee's Summit School District for the proposed development of the property located south of Bailey Road between Dalton Drive and Ranson Road, in Lee's Summit, Jackson County, Missouri. This property is an existing terraced row crop field with no existing buildings. This final report is being submitted to the City of Lee's Summit with the Final Development Plan for approval of this institutional development.

# 1. INTRODUCTION

This final stormwater management study is being submitted on behalf of Lee's Summit School District for a development on a 51.85 acre parcel of land generally located south of Bailey Road between Dalton Drive and Ranson Road, in Lee's Summit, Jackson County, Missouri. .

## 1.1. Project Location and Description

The proposed site is located in the northeast quarter of Section 16, Township 47 North, Range 31 West. The existing site is currently undeveloped consisting of terraced row crop. The site drains to the southeast into an unnamed tributary that runs along the entirety of the east side of the property. The tributary flows south to Big Creek. The site is not located within the flood plain.

## 1.2. Study Purpose

The purpose of this report is to verify this development's conformance with the City of Lee's Summit Design Criteria and Plan Requirements for Public Improvement Plans 2019 edition. Storm water drainage facilities are designed according to section F of the aforementioned criteria. This study will outline methods to mitigate impacts on storm water runoff resulting from the development for the 2, 10 and 100-year rainfall events and for treatment of stormwater runoff with the use of permanent stormwater treatment facilities.

# 2. METHODOLOGY

## 2.1. General Criteria and References

Analytical and design criteria conform to those of Division V - Section 5600 – “Storm Drainage Systems and Facilities” of the Kansas City Metropolitan Chapter of the American Public Works Association’s “Standard Specifications and Design Criteria”. Based on these criteria’s, Post-development discharge rates for the 2, 10, and 100-year storm events will be limited to provisions in section 5608.4-C1 Performance Criteria – “Comprehensive Control”. Post-development discharge rates are limited to 0.5 cfs per acre for 2-Year, 2.0 cfs per acre for 10-year, and 3.0 cfs per acre for 100-year storm events.

Post development flows from the site are shown below and were calculated using HEC-HMS for the 2, 10 and 100-year storm events. Existing and proposed hydrographs were calculated using the 24-hour SCS Type II rainfall distribution. Existing times of concentration were determined using Inlet Time and Travel Time equations found in Section 5602.7 of APWA Section 5600.

## 2.2. Soils Description

Soil classifications by the United States Department of Agriculture (USDA) on the Natural Resources Conservation Service (NRCS) Soils website for Johnson County, Kansas show the existing site consisting of the following soil types:

10117 – Sampsel Silty Clay Loams, 5 to 9 percent slopes – HSG Type C/D

10082 – Arisburg-Urban Land Complex, 1 to 5 percent slopes – HSG Type C

\*HSG – *Hydrologic Soils Group (The NRCS information is included in the appendix).*

# 3. HYDROLOGIC/HYDRAULIC ANALYSES

## 3.1. Existing Conditions

The property is bounded by residential lots to the west and north. Bailey Road is also located on the north side of the property. To the south and east the adjacent properties are currently undeveloped. A tributary to Big Creek, that flows to the south, lies along the entire east property line of the site. The storm drainage from the residential lots to the north comes under Bailey Road and empties into the north end of the tributary. The property currently contains no impervious area and runoff flows southeasterly to the tributary. An Exhibit of the Existing Conditions is included in Appendix A.

With the comprehensive control method is being used for drainage design, an existing curve number analysis is not required for the site.

There are existing developments to the west and north of the property. Runoff from the development to the north is collected by an enclosed drainage system that empties into the stream on the east side of the site. Runoff from a portion of the backyards of the residences to the west do drain on to the site (approximately 1.2 acres).

## 3.2. Stream Protection and Buffer Zones

A portion of the property will be defined as a Stream Protection Buffer Zone. The proposed buffer zone will meet the requirements established Section 5603.5 of the APWA Section 5600 Design Criteria.

The width of the setback is determined by the drainage area to the stream. Using USGS contours the drainage area for the stream was determined at different points. A minor tributary from the east is the location for Point 1. The drainage area to Point 1 is 138 acres. Therefore a 60' offset from the ordinary high-water mark (OHM), ie surveyed top of bank, is used to determine the buffer extent to that point. Point 2 is located where the stream exits at the

southern edge of the property. The total drainage to this point is 210 acres. The setback from Point 1 to Point 2 is 100'. An exhibit of the stream setback drainage areas is included in Appendix A.

The final development plan will require a waiver/modification to the Stream Setback Buffer in order to complete the construction of the improvements shown. The encroachment is needed due to the nature of the site being narrow in the east/west direction and meeting the program requirements for all of the components needed on site by the school district. The grade of the site falls from west to east towards the existing streamway. Again, with the narrow site it is difficult grade out the site for buildings, fields, and parking and not have the slope embankment encroach into the buffer.

According to the requirements of Section 5605.3, a total of 2.08 acres should be dedicated to the stream setback. To accommodate the improvements noted above a total of 0.74 acres of stream setback will be encroached upon. . To offset this, an additional 0.76 acres adjacent to the stream setback will be added back into the setback. This results in 2.10 acres of permanent stream setback dedication.

### **3.3. Proposed Conditions Analysis**

Post development, the entirety of the property will continue to flow to the tributary to the east. The proposed site will include the middle school, a softball/baseball complex (with 4 fields), a track, practice fields, outdoor classrooms, parking, three extended dry detention basins, private storm, and associated utilities. Roof drains, private storm sewer pipe and inlets will allow adequate drainage of the proposed school, athletic facilities and parking areas. The private storm will drain into the detention basins and then be routed to the tributary. A private road will be constructed for access to the bus turnaround and parking areas. The road will connect to the existing Bailey Road on the north to proposed Cape Road on the south.

The proposed Cape Road will be located on the southern portion of the property. The right of way will be dedicated to the city with a portion the road being constructed to connect to existing Cape Road to the west. When the road is completely constructed a public storm system will drain the road to the tributary. Temporary provisions will be implemented to drain the constructed road to the stream.

The backyards of the residential subdivisions to the west also drain onto the existing sight. This 2.5 acres will drain to the proposed north-south private road and will enter into the proposed storm system for the road.

The site will be divided into three main drainage areas. An exhibit of the Stormwater Management Plan drainage areas is included in Appendix A. Each drainage area will have

collection system and an extended dry detention basin with control structure. A general description of what is draining to each area is as follows:

Drainage Area 1 (3.5 acres) - northwest ball field ball field and a portion of the common area in the ball fields

Drainage Area 2 (8.2 acres) - northeast ball field, a portion of the common areas in the ball fields and the northeast quarter of the roof for the middle school

Drainage Area 3 (22.6 acres) – 2 southern ball fields, the remainder of middle school building roof, north-south drive, main parking area, bus turnaround area, the practice fields and the track.

The ball fields and the track will have synthetic surfacing with underdrain systems. The current plan is for the two north fields to have synthetic turf on the infields and outfields. The two south fields will have synthetic turf on the infields only. If the budget allows, there is a possibility that the two south fields will have also have synthetic turf in the outfields. For the purposes of this report, the ballfields will be treated as if they have a complete synthetic surface.

The synthetic surface will act as impervious surface. However, the underdrain system, with its aggregate subsurface rock layer and underdrain piping, will increase the time of concentration ( $T_c$ ) for the runoff that is guided through the underdrain system. The increase in  $T_c$  will be 32 minutes based on the final underdrain design. The HEC-HMS model based its  $T_c$ 's on a time to inlet of 5 minutes and then an estimation of pipe travel time. This was used as the  $T_c$  for the impervious and pervious areas in the drainage area. The synthetic fields had an additional time of 32 minutes added to their  $T_c$ 's.

Based on the completed models the peak flows for each area are included in the table below:

**Table 1. Post-Development Peak Flows**

Site Description	Total Area (ac)	CN	Storm Event	Runoff Q (cfs)
Area 1	3.5	79.4	2-YR	<b>5.7</b>
			10-YR	<b>8.6</b>
			100-YR	<b>12.5</b>
Area 2	8.2	89.6	2-YR	<b>10.9</b>
			10-YR	<b>25.5</b>
			100-YR	<b>37.5</b>
Area 3	22.6	87.5	2-YR	<b>38.4</b>
			10-YR	<b>90.7</b>
			100-YR	<b>133.8</b>

### 3.4. Stormwater Detention

As stated previously, a new detention basin will be constructed for each area to mitigate the increase in flow due to the increase in impervious area. A control structure will be located at the outlet of the basin. An orifice/weir plate in the control structure will limit outflow in the 2, 10, and 100-year storms.

The control structure for each basin is designed to limit the outlet flow to the allowable release rate for each storm based on the Comprehensive Control Strategy. Hydrographs for the combined flows of the detained and undetained areas are shown in Appendix D.

To meet water treatment requirements, the basin will act as extended dry detention. The water quality volume (WQv) will be controlled by a series of 1" orifices at the bottom of the orifice plate. The conduit will release the water quality volume over a 40-hour period to allow pollutants to settle out of this precipitation event.

Per Section 5600 of the Design and Construction Manual an emergency spillway has been designed for each basin. The emergency spillway for each basin is located the top of the dam of each structure. The emergency spillway has been sized to accommodate the 100-year event assuming that 100% of the primary outlet structure is clogged and there is zero available

storage in the basin. Each spillway is a minimum of 0.5 feet above the nominal 100-year water surface elevation. There is also least 1 foot of freeboard between the clogged condition with and the water surface elevation of the spillway handling the 100-year overflow and top of the dam. The details for the emergency spillway have been included in Appendix D of this report and in the construction documents.

**Table 2. EDD-1 WSE's and Peak Flows**

Description	Detention Basin
Bottom of Basin	1007.16
Total Storage Volume	0.85 ac-ft
Top of Dam Elevation	1012.60
WQv Orifice (IE Elevation, Pipe Size)	1007.16, 6 – 1" (ft, # hole - diam)
Water Quality Volume WSE, Storage	1008.41, 0.18 (ft, ac-ft)
2-year & 10-Year Orifice (IE Elevation, Pipe Size)	1008.43, 1-6" (ft, orifice size)
10-Year Storm WSE, Storage, Peak Outflow	1010.3, 0.5, 4.2 (ft, ac-ft, cfs)
100-Year Storm Weir (Elevation, Length)	1009.58, 6.0 (ft, lf)
100-Year Storm WSE, Storage, Peak Outflow	1010.8, 0.6, 9.9 (ft, ac-ft, cfs)

**Table 3. EDD-2 WSE's and Peak Flows**

Description	Detention Basin
Bottom of Basin	995.13
Total Storage Volume	1.34 ac-ft
Top of Dam Elevation	1002.99
WQv Orifice (IE Elevation, Pipe Size)	995.13, 10 – 1" (ft, # hole - diam)
Water Quality Volume WSE, Storage	997.40, 0.42 (ft, ac-ft)
2-year & 10-Year Orifice (IE Elevation, Pipe Size)	997.50, 1-9" (ft, orifice size)
10-Year Storm WSE, Storage, Peak Outflow	1000.3, 0.8, 14.0 (ft, ac-ft, cfs)
100-Year Storm Weir (Elevation, Length)	999.03, 8.0 (ft, lf)
100-Year Storm WSE, Storage, Peak Outflow	1001.10, 1.2, 24.1 (ft, ac-ft, cfs)

**Table 4. EDD-3 WSE's and Peak Flows**

Description	Detention Basin
Bottom of Basin	989.29
Total Storage Volume	5.3 ac-ft
Top of Dam Elevation	1001.07
WQv Orifice (IE Elevation, Pipe Size)	989.22, 15 – 2" (ft, # hole - diam)
Water Quality Volume WSE, Storage	994.40, 1.95 (ft, ac-ft)
2-year & 10-Year Orifice (IE Elevation, Pipe Size)	994.50, 1-15" (ft, orifice size)
10-Year Storm WSE, Storage, Peak Outflow	997.40, 3.7, 35.9 (ft, ac-ft, cfs)
100-Year Storm Weir (Elevation, Length)	996.10, 16 (ft, lf)
100-Year Storm WSE, Storage, Peak Outflow	998.40, 4.7, 63.0 (ft, ac-ft, cfs)

**Table 5. Detention Basin Information**

Area	Drainage Area (acres)	Storm Event	Allowable Release Rate (cfs)	Design Release Rate (cfs)	Storage Required (ac-ft)	WSE (ft elev)
1	3.5	2-YR	1.8	1.6	0.3	1009.7
		10-YR	7.0	4.2	0.5	1010.3
		100-YR	10.4	9.9	0.6	1010.8
2	8.2	2-YR	4.1	3.7	0.5	998.9
		10-YR	16.4	14.0	0.9	1000.3
		100-YR	24.5	24.1	1.3	1001.1
3	22.6	2-YR	11.3	11.1	2.9	995.7
		10-YR	45.3	35.9	3.7	997.4
		100-YR	67.9	63.0	4.7	998.4

## **4. STORM WATER TREATMENT REQUIREMENTS**

As stated previously, the three detention basins will be designed to act as extended dry bottom detention facilities to treat stormwater per MARC water quality standards. The orifice plate for the basin are sized to release the water quality volume (1.37") over a 40-hour period to allow pollutants to settle from runoff before entering the public stormwater system. The size and quantities of the orifice holes are included in Tables 3-5.

## **5. CLEANWATER ACT SECTION 404 PERMITTING REQUIREMENTS**

Construction will not be occurring within jurisdictional Waters of the United States. Therefore, a Section 404 permit is not required.

## **6. FEMA/DWR PERMIT REQUIREMENTS**

No FEMA permitting or submittals will be required on this site because there are no FEMA delineated floodplains on the site. A copy of the FIRM map for this area has been included in Appendix B.

## 7. CONCLUSIONS AND RECOMMENDATIONS

As outlined in the preceding report, the stormwater management plan for this development meets the requirements set forth in Section 5600 of the Lee's Summit Design and Construction Manual.

The development will increase impervious areas on the site and drainage patterns on the site remain will relatively unchanged. Increased runoff rates in the post-development condition will be controlled by three detention structures. The control structures have been designed to limit the peak flows below the allowable release rates defined in the Comprehensive Control Strategy of Section 5600. All three basins will be constructed as extended dry detention basins to satisfy the Section 5600 storm water quality requirements.

The eastern portion of the property will be dedicated in a stream buffer easement per Section 5605.3. To totally satisfy the stream setback requirements, a waiver will be required for areas where site improvements impede in the setback areas.

The existing property drains in a southeasterly direction limited on the east by the stream. There are no existing developments in that direction. Therefore no waivers are required for the existing development adjacent to the site under Section 5601.6B.

No 404 or FEMA will be required. Based on these facts and other information provided herein, we request approval of this stormwater study.

## **APPENDIX A**

### **Report Exhibits**

Existing Conditions

Stream Setback

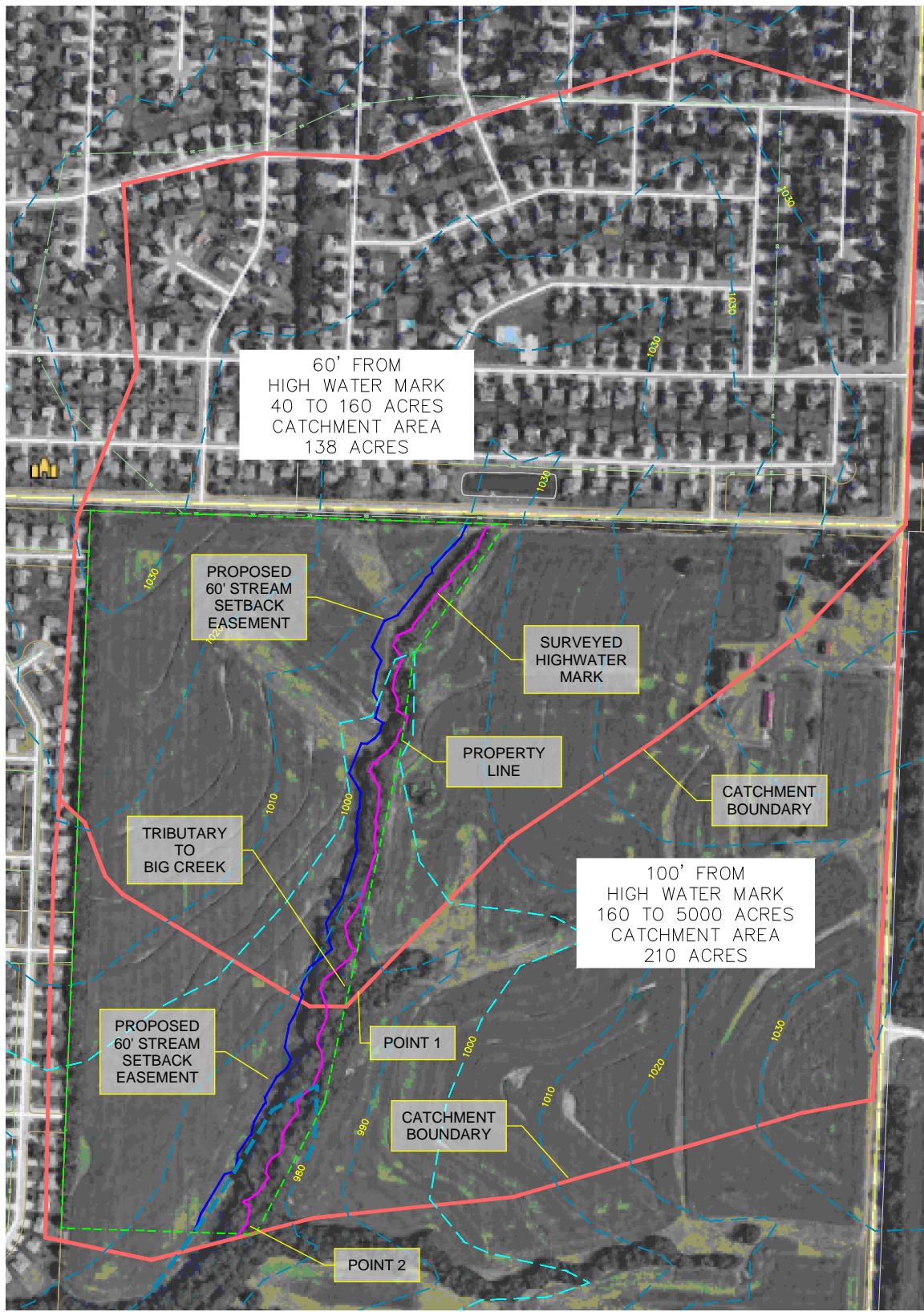
Site Plan

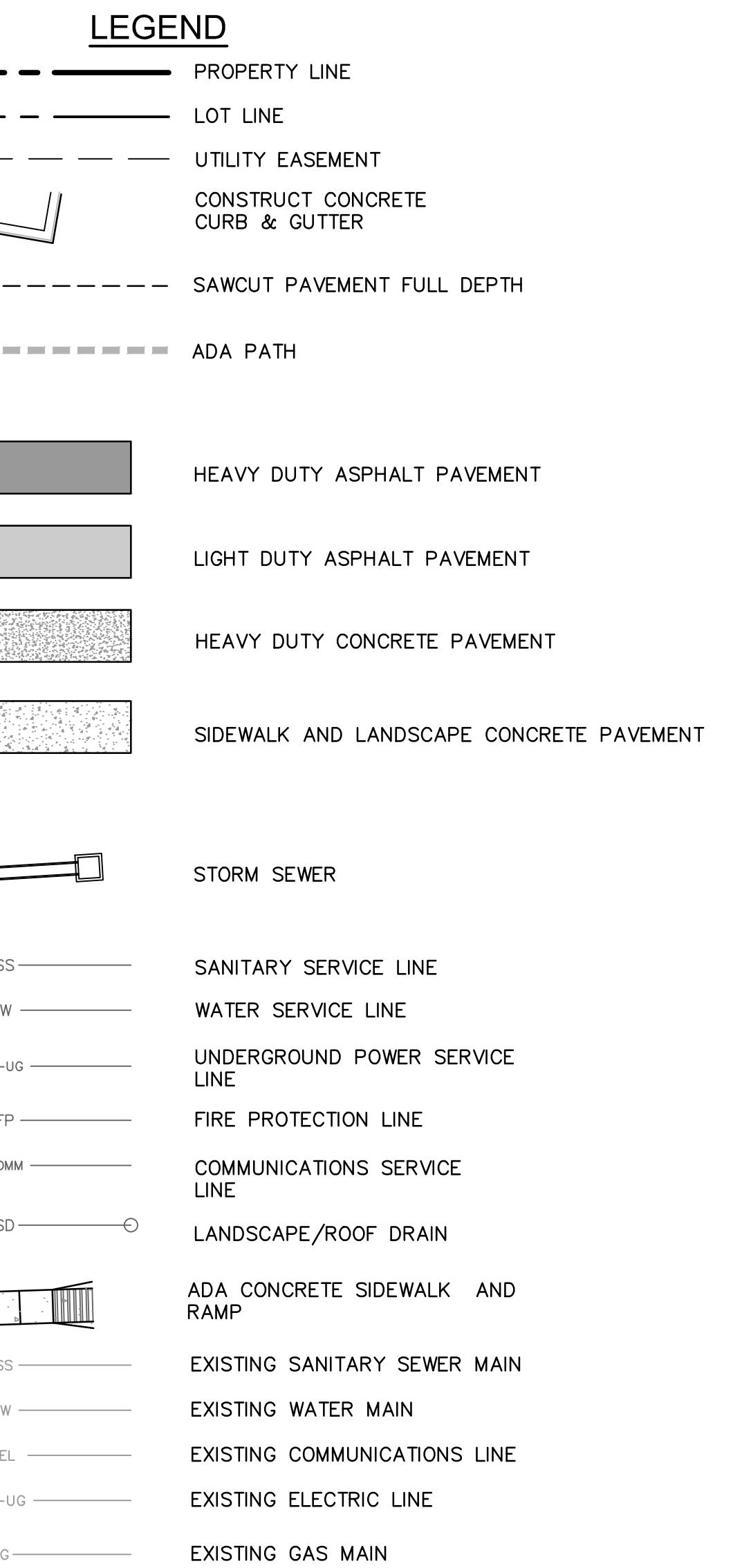
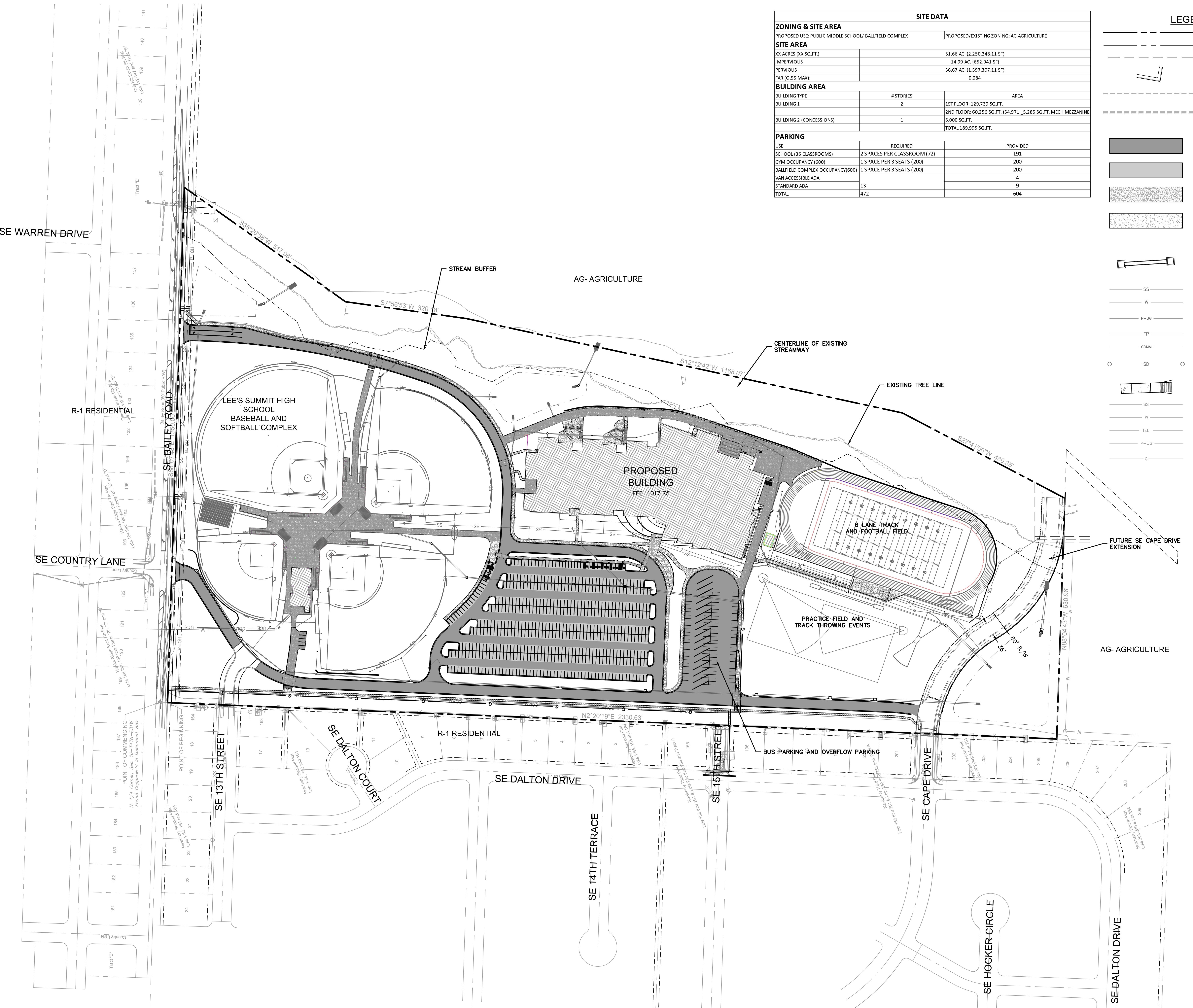
Stormwater Management Plan

# LS MIDDLE SCHOOL #4 EXISTING CONDITIONS



# LS MIDDLE SCHOOL #4 STREAM SETBACK EXHIBIT





## LEE'S SUMMIT MIDDLE SCHOOL #4

LEE'S SUMMIT R-7 SCHOOL DISTRICT  
100 SE BAILEY ROAD  
LEE'S SUMMIT, MO 64081

ISSUE FOR BID  
08/28/20  
REVISIONS

13-20102-00

GENERAL LAYOUT PLAN

C1002

N

0' 50' 100' 200'  
SCALE IN FEET

**olsson**  
NOT FOR CONSTRUCTION

© DLR Group  
© olsson group, Inc.  
All Rights Reserved  
Missouri Certificate of Authority #000089

7201 Ward 123rd Street, Suite 200  
Overland Park, KS 66213-4750 | TEL: 913.381.1170 | www.olsson.com



STORM SEWER PIPE AND STRUCTURE TABLE																																	
STRUCTURES RUNOFF CALCULATIONS PIPE DESIGN																																	
FROM	TO	DIRECT AREA (ACRES)	TOTAL AREA (ACRES)	C	Kc (K=1.25)	Tc (MIN)	FLOW TIME (MIN)	INTENSITY (IN/HR)	DESIGN Q (CFS)	DESCRIPTION	PIPE LENGTH (L.F.)	PIPE SLOPE (%)	PIPE DIA (IN)	Q FULL (CFS)	PIPE AREA (SQ.FT.)	V FULL (F/S)	DESIGN V (F/S)	Hw/D	MH TOP ELEVATION	UPSTREAM FLOWLINE	DOWNSTREAM FLOWLINE	DOWNSTREAM WATER ELEVATION	FRICITION HEAD (h f)	ENTRY LOSS COEFFICIENT (k)	ACTUAL ENTRY LOSS (k)	ENTRY LOSS (h m)	h f + h m (FT)	HW, INLET CONTROL	HW, OUTLET CONTROL	HYDRAULIC GRADE ELEV.	HYDRAULIC GRADE (MAX)	HG (Max) - HGL	Comments
A6	A5	0.35	0.30	1.00	0.50	0.85	10.32	3.61	15 in. HDPE	210.61	0.50	15	4.56	1.23	3.73	4.13	0.95	1016.21	1012.83	1011.78	1013.00	0.67	1.00	1.00	0.27	0.93	1014.02	1013.93	1.19				
A5	A4	0.15	0.45	0.56	5.0	0.85	10.32	4.99	18 in. HDPE	228.76	0.50	18	7.45	1.77	4.21	4.51	0.88	1015.02	1011.48	1010.34	1011.67	0.52	0.30	0.30	0.09	0.62	1012.80	1012.80	1.22				
A4	A3	0.39	0.30	0.38	5.0	0.85	10.32	4.99	18 in. HDPE	199.51	0.50	24	16.04	3.14	5.11	5.09	0.80	1015.30	1010.04	1009.44	1010.94	0.15	0.20	0.20	0.08	0.23	1011.63	1011.17	1011.63	1014.00	2.37		
A3	A2	0.27	0.89	0.74	0.93	6.7	0.39	9.66	7.95	24 in. HDPE	119.51	0.50	24	16.04	3.14	5.11	5.31	0.85	1017.13	1009.14	1008.54	1010.20	0.22	0.20	0.20	0.09	0.30	1010.84	1010.84	1010.84	1016.13	5.29	
A2	A1	0.05	1.16	0.69	0.66	7.1	0.38	9.52	9.53	24 in. HDPE	120.29	0.50	24	16.04	3.14	5.11	5.31	0.85	1015.66	1008.24	1008.07	1010.80	0.08	0.15	0.15	0.07	0.13	1009.96	1010.93	1010.93	1014.66	3.73	
A1		1.21	0.69	0.55	0.50	10.32	4.99	9.80	24 in. HDPE	33.37	0.50	24	16.04	3.14	5.11	5.35	0.86	1008.24	1008.07	1010.80	0.08	0.15	0.15	0.07	0.13	1009.96	1010.93						
C7	C6	0.15	0.85	1.00	5.0	10.32	4.99	15 in. HDPE	118.91	1.00	15	6.48	1.23	5.28	4.33	0.72	1016.91	1011.68	1010.49	1011.15	0.07	1.00	1.00	0.29	0.36	1012.58	1011.68	1012.58	1015.91	3.33			
C6	C5	0.10	0.85	1.00	5.0	10.32	4.99	15 in. HDPE	189.11	3.00	15	11.22	1.23	9.14	7.39	0.81	1015.56	1010.19	1004.52	1005.24	0.29	0.20	0.20	0.17	0.46	1011.20	1011.20	1011.20	1014.56	3.36			
C5	C4	0.24	0.25	0.83	1.00	5.5	0.43	10.14	2.53	15 in. HDPE	100.46	3.00	15	11.22	1.23	9.14	10.11	2.32	1016.82	1004.22	1002.41	1003.82	1.15	0.40	0.40	0.63	1.78	1007.12	1009.82	1007.12	1009.82	2.70	
C4	C3	0.52	1.29	0.55	0.69	5.9	0.10	9.97	8.84	15 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	24 in. HDPE	ADD LINE CC					
C3	C2	1.81	0.60	0.52	0.55	5.0	0.30	9.35	11.68	15 in. HDPE	128.71	1.00	24	22.68	3.14	7.22	7.26	0.95	1006.89	1002.11	1000.82	1002.45	0.35	0.30	0.30	0.25	0.59	1004.00	1003.04	1004.00	1005.89	1.89	
C2	C1	0.56	2.41	0.46	0.58	6.3	0.25	9.82	13.60	30 in. RCP	86.50	0.50	24	29.08	4.91	5.92	5.82	0.79	1005.42	1000.09	1000.29	1002.12	0.10	0.15	0.15	0.08	0.17	1002.07	1002.29	1002.07	1003.39	1.10	
C1	L1	2.97	1.33	0.44	0.55	6.5	0.16	9.72	15.88	30 in. RCP	58.52	0.50	24	29.08	4.91	5.92	6.05	0.84	1001.10	999.79	999.50	1001.10	0.09	0.30	0.30	0.17	0.26	1001.88	1004.42	1001.88	1004.42	2.54	
CC2	CC1	0.50	0.50	0.45	0.56	5.0	10.32	4.99	15 in. HDPE	176.95	1.00	15	6.48	1.23	5.28	5.13	0.85	1009.66	1007.62	1005.85	1006.78	0.36	1.00	1.00	0.41	0.77	1008.68	1007.62	1007.62	1008.16	1.13		
M4	M3	0.28	0.28	0.52	0.65	5.0	10.32	4.99	15 in. HDPE	103.39	1.00	15	6.48	1.23	5.28	4.57	0.74	1006.67	1002.57	1001.54	1002.27	0.09	1.00	1.00	0.32	0.41	1003.50	1002.69	1003.50	1005.67	2.17		
M3	M2	0.23	0.51	0.55	0.69	5.0	10.32	4.99	15 in. HDPE	134.42	1.00	15	6.48	1.23	5.28	5.35	0.92	1006.54	1001.14	999.80	1000.82	0.38	0.30	0.30	0.13	0.52	1002.29	1001.34	1002.29	1005.54	3.25		
M2	M1	0.20	0.71	0.51	0.65	6.0	10.32	4.99	15 in. HDPE	32.61	1.00	15	6.48	1.23	5.28	5.77	1.16	1006.57	999.66	999.34	1001.10	0.18	0.40	0.40	0.21	0.39	1001.11	1001.49	1001.11	1005.57	4.08		
K3	K2	0.76	2.09	0.57	0.71	5.0	0.12	10.32	15.37	24 in. HDPE	86.84	3.00	18	39.29	3.14	12.51	11.72	1.15	1007.02	1002.97	1000.36	1001.94	0.40	1.00	1.00	2.13	2.54	1005.26	1004.47	1005.26	1006.92	1.66	
K2	K1	0.18	2.27	0.59	0.74	5.1	0.08	10.27	17.20	24 in. HDPE	36.25	1.00	24	22.68	3.14	7.22	7.92	1.27	1007.02	999.86	999.50	1001.10	0.21	0.40	0.40	0.39	0.60	1002.39	1006.02	1002.39	1006.02	3.63	
L1	K1	1.33																															

**olsson**

OLSSON - CIVIL ENGINEERING

# LEE'S SUMMIT MIDDLE SCHOOL #4

## LEE'S SUMMIT R-7 SCHOOL DISTRICT

001 SE BAILEY ROAD  
EE'S SUMMIT, MO 64081

# IAL DEVELOPMENT PLAN 28/20 ISIONS REVISED PER CITY CITY OF TORONTO

3-20102-00

# RAINAGE CALCULATIONS - 10 EAR

STRUCTURES		RUNOFF CALCULATIONS										PIPE DESIGN																							
FROM	TO	DIRECT AREA (ACRES)	TOTAL AREA (ACRES)	C	KC (K=1.25)	Tc (MIN)	FLOW TIME (MIN)	INTENSITY (IN/HR)	DESIGN Q (CFS)	DESCRIPTION	PIPE LENGTH (L.F.)	PIPE SLOPE (%)	PIPE DIA (IN)	Q FULL (CFS)	PIPE AREA (SQ.FT.)	V FULL (F/S)	DESIGN V (F/S)	Hw/D	MH TOP ELEVATION	UPSTREAM FLOWLINE	DOWNSTREAM FLOWLINE	DOWNSTREAM WATER ELEVATION	FRICITION HEAD (h f)	ENTRY LOSS COEFFICIENT (k)	ACTUAL ENTRY LOSS (k)	ENTRY LOSS (h m)	h f + h m (FT)	HW, INLET CONTROL	HW, OUTLET CONTROL	PIPE CROWN	PIPE CROWN - HGL	HYDRAULIC GRADE ELEV.	HYDRAULIC GRADE (MAX)	Comments	
EDD1	A6	0.35	0.35	0.90	0.90	5.0		7.35		Area Inlet									1016.21										1014.08	0.27	1013.81	1015.21			
	A5	0.35	0.35	0.90	0.90	5.0	0.94	7.35	2.32	15 in. HDPE	210.61	0.50	15	4.58	1.23	3.73	2.76	0.78		1012.83	1011.78	1012.71	0.27	1.00	1.00	0.22	0.49	1013.81	1013.20						
	A5	0.15	0.45	0.45	0.45	5.0		7.35		Area Inlet									1015.02										1012.98	0.38	1012.60	1014.02			
	A4	0.50	0.86	0.86	5.9	0.95		7.07	3.04	18 in. HDPE	228.76	0.50	18	7.45	1.77	4.21	4.00	0.75		1015.00		1011.48	1010.34	1011.34	0.19	0.30	0.30	0.07	0.27	1012.60	1011.60				
	A4	0.39	0.30	0.30	5.0			7.35		Area Inlet									1017.13			1010.04	1009.44	1010.53	0.05	0.20	0.20	0.06	0.11	1011.46	1010.64				
	A3	0.89	0.74	0.74	6.9	0.46		6.81	4.49	24 in. HDPE	119.51	0.50	24	16.04	3.14	5.11	4.37	0.71		1017.13										1011.44	0.54	1010.59	1016.13		
	A3	0.27	0.30	0.30	5.0			7.35		Area Inlet									1015.66			1009.14	1008.54	1009.74	0.07	0.20	0.20	0.07	0.13	1010.59	1009.88				
	A2	1.16	0.69	0.69	7.3	0.44		6.69	5.36	24 in. HDPE	120.29	0.50	24	16.04	3.14	5.11	4.59	0.73		1015.66										1011.14	0.54	1010.59	1016.13		
	A2	0.05	0.55	0.55	5.0			7.35		Area Inlet									1008.24			1008.07	1010.30	0.02	0.15	0.20	0.07	0.09	1009.70	1010.15					
	A1	1.21	0.69	0.69	7.8	0.12		6.58	5.50	24 in. HDPE	33.37	0.50	24	16.04	3.14	5.11	4.62	0.73		1008.24															
EDD2	C7	0.15	0.85	0.85	5.0			7.35		Area Inlet									1016.91										1012.93	0.39	1012.54	1015.91			
	C6	0.15	0.85	0.85	5.0	0.53		7.35	0.94	15 in. HDPE	118.91	1.00	15	6.48	1.23	5.28	3.76	0.69		1011.68	1010.49	1011.00	0.03	1.00	1.00	0.22	0.24	1012.54	1011.68						
	C6	0.10	0.80	0.80	5.0			7.35		Area Inlet									1015.56										1011.44	0.35	1011.09	1014.56			
	C5	0.25	0.83	0.83	5.5	0.50		7.19	1.49	15 in. HDPE	189.11	3.00	15	11.22	1.23	9.14	6.36	0.72		1010.82		1005.07	0.10	0.20	0.20	0.13	0.23	1011.09	1010.19						
	C5	0.24	0.45	0.45	5.0			7.35		Area Inlet									1004.22	1002.41	1003.45	0.37	0.40	0.40	0.49	0.86	1005.72	1004.30							
	C4	1.29	0.55	0.55	6.0	0.11		7.05	5.00	15 in. HDPE	60.46	3.00	15	11.22	1.23	9.14	8.87	1.20		1006.89										1004.11	0.48	1003.63	1005.89	ADD LINE CC	
	C3	1.81	0.52	0.52	6.1	0.34		7.02	6.61	24 in. HDPE	128.71	1.00	24	22.68	3.14	7.22	6.25	0.76		1002.11	1000.82	1002.02	0.11	0.30	0.30	0.18	0.29	1003.63	1002.31						
	C3	0.60	0.40	0.40	5.0			7.35		Area Inlet									1004.39										1002.09	0.15	1001.94	1003.39			
	C2	2.41	0.46	0.46	6.5	0.29		6.92	7.67	24 in. HDPE	86.50	0.50	24	16.04	3.14	5.11	5.04	0.79		1000.09	1000.29	1001.76	0.10	0.15	0.20	0.08	0.18	1001.67	1001.94						
	C2	0.56	0.40	0.40	5.0			7.35		Area Inlet									1005.42										1001.79	0.34	1001.46	1004.42			
EDD3	C1	2.97	0.44	0.44	6.8	0.19		6.85	8.95	24 in. HDPE	58.52	0.50	24	16.04	3.14	5.11	5.23	0.83		999.79	999.50	1000.30	0.09	0.30	0.30	0.13	0.22	1001.46	1000.52						
	CC2	0.50	0.45	0.45	5.0			7.35		Curb Inlet									1012.74										1008.87	0.34	1008.53	1011.24			
	CC1	0.50	0.45	0.45	5.0	0.67		7.35	1.65	15 in. HDPE	176.95	1.00	15	6.48	1.23	5.28	4.42	0.73		1007.62	1005.85	1006.54	0.12	1.00	1.00	0.30	0.42	1008.53	1007.62						
	CC1	0.30	0.55	0.55	5.0			7.35		Curb Inlet									1009.66										1006.80	0.20	1006.60	1008.16			
	M4	0.28	0.52	0.52	5.0			7.35		Area Inlet									1006.67										1003.82	0.38	1003.44	1005.67			
	M3	0.28	0.52	0.52	5.0	0.44		7.35	1.07	15 in. HDPE	103.39	1.00	15	6.48	1.23	5.28	3.91	0.69		1002.57	1001.54	1002.09	0.03	1.00	1.00	0.24	0.27	1003.							

DWG: F:\2020\0001-0500\020-0103\40-Design\AutoCAD\Final Plans\Sheets\GNCV\CONSTRUCTION DOCUMENTS\C\_DRN01\_02000103.dwg  
DATE: Nov 04, 2020 1:21pm XREFS: C\_XBASF 02000103 C\_PTBLK 02000103 C\_PSURF 02000103  
USER: bkimmich T\_PBASEF 02000103 T\_PSAS 02000103 C\_PSTRM 02000103 V\_VX

## **APPENDIX B**

### **Accompanying Documents**

Soils Map

FEMA Firmette

Soil Map—Jackson County, Missouri  
(LS MIDDLE SCHOOL #4)



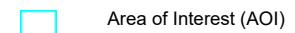
Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

5/5/2020  
Page 1 of 3

## MAP LEGEND

### Area of Interest (AOI)



Area of Interest (AOI)

### Soils



Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

### Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

### Water Features

Streams and Canals

### Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

### Background

Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri

Survey Area Data: Version 20, Sep 16, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 6, 2019—Nov 16, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	28.5	61.1%
10117	Sampsel silty clay loam, 5 to 9 percent slopes	18.1	38.9%
<b>Totals for Area of Interest</b>		<b>46.6</b>	<b>100.0%</b>

## Jackson County, Missouri

### 10117—Samsel silty clay loam, 5 to 9 percent slopes

#### Map Unit Setting

*National map unit symbol:* 2qkzz

*Elevation:* 600 to 900 feet

*Mean annual precipitation:* 33 to 41 inches

*Mean annual air temperature:* 50 to 55 degrees F

*Frost-free period:* 177 to 220 days

*Farmland classification:* Prime farmland if drained

#### Map Unit Composition

*Samsel and similar soils:* 85 percent

*Estimates are based on observations, descriptions, and transects of  
the mapunit.*

#### Description of Samsel

##### Setting

*Landform:* Hillslopes

*Landform position (two-dimensional):* Shoulder

*Landform position (three-dimensional):* Side slope

*Down-slope shape:* Concave

*Across-slope shape:* Convex, concave

*Parent material:* Residuum weathered from shale

##### Typical profile

*Ap - 0 to 13 inches:* silty clay loam

*Bt - 13 to 80 inches:* silty clay

##### Properties and qualities

*Slope:* 5 to 9 percent

*Depth to restrictive feature:* More than 80 inches

*Natural drainage class:* Somewhat poorly drained

*Runoff class:* Very high

*Capacity of the most limiting layer to transmit water (Ksat):*

Moderately low to moderately high (0.06 to 0.20 in/hr)

*Depth to water table:* About 0 to 18 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

*Available water storage in profile:* Moderate (about 8.6 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3e

*Hydrologic Soil Group:* C/D

*Ecological site:* Interbedded Sedimentary Upland Savanna  
(R109XY010MO)



*Other vegetative classification:* Grass/Prairie (Herbaceous  
Vegetation)  
*Hydric soil rating:* No

## Data Source Information

Soil Survey Area: Jackson County, Missouri  
Survey Area Data: Version 20, Sep 16, 2019



## Jackson County, Missouri

### 10082—Arisburg-Urban land complex, 1 to 5 percent slopes

#### Map Unit Setting

*National map unit symbol:* 2w7ld

*Elevation:* 750 to 1,130 feet

*Mean annual precipitation:* 39 to 45 inches

*Mean annual air temperature:* 50 to 55 degrees F

*Frost-free period:* 177 to 220 days

*Farmland classification:* All areas are prime farmland

#### Map Unit Composition

*Arisburg and similar soils:* 61 percent

*Urban land:* 30 percent

*Minor components:* 9 percent

*Estimates are based on observations, descriptions, and transects of  
the mapunit.*

#### Description of Arisburg

##### Setting

*Landform:* Interfluves

*Landform position (two-dimensional):* Summit

*Landform position (three-dimensional):* Interfluvе

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Loess

##### Typical profile

*Ap - 0 to 6 inches:* silt loam

*A - 6 to 13 inches:* silt loam

*Bt - 13 to 19 inches:* silty clay loam

*Btg - 19 to 56 inches:* silty clay loam

*BCg - 56 to 79 inches:* silty clay loam

##### Properties and qualities

*Slope:* 1 to 5 percent

*Depth to restrictive feature:* More than 80 inches

*Natural drainage class:* Somewhat poorly drained

*Capacity of the most limiting layer to transmit water (Ksat):*

Moderately high (0.20 to 0.60 in/hr)

*Depth to water table:* About 18 to 30 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

*Available water storage in profile:* High (about 11.5 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 2e



*Hydrologic Soil Group:* C  
*Ecological site:* Loess Upland Prairie (R107BY007MO)  
*Hydric soil rating:* No

### Description of Urban Land

#### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 8  
*Hydric soil rating:* No

### Minor Components

#### Sampsel

*Percent of map unit:* 3 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Concave  
*Ecological site:* Interbedded Sedimentary Upland Savanna (R109XY010MO)  
*Hydric soil rating:* Yes

#### Greenton

*Percent of map unit:* 3 percent  
*Landform:* Hillslopes  
*Landform position (two-dimensional):* Shoulder  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Ecological site:* Loess Upland Prairie (R109XY002MO)  
*Hydric soil rating:* No

#### Sharpsburg

*Percent of map unit:* 3 percent  
*Landform:* Ridges  
*Landform position (two-dimensional):* Summit  
*Landform position (three-dimensional):* Interfluve  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Ecological site:* Loess Upland Prairie (R109XY002MO)  
*Hydric soil rating:* No

## Data Source Information

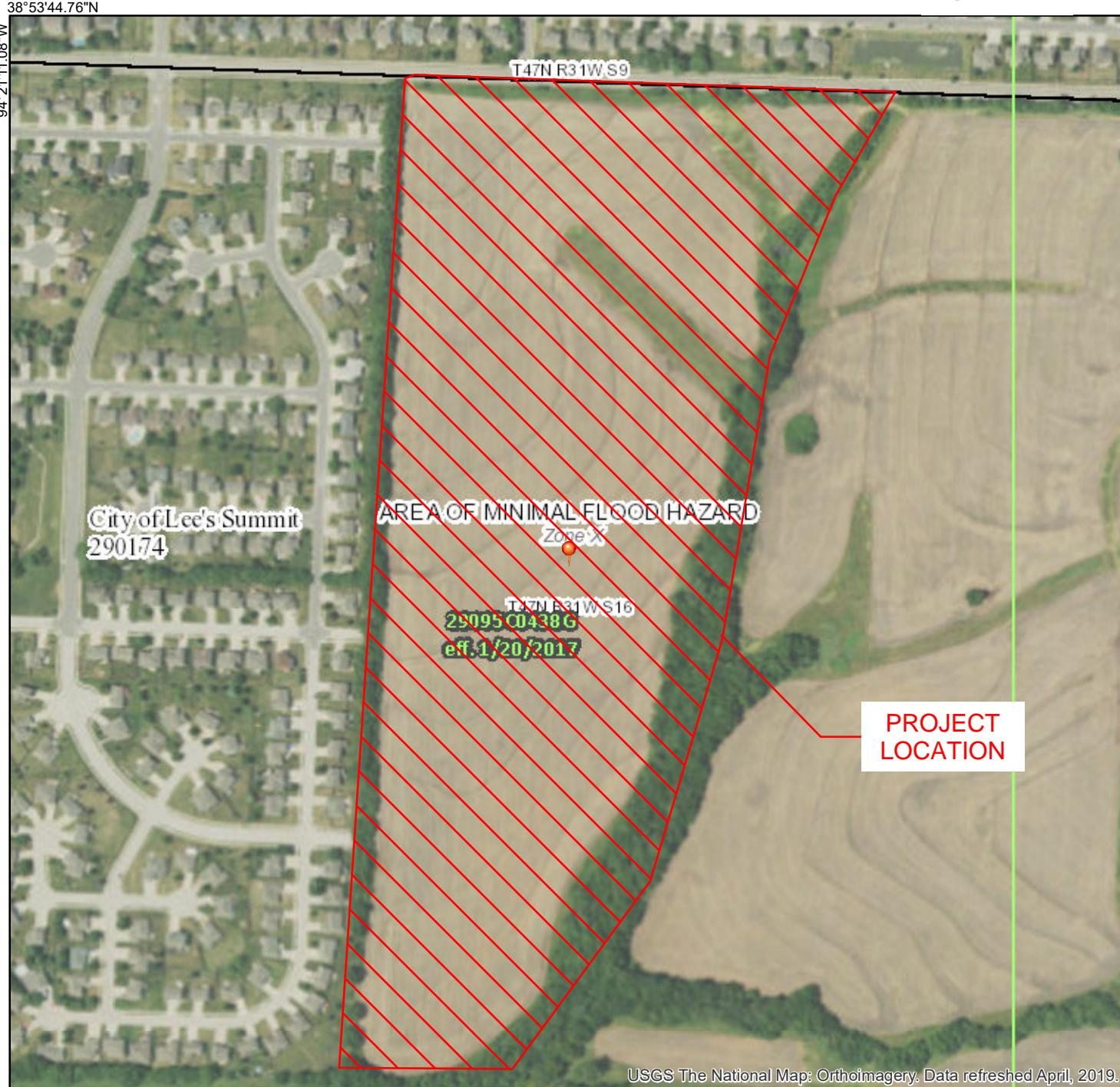
Soil Survey Area: Jackson County, Missouri  
Survey Area Data: Version 20, Sep 16, 2019



# National Flood Hazard Layer FIRMette



FEMA



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

### SPECIAL FLOOD HAZARD AREAS

- Without Base Flood Elevation (BFE)  
Zone A, V, A99
- With BFE or Depth Zone AE, AO, AH, VE, AR
- Regulatory Floodway

- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X

- Future Conditions 1% Annual Chance Flood Hazard Zone X

- Area with Reduced Flood Risk due to Levee. See Notes. Zone X

- Area with Flood Risk due to Levee Zone D

- NO SCREEN Area of Minimal Flood Hazard Zone X
- Effective LOMRs

- Area of Undetermined Flood Hazard Zone D

### OTHER AREAS

- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

- 20.2 Water Surface Elevation
- 17.5 Coastal Transect

- 513 Base Flood Elevation Line (BFE)

- Limit of Study

- Jurisdiction Boundary

- Coastal Transect Baseline

- Profile Baseline

- Hydrographic Feature

### OTHER FEATURES

- Digital Data Available
- No Digital Data Available
- Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

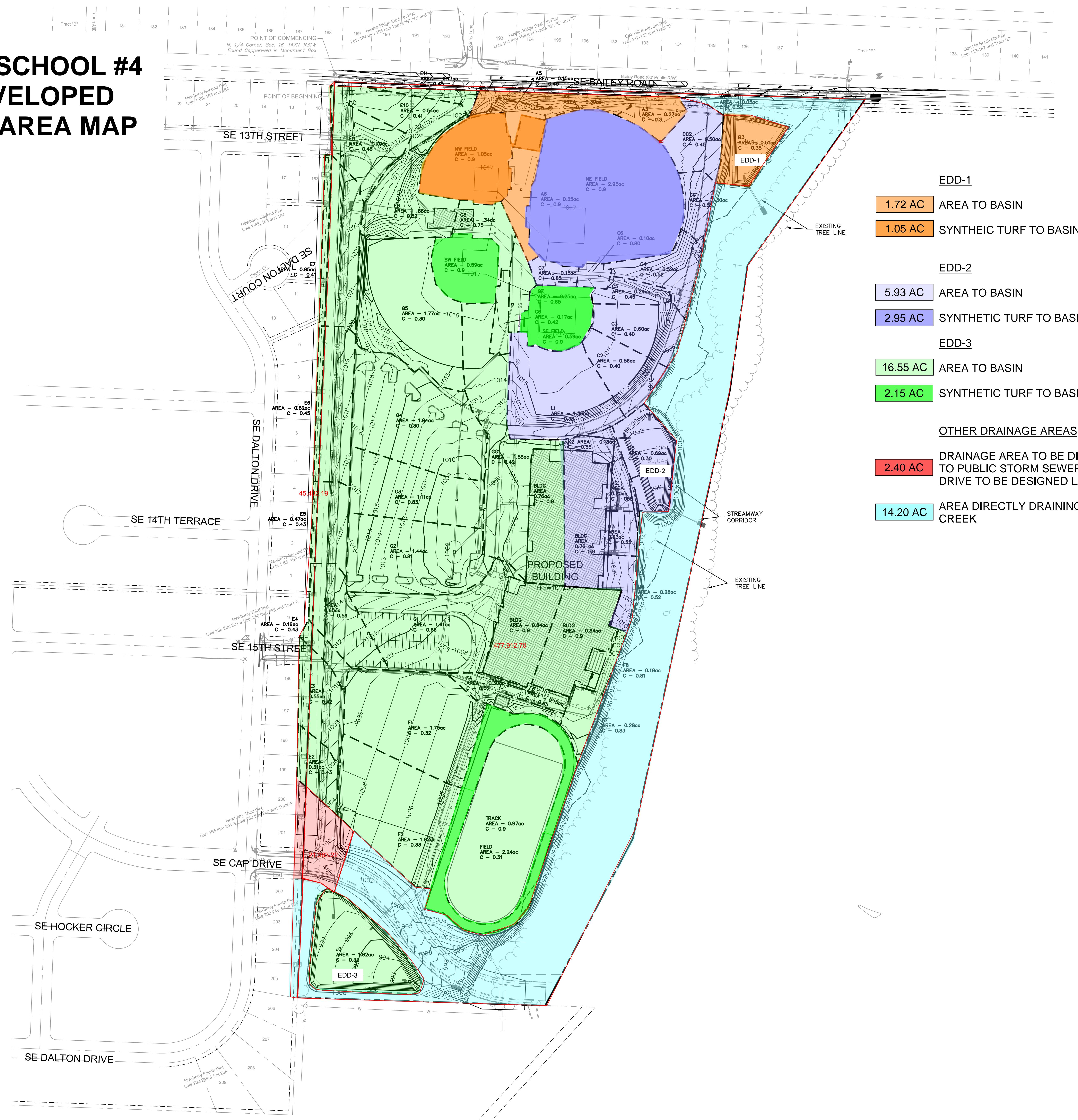
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/5/2020 at 4:01:03 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

## **APPENDIX C**

### **Detention Calculations**

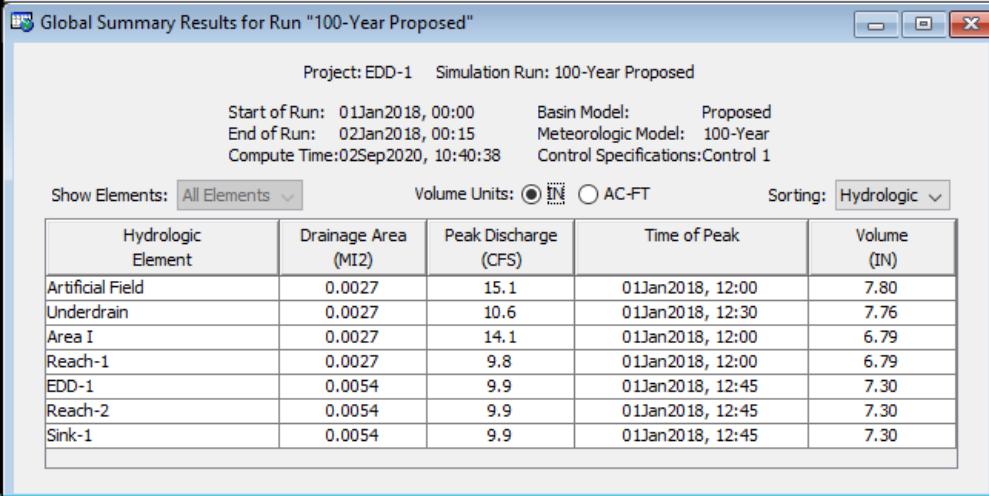
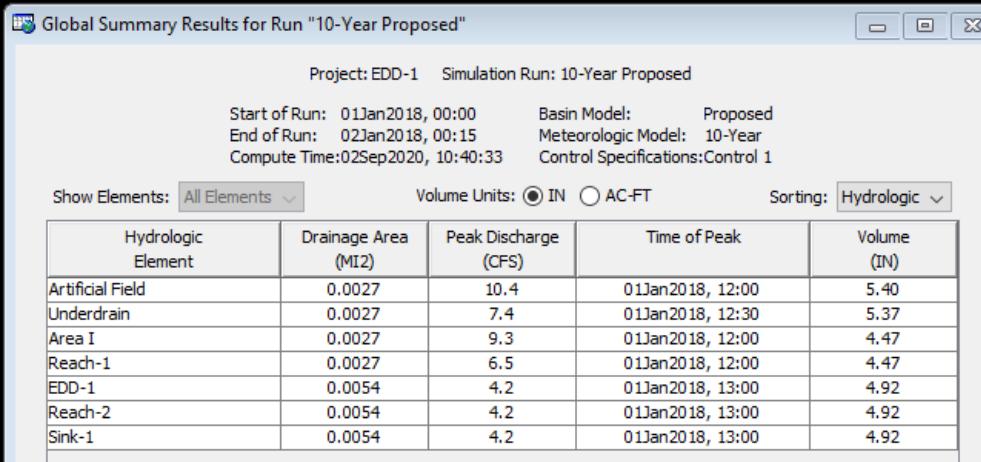
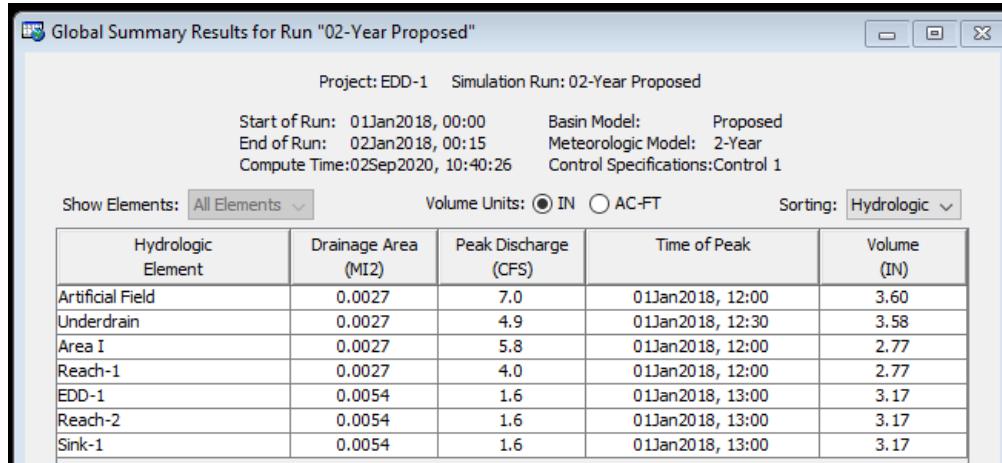
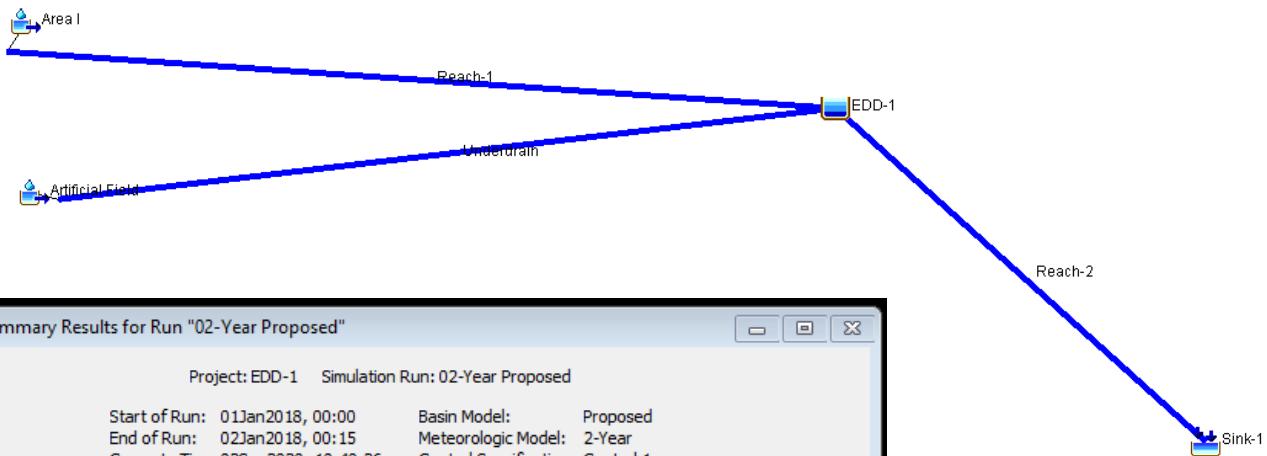
# LS MIDDLE SCHOOL #4 POST DEVELOPED DRAINAGE AREA MAP



# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 1 (EDD-1)

### HEC-HMS BASIN MODEL AND GLOBAL SUMMARIES



# LS MIDDLE SCHOOL #4

## HEC-HMS-INPUT

### EDD-1 INPUT

**Basin Name:** Proposed  
**Element Name:** EDD-1

Description:	<input type="text"/>
Downstream:	Reach-2
Method:	Outflow Structures
Storage Method:	Elevation-Area
*Elev-Area Function:	Detention 1
Initial Condition:	Inflow = Outflow
Main Tailwater:	Assume None
Auxiliary:	--None--
Time Step Method:	Automatic Adaption
Outlets:	1
Spillways:	1
Dam Tops:	0
Pumps:	0
Dam Break:	No
Dam Seepage:	No
Release:	No
Evaporation:	No

### EDD-2 INPUT

**Basin Name:** Proposed  
**Element Name:** EDD-2

Description:	<input type="text"/>
Downstream:	Reach-2
Method:	Outflow Structures
Storage Method:	Elevation-Area
*Elev-Area Function:	Detention 2
Initial Condition:	Inflow = Outflow
Main Tailwater:	Assume None
Auxiliary:	--None--
Time Step Method:	Automatic Adaption
Outlets:	1
Spillways:	1
Dam Tops:	0
Pumps:	0
Dam Break:	No
Dam Seepage:	No
Release:	No
Evaporation:	No

### EDD-3 INPUT

**Basin Name:** Proposed  
**Element Name:** EDD-3

Description:	<input type="text"/>
Downstream:	Reach-2
Method:	Outflow Structures
Storage Method:	Elevation-Area
*Elev-Area Function:	Detention 3
Initial Condition:	Inflow = Outflow
Main Tailwater:	Assume None
Auxiliary:	--None--
Time Step Method:	Automatic Adaption
Outlets:	1
Spillways:	1
Dam Tops:	0
Pumps:	0
Dam Break:	No
Dam Seepage:	No
Release:	No
Evaporation:	No

**Basin Name:** Proposed  
**Element Name:** EDD-1

Method:	Orifice Outlet
Direction:	Main
Number Barrels:	1
*Center Elevation (FT)	1008.68
*Area (FT <sup>2</sup> )	0.196
*Coefficient:	0.6

**Basin Name:** Proposed  
**Element Name:** EDD-2

Method:	Orifice Outlet
Direction:	Main
Number Barrels:	1
*Center Elevation (FT)	997.87
*Area (FT <sup>2</sup> )	0.442
*Coefficient:	0.6

**Basin Name:** Proposed  
**Element Name:** EDD-3

Method:	Orifice Outlet
Direction:	Main
Number Barrels:	1
*Center Elevation (FT)	995.13
*Area (FT <sup>2</sup> )	1.22
*Coefficient:	0.6

**Basin Name:** Proposed  
**Element Name:** EDD-1

Method:	Broad-Crested Spillway
Direction:	Main
*Elevation (FT)	1009.58
*Length (FT)	6
*Coefficient (FT <sup>0.5</sup> /S)	1.2
Gates:	0

**Basin Name:** Proposed  
**Element Name:** EDD-2

Method:	Broad-Crested Spillway
Direction:	Main
*Elevation (FT)	999.03
*Length (FT)	8
*Coefficient (FT <sup>0.5</sup> /S)	1.2
Gates:	0

**Basin Name:** Proposed  
**Element Name:** EDD-3

Method:	Broad-Crested Spillway
Direction:	Main
*Elevation (FT)	996.1
*Length (FT)	16
*Coefficient (FT <sup>0.5</sup> /S)	1.2
Gates:	0

# LS MIDDLE SCHOOL #4

## DETENTION BASIN ELEVATION AREA TABLE

### EDD-1 INPUT

Elevation (FT)	Area (AC)
1007.0	0.00
1008.0	0.04
1009.0	0.14
1010.0	0.26
1011.0	0.38
1012.0	0.41
1013.0	0.44
1014.0	0.48
1015.0	0.55

### EDD-2 INPUT

Elevation (FT)	Area (AC)
995.0	0.00
996.0	0.03
997.0	0.08
998.0	0.19
999.0	0.29
1000.0	0.36
1001.0	0.41
1002.0	0.45
1003.0	0.49
1004.0	0.54
1005.0	0.62

### EDD-3 INPUT

Components Compute Results		
Components	Compute	Results
Elevation (FT)	Area (AC)	
889.0	0.00	
990.0	0.04	
991.0	0.28	
992.0	0.65	
993.0	0.76	
994.0	0.82	
995.0	0.88	
996.0	0.93	
997.0	0.99	
998.0	1.06	
999.0	1.12	
1000.0	1.23	
1001.0	1.27	
1002.0	1.33	

# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 1 (EDD-1)

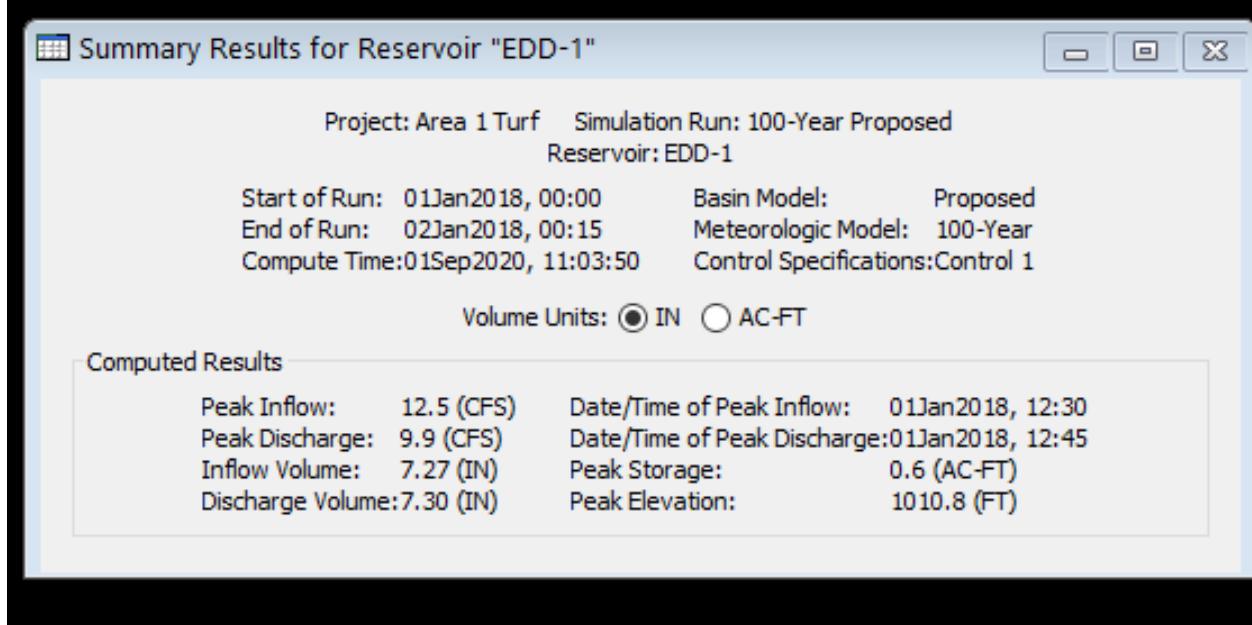
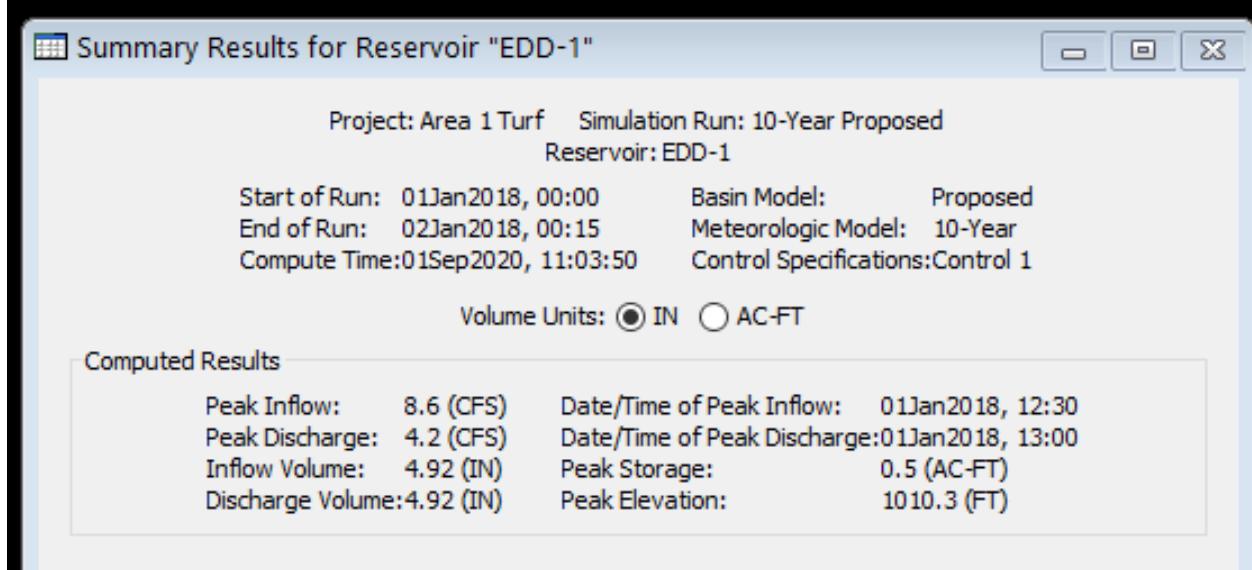
### SUBBASIN SUMMARIES

Subbasin	Project	Simulation Run	Basin Model	Meteorologic Model	Compute Time	Volume Units	Peak Discharge	Precipitation Volume	Loss Volume	Baseflow Volume	Excess Volume	Date/Time of Peak Discharge	Direct Runoff Volume	Baseflow Volume	Discharge Volume
Area I	EDD-1	02-Year Proposed	Proposed	2-Year	02Sep2020, 10:40:26	IN	5.8 (CFS)	3.60 (IN)	0.83 (IN)	0.00 (IN)	2.77 (IN)	01Jan2018, 12:00	2.77 (IN)	0.00 (IN)	2.77 (IN)
Artificial Field	EDD-1	02-Year Proposed	Proposed	2-Year	02Sep2020, 10:40:26	IN	7.0 (CFS)	3.60 (IN)	0.00 (IN)	0.00 (IN)	3.60 (IN)	01Jan2018, 12:00	3.60 (IN)	0.00 (IN)	3.60 (IN)
Area I	EDD-1	10-Year Proposed	Proposed	10-Year	02Sep2020, 10:40:33	IN	9.3 (CFS)	5.40 (IN)	0.93 (IN)	0.00 (IN)	4.47 (IN)	01Jan2018, 12:00	4.47 (IN)	0.00 (IN)	4.47 (IN)
Artificial Field	EDD-1	10-Year Proposed	Proposed	10-Year	02Sep2020, 10:40:33	IN	10.4 (CFS)	5.40 (IN)	0.00 (IN)	0.00 (IN)	5.40 (IN)	01Jan2018, 12:00	5.40 (IN)	0.00 (IN)	5.40 (IN)
Area I	EDD-1	100-Year Proposed	Proposed	100-Year	02Sep2020, 10:40:38	IN	14.1 (CFS)	7.80 (IN)	1.01 (IN)	0.00 (IN)	6.79 (IN)	01Jan2018, 12:00	6.79 (IN)	0.00 (IN)	6.79 (IN)
Artificial Field	EDD-1	100-Year Proposed	Proposed	100-Year	02Sep2020, 10:40:38	IN	15.1 (CFS)	7.80 (IN)	0.00 (IN)	0.00 (IN)	7.80 (IN)	01Jan2018, 12:00	7.80 (IN)	0.00 (IN)	7.80 (IN)

# LS MIDDLE SCHOOL #4

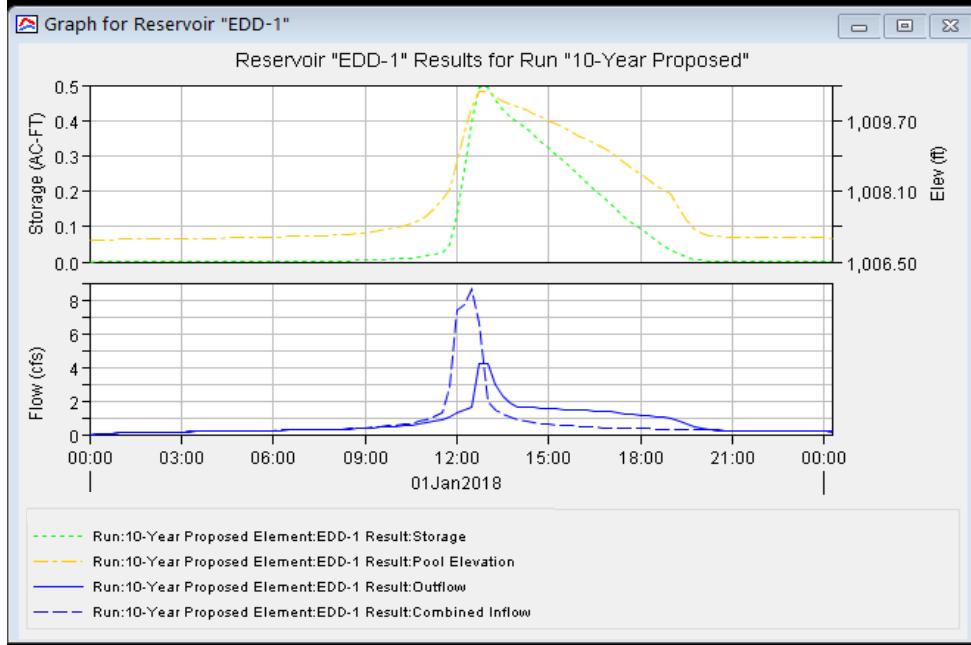
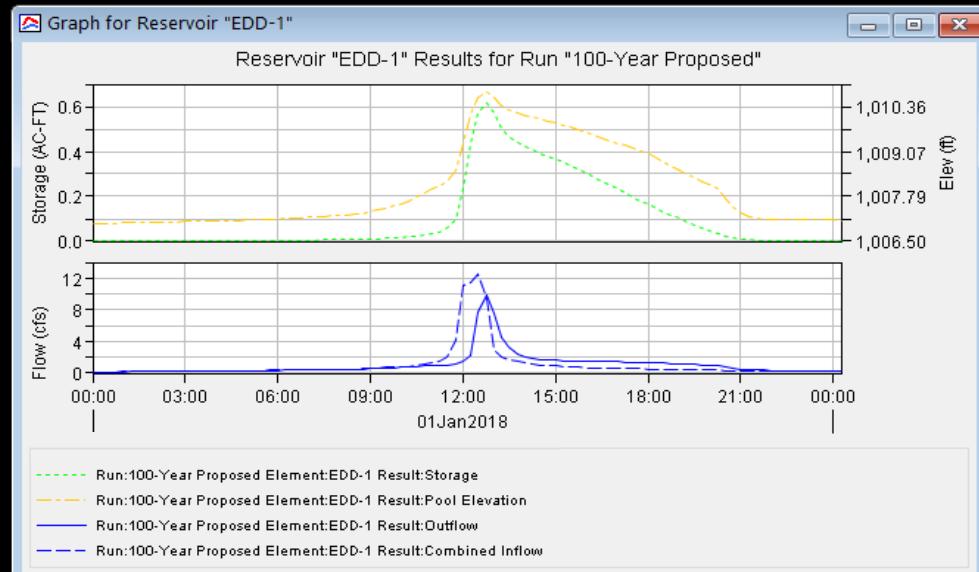
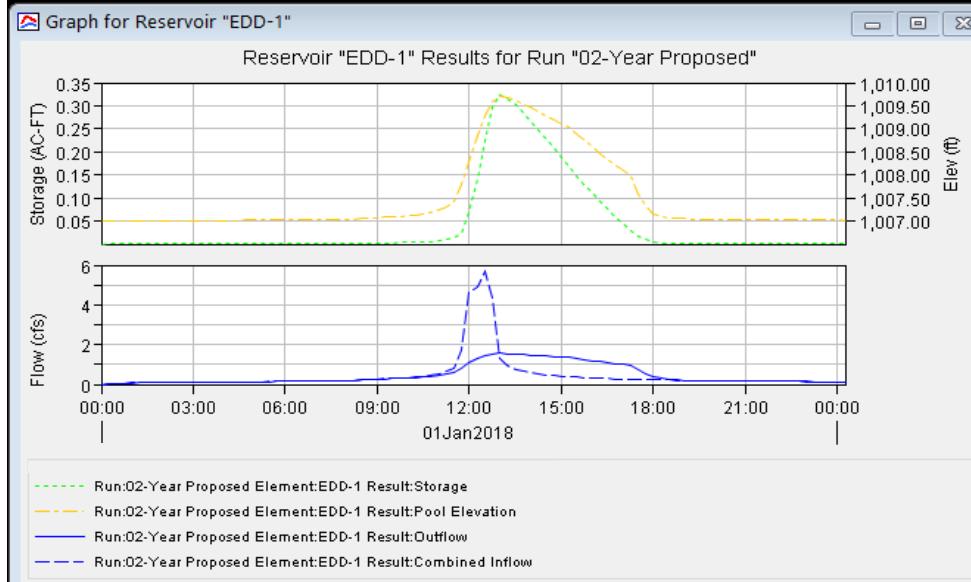
## EXTENDED DRY DETENTION BASIN 1 (EDD-1)

### DETENTION FLOWS



# LS MIDDLE SCHOOL #4

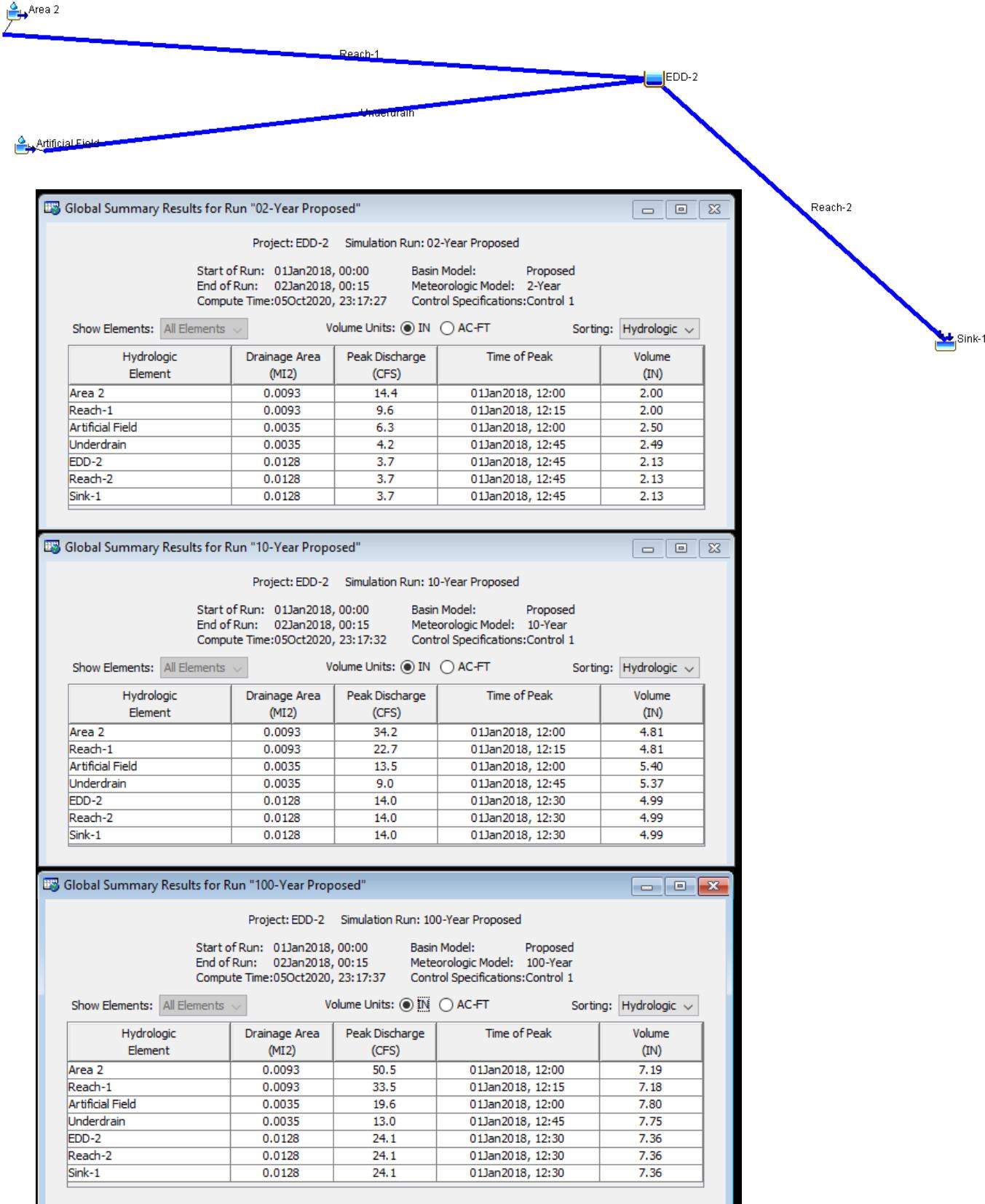
## EXTENDED DRY DETENTION BASIN 1 (EDD-1) - HYDROGRAPHS



# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 2 (EDD-2)

### HEC-HMS BASIN MODEL AND GLOBAL SUMMARIES



# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 2 (EDD-2)

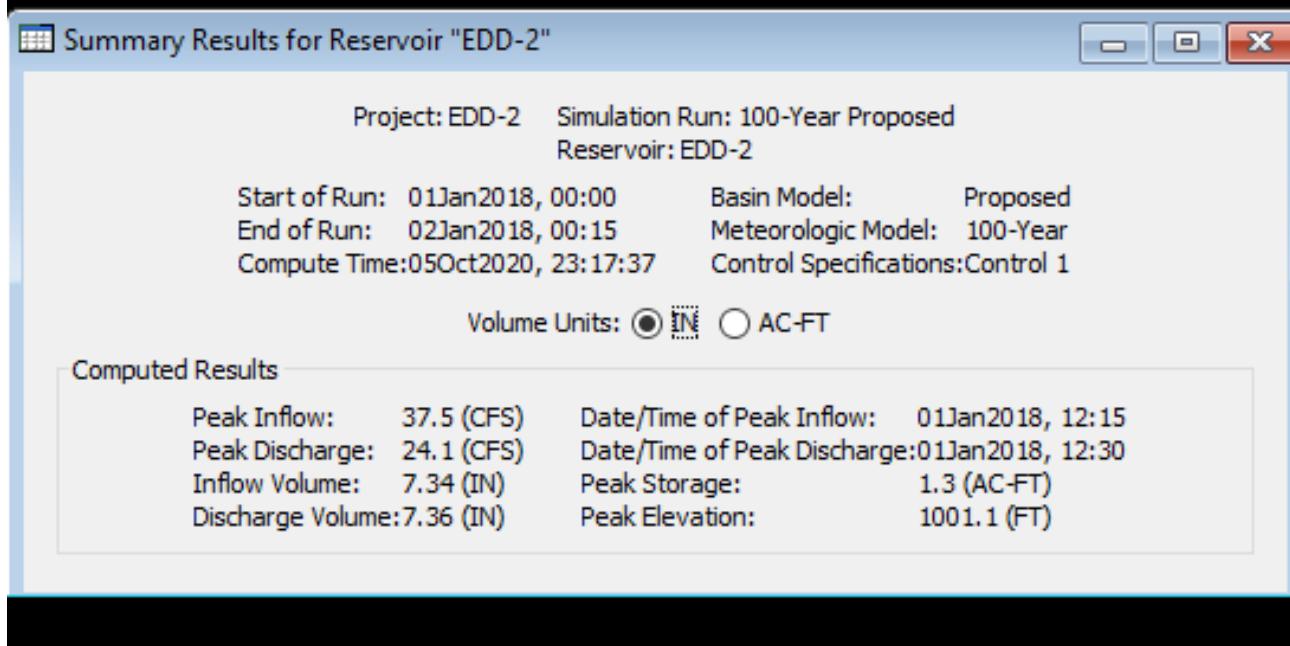
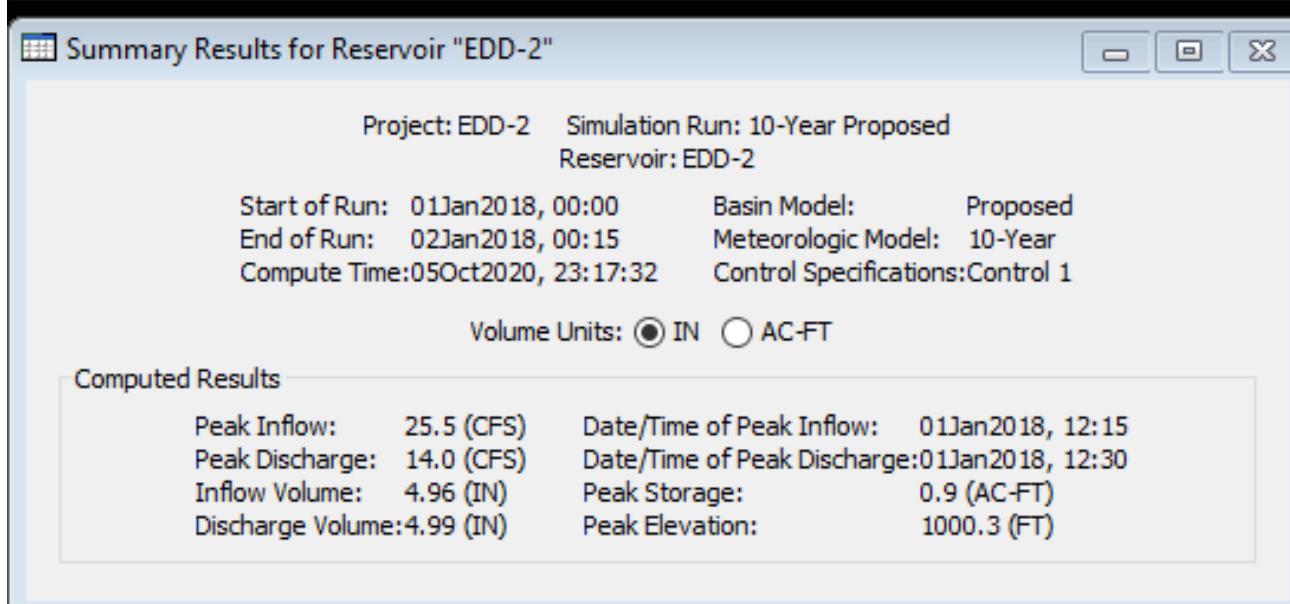
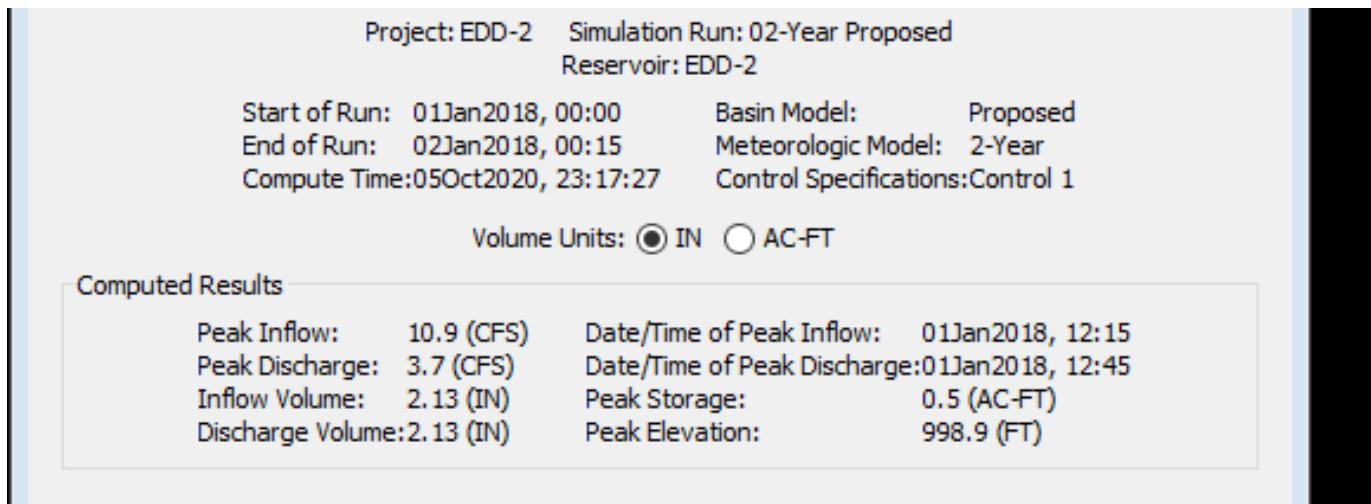
### SUBBASIN SUMMARIES

Subbasin	Project: EDD-2 Simulation Run: 02-Year Proposed	Project: EDD-2 Simulation Run: 10-Year Proposed	Project: EDD-2 Simulation Run: 100-Year Proposed																								
"Area 2"	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:27</p> <p>Basin Model: Proposed Meteorologic Model: 2-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 14.4 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 2.50 (IN)</td><td>Direct Runoff Volume: 2.00 (IN)</td></tr><tr><td>Loss Volume: 0.50 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 2.00 (IN)</td><td>Discharge Volume: 2.00 (IN)</td></tr></table>	Peak Discharge: 14.4 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.00 (IN)	Loss Volume: 0.50 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 2.00 (IN)	Discharge Volume: 2.00 (IN)	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:32</p> <p>Basin Model: Proposed Meteorologic Model: 10-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 6.3 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 2.50 (IN)</td><td>Direct Runoff Volume: 2.50 (IN)</td></tr><tr><td>Loss Volume: 0.00 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 2.50 (IN)</td><td>Discharge Volume: 2.50 (IN)</td></tr></table>	Peak Discharge: 6.3 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.50 (IN)	Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 2.50 (IN)	Discharge Volume: 2.50 (IN)	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:37</p> <p>Basin Model: Proposed Meteorologic Model: 100-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 34.2 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 5.40 (IN)</td><td>Direct Runoff Volume: 4.81 (IN)</td></tr><tr><td>Loss Volume: 0.59 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 4.81 (IN)</td><td>Discharge Volume: 4.81 (IN)</td></tr></table>	Peak Discharge: 34.2 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 5.40 (IN)	Direct Runoff Volume: 4.81 (IN)	Loss Volume: 0.59 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 4.81 (IN)	Discharge Volume: 4.81 (IN)
Peak Discharge: 14.4 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.00 (IN)																										
Loss Volume: 0.50 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 2.00 (IN)	Discharge Volume: 2.00 (IN)																										
Peak Discharge: 6.3 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.50 (IN)																										
Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 2.50 (IN)	Discharge Volume: 2.50 (IN)																										
Peak Discharge: 34.2 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 5.40 (IN)	Direct Runoff Volume: 4.81 (IN)																										
Loss Volume: 0.59 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 4.81 (IN)	Discharge Volume: 4.81 (IN)																										
"Artificial Field"	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:27</p> <p>Basin Model: Proposed Meteorologic Model: 2-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 6.3 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 2.50 (IN)</td><td>Direct Runoff Volume: 2.50 (IN)</td></tr><tr><td>Loss Volume: 0.00 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 2.50 (IN)</td><td>Discharge Volume: 2.50 (IN)</td></tr></table>	Peak Discharge: 6.3 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.50 (IN)	Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 2.50 (IN)	Discharge Volume: 2.50 (IN)	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:32</p> <p>Basin Model: Proposed Meteorologic Model: 10-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 13.5 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 5.40 (IN)</td><td>Direct Runoff Volume: 5.40 (IN)</td></tr><tr><td>Loss Volume: 0.00 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 5.40 (IN)</td><td>Discharge Volume: 5.40 (IN)</td></tr></table>	Peak Discharge: 13.5 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 5.40 (IN)	Direct Runoff Volume: 5.40 (IN)	Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 5.40 (IN)	Discharge Volume: 5.40 (IN)	<p>Start of Run: 01Jan2018, 00:00 End of Run: 02Jan2018, 00:15 Compute Time: 05Oct2020, 23:17:37</p> <p>Basin Model: Proposed Meteorologic Model: 100-Year Control Specifications: Control 1</p> <p>Volume Units: <input checked="" type="radio"/> IN <input type="radio"/> AC-FT</p> <p><b>Computed Results</b></p> <table><tr><td>Peak Discharge: 19.6 (CFS)</td><td>Date/Time of Peak Discharge: 01Jan2018, 12:00</td></tr><tr><td>Precipitation Volume: 7.80 (IN)</td><td>Direct Runoff Volume: 7.80 (IN)</td></tr><tr><td>Loss Volume: 0.00 (IN)</td><td>Baseflow Volume: 0.00 (IN)</td></tr><tr><td>Excess Volume: 7.80 (IN)</td><td>Discharge Volume: 7.80 (IN)</td></tr></table>	Peak Discharge: 19.6 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00	Precipitation Volume: 7.80 (IN)	Direct Runoff Volume: 7.80 (IN)	Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)	Excess Volume: 7.80 (IN)	Discharge Volume: 7.80 (IN)
Peak Discharge: 6.3 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 2.50 (IN)	Direct Runoff Volume: 2.50 (IN)																										
Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 2.50 (IN)	Discharge Volume: 2.50 (IN)																										
Peak Discharge: 13.5 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 5.40 (IN)	Direct Runoff Volume: 5.40 (IN)																										
Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 5.40 (IN)	Discharge Volume: 5.40 (IN)																										
Peak Discharge: 19.6 (CFS)	Date/Time of Peak Discharge: 01Jan2018, 12:00																										
Precipitation Volume: 7.80 (IN)	Direct Runoff Volume: 7.80 (IN)																										
Loss Volume: 0.00 (IN)	Baseflow Volume: 0.00 (IN)																										
Excess Volume: 7.80 (IN)	Discharge Volume: 7.80 (IN)																										

# LS MIDDLE SCHOOL #4

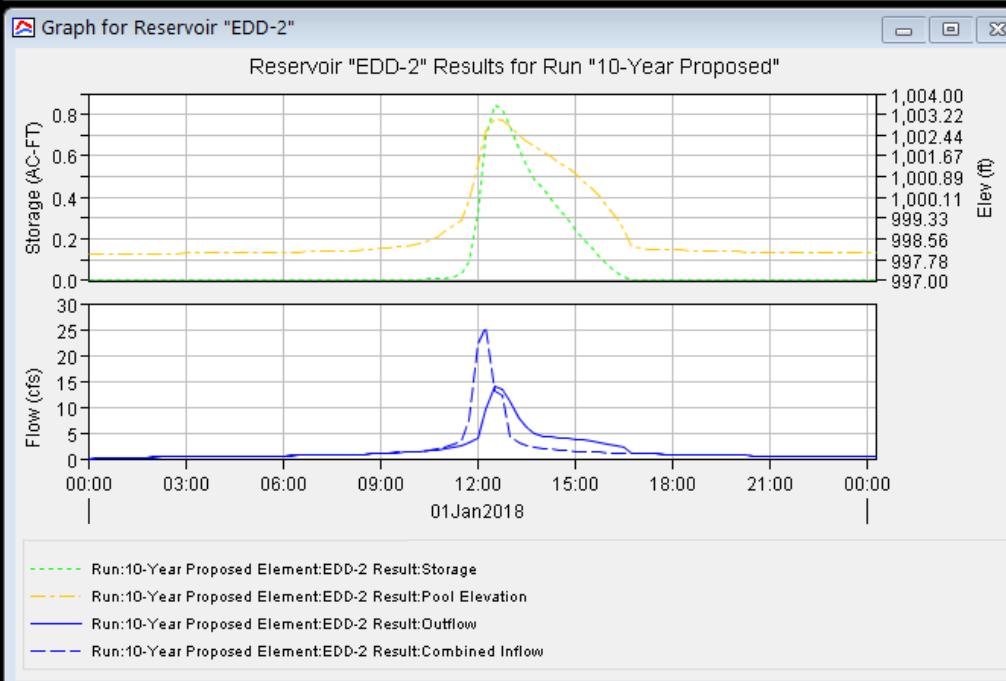
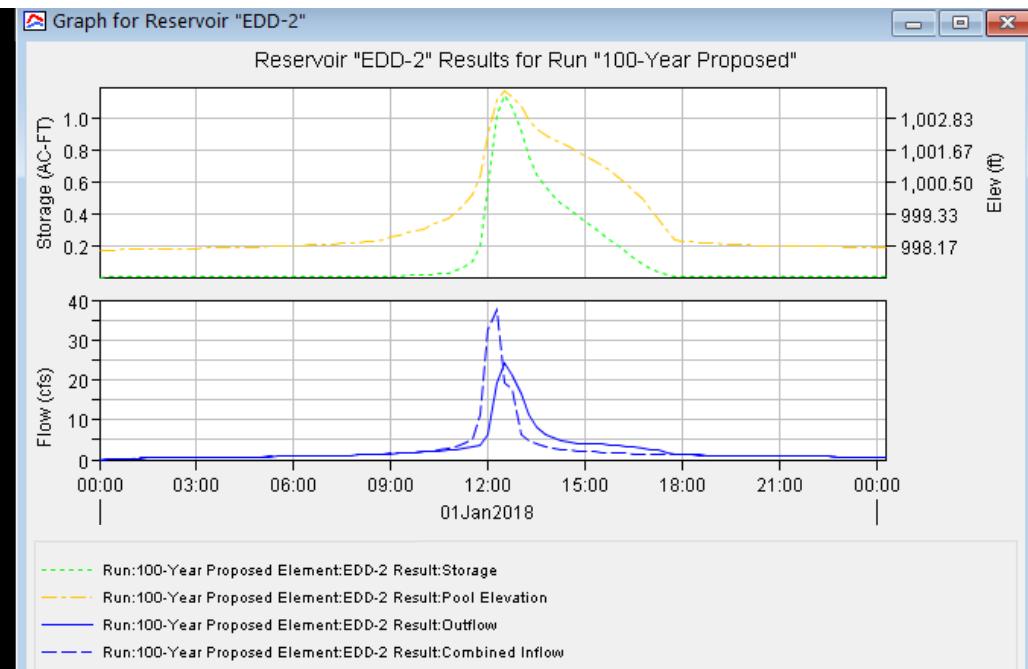
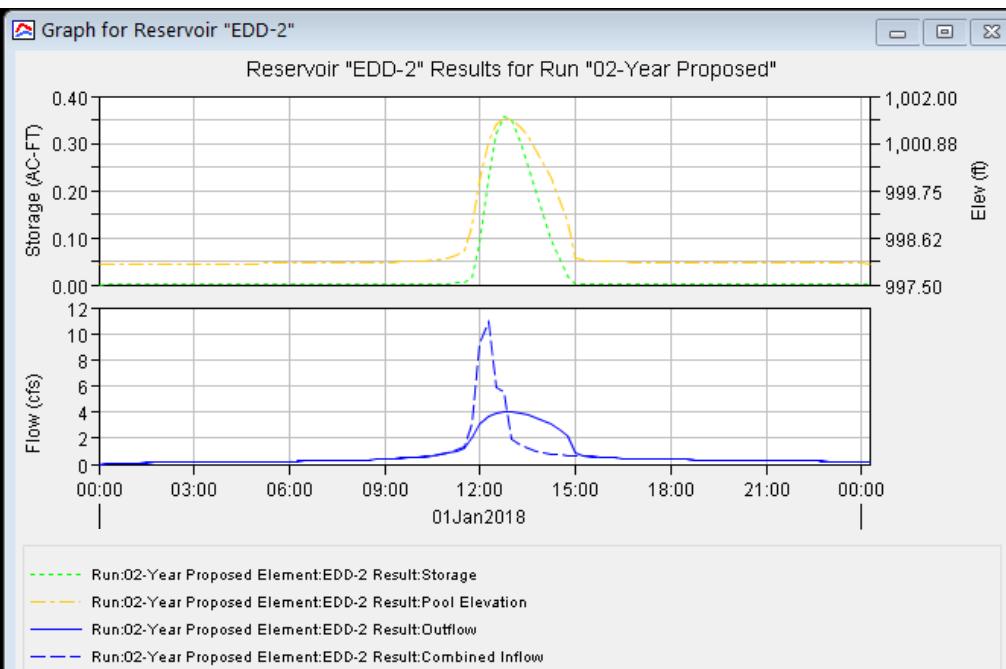
## EXTENDED DRY DETENTION BASIN 2 (EDD-2)

### DETENTION FLOWS



# LS MIDDLE SCHOOL #4

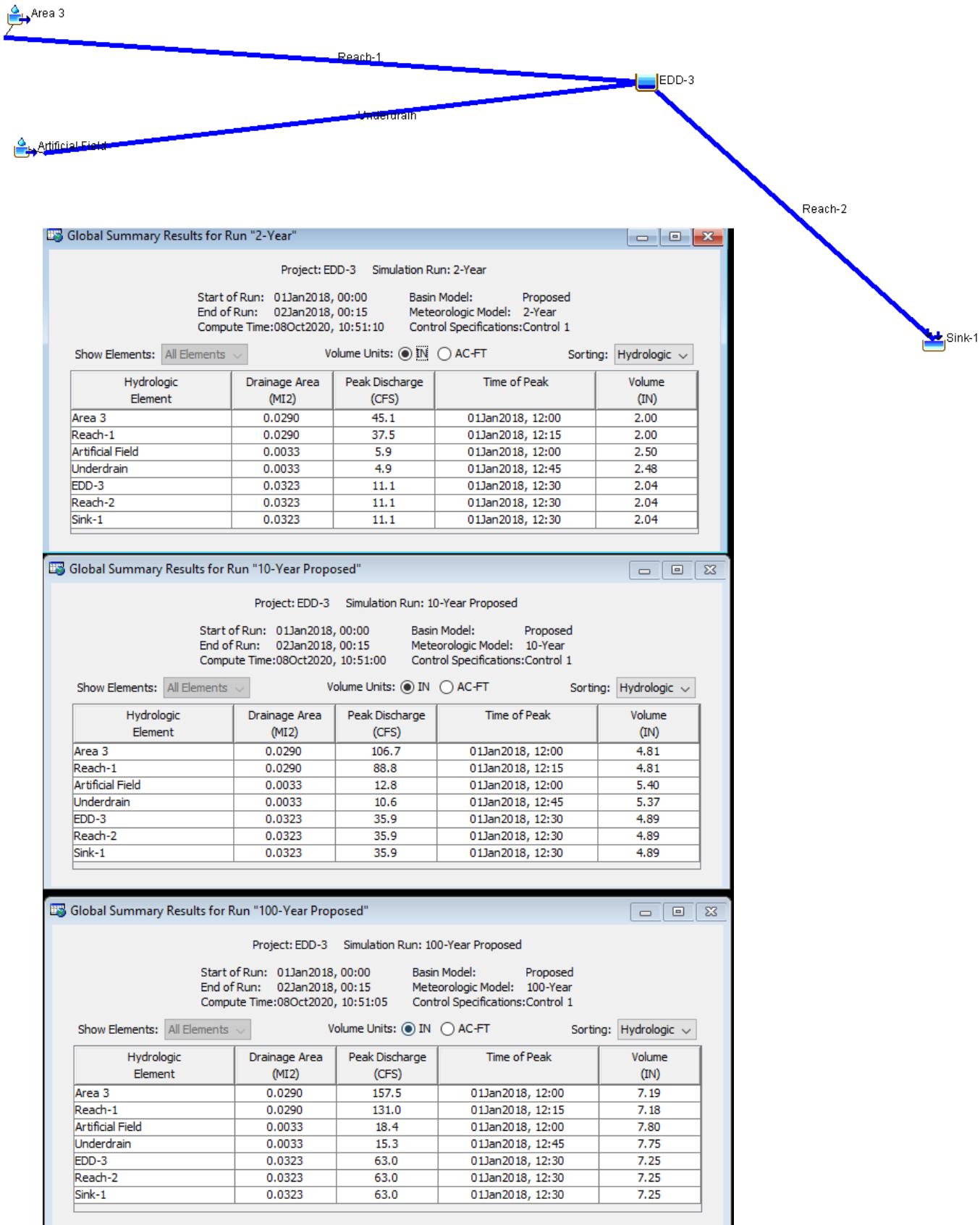
## EXTENDED DRY DETENTION BASIN 2 (EDD-2) - HYDROGRAPHS



# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 3 (EDD-3)

### HEC-HMS BASIN MODEL AND GLOBAL SUMMARIES



# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 3 (EDD-3)

### SUBBASIN SUMMARIES

Subbasin	Project	Simulation Run	Basin Model	Meteorologic Model	Control Specifications	Volume Units	Peak Discharge (CFS)	Precipitation Volume (IN)	Loss Volume (IN)	Excess Volume (IN)	Date/Time of Peak Discharge	Direct Runoff Volume (IN)	Baseflow Volume (IN)	Discharge Volume (IN)
Area 3	EDD-3	2-Year	Proposed	2-Year	Control 1	IN	45.1	2.50	0.50	2.00	01Jan2018, 12:00	2.00	0.00	2.00
Artificial Field	EDD-3	2-Year	Proposed	2-Year	Control 1	IN	5.9	2.50	0.00	2.50	01Jan2018, 12:00	2.50	0.00	2.50
Area 3	EDD-3	10-Year	Proposed	10-Year	Control 1	IN	106.7	5.40	0.59	4.81	01Jan2018, 12:00	4.81	0.00	4.81
Artificial Field	EDD-3	10-Year	Proposed	10-Year	Control 1	IN	12.8	5.40	0.00	5.40	01Jan2018, 12:00	5.40	0.00	5.40
Area 3	EDD-3	100-Year	Proposed	100-Year	Control 1	IN	157.5	7.80	0.61	7.19	01Jan2018, 12:00	7.19	0.00	7.19
Artificial Field	EDD-3	100-Year	Proposed	100-Year	Control 1	IN	18.4	7.80	0.00	7.80	01Jan2018, 12:00	7.80	0.00	7.80

# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 3 (EDD-3)

### DETENTION FLOWS

Summary Results for Reservoir "EDD-3"

Project: EDD-3 Simulation Run: 2-Year  
Reservoir: EDD-3

Start of Run: 01Jan2018, 00:00 Basin Model: Proposed  
End of Run: 02Jan2018, 00:15 Meteorologic Model: 2-Year  
Compute Time: 05Oct2020, 22:57:30 Control Specifications: Control 1

Volume Units:  IN  AC-FT

Computed Results

Peak Inflow:	38.4 (CFS)	Date/Time of Peak Inflow:	01Jan2018, 12:15
Peak Discharge:	11.1 (CFS)	Date/Time of Peak Discharge:	01Jan2018, 12:30
Inflow Volume:	2.05 (IN)	Peak Storage:	2.1 (AC-FT)
Discharge Volume:	2.04 (IN)	Peak Elevation:	995.7 (FT)

Summary Results for Reservoir "EDD-3"

Project: EDD-3 Simulation Run: 10-Year Proposed  
Reservoir: EDD-3

Start of Run: 01Jan2018, 00:00 Basin Model: Proposed  
End of Run: 02Jan2018, 00:15 Meteorologic Model: 10-Year  
Compute Time: 05Oct2020, 22:57:20 Control Specifications: Control 1

Volume Units:  IN  AC-FT

Computed Results

Peak Inflow:	90.7 (CFS)	Date/Time of Peak Inflow:	01Jan2018, 12:15
Peak Discharge:	35.9 (CFS)	Date/Time of Peak Discharge:	01Jan2018, 12:30
Inflow Volume:	4.87 (IN)	Peak Storage:	3.7 (AC-FT)
Discharge Volume:	4.89 (IN)	Peak Elevation:	997.4 (FT)

Summary Results for Reservoir "EDD-3"

Project: EDD-3 Simulation Run: 100-Year Proposed  
Reservoir: EDD-3

Start of Run: 01Jan2018, 00:00 Basin Model: Proposed  
End of Run: 02Jan2018, 00:15 Meteorologic Model: 100-Year  
Compute Time: 05Oct2020, 22:57:25 Control Specifications: Control 1

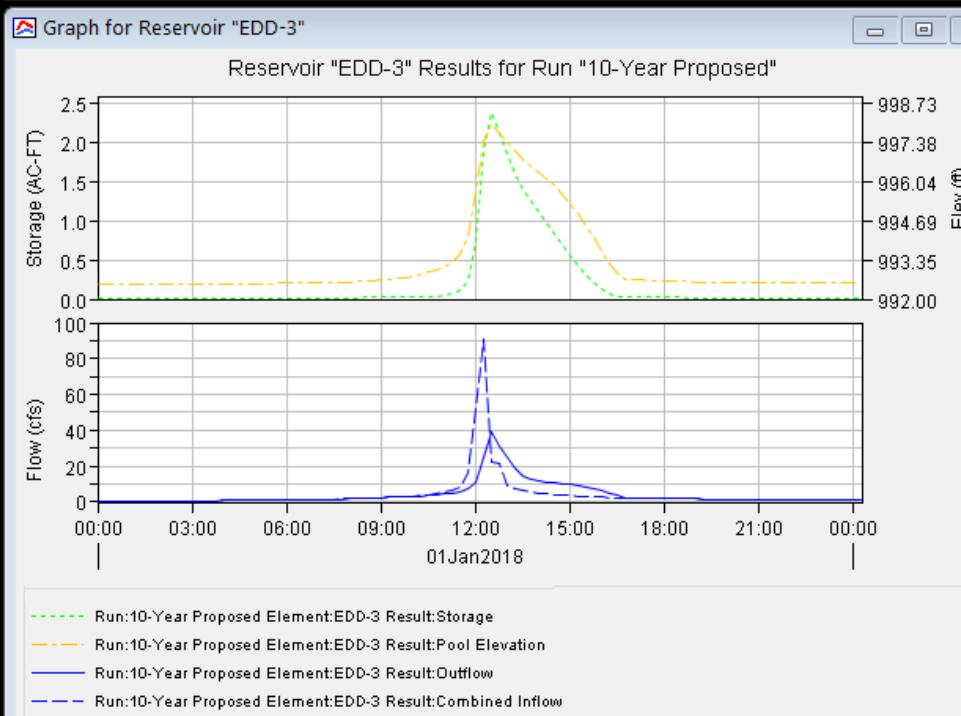
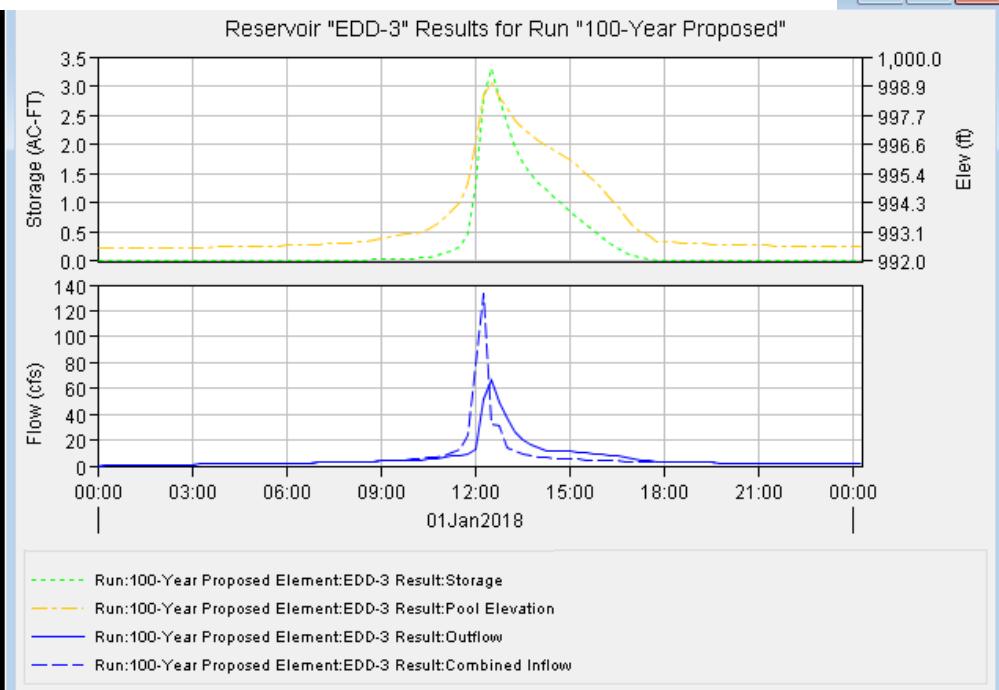
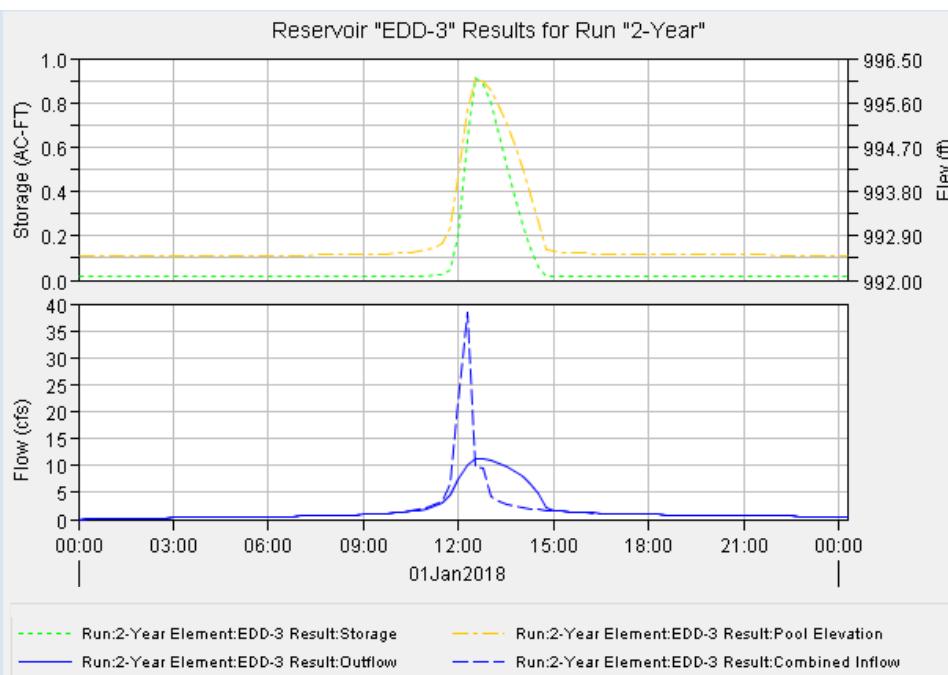
Volume Units:  IN  AC-FT

Computed Results

Peak Inflow:	133.8 (CFS)	Date/Time of Peak Inflow:	01Jan2018, 12:15
Peak Discharge:	63.0 (CFS)	Date/Time of Peak Discharge:	01Jan2018, 12:30
Inflow Volume:	7.24 (IN)	Peak Storage:	4.7 (AC-FT)
Discharge Volume:	7.25 (IN)	Peak Elevation:	998.4 (FT)

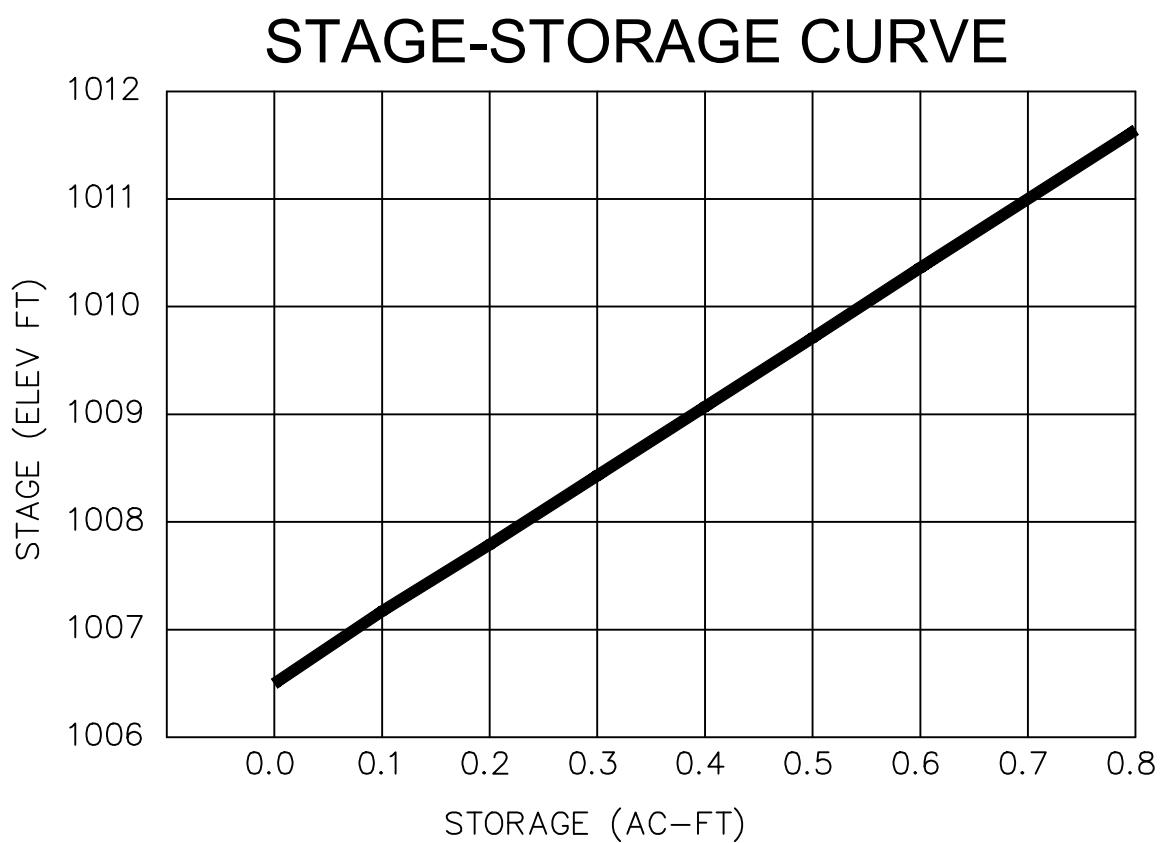
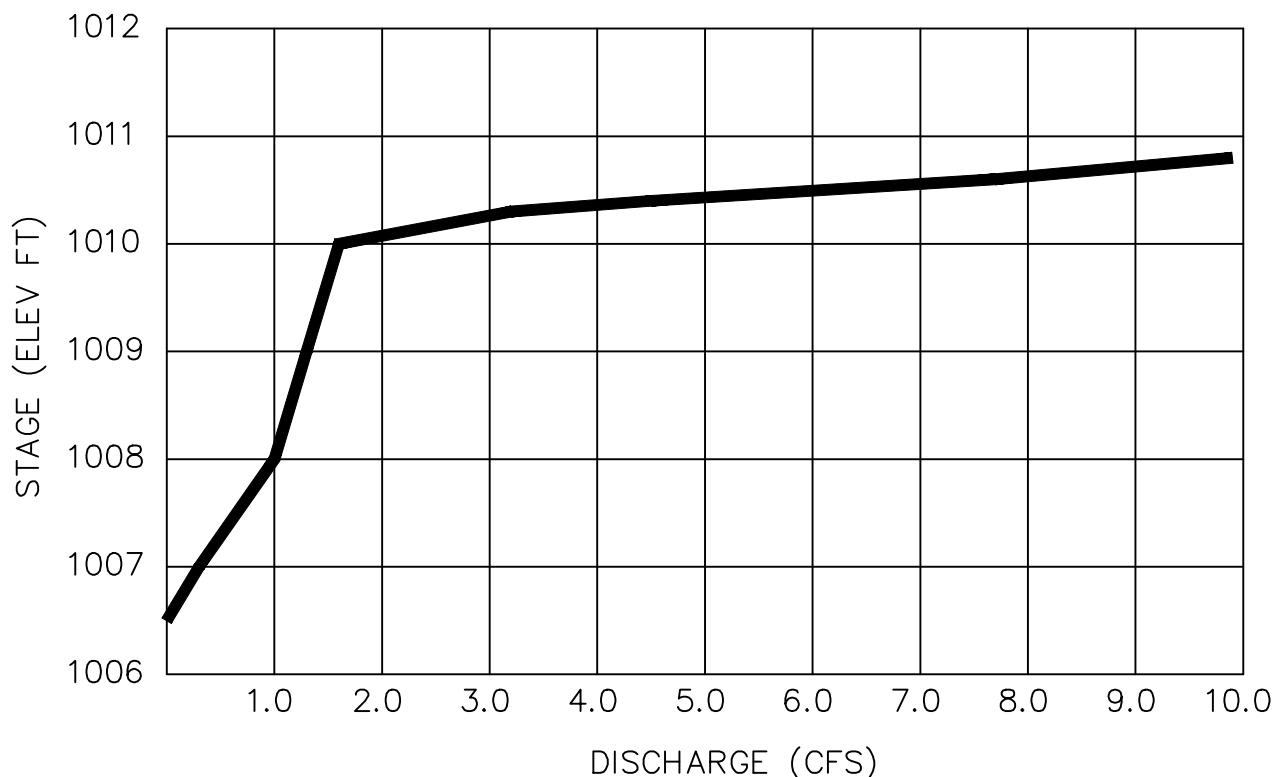
# LS MIDDLE SCHOOL #4

## EXTENDED DRY DETENTION BASIN 3 (EDD-3) - HYDROGRAPHS

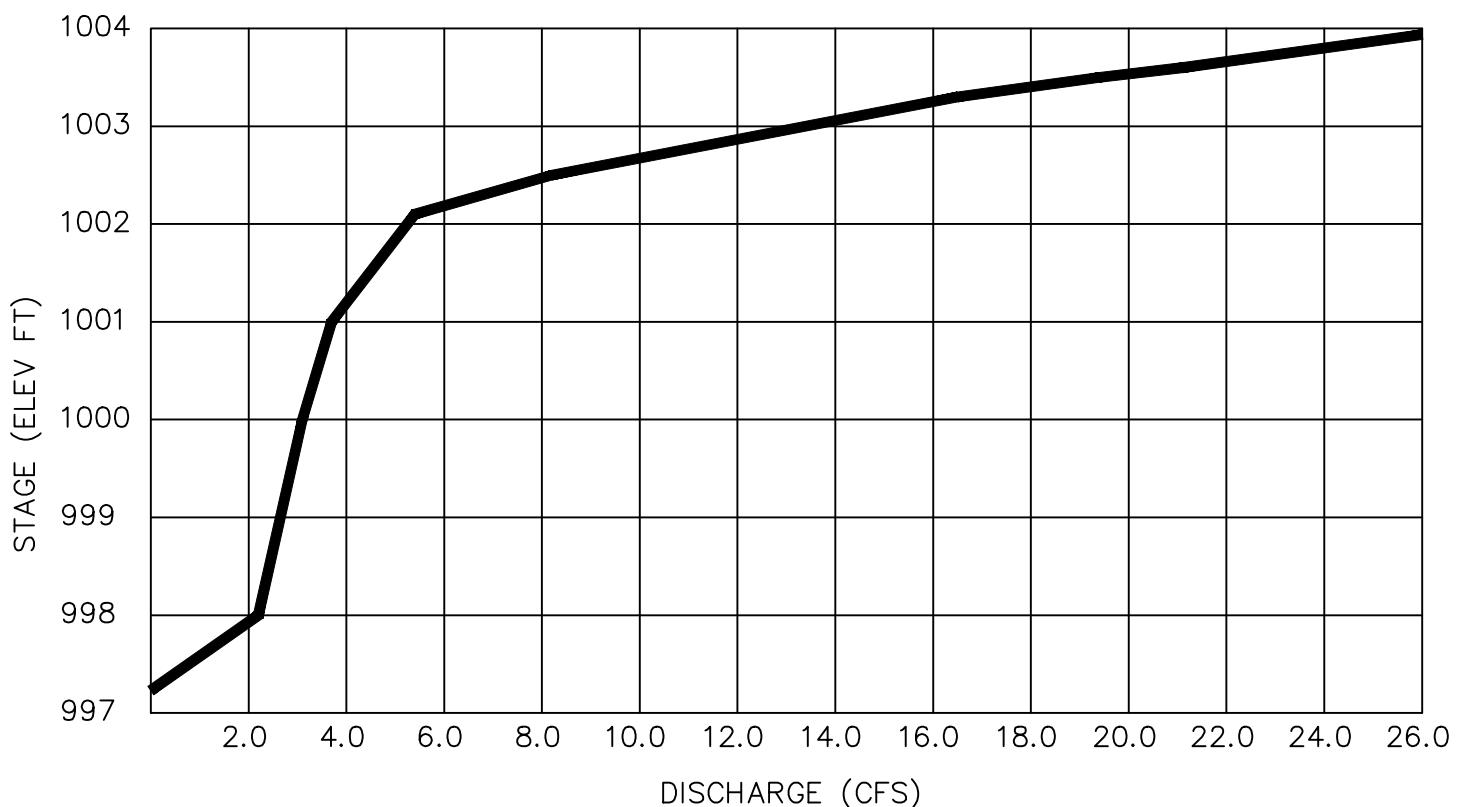


# LSMS EDD-1

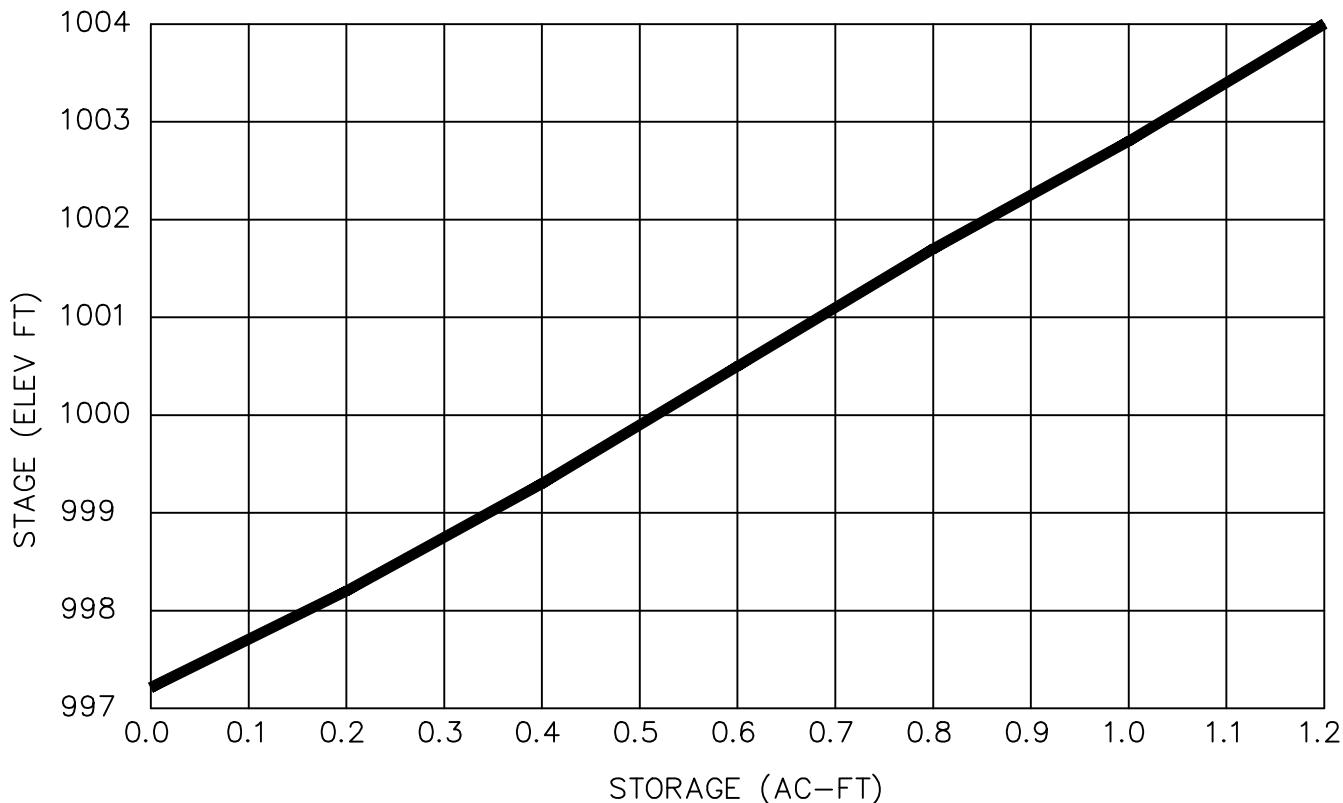
## STAGE-DISCHARGE CURVE



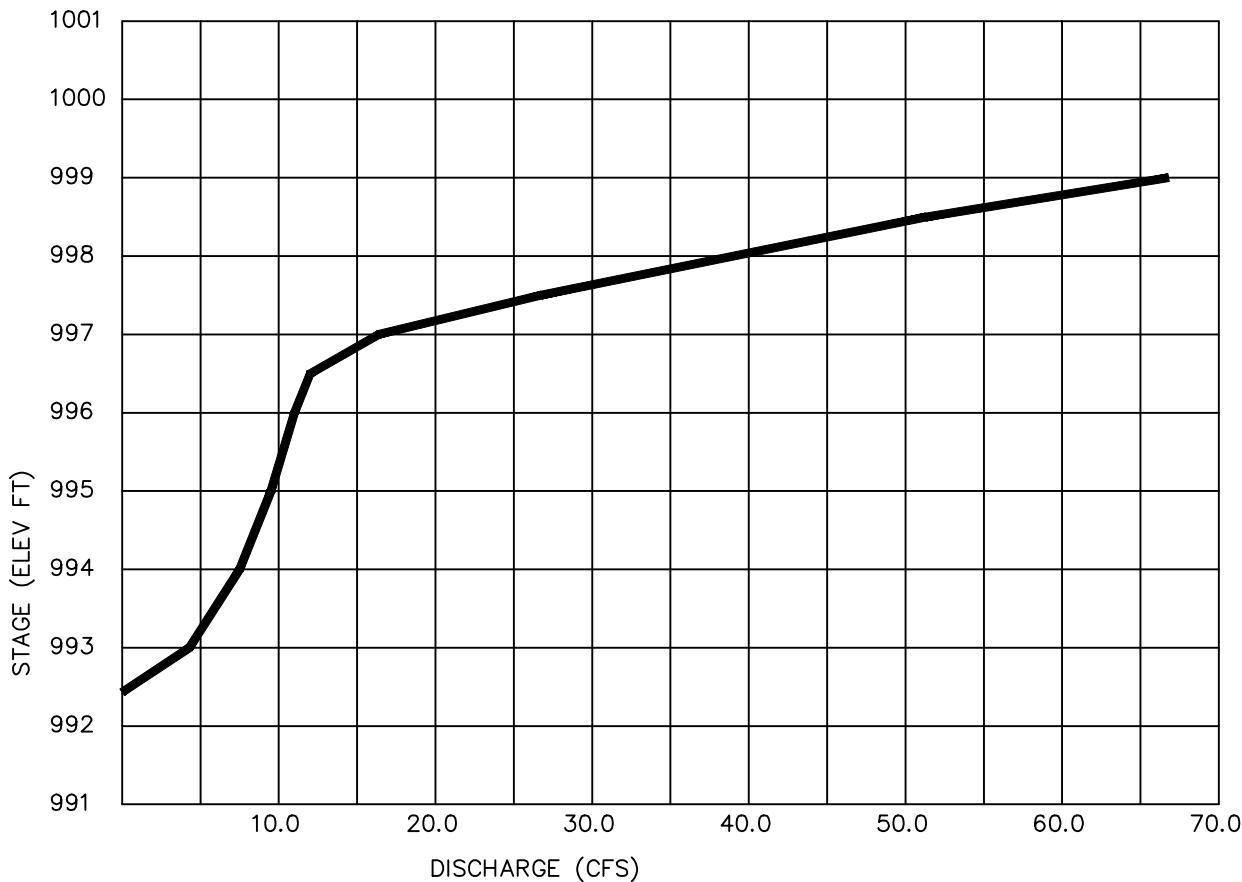
**LSMS EDD-2**  
**STAGE-DISCHARGE CURVE**



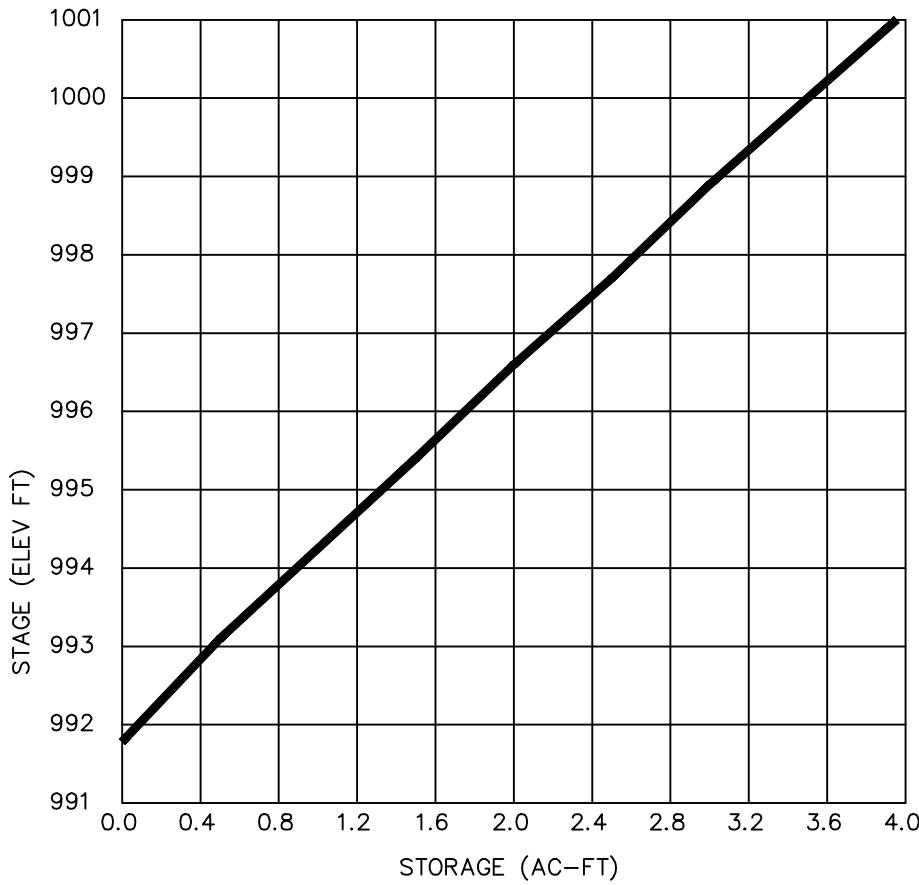
**STAGE-STORAGE CURVE**

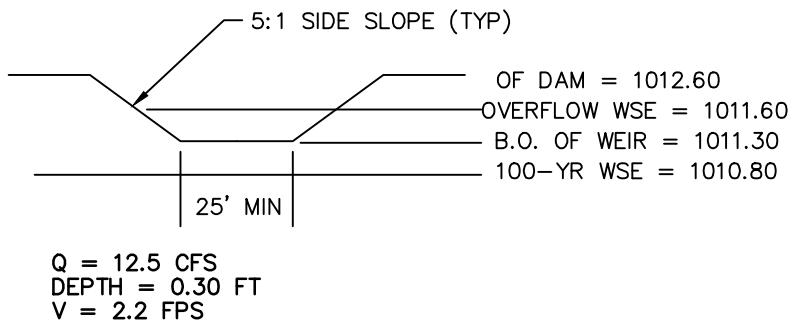


**LSMS EDD-3**  
**STAGE-DISCHARGE CURVE**

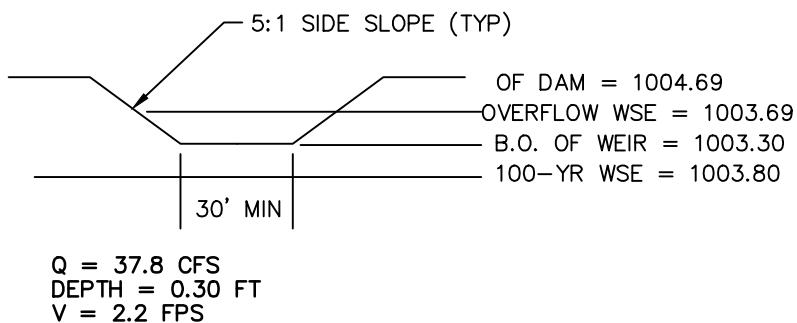


**STAGE-STORAGE CURVE**

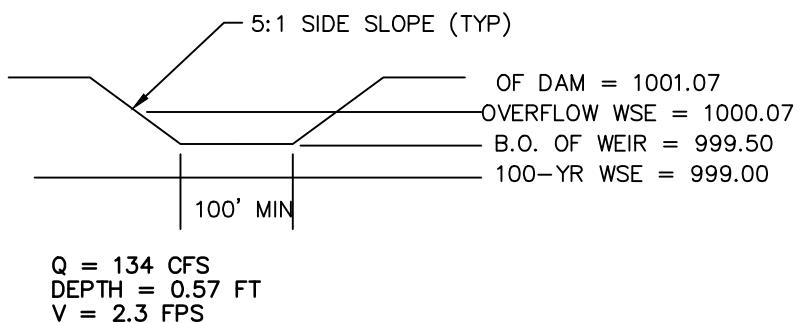




### EDD-1 EMERGENCY SPILLWAY DETAIL



### EDD-2 EMERGENCY SPILLWAY DETAIL



### EDD-3 EMERGENCY SPILLWAY DETAIL