SANITARY STUDY

Monticello, Lots 1 - 160PART OF SEC. 4 & 5 - T. 48 N- R. 31 W

DRAINAGE AREA ACREAGE: 67.71 ACRES

LEE'S SUMMIT, JACKSON COUNTY, MISSOURI

RECEIVED

MAY 0 4 2015

Planning & Codes Admin

-2015-066-

PREPARED BY:

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3. GENERAL INFORMATION

- The study is to evaluate residential uses from:
 - i. Monticello of 67.71 Acres
- The site is 67.71 acres more or less
- The site is currently undeveloped land
- The sanitary facilities are located near the Blue Springs Lake and owned by Little Blue Valley Sewer District

The system was analyzed to drain to the east and connect to the existing City of Lee's Summit interceptor. This system has been studied and determined to be at capacity and will not accept the added flows from the proposed subdivision. The system will be designed to drain north to the Little Blue Valley Interceptor.

LIST OF ABBREVIATIONS

Gallons per Day (gpd)
Cubic Feet per Second (cfs)
Acre (ac)
Inch per hour (iph)
Time of Concentrations, T_c (min)

4. METHODOLOGY

The sanitary flows for the proposed developed were determined utilizing Section 6500 of the City of Lee's Summit Design and Construction Manual Revised September 15, 2005.

The sanitary flows for the existing site were determined utilizing Section 5500 of American Public Works Association, Standard Specifications and Design Criteria.

Peak Wastewater Flows (PWF)

Reference: Section 6501.C.1

PWF = PBF + PIG + PIF (see below for definition of PBF, PIG, & PIF)

Peak Base Flows (PBF)

Reference: Section 6501.C.1.a.i

• 1,500 gpd/ac

PBF = 1,500 gpd/ac* 67.71 ac = 101,565 gpd

Peak Infiltration (PIG)

Reference: Section 6501.C.1.b.i

Peak infiltration to be used for residential land in Lee's Summit is 500 gpd / ac PIG = 500 gpd/ac * 67.71 ac = 33,855 gpd

Peak Inflow (PIF)

Reference: Section 6501.C.1.c

Design for the 50-year storm event

Q = Kia

Where:

Q = peak inflow, cfs

K = inflow factor, unitless (K = 0.006 as per Design and Construction Manual)

i = rainfall intensity that corresponds to a tributary area's time of concentration, inh

A = tributary area, ac

Time of Concentration, T_c calculated by:

 $T_c \text{ (min)} = 18.56 * (Area, ac)^{0.2524}$

 $Tc(min) = 18.56 * (67.71)^{0.2524}$

Tc(min) = 74 min

Q = 0.006*2.96*67.71

Q = 1.20 cfs = 775,580 gpd

Rainfall intensity is interpolated by Section 6501.d a figure relating Time of Concentration and Frequency are shown.

Total Flow = 911,000 gpd

5. Existing Condition Analysis

a. Downstream pipe system is the Little Blue Valley Interceptor

6. Proposed Condition Analysis

a. Study is to evaluate the flows to the existing Interceptor

7. Summary

Total site flows generated upstream of the new10 inch sanitary sewer main located in the draw draining northerly toward the Little Blue Valley Interceptor

8. Conclusion & Recommendations

CONCLUSION

The downstream system has capacity as per a 1998 study of the City of Lee's Summit sanitary sewer system. The proposed development will create not create a capacity issue for the downstream interceptor

9. SUPPORTING CALCULATIONS

EXHIBITS:

• Sanitary flow tables

10. MAPS & EXHIBITS

EXHIBITS:

- o FIGURE 1
 - SITE PLAN
 - STUDY BY HDR FOR PROJECTS TO THE SUBDIVISION

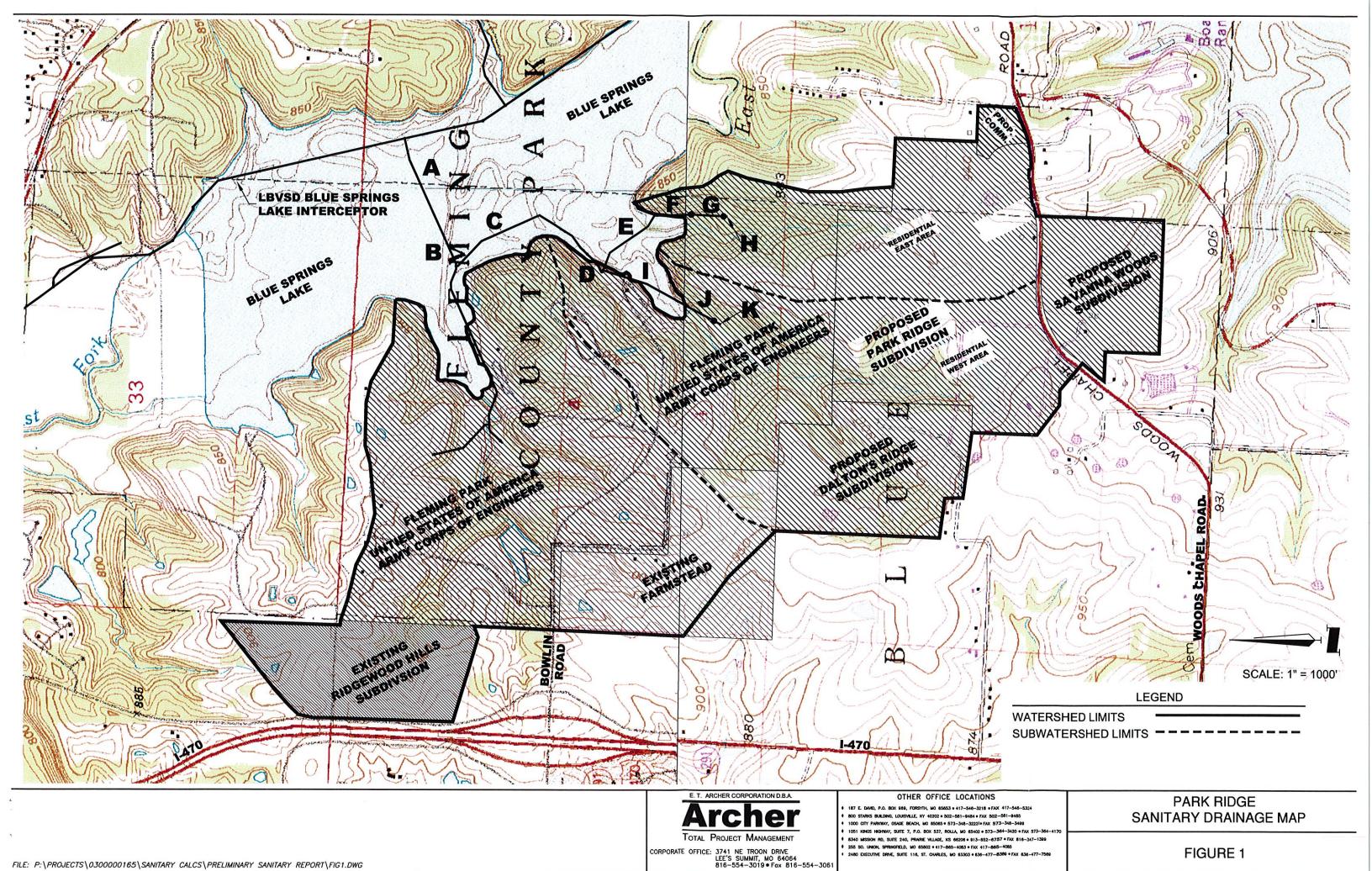
				City of Lee's Summ	it Criteria (Existing)				
	Gravity Flow Capacity	Segment Flow	Excess Capacity	Upstream	Downstream	Upstream	Downstream	Upstream	Downstream
Line Segment	MGD	MGD	MGD	Flowline Elev	Flowline Elev.	Ground Elev.	Ground Elev	HGL	HGL
E	1.08	2.03	-0.95	781.55	778.54	802	821	805.12	794.48
K	3.97	2.29	1.68	803	800	815	806	810.43	809.43
J	3.48	2.29	1.19	793	780.93	806	802	809.39	804.17
1	1.08	2.29	-1.21	780.93	778.78	802	821	804.12	794.41
D	1.85	4.32	-2.47	778.44	778.05	821	802	794.01	791.89
С	1.85	4.32	-2.47	778.05	775.28	802	802	791.64	776.61
В	13.53	5.75	7.78	775.28	774.07	802	802	776.33	775.39
Α	11.13	5.75	5.38	774.047	772.08	802	802	775.35	773.37
A-1	2.42	2.29	0.13	802.49	804.76	810.21	807.39	812.13	810.05
A-2	2.77	2.29	0.48	804.96	807.87	813.87	810.21	814.17	812.13
A-3	2.4	2.29	0.11	808.07	812.07	819.07	813.87	817.86	814.17
A-4	3.57	2.29	1.28	812.27	818.13	825.78	819.07	820.59	817.86
				City of Lee's Summit C	riteria (w/ Monticello)				
	Gravity Flow Canacity	Segment Flow		*	riteria (w/ Monticello)	Unstroam	Downstroam	Unstroam	Downstroam
line Segment	Gravity Flow Capacity	Segment Flow	Excess Capacity	Upstream	Downstream	Upstream	Downstream Ground Floy	Upstream	Downstream
Line Segment	MGD	MGD	Excess Capacity MGD	Upstream Flowline Elev	Downstream Flowline Elev.	Ground Elev.	Ground Elev	HGL	HGL
E	MGD 1.08	MGD 2.03	Excess Capacity MGD -0.95	Upstream Flowline Elev 781.55	Downstream Flowline Elev. 778.54	Ground Elev. 802	Ground Elev 821	HGL 805.12	HGL 793.68
-	MGD 1.08 3.97	MGD 2.03 3.26	Excess Capacity MGD -0.95 0.71	Upstream Flowline Elev 781.55 803	Downstream Flowline Elev. 778.54 800	Ground Elev. 802 815	Ground Elev 821 806	HGL 805.12 835.08	HGL 793.68 833.08
E	MGD 1.08 3.97 3.48	MGD 2.03 3.26 3.26	Excess Capacity MGD -0.95 0.71 0.22	Upstream Flowline Elev 781.55 803 793	Downstream Flowline Elev. 778.54 800 780.93	Ground Elev. 802 815 806	Ground Elev 821 806 802	HGL 805.12 835.08 833.08	HGL 793.68 833.08 822.47
E K J I	MGD 1.08 3.97 3.48 1.08	MGD 2.03 3.26 3.26 3.26	Excess Capacity MGD -0.95 0.71 0.22 -2.18	Upstream Flowline Elev 781.55 803 793 780.93	Downstream Flowline Elev. 778.54 800 780.93 778.78	Ground Elev. 802 815 806 802	Ground Elev 821 806 802 821	HGL 805.12 835.08 833.08 822.47	HGL 793.68 833.08 822.47 802.8
E K J I D	MGD 1.08 3.97 3.48 1.08 1.85	MGD 2.03 3.26 3.26 3.26 5.31	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46	Upstream Flowline Elev 781.55 803 793 780.93 778.44	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05	Ground Elev. 802 815 806 802 821	6round Elev 821 806 802 821 802	HGL 805.12 835.08 833.08 822.47 802.8	HGL 793.68 833.08 822.47 802.8 791.15
E K J I D	MGD 1.08 3.97 3.48 1.08 1.85	MGD 2.03 3.26 3.26 3.26 5.31 5.31	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28	Ground Elev. 802 815 806 802 821 802	821 806 802 821 802 802	HGL 805.12 835.08 833.08 822.47 802.8 799.15	HGL 793.68 833.08 822.47 802.8 791.15 776.61
E K J I D C B	MGD 1.08 3.97 3.48 1.08 1.85 1.85	MGD 2.03 3.26 3.26 3.26 5.31 5.31 6.73	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46 6.8	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05 775.28	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28 774.07	Ground Elev. 802 815 806 802 821 802 802	821 806 802 821 802 802 802	HGL 805.12 835.08 833.08 822.47 802.8 799.15 776.41	HGL 793.68 833.08 822.47 802.8 791.15 776.61 775.17
E K J I D C B A	MGD 1.08 3.97 3.48 1.08 1.85 1.85 13.53 11.13	MGD 2.03 3.26 3.26 3.26 5.31 5.31 6.73 6.73	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46 6.8 4.4	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05 775.28 774.047	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28 774.07 772.08	Ground Elev. 802 815 806 802 821 802 802 802	821 806 802 821 802 802 802 802 802	HGL 805.12 835.08 833.08 822.47 802.8 799.15 776.41 775.35	HGL 793.68 833.08 822.47 802.8 791.15 776.61 775.17
E K J I D C B A A-1	MGD 1.08 3.97 3.48 1.08 1.85 1.85 13.53 11.13 2.42	MGD 2.03 3.26 3.26 3.26 5.31 5.31 6.73 6.73 3.26	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46 6.8 4.4 -0.84	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05 775.28 774.047 802.49	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28 774.07 772.08 804.76	802 815 806 802 821 802 802 802 802 810.21	821 806 802 821 802 802 802 802 802 807.39	HGL 805.12 835.08 833.08 822.47 802.8 799.15 776.41 775.35 839.39	HGL 793.68 833.08 822.47 802.8 791.15 776.61 775.17 773.37 835.18
E K J I D C B A A-1 A-2	MGD 1.08 3.97 3.48 1.08 1.85 1.85 13.53 11.13 2.42 2.77	MGD 2.03 3.26 3.26 3.26 5.31 5.31 6.73 6.73 3.26 3.26	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46 6.8 4.4 -0.84 -0.84	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05 775.28 774.047 802.49 804.96	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28 774.07 772.08 804.76 807.87	Ground Elev. 802 815 806 802 821 802 802 802 802 810.21 813.87	821 806 802 821 802 802 802 802 802 807.39 810.21	HGL 805.12 835.08 833.08 822.47 802.8 799.15 776.41 775.35 839.39 843.53	HGL 793.68 833.08 822.47 802.8 791.15 776.61 775.17 773.37 835.18 839.39
E K J I D C B A A-1	MGD 1.08 3.97 3.48 1.08 1.85 1.85 13.53 11.13 2.42	MGD 2.03 3.26 3.26 3.26 5.31 5.31 6.73 6.73 3.26	Excess Capacity MGD -0.95 0.71 0.22 -2.18 -3.46 -3.46 6.8 4.4 -0.84	Upstream Flowline Elev 781.55 803 793 780.93 778.44 778.05 775.28 774.047 802.49	Downstream Flowline Elev. 778.54 800 780.93 778.78 778.05 775.28 774.07 772.08 804.76	802 815 806 802 821 802 802 802 802 810.21	821 806 802 821 802 802 802 802 802 807.39	HGL 805.12 835.08 833.08 822.47 802.8 799.15 776.41 775.35 839.39	HGL 793.68 833.08 822.47 802.8 791.15 776.61 775.17 773.37 835.18

Little Blue Valley Sewer District Criteria (Existing)

	Gravity Flow Capacity	Segment Flow	Excess Capacity	Upstream	Downstream	Upstream	Downstream	Upstream	Downstream
Line Segment	MGD	MGD	MGD	Flowline Elev	Flowline Elev.	Ground Elev.	Ground Elev	HGL	HGL
E	1.08	0.59	0.49	781.55	778.54	802	821	782.02	779.46
K	3.97	0.82	3.15	803	800	815	806	803.48	800.31
J	3.48	0.82	2.66	793	780.93	806	802	793.48	781.63
1	1.08	0.82	0.26	780.93	778.78	802	821	781.57	779.44
D	1.85	1.41	0.44	778.44	778.05	821	802	779.33	779.02
С	1.85	1.41	0.44	778.05	775.28	802	802	778.92	776.15
В	13.53	2.32	11.21	775.28	774.07	802	802	775.84	774.8
Α	11.13	2.32	8.81	774.047	772.08	802	802	774.71	773.37
A-1	2.42	0.82	1.6	802.49	804.76	810.21	807.39	805.24	802.89
A-2	2.77	0.82	1.95	804.96	807.87	813.87	810.21	808.35	805.33
A-3	2.4	0.82	1.58	808.07	812.07	819.07	813.87	812.55	808.47
A-4	3.57	0.82	2.75	812.27	818.13	825.78	819.07	818.61	812.6

Little Blue Valley Sewer District Criteria (w/ Monticello)

	Gravity Flow Capacity	Segment Flow	Excess Capacity	Upstream	Downstream	Upstream	Downstream	Upstream	Downstream
Line Segment	MGD	MGD	MGD	Flowline Elev	Flowline Elev.	Ground Elev.	Ground Elev	HGL	HGL
E	1.08	0.59	0.49	781.55	778.54	802	821	802.12	794.48
K	3.97	1.04	2.93	803	800	815	806	810.43	809.43
J	3.48	1.04	2.44	793	780.93	806	802	809.39	804.17
Ĭ	1.08	1.04	0.04	780.93	778.78	802	821	804.12	794.41
D	1.85	1.59	0.26	778.44	778.05	821	802	794.01	791.89
С	1.85	1.59	0.26	778.05	775.28	802	802	791.64	776.61
В	13.53	2.5	11.03	775.28	774.07	802	802	776.33	775.39
Α	11.13	2.5	8.63	774.047	772.08	802	802	775.35	773.37
A-1	2.42	1.04	1.38	802.49	804.76	810.21	807.39	805.3	802.95
A-2	2.77	1.04	1.73	804.96	807.87	813.87	810.21	808.41	805.39
A-3	2.4	1.04	1.36	808.07	812.07	819.07	813.87	812.61	808.53
A-4	3.57	1.04	2.53	812.27	818.13	825.78	819.07	818.67	812.64



SANITARY SEWER EVALUATION

INTRODUCTION

ACH, L.L.C. is proposing a development in northeast Lee's Summit entitled Park Ridge. The proposed project site is located approximately one mile east of Interstate 470 on the north side of Woods Chapel Road. The site contains approximately 180 acres and is proposed to be developed as single-family residential and commercial. The proposed development location is indicated on Figure 1 in Appendix A.

EXISTING FACILITIES

The proposed development is located within the Blue Springs Lake Watershed. Figure 1 depicts the watershed limits and existing wastewater conveyance system for the Blue Springs Lake Watershed. The system available to serve the Park Ridge Development consists of a branch of the Little Blue Valley Sewer District Blue Springs Lake Interceptor within Fleming Park that conveys flows to the Blue Springs Lake Interceptor main line under Blue Springs Lake.

An initial analysis was performed to determine the capacities of the existing branches of Blue Springs Lake Interceptor serving the Park Ridge Development. The capacities of the interceptors are indicated in Table 1 in Appendix B, with segment designations H–E representing the east branch, K-I representing the west branch, and D-A representing the line that connects the east and west branch to the Blue Springs Lake Interceptor main line.

TRIBUTARY AREAS

Lee's Summit sewer maps and USGS maps were used to delineate the tributary areas contributing to each segment. The tributary areas for each segment are depicted on Figure 1.

Approximately 50-percent of this watershed will remain undeveloped since it is within Fleming Park and belongs to the United States Army Corps of Engineers. Presently, one subdivision, Ridgewood Hills, is contributing flows to this branch of the interceptor. Park Ridge, Dalton's Ridge, and Savanna Woods are proposed subdivisions that will be preliminary platted this year. The available development areas within the east and west branch watersheds will be 100-percent developed and the available development areas in the entire watershed, contributing to this branch, will be approximately 80-percent developed when these proposed subdivisions are constructed. As a result, the entire watershed, excluding Fleming Park, was considered as tributary to the interceptor.

The Savanna Woods development is located in a watershed without sanitary sewer service. Savanna Woods is proposing to construct a lift station that will pump flows to the Park Ridge gravity sewers. Savanna Woods is scheduled to be developed when the west half of Park Ridge is developed. The Park Ridge gravity sewers, that convey flows to interceptor Segment H, will be constructed when the east half of Park Ridge is developed. Therefore, it is proposed to build a diversion structure at the intersection of the Savanna Woods force main and Park Ridge gravity sewer system that will divert flows to Park Ridge gravity sewers flowing to interceptor Segment K. Ultimately, when the east half of Park Ridge is developed, all Savanna Woods sewer flows will be diverted to the gravity sewer lines flowing to interceptor Segment H. This sanitary sewer analysis evaluates the ultimate condition. Therefore, the Savanna Woods tributary area is shown contributing to Segment H.

FLOWS

The tributary flows for each branch were determined using two options. Option 1 utilizes the City of Lee's Summit's flow criteria, as specified in the 2004 Lee's Summit Design and Construction Manual. Option 2 utilizes Little Blue Valley Sewer District (LBVSD) peak flow criteria, as established in the 2000 LBVSD Master Plan.

Option 1 Flows

Option 1 peak residential wastewater flows are determined by summing a peak dry weather flow of 1,500 gallons per acre, a peak infiltration of 500 gallons per acre, and a peak inflow that is calculated using the following formula:

Peak Inflow = $KiA \times 0.6463167 = million gallons per day$

Where:

K=dimensionless inflow factor (0.006-residential)

i=intensity (inches per hour) A=tributary area (acres)

The rainfall intensity, *i*, corresponds to the tributary area's time of concentration for a 50-year storm event. The time of concentration is determined as follows:

Time of Concentration = $18.46 \times Area^{0.2524}$

After determining the time of concentration, the intensity is obtained from the table in Section 6501-C of the 2004 Lee's Summit Design and Construction Manual.

Option 1 peak commercial flows are determined by summing a peak dry weather flow, a peak infiltration of 250 gallons per day per acre, and a peak inflow. Peak inflow is determined using the same equation indicated above for residential use, except the K-value is 0.003. The peak dry weather flow is determined by the type of non-residential use, building area, and the equivalent development units (EDU) established in Table 6501-1 of the 2004 Lee's Summit Design and Construction Manual. The peak dry weather flow is determined as follows:

Non-residential Peak Dry Weather Flow = EDU x Building Area x Stories x 300 GPD

Individual existing and proposed flow contributions and their expected entry points into the Blue Springs Lake Interceptor are indicated on Table 2A and Table 2B in Appendix B.

Option 2 Flows

The Option 2 peak wastewater flows are determined by multiplying average wastewater flows by a peaking factor. The average flow is calculated as follows:

Average Flow = 2.6 people/home x # of homes x 119 gallons/capita/day = gallons per day

The number of homes for the existing and proposed subdivisions was determined from preliminary plats. Since full (ultimate) development is projected in the watershed, Lee's Summit maximum R-1 zoning density (4.0 homes per acre) was used for the existing farmstead. After determining the

average flow, the peak flow is obtained by using a peaking factor of 6.20, which is specified in the 2000 LBVSD Master Plan. Individual existing and proposed flow contributions and their expected entry points into the Blue Springs Lake Interceptor are indicated on Table 3A and Table 3B in Appendix B.

ANALYSIS

A hydraulic analysis was completed for existing and proposed flows contributing to the interceptor. The analysis was completed using Lee's Summit Design Criteria (Option 1 Flows) and using the Little Blue Valley Sewer District Criteria (Option 2 Flows). Table 4A and Table 4B, in Appendix B, provide an individual segment summary utilizing Option 1 Flows. Table 5A and Table 5B, in Appendix B, provide an individual segment summary using Option 2 Flows.

RESULTS

Based on Lee's Summit Design Flow Criteria, Segment E, Segment I, Segment D, and Segment C will have their respective gravity flow capacity exceeded at ultimate development in the watershed. However, each of these segments is a sealed system beneath the normal and full pool of the lake, which contains flows within the segments allowing the system to have pressure capacity. The hydraulic grade line elevations are higher than the manhole located between Segment J and Segment K. Again, the pipe connections within these structures are sealed connections and contain flows within the system allowing the system to have pressure capacity. However, there is a 2-inch air vent within this manhole. Therefore, to ensure the hydraulic grade line remains within the system we recommend the manhole and air vent be raised so the top of the air vent is at least 1-foot above the hydraulic grade line elevation highlighted in Table 5B.

Based on Little Blue Valley Sewer District Flow Criteria, all segments have gravity flow capacity for ultimate development in the watershed.

CONCLUSIONS

Based on an evaluation of the existing system and peak flow rates, this branch of the Blue Springs Lake Interceptor has adequate capacity to serve the Park Ridge Development. Although the hydraulic grade line is above the pipe in some segments, when using Lee's Summit Design Flow Criteria, this system will still convey flows under pressure without adverse effect to public health, safety, and welfare.

RECOMMENDATIONS

As stated in the results, to ensure the hydraulic grade line remains within the system we recommend the manhole and air vent be raised so the top of the air vent is at least 1-foot above the hydraulic grade line elevation highlighted in Table 5B. This modification would increase the Segment J-K manhole rim elevation approximately 6-feet.

Park Ridge and Dalton's Ridge will contribute flows to the west branch. Since each of these developments is contributing to the interceptor we recommend the manhole modification cost be shared between the developments based on the tributary area to the branch.

In addition to the above-described improvements, Archer has made the following recommendation to ACH, L.L.C. to help reduce the peak flows to the Blue Springs Lake Interceptor:

- 1. Through the Subdivisions Protective Covenants, the Park Ridge Developer should enforce the design of foundation drain systems that minimize the introduction of inflow into the sanitary sewer system. The proposed requirements should include:
 - a. Placement of foundation drain pipe below the basement slab. Normal construction practice is to place this drain at or above basement floor level.
 - b. All foundation drains should be piped to a sump that is located below the lowest end of the drain pipe with a sump pump that is capable of pumping the capacity of the foundation drain. If gravity discharge of the foundation drain is proposed (i.e. walkout basements), the builder should provide the Developers' engineer with elevations and slopes of the pipe from the building to the point of discharge.
 - c. Use of sanitary sewers, via foundation drain taps to basement floor drains or taps to the laterals, should be strictly prohibited. This restriction should be incorporated into the Protective Covenants.
 - d. The Developer will provide engineering inspection of all foundation drains, lateral installation, and connections to the public sewers. This will include an inspection of basement floor drains prior to occupancy of all homes.

TABLE 1
BLUE SPRINGS LAKE INTERCEPTOR SEWER ANALYSIS
FULL FLOW GRAVITY CAPACITY

		Length	Existing	Slope	Velocity	Gravity Flow	Gravity Flow
	Line Segment	(ft)	Diameter (in)	(ft/ft)	(saj)	Capacity (cfs)	Capacity (MGD)
H	Н	22.00	12	0.0300	7.82	6.14	3.97
NCI ZL	G	400.00	12	0.0300	7.82	6.14	3.97
	F	425.00	12	0.0300	7.82	6.14	3.97
I	E	1,368.18	12	0.0022	2.12	1.66	1.08
	K	100.00	12	0.0300	7.82	6.14	3.97
VIO AES	J	524.78	12	0.0230	6.85	5.38	3.48
	I	977.27	12	0.0022	2.12	1.66	1.08
ED	D	278.57	91	0.0014	2.05	2.86	1.85
INI	C	1,978.00	16	0.0014	2.05	2.86	1.85
IMC	В	484.00	2-18	0.0025	5.92	10.47	13.53
S	А	1,191.62	2-18	0.0017	4.89	8.63	11.16

Value of .013 used for pipe type

	Tributary Area	Entering Sewer Segment	Area (acres)	Peak Base Flow (MGD)	Peak Infiltration Total Peak Flow (MGD)	· Total Peak Flow (MGD)
COMB.	Ridgewood Hills	В	67.45	0.10	0.03	0.74

TABLE 2B LBVSD BLUE SPRINGS LAKE INTERCEPTOR SEWER ANALYSIS ULITMATE DEVELOPMENT CONTRIBUTING FLOWS

OPTION I FLOWS

	Tributory Area	Entering Sewer	Area	Peak Base Flow	Peak Infiltration	Total Peak Flow
	Tilbutaly Alca	Segment	(acres)	(MGD)	(MGD)	(MGD)
Н	Park Ridge (Residential-East Area)	Н	91.20	0.14	0.05	1.24
JS.	Corps Ground (Undeveloped)	E	63.89	ï		ì
E∀	Park Ridge (Commercial)*	Н	6.25	0.0013	0.0016	0.04
B	Savanna Woods	H	55.00	0.08	0.03	0.75
Н	Dalton's Ridge	K	76.00	0.11	0.04	0.99
ON LS3	Corps Ground (Undeveloped)	-	132.27	ï	1	
ME ME	Park Ridge (Residential-West Area)	K	88.35	0.13	0.04	1.16
В	Existing Farmstead	K	10.75	0.02	0.01	0.14
B'	Ridgewood Hills	В	67.45	0.10	0.03	0.74
WC	Corps Ground (Undeveloped)	ľ	281.00	-	-	
CC	Existing Farmstead	В	62.34	0.09	0.03	89.0

Peak Base Flow = 1,500 GPD/Acre

Peak Infiltration = 500 GPD/Acre

934.50

 $Peak\ Inflow = KIA\ (FOR\ 50-YEAR\ STORM)$

Total Peak Flow = Peak Base + Peak Infiltration + Peak Inflow

*Commercial Flows Calculations Are Shown Below

Non-Residential Source	Building Area (SF)	EDU	Stories	Peak Base Flow (MGD)
Offices	2400	0.3/1000 SF	I	0.0002
Convenience Store	2400	I+0.3/1000 SF	I	8000'0
Retail	0045	0.2/1000 SF	I	0.0003

Commercial Peak Base Flow = EDU x Building Area x Stories x 300GPD

0.0013

TOTAL

Commerial Peak Infiltration = 250 GPD/Acre

Commerial Peak Inflow = KIA (50-YEAR STORM) (K=0.003)

	Tributary Area	Entering Sewer Segment	. Homes	Area (acres)	Total Average Flow (MGD)	Total Peak Flow (MGD)
COMB.	Ridgewood Hills	В	224	67.45	0.07	0.43

TABLE 3B LBVSD BLUE SPRINGS LAKE INTERCEPTOR SEWER ANALYSIS ULITMATE DEVELOPMENT CONTRIBUTING FLOWS OPTION 2 FLOWS

	Tributary Area	Entering Sewer Segment	Homes	Area (acres)	Total Average Flow (MGD)	Total Peak Flow (MGD)
СН	Park Ridge (Residential-East Area)	Н	204	91.20	0.063	0.39
KYN	Corps Ground (Undeveloped)	T.		63.89	1	
a Ts	Park Ridge (Commercial)*	Н	25	6.25	0.0077	0.05
E¥	Savanna Woods	Н	81	55.00	0.025	0.16
СН	Dalton's Ridge	K	193	76.00	090.0	0.37
KAN	Corps Ground (Undeveloped)	-		132.27	ť	
a Te	Park Ridge (Residential-West Area)	K	190	88.35	0.059	0.36
ME	Existing Farmstead**	K	43	10.75	0.013	0.08
.8	Ridgewood Hills	В	224	67.45	690.0	0.43
IMO	Corps Ground (Undeveloped)	T	-	281.00	ī	
)	Existing Farmstead**	В	250	62.34	0.077	0.48

*Used Equivalent Home Count For Stewart Farm Commercial Area with 4.0 homes/acre

**Assumed 4.0 homes/acre For Farmstead

NOTE:

Average Flow = 2.6 People/Home * No. of Homes x 119 Gallons Per Day Per Capita (Specified By 2000 Little Blue Valley Sewer District Facility Plan)

Peak Flow = 6.20 x Average Flow (6.20:1 Peak As Determined By 2000 Little Blue Valley Sewer District Facility Plan)



Preliminary Plat Monticello

Lots 1 - 160 & Tracts A-F Section 4 & 5, Township 48 North, Range 31 West Lee's Summit, Jackson County, Missouri

Legal Description:

A tract of land located in part of Section 4 and Section 5, Township 48 North, Range 31 West, more particularly described as follows: Beginning at the Southwest corner of Section 4, thence North 88 "14 60" West, a distance of 20.001 feet; thence North 02" 18" 05" East, a distance of 659.95 feet; thence South 87" 58" 48" East, a distance of 1171.74 feet; thence South 02" 12" 5" West, a distance of 20.04 feet; thence South 02" 12" 5" Sez" East, a distance of 10.305 feet; thence South 87" 58 5" 2" East, a distance of 10.305 feet; thence South 5" 2" 12" Sez, a distance of 10.91 feet; thence South 5" 2" 12" West, a distance of 10.91 feet; thence South 5" 2" 12" West, a distance of 10.91 feet; thence South 5" 2" 12" East, a distance of 20.97.01 feet, returning to the Point of Beginning. Containing 67.71 acres more or less

FEMA Note: See FEMA Site for Flood Data Website: www.fema.gov Panel Number: 29095CO312F

Site Data Table :

2,949,550.09 Sq. Ft. (67.71 Acres)

2.36 Lots / Acre

Sanitary Sewer Service
Sanitary sewer main will be extended to the north and connected to the Little Blue Valley
Sewer District Interceptor Following final design a sewer easement will be drafted and
dedicated to the City of Lee's Summit by separate document

Water Service
Water will be extended to the site from the existing City of Lee's Summit water located within
the existing subdivisions to the south. The water will be looped in phase 1 to provide water
capacity and volume to the subdivision

Storm Sewer
Storm sewer system will be installed to convey the storm water runoff to the detention facility, which will meet the current standards of APWA Section 5600

Storm Water Detention
The increase in storm water runoff will be controlled by the proposed delention facility located in the north portion of the site. The flows will be reduced to meet APWA Section 5600 required flow rates. BMP facilities will be provided within the pand system.

SURVEYOR'S GENERAL NOTES:

This survey is based upon the following information or researched by this surveyor.
 (A). Ex[8]. Final Plat of Viscotive Estates
 (C). Final Plat of Surrup Broot. 181-58 Plat
 (D). Final Plat of Foxenod East 58 Plat
 (D). Final Plat of Foxer Addition
 (F). Final Plat of J. Robinson Suburban Addition
 (F). Final Plat of J. Robinson Suburban Addition

This survey meets or exceeds the accuracy standards of a (SUBURBAN) Survey as defined by the Missouri Standards for Property Boundary Surveys.

5). This company assumes no responsibility in the location of existing utilities within the subject premises. This is an above-ground survey. The underground utilities, if shown, are based on information provided by the various utility companies and these locations should be considered approximate. There may be additional underground utilities not shown on this drawing. Dig Rite Tables #1507/1205, 15507/1179, 15007/1179.

6). Subsurface and environmental conditions were not surveyed or examined or considered as a part of this survey. No evidence or statement is made concerning the existence of underground or ownless do conditions, containers or facilities that may after the use or development of this proper. No attempt has been made to obtain or show data concerning austience, size, depth, conditions, capacity or fociation of any utility existing on the size, whether private, muricipal or public owned.

OIL - GAS WELLS
ACCORDING TO EDWARD ALTON'S ENVIRONMENTAL IMPACT STUDY OF
ABANDONED OIL AND GAS WELLS IN LEE'S SUMMIT, MISSOURI IN 1995, THERE ARE
NOT OIL AND GAS WELLS WITHIN 185 FEET OF THE PROPERTY AS SURVEYED

31 W SCALE

MGINEERING

BOLUTIONS

SOLUTIONS

SOR SMIT STREET

LEES SUMMAT, NO 4002

PIRIO 622-988 PRINGES-949



SUPPLEMENTAL SANITARY SEWER EVALUATION PARK RIDGE LEE'S SUMMIT, JACKSON COUNTY, MO

August, 2005

Prepared for:

ACH, L.L.C. 839 NE Woods Chapel Road Lee's Summit, MO 64064

PROPOSED INTERCEPTOR EXTENSION

The west and east branches of the Blue Springs Lake Interceptor will be extended to provide service to Dalton's Ridge, Park Ridge, and Savanna Woods. Both branches will be extended using 12-inch diameter PVC, or DIP if underneath a creek crossing. The proposed extensions, lines A and B, are capable of handling Ultimate Development Option 1 and Option 2 flows. Attached Tables 6A and 6B show the capacities and hydraulic grade lines of the proposed segments using the ultimate flows for both options.

The connections to the branches within the Park Ridge Subdivision will consist of 12-inch diameter PVC pipe. These segments will be installed at slopes capable of conveying the Option 1 Ultimate Development flows. The west connection will handle 1.16 MGD, and the east connection will handle 2.03 MGD.