

JJM DESIGN BY: DWM DRAWN BY: "PREL IMINARY 12720 PROJECT NO.: PLANS NOT architects APPROVED FOR engineers SHEETS CONSTRUCTION. 9801 Renner Boulevard Lenexa, Kansas 66219 9 1 3 . 4 9 2 . 0 4 0 0 33 www.gbateam.com JOSHUA J. MILLER Paragon Star Development PROFESSIONAL ENGINEER PE-2009010386 REVISIONS DATE BY APPROVI

General Notes: Design Specifications: 2012 AASHTO LRFD Bridge Design Specifications (6th Ed.) and 2013 Interim Revisions. Seismic Design Category = A All referenced specifications shall refer to Missouri Standard Specifications for Highway Construction Design Loading: Vehicular = HL-93 Future Wearing Surface = 35 lb/sf Earth = 120 lb/cfEquivalent Fluid Pressure = 45 lb/cf Design Unit Stresses: f'c = 3,000 psiClass B Concrete (Substructure) Class B-1 Concrete (Barrier Curb) f'c = 4,000 psiClass B-2 Concrete (Superstructure except Barrier Curb f'c = 4,000 psify = 60,000 psiReinforcing Steel (Grade 60) fy = 50,000 psiStructural Steel HP Pile (ASTM A709 Grade 50S) For Precast Prestressed Panel Stresses, see Sheet No. __1. For Prestressed Girder Stresses, See Sheets No. __ & __. Neoprene Pads: Plain and Laminated Neoprene Bearing Pads shall be 60 durometer and shall be in accordance with Sec 716. Joint Filler: All joint filler shall be in accordance with Section 1057 for preformed sponge rubber expansion and partition joint filler, except as noted. Reinforcing Steel: Minimum clearance to reinforcing steel shall be 1 1/2", unless otherwise shown.

FOUNDATION DATA BENT NUMBER DESIGN TYPE DATA HP12×53 HP12×53 HP12×53 HP12×53 Pile Type and Size Number 8 Approximate Length per Each ___ Pile Point Reinforcement ___ Min. Galvanized Penetration (Elev.) ft Bearing Minimum Nominal Axial Compressive Resistance

Minimum clearance between galvanized piles and uncoated (plain) reinforcing steel including bar supports shall be 1 1/2". Nylon, PVC, or other polyethylene spacers shall be used to maintain

clearance. Nylon cable ties shall be used to bind the spacers to the reinforcement.

Structure to be closed during construction. See roadway plans for traffic control.

City Construction personnel will indicate the type of joint filler option used under

DT = Dynamic Testing

Traffic Handling:

the precast panels for this structure:

Constant Joint Filler

☐ Variable Joint Filler

Miscellaneous:

Minimum Nominal Axial Compressive Resistance = Maximum Factored Loads/Resistance Factor

HP piles are anticipated to be driven to refusal on rock. Review all borings for depth of rock and restrict driving as appropriate to comply with hard rock driving criteria in accordance with Sec 702.

- All piles shall be galvanized down to the minimum galvanized penetration (elevation).
- Pile point reinforcement need not be galvanized. Shop drawings will not be required for pile point reinforcement.

The contractor shall make every effort to achieve the minimum galvanized penetration (elevation) shown on the plans for all piles. Deviations in penetration less than 5 feet of the minimum will be considered acceptable provided the contractor makes the necessary corrections to ensure the minimum penetration is achieved on subsequent piles.

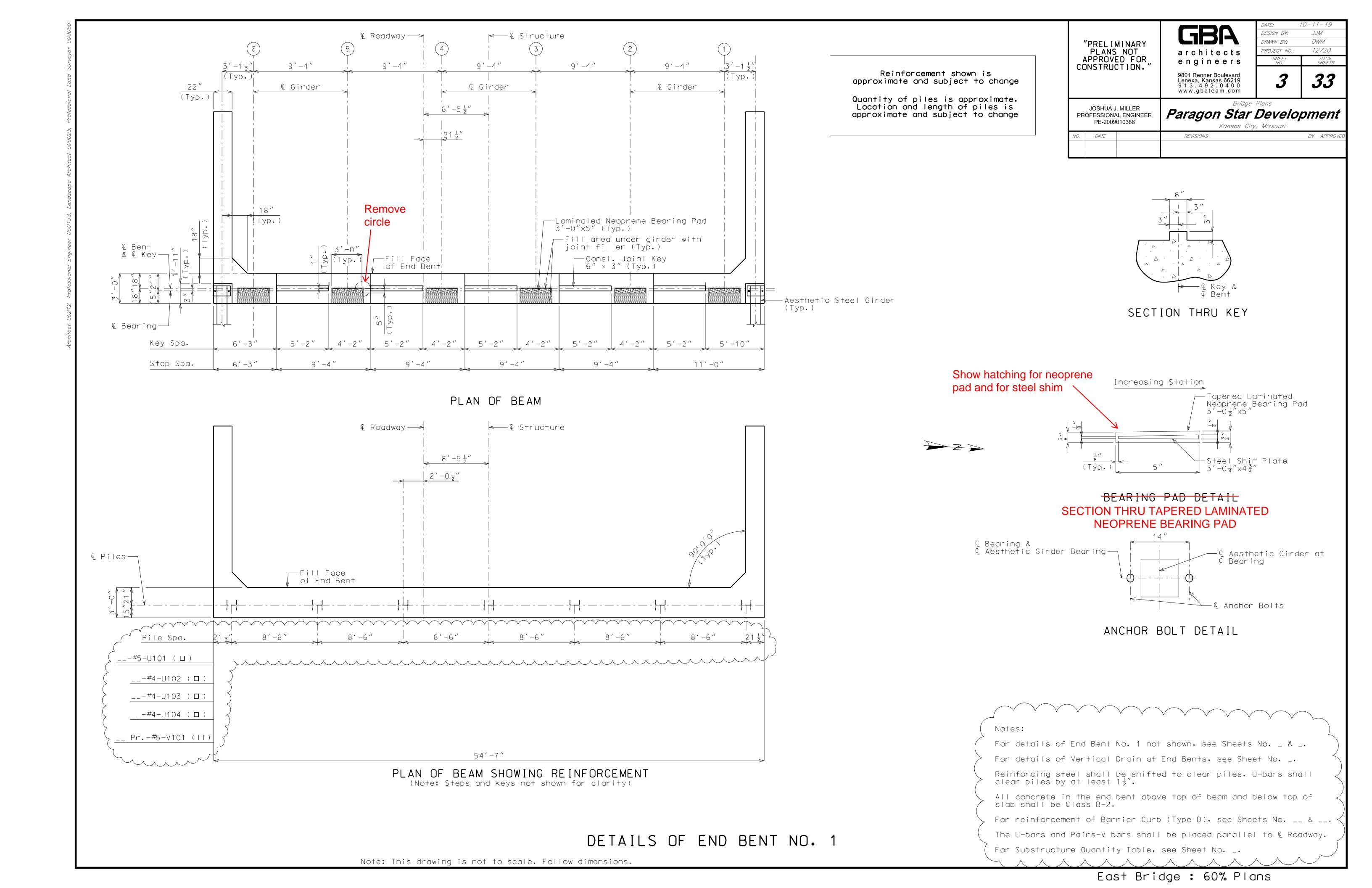
Reinforcement quantity provided is based on _____lbs/cy of concrete.

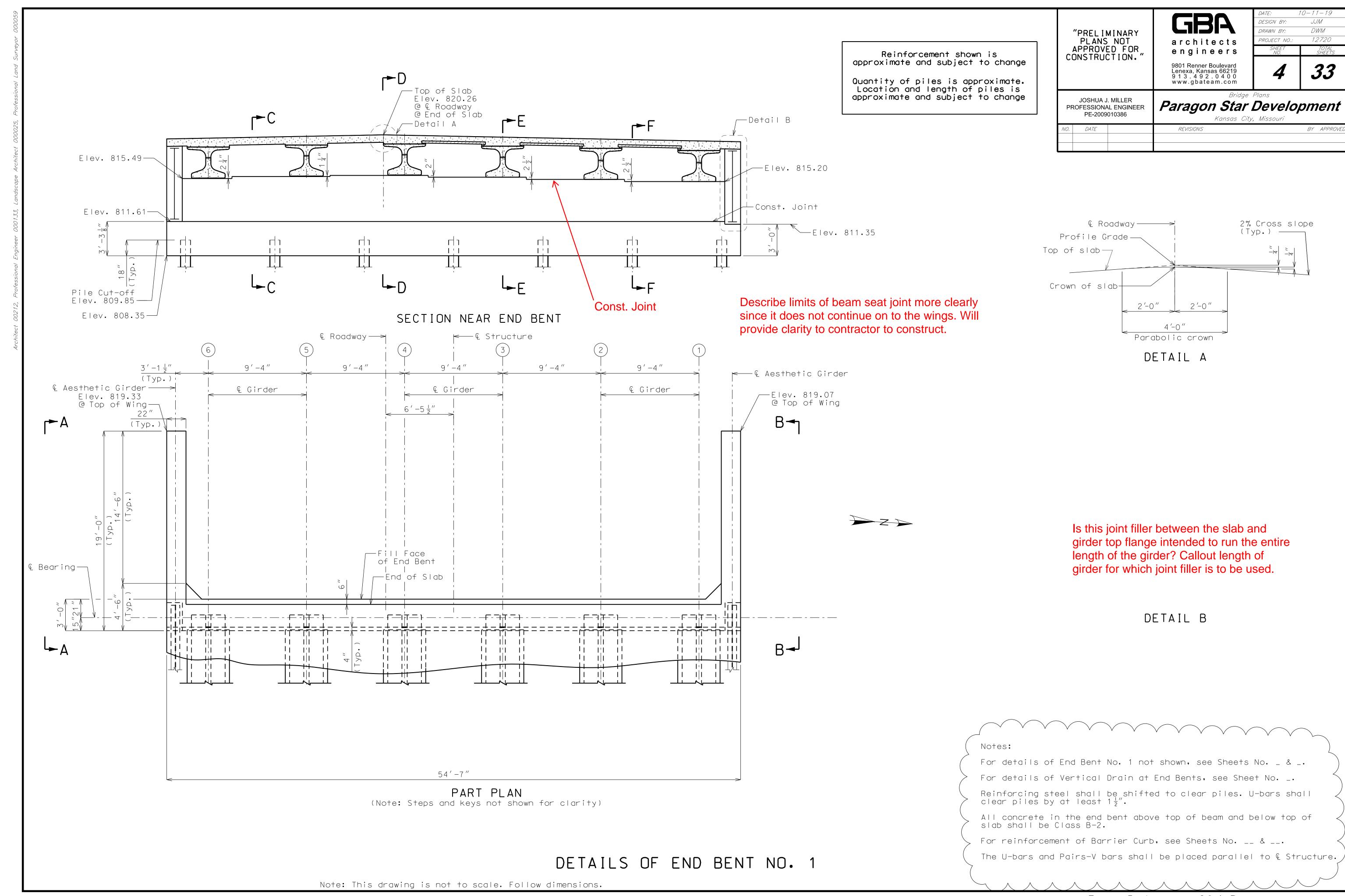
Estimated Quantities		
I tem		Total
Class B-2 Concrete (Superstructure Concrete on NU-Girder)	cu, yard	
Reinforcing Steel (Epoxy Coated)	pound	

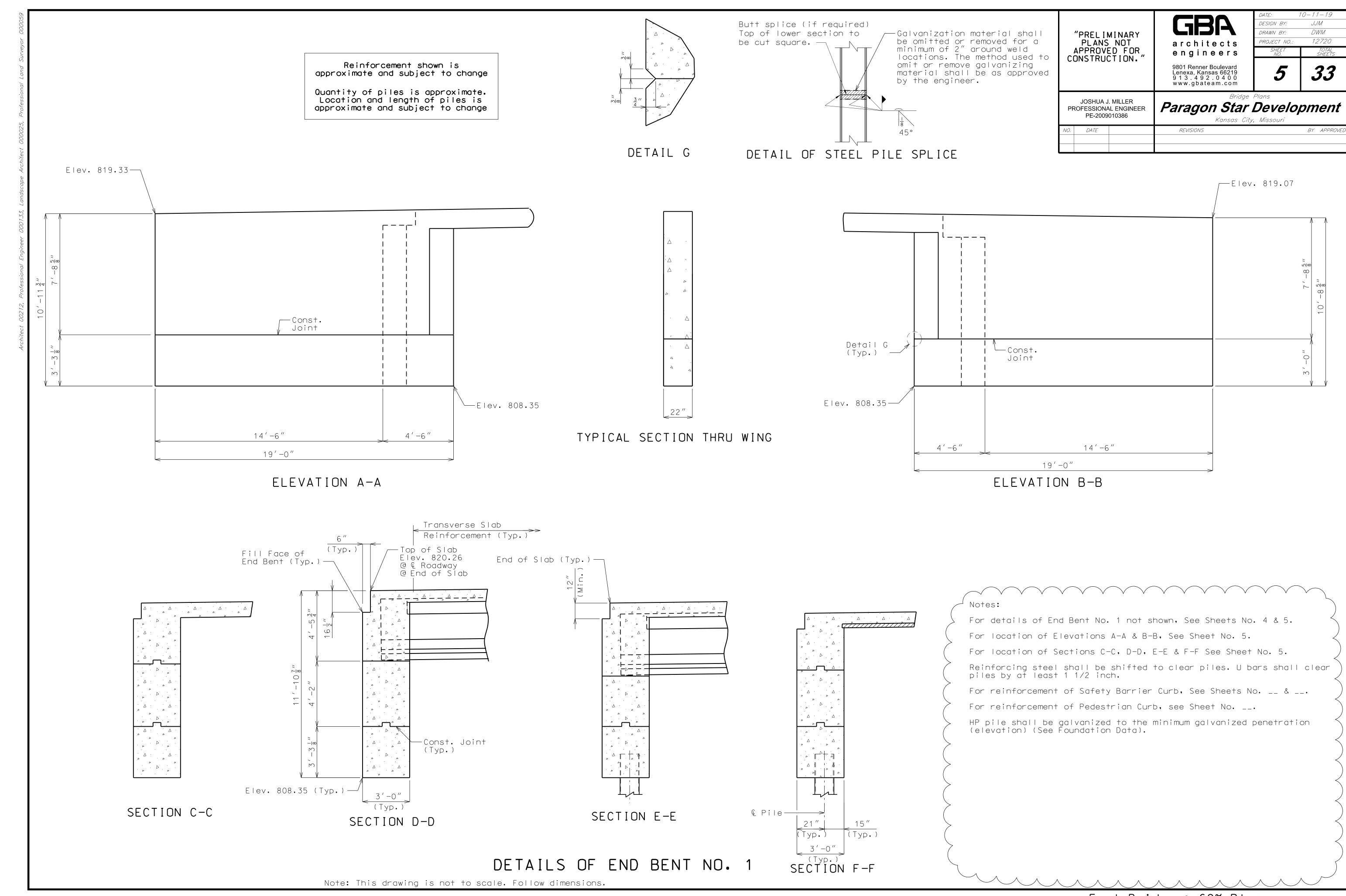
The table of Estimated Quantities represents the quantities used by the Engineer in preparing the cost estimate. Payment for the Bridge will be considered completely covered by the contract Lump sum price. Variations may be encountered in the estimated quantities but the variations cannot be used for adjustment in the contract Lump sum price.

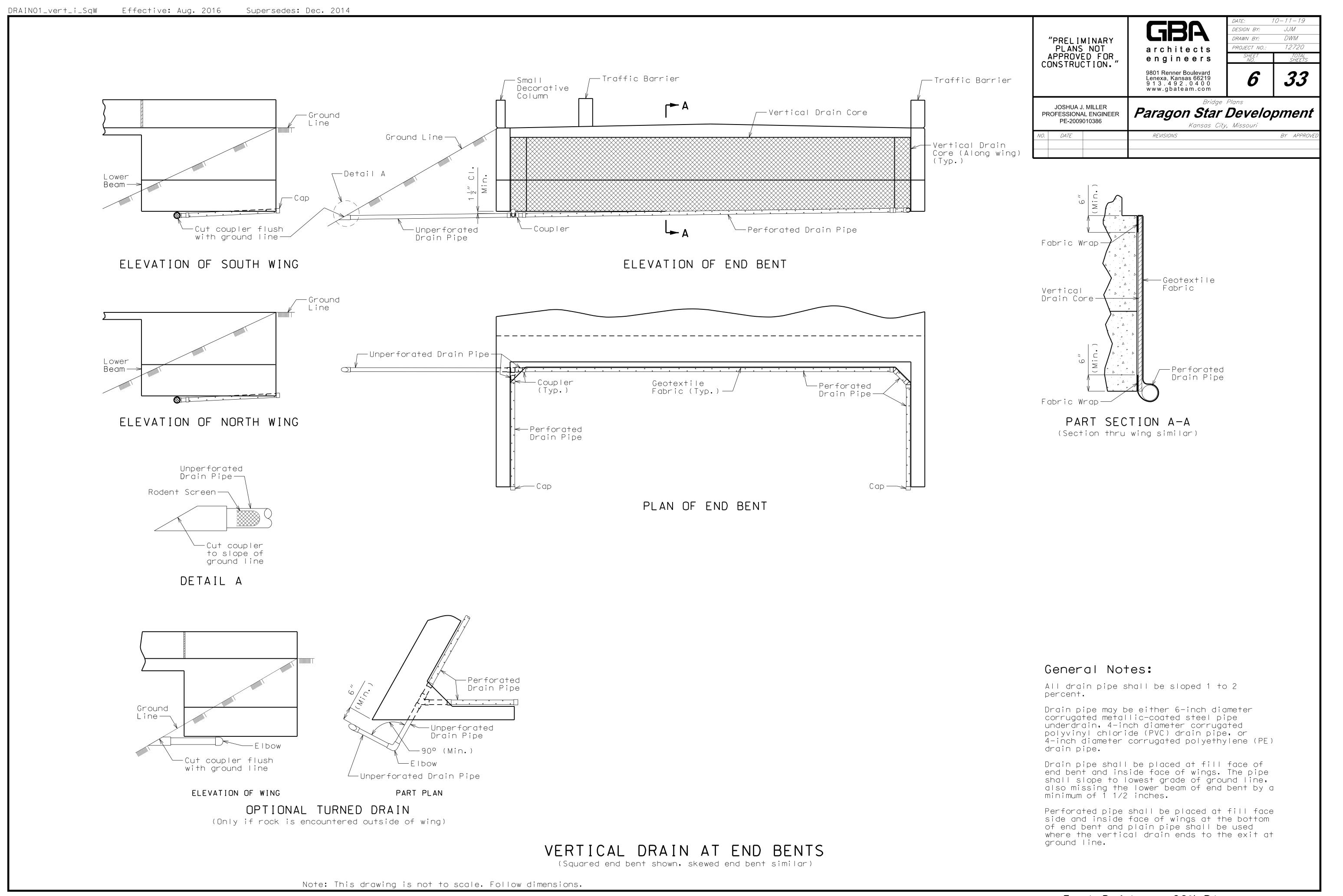
Method of forming the slab shall be as shown on the plans and in accordance with Sec 703. All hardware for forming the slab to be left in place as a permanent part of the structure shall be coated in accordance with ASTM A123 or ASTM B633 with a thickness class SC 4 and a finish type I, II, or III.

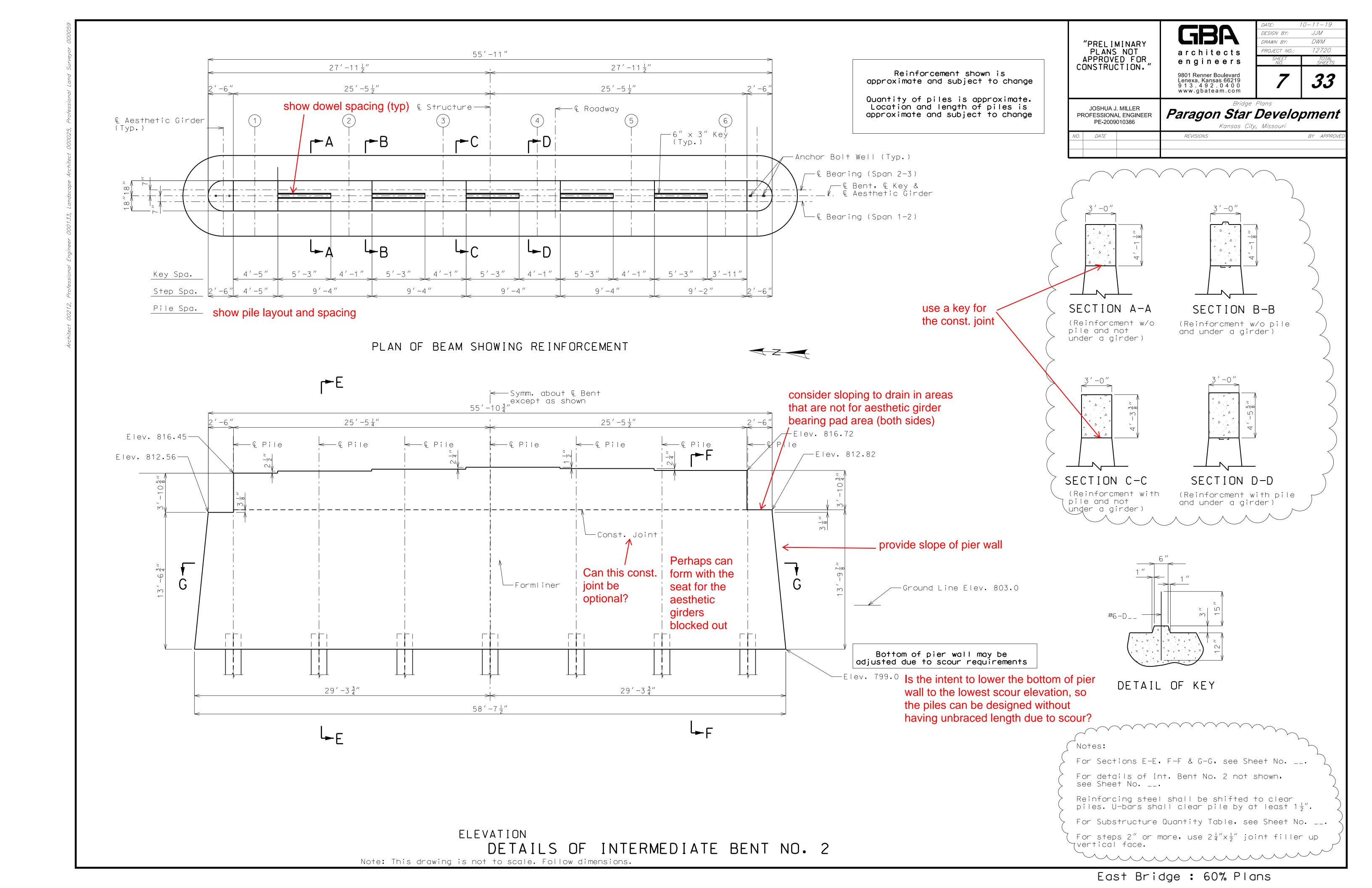
GENERAL NOTES AND QUANTITIES

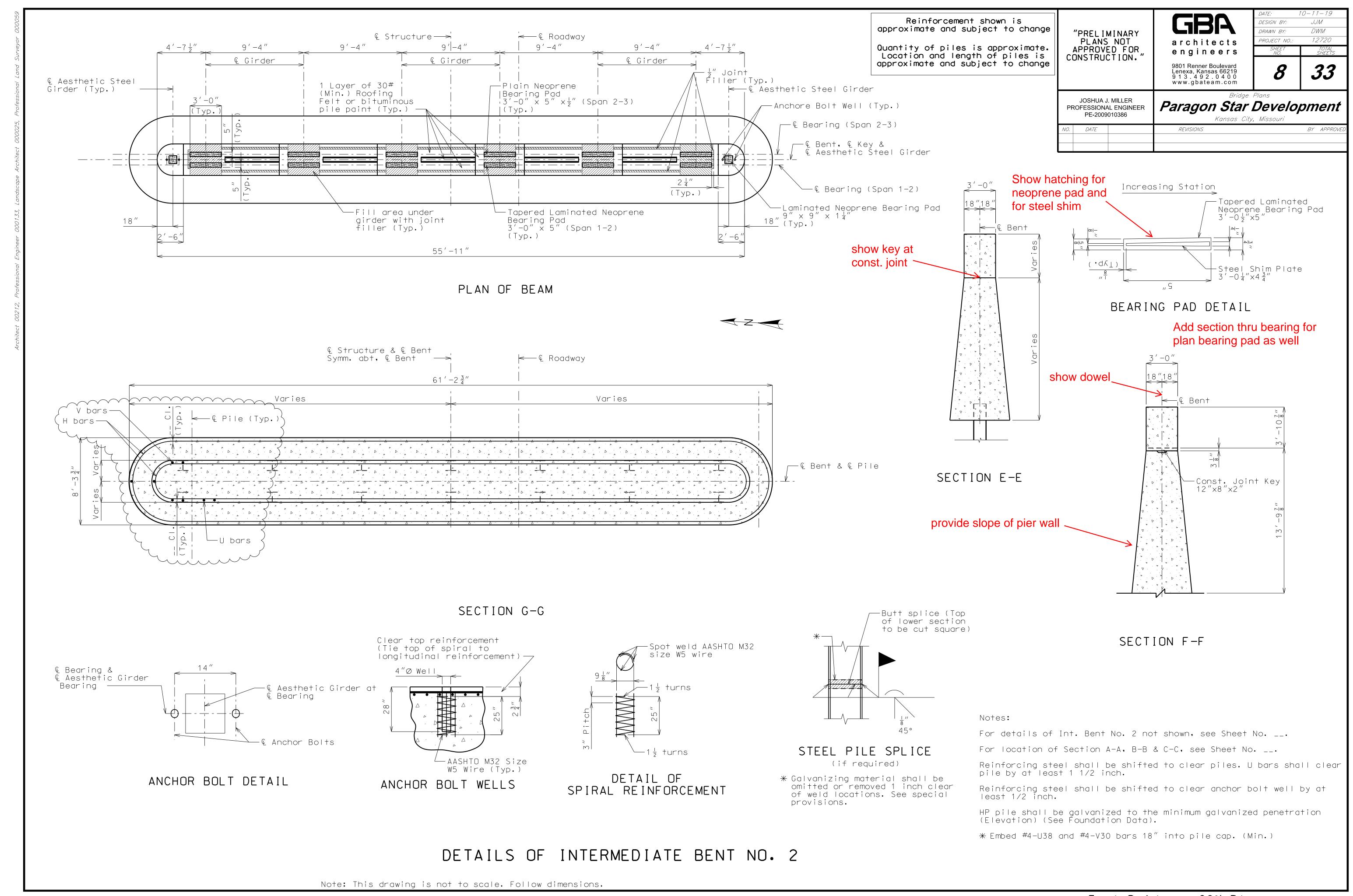


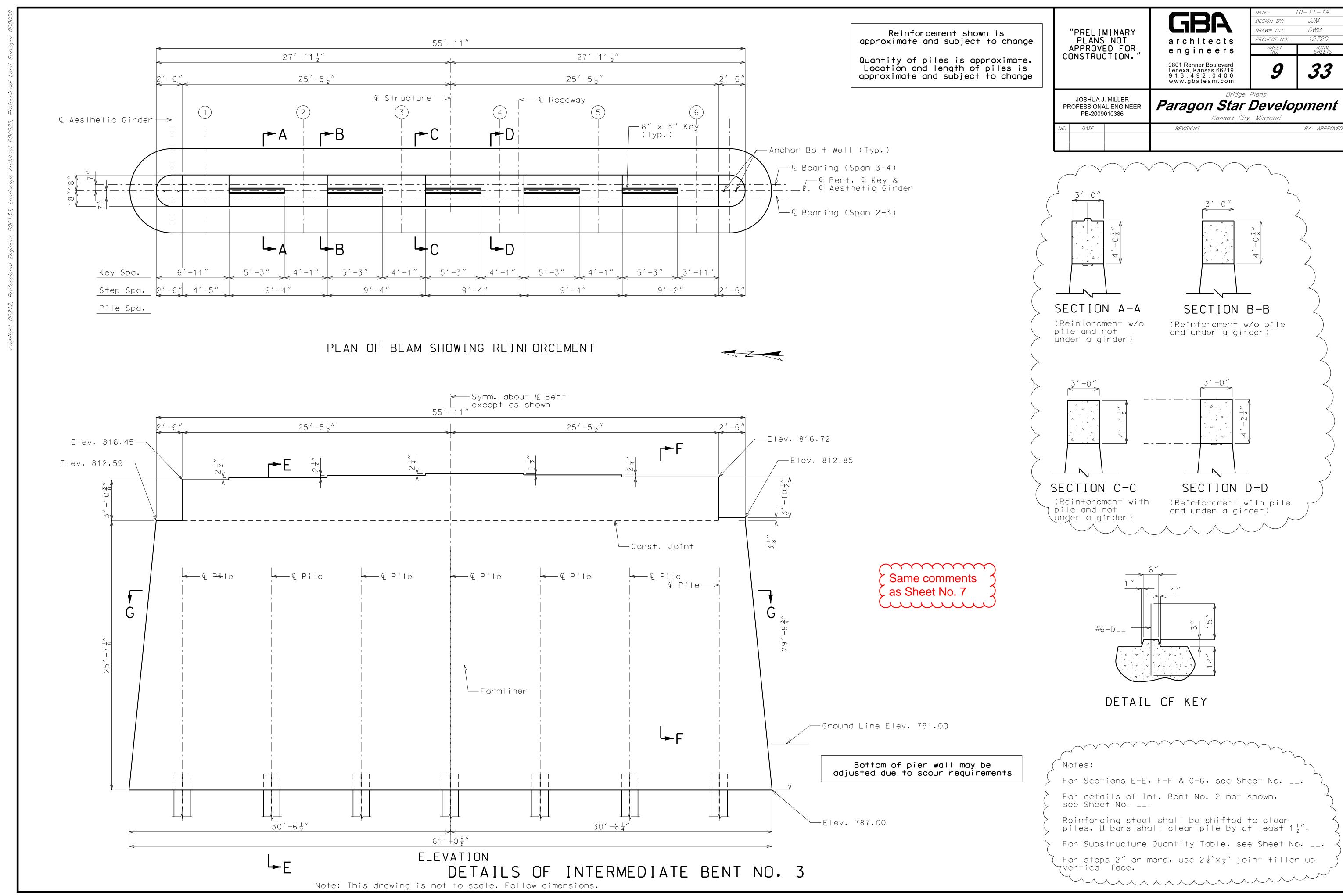


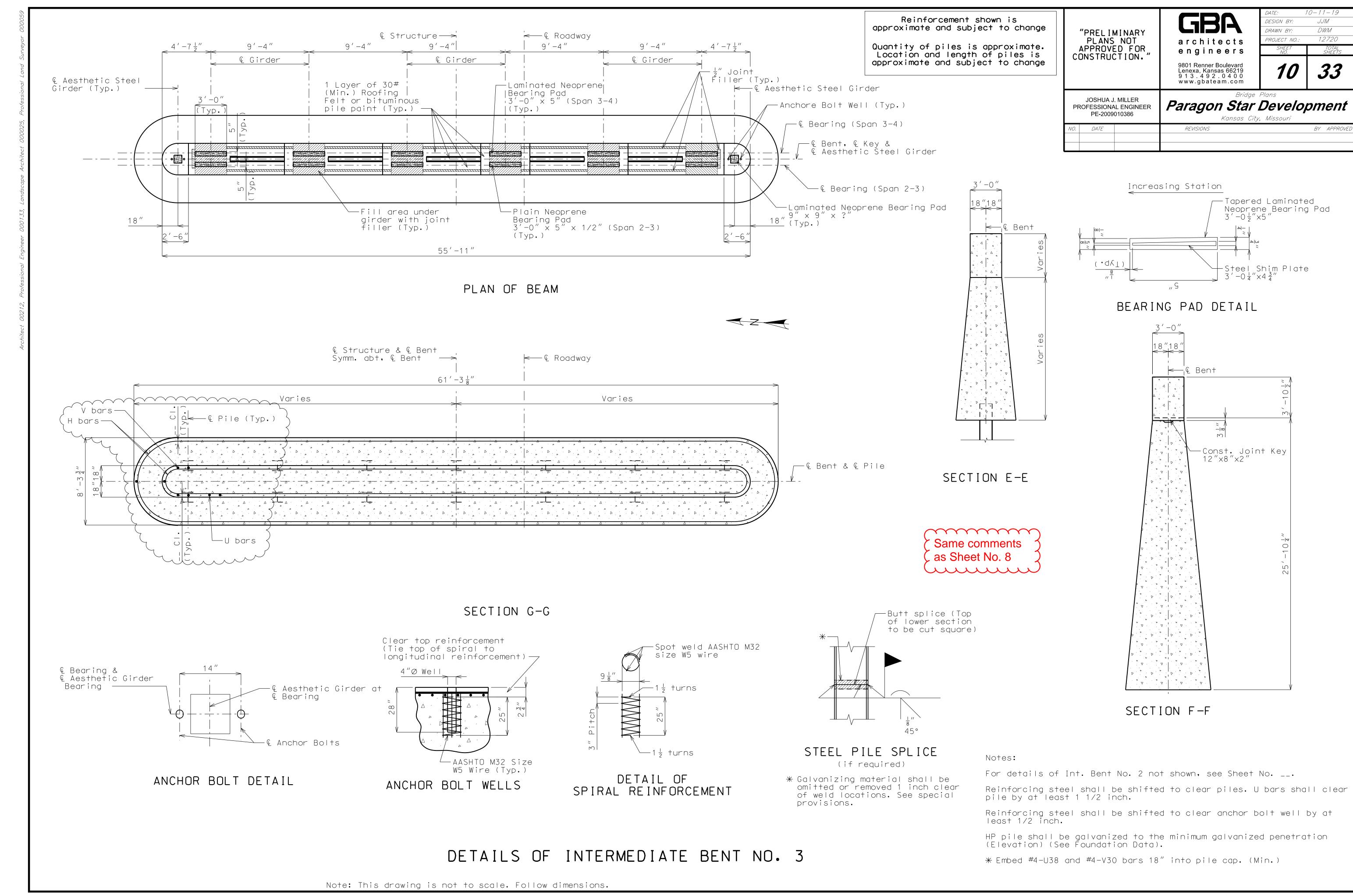


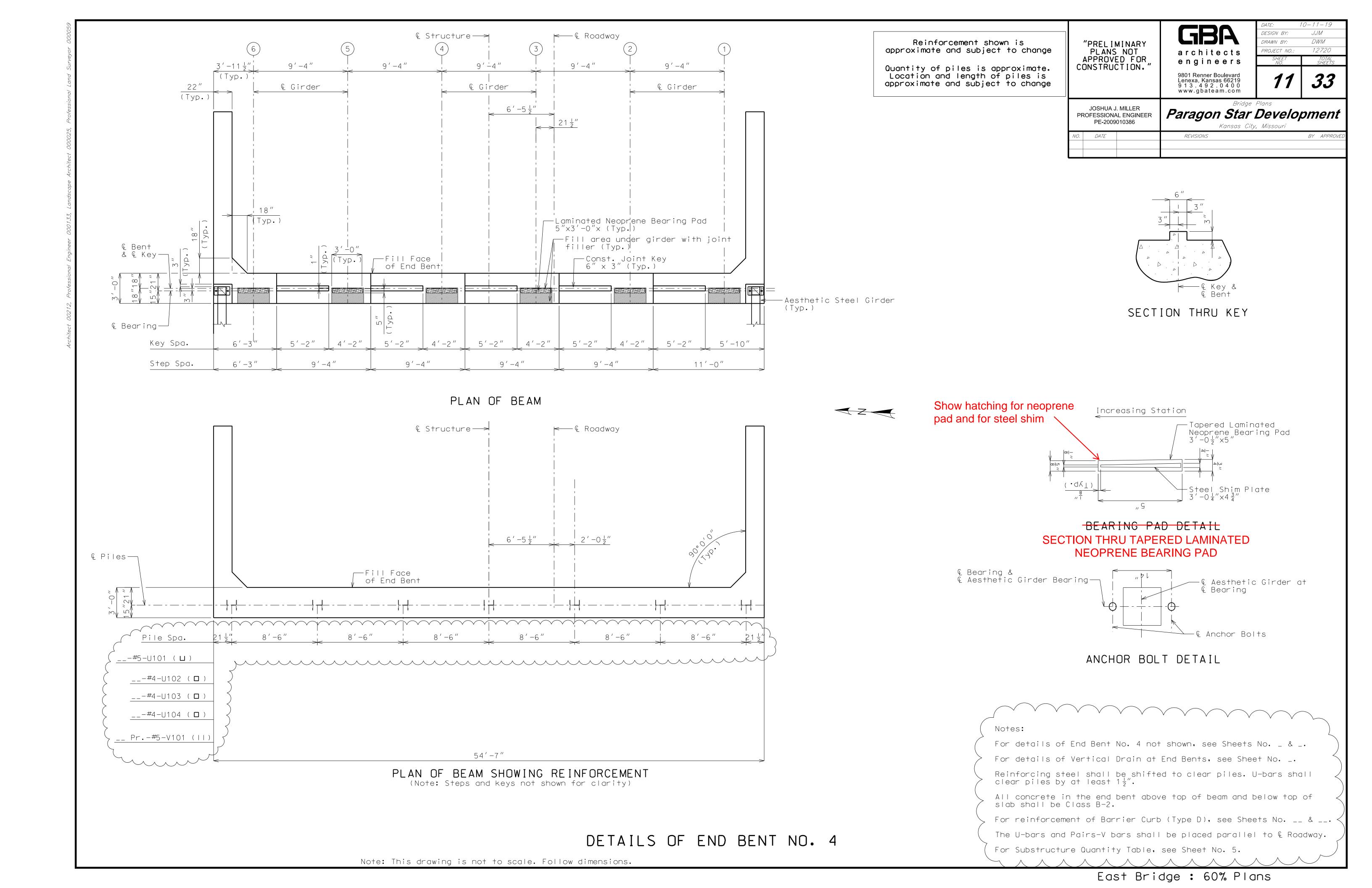


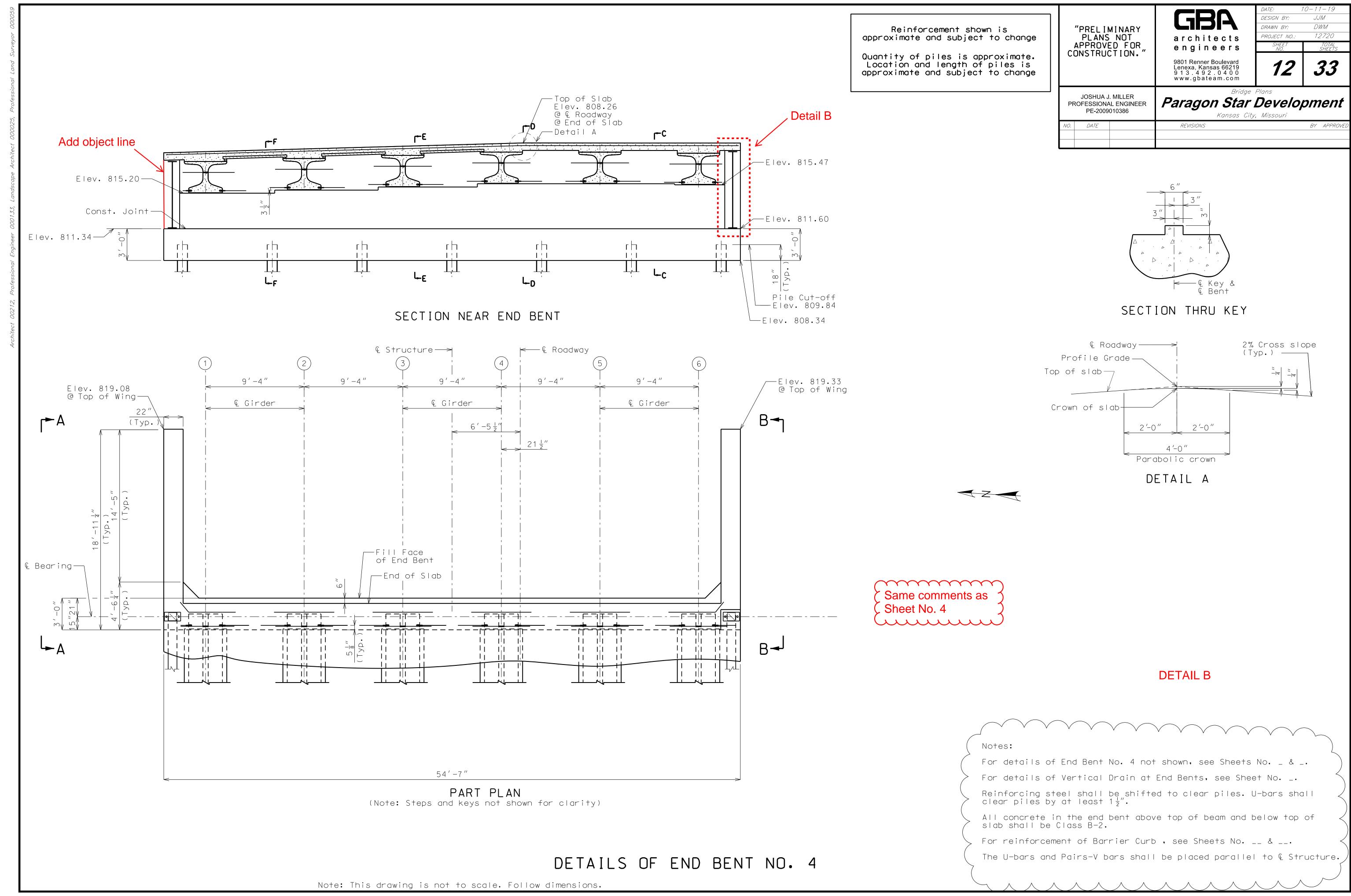


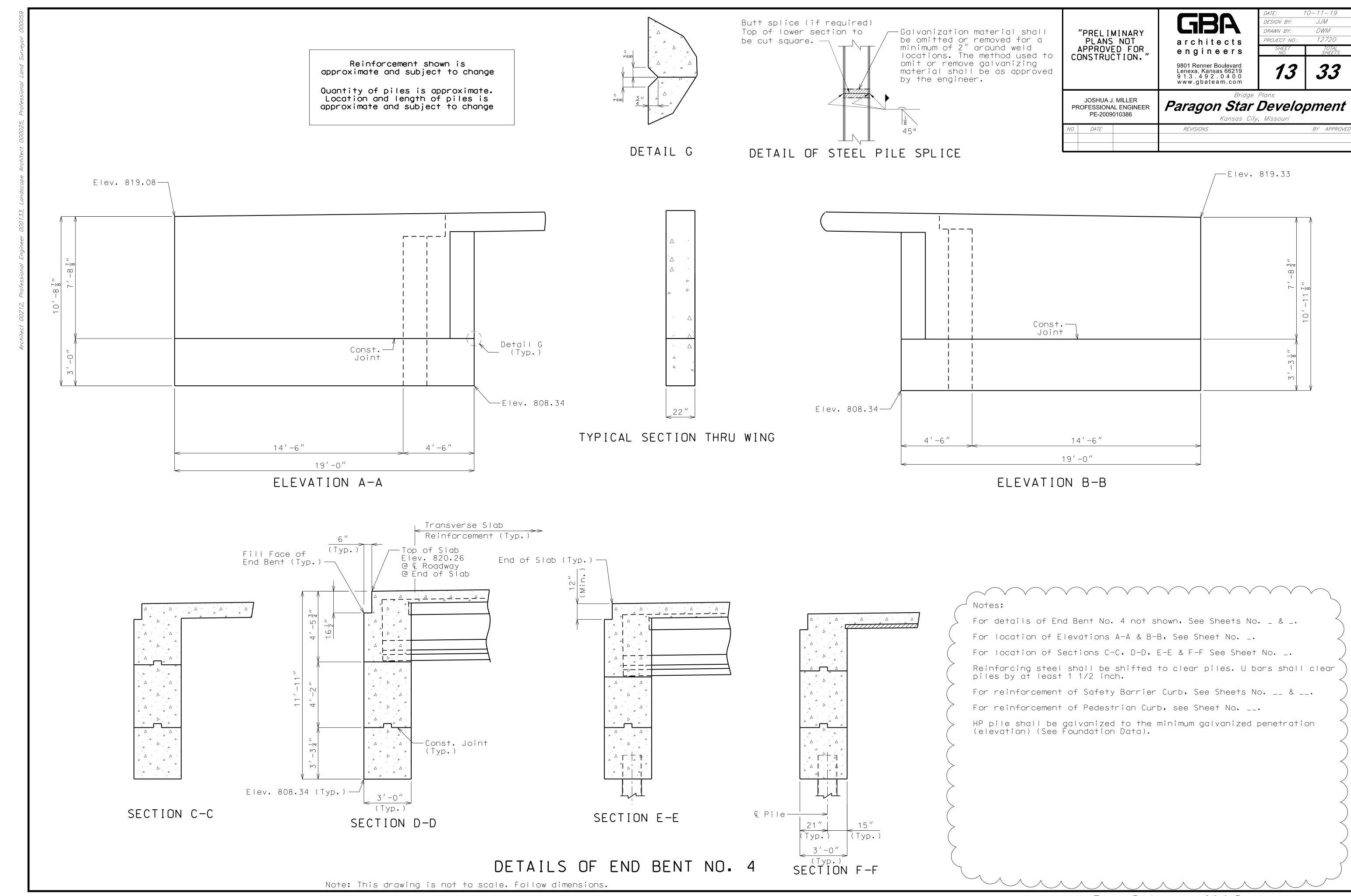














JOSHUA J. MILLER

PROFESSIONAL ENGINEER

GBA architects engineers

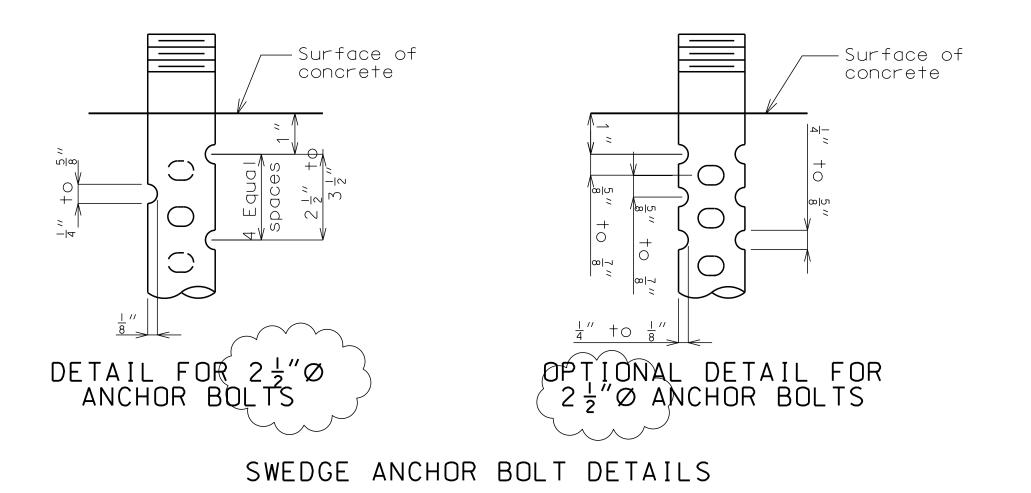
DESIGN BY: JJM DWM DRAWN BY: 12720 *33*

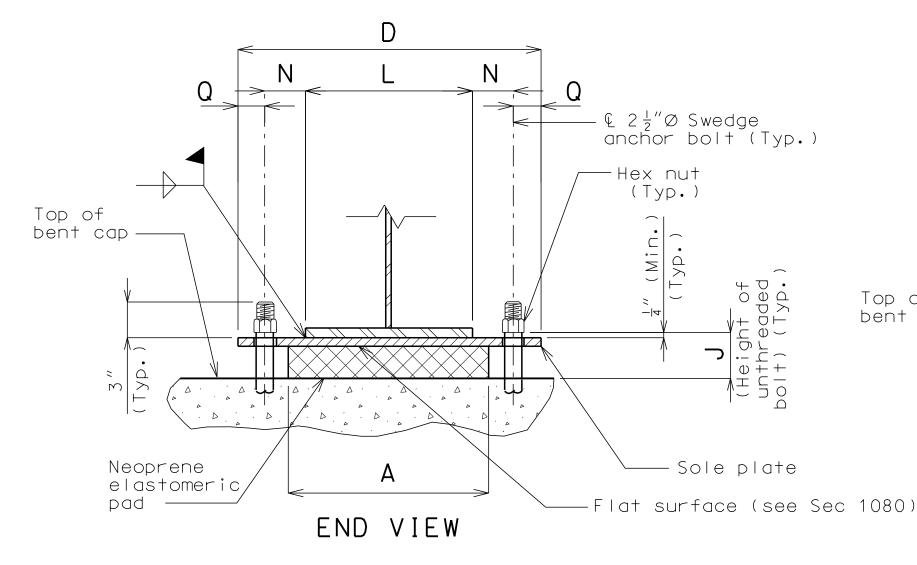
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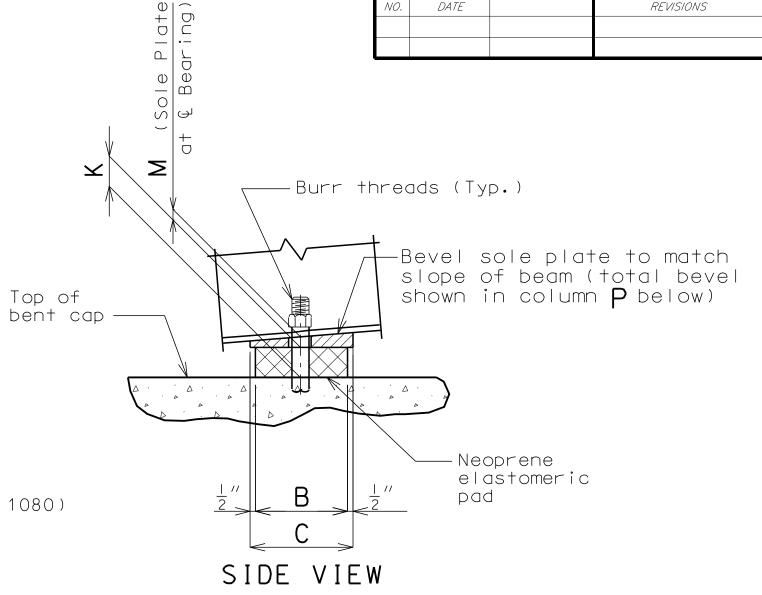
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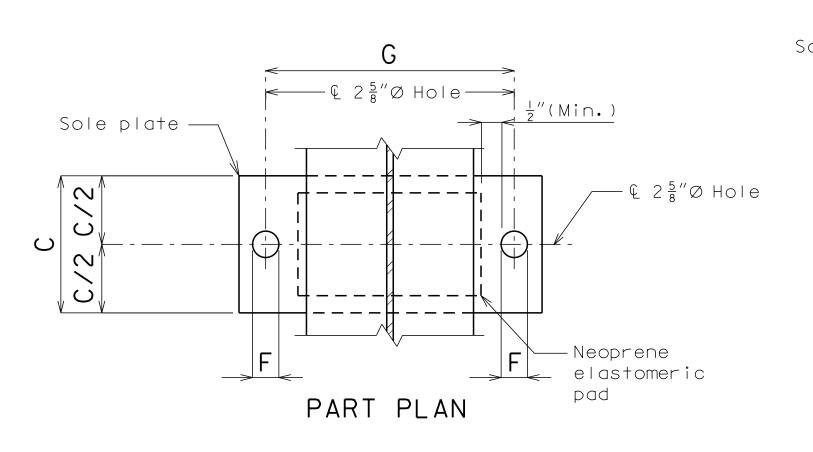
Paragon Star Development

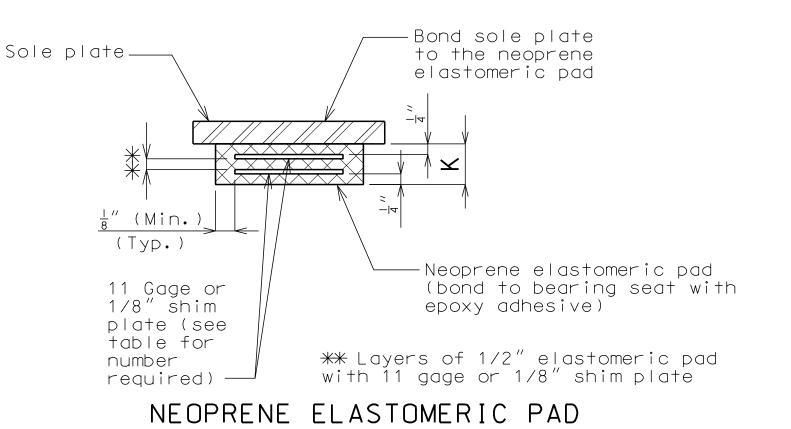
PE-2009010386 REVISIONS











								F	IXE	D BE	ARI	NGS	· >		
BENT NO.	А	В	С	D	F	G	J	K	L	М	N	Р	Q	NUMBER OF SHIM PLATES *	NUMBER REQUIRED
1	9 "	9 "	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	"	2 ½ "	X	2
2	9 "	9 "	10"	18 ½"	2 5 "	14"	6 ½"	4 3/8	10"	1 ½"	2 "	''	2 ¼"	X	2
3	9 "	9 "	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	"	2 ½ "	X	2
4	9 "	9"	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	′′	2 ¼"	X	2
	* Th	e re	quire	d shim p	olate	shall	be p	olace	d be-	tween	layer	s of	_	TOTAL BEARINGS	8 .
	R I	astor	mer a	nd,molde	ed to	gether	+0 -	form	an ir	ntegra	l ūni ∧ ∧	+.			

GENERAL NOTES:

Anchor bolts shall be $2\frac{1}{2}$ "Ø ASTM F1554 Grade 55 swedged bolts and shall extend 25" into the concrete with ASTM A563 Grade A Hex or Heavy Hex nuts. Actual manufacturer's certified mill test reports (chemical and mechanical) shall be provided. Swedging shall be 1" less than extension into the concrete.

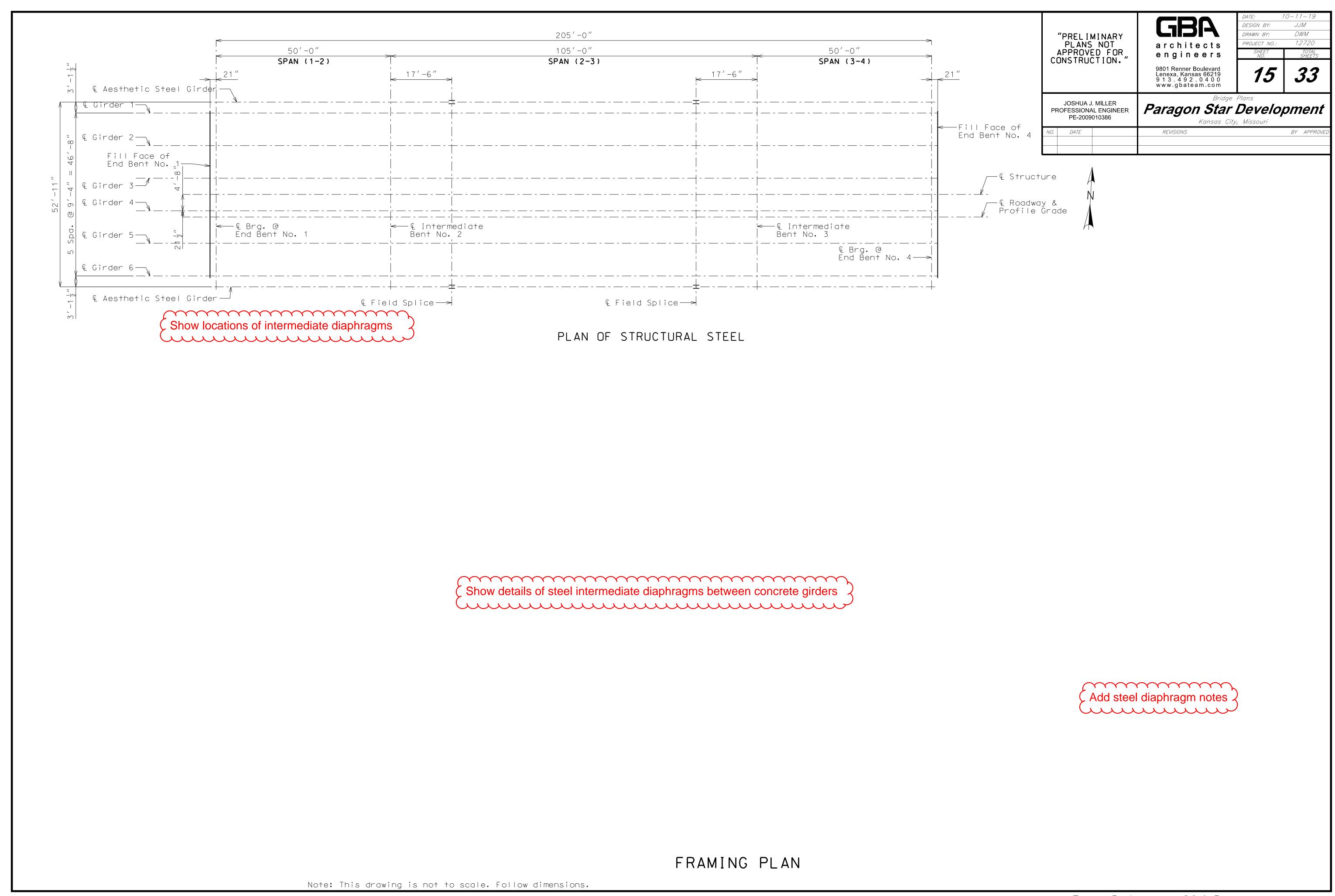
All structural steel for the anchor bolts and heavy hexagon nuts shall be coated with a minimum of two coats of inorganic zinc primer (5 mils minimum).

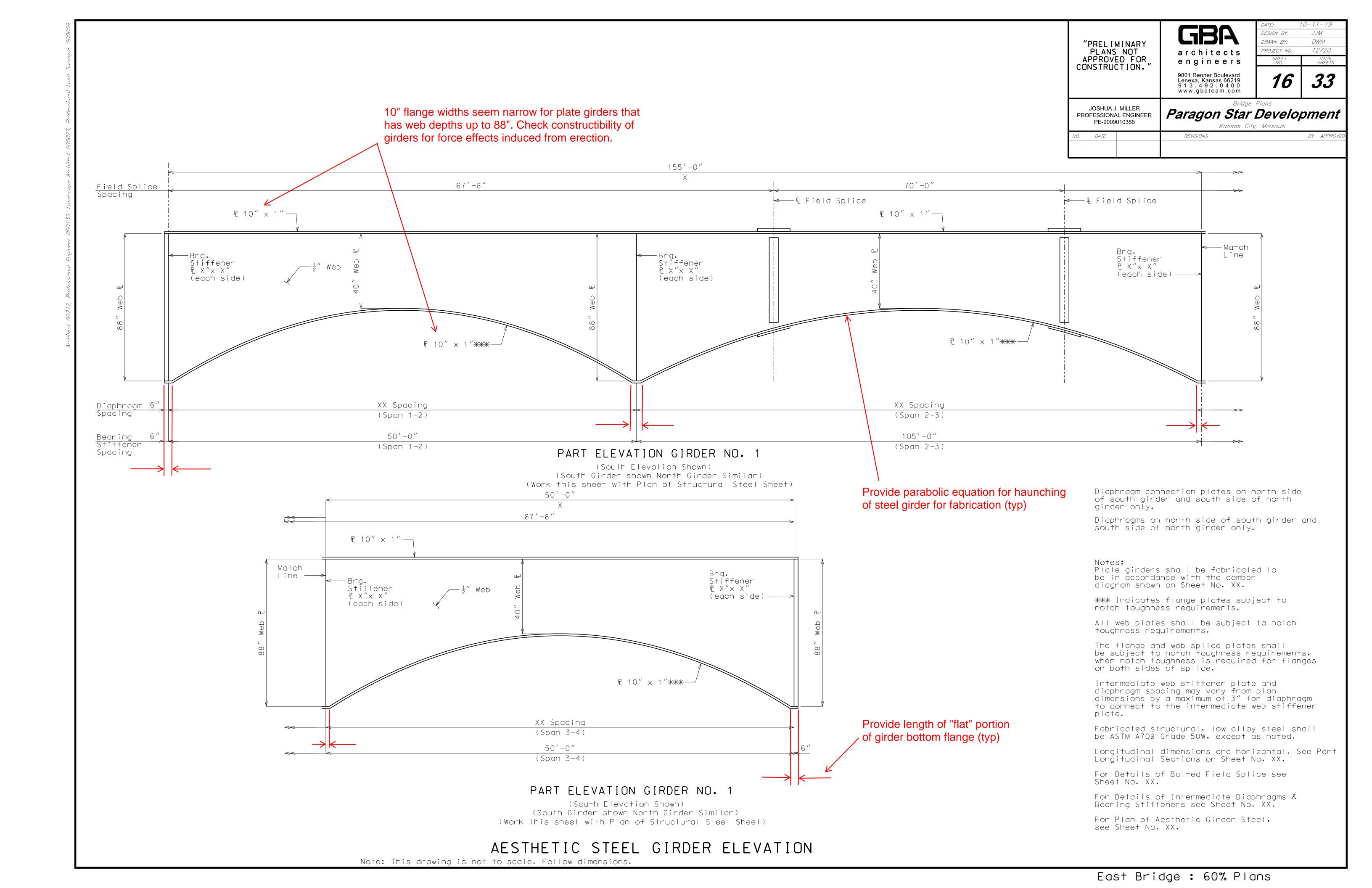
Neoprene Elastomeric Pads shall be 60 Durometer.

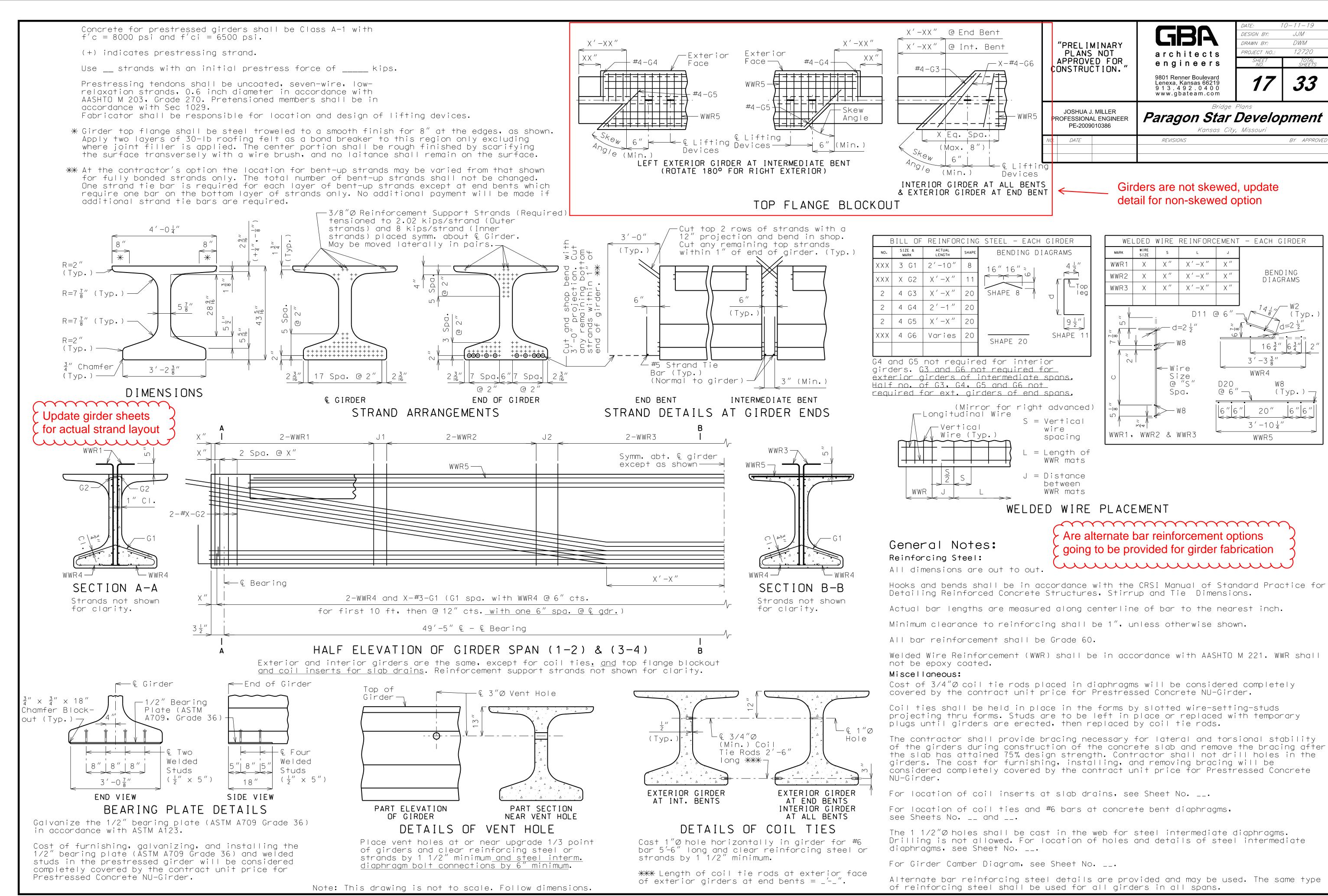
Structural steel for sole plate shall be ASTM A709 Grade 50W. The welds shall have corrosion resistance and weathering characteristics compatible with the base material.

Laminated Neoprene Bearing Pad Assembly shall be in accordance with Sec

DETAILS OF LAMINATED NEOPRENE BEARING PAD ASSEMBLY



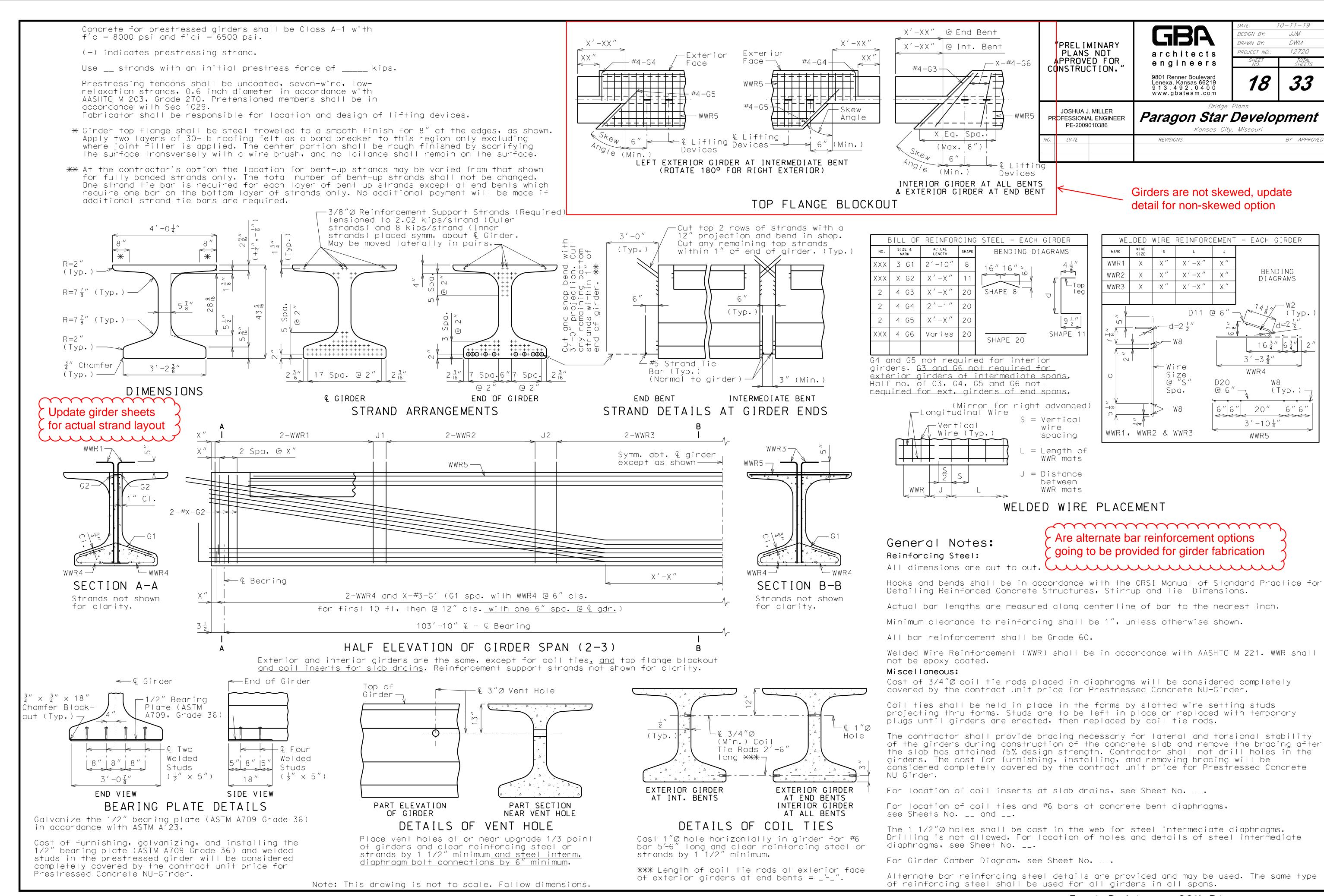




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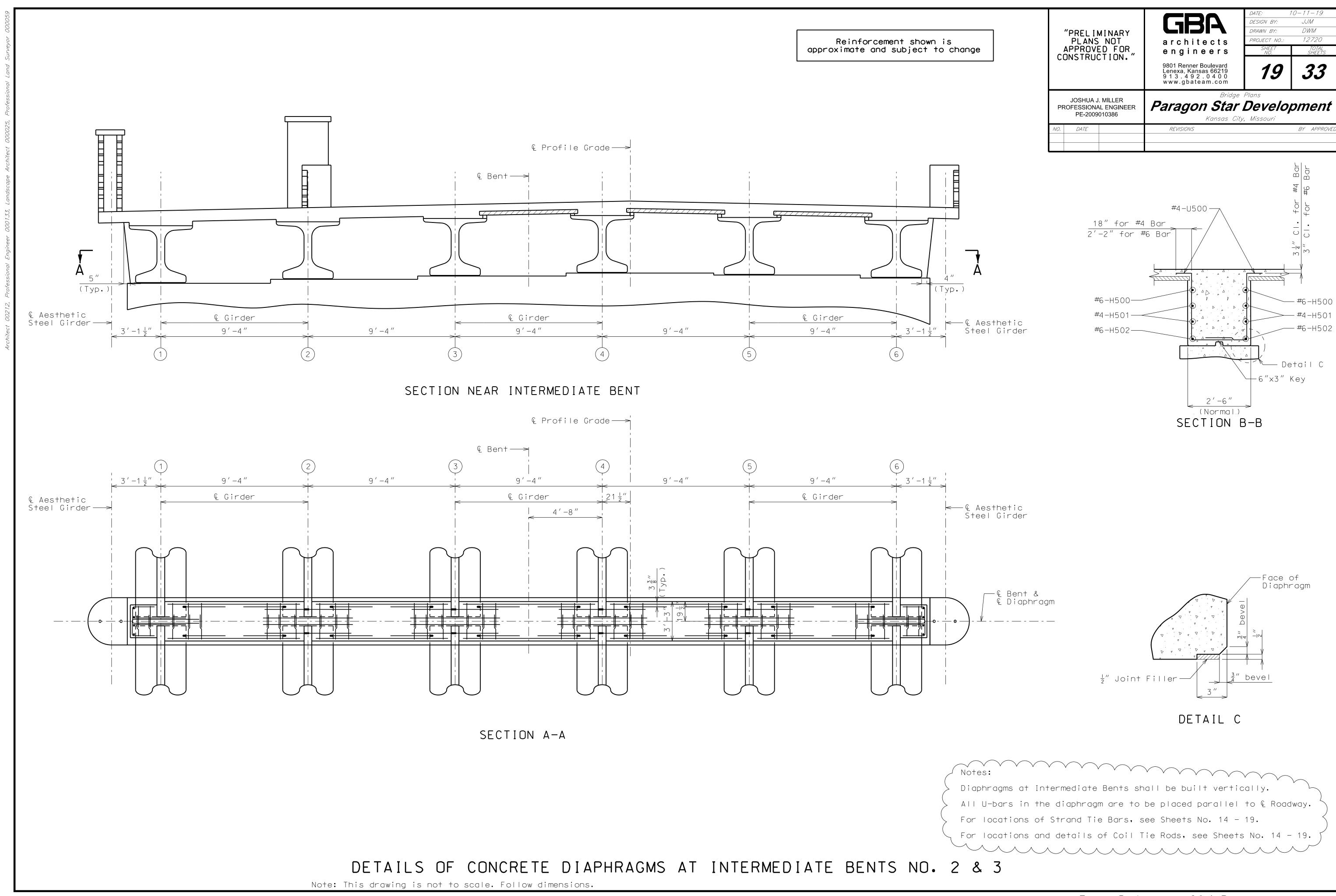
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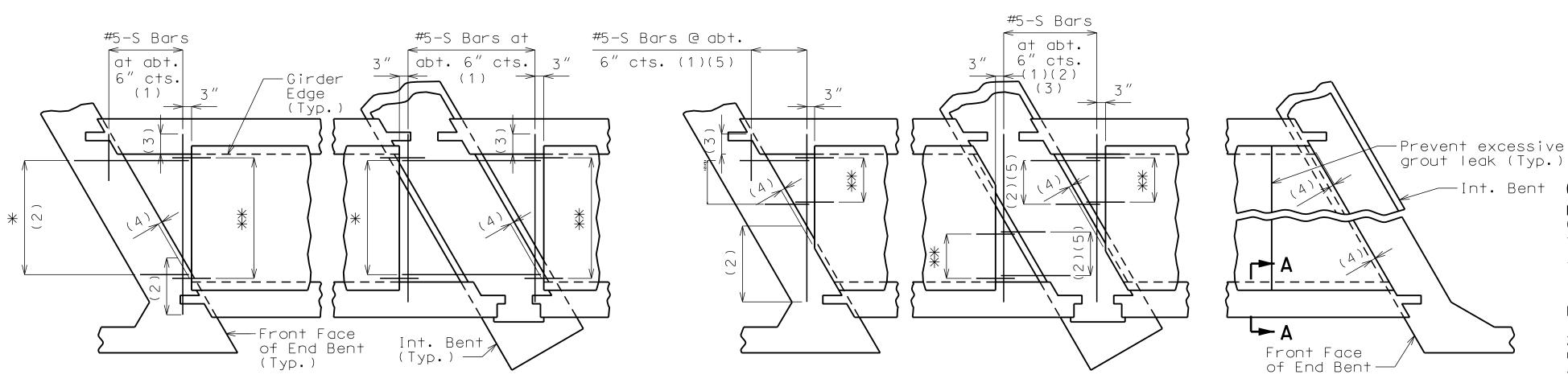


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SQUARED END PANELS OR TRUNCATED END PANELS

L/4 : L/4 : L/4 : L/4

© Strand

 $\frac{1}{2}$ " (Min.)

M M X

 ∞ \leftarrow

DW)

 $\frac{1}{2}$ " (Min.)

(Max.)

2/m

BENDING DIAGRAM FOR U1 BAR

U1 Bars may be oriented at right angles to location and spacing shown. U1 Bars shall

#3-P2 at abt.

6" cts. at top

Panel Width

SECTION B-B

(10) —

#3-P2 at abt.

6" cts. at top

Panel Width

*** 3" (Min.), 6" (Max.)

PLAN OF OPTIONAL TRUNCATED END PANEL

be placed between P1 bars.

5-#3-P3 at 6" cts.

between P2 bars (8)

#3-P1 at 12" cts.

at top (6)

3" (Min.)

(Typ.)

3/8″Ø

Strand—

 $1\frac{1}{2}''$ (Min.

3" (Max.)

May be cast

sawn to skew-

× D X

 $\infty \sqrt{}$

 $1\frac{1}{2}''$ (Min.)

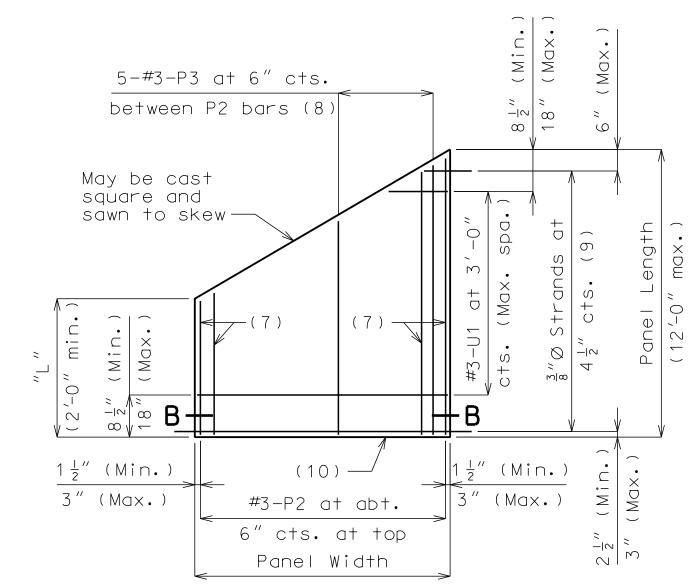
3" (Max.)

B#

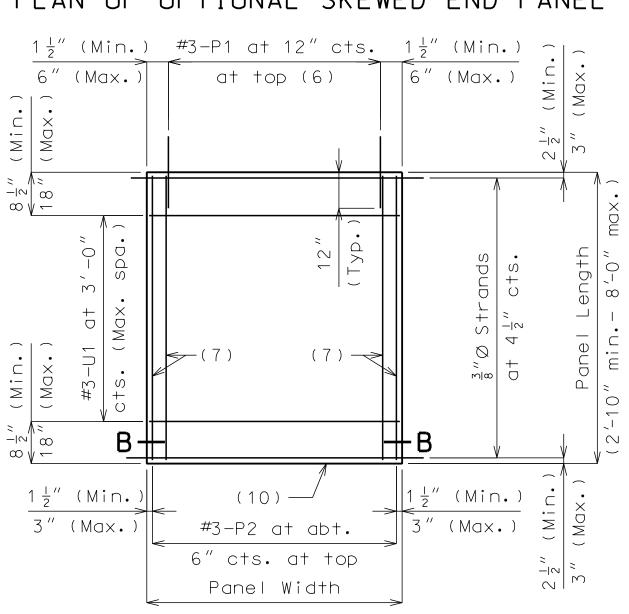
square and

PLAN SHOWING PANELS PLACEMENT

* #5-S Bars at abt. 9" cts. (1)
** #3-P1 at 12" cts. (End panels only)



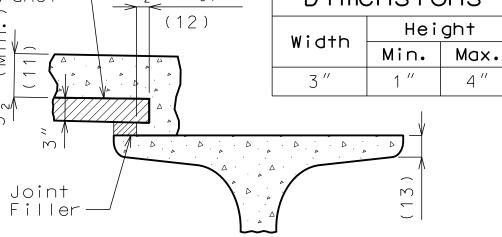
PLAN OF OPTIONAL SKEWED END PANEL



PLAN OF SQUARED PANEL

Joint Filler $1\frac{1}{2}''$ (Typ.) Dimensions Panel

SKEWED END PANELS



SECTION A-A

Reference Notes:

Plan of Panels Placement:

(1) S-bars shown are bottom steel in slab between panels and used with squared and truncated end panels only.

of end bents and int. bents for squared and truncated end panels only.

(3) Extend S-bars 9 inches beyond edge of girder (Typ.).

(4) End panels shall be dimensioned 1/2" min. to 1 1/2" max. from the inside face of diaphragm.

(5) For truncated end panels, use a min. of #5-S than 2 feet. bars at 6" crossings in openings, or min. $4 \times 4 - W7 \times W7$.

Plans of Panels:

(6) For end panels only, P1 bars shall be 2'-0'' in length and embedded 12". P1 bars will not be

(7) #3-P2 bars near edge of panel at bottom (under strands).

(8) Use #3-P3 bars if panel is skewed 45° or greater.

(9) Any strand 2'-0'' or shorter shall have a #4 reinforcing bar on each side of it, centered between strands. Strands 2'-0" or shorter may then S-bars are not listed in the bill of reinforcing. be debonded at the fabricator's option.

(10) Optional 1/2" x 45° Chamfer one or both sides at bottom.

Section A-A:

(11) Slab thickness over prestressed panels varies due to girder camber. In order to maintain Use Slab Haunching Diagram on Sheet No. XX for determining thickness of joint filler minimum slab thickness, it may be necessary to raise the grade uniformly throughout the

labor or materials required for necessary grade adjustment.

under and between panels.

(13) At the contractor's option, the variation in top of flange. slab thickness over prestressed panels may be eliminated or reduced by increasing and varying the girder top flange thickness. Dimensions shall be shown on the shop drawings.

DETAILS OF PRESTRESSED PANELS

-Int. Bent **General Notes:**

Prestressed Panels: Concrete for prestressed panels shall be Class A-1 with f'c = 6,000 psi, f'ci = 4.000 psi.

The top surface of all panels shall receive a scored finish with a depth of scoring of 1/8" perpendicular to the prestressing strands in the panels.

"PREL IMINARY

PLANS NOT

APPROVED FOR

JOSHUA J. MILLER

PROFESSIONAL ENGINEER PE-2009010386

DATE

CONSTRUCTION.

GBA

architects

engineers

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SHEETS

DESIGN BY

DRAWN BY:

Paragon Star Development

PROJECT NO.:

Prestressing tendons shall be high-tensile strength, uncoated, seven-wire, low-relaxation strands for prestressed concrete in accordance with AASHTO M 203 Grade 270, with nominal diameter of strand = 3/8" and nominal area = 0.085 sq.in. and minimum ultimate strength = 22.95 kips (270 ksi). Larger strands may be used with the same spacing and initial tension.

Initial prestressing force = 17.2 kips/strand.

The method and sequence of releasing the strands shall be shown on the shop drawings.

Suitable anchorage devices for lifting panels may be cast in panels, provided the devices are shown on the shop drawings and approved by the engineer. Panel lengths shall be determined by the contractor and shown on the shop drawings.

When squared end panels are used at skewed bents, the skewed portion shall be cast full depth. No separate payment will be made for additional concrete and reinforcing required.

Support from diaphragm forms is required under the optional skewed end until cast-in-place concrete has reached 3,000 psi compressive strength.

Prestressed panels shall be brought to saturated surface-dry (SSD) condition just prior to the deck pour. There shall be no free standing water on the panels or in the area to

The prestressed panel quantities are not included in the table of estimated quantities for the slab. Reinforcing Steel:

All dimensions are out to out.

Hooks and bends shall be in accordance with the CRSI Manual of Standard Practice for Detailing Reinforced Concrete Structures, Stirrup and Tie Dimensions.

(2) Extend S-bars 18 inches beyond the front face Minimum clearance to reinforcing steel shall be 1 1/2", unless otherwise shown.

If U1 bars interfere with placement of slab steel, U1 loops may be bent over, as necessary, to clear slab steel.

Deformed welded wire reinforcement (WWR) providing a minimum area of reinforcing perpendicular to strands of 0.22 sq in./ft, with spacing parallel to strands sufficien to ensure proper handling, may be used in lieu of the #3-P2 bars shown. Wire diameter shall not be larger than 0.375 inch. The above alternative reinforcement criteria may be used in lieu of the #3-P3 bars, when required, and placed over a width not less

The following reinforcing steel shall be tied securely to the strands with the following maximum spacing in each direction: #3-P2 bars at 16 inches.

WWR at 24 inches.

required for panels at squared integral end bents. The #3-U1 bars shall be tied securely to #3-P2 bars, to WWR or to strands (when placed between P1 bars) at about 3-foot centers.

Minimum reinforcement steel length shall be 2'-0".

All reinforcement other than prestressing strands shall be epoxy coated.

Precast panels may be in contact with stirrup reinforcing in diaphragms.

Cost of S-bars will be considered completely covered by the contract unit price for the slab.

Joint Filler: Joint filler shall be preformed fiber expansion joint material in accordance with Sec 1057 or expanded or extruded polystyrene bedding material in accordance with

Sec 1073.

within the limits noted in the table of Joint Filler Dimensions.

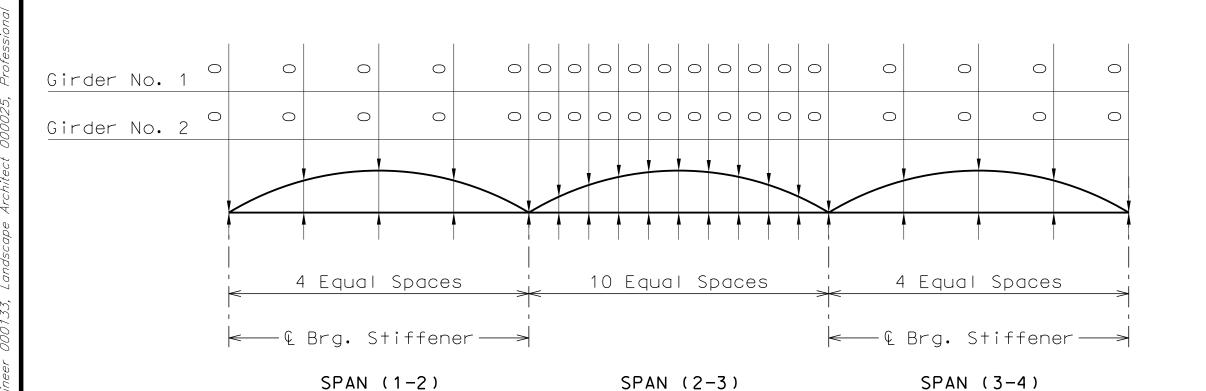
structure. No payment will be made for additional Thicker material may be used on one or both sides of the girder to reduce cast-in-place concrete thickness to within tolerances.

The same thickness of preformed fiber expansion joint material shall be used under any (12) Contractor shall ensure proper consolidation one edge of any panel except at locations where top flange thickness may be stepped. The maximum change in thickness between adjacent panels shall be 1/4 inch. The polystyrene bedding material may be cut with a transition to match haunch height above

> Joint filler shall be glued to the girder. When thickness exceeds 1 1/2 inches, the joint filler shall be glued top and bottom. The glue used shall be the type recommended by the joint filler manufacturer.

Edges of panels shall be uniformly seated on the joint filler before slab reinforcement is placed.

Note: This drawing is not to scale. Follow dimensions.



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Bridge Plans

Paragon Star Development
Kansas City, Missouri

NO. DATE

REVISIONS

PARAPROVED

architects engineers

"PRELIMINARY

PLANS NOT APPROVED FOR CONSTRUCTION." JJM

DWM

12720

DESIGN BY:

DRAWN BY:

PROJECT NO.:

CAMBER DIAGRAM

Note:
Camber includes allowance for vertical curve and for dead load deflection due to concrete slab, barrier curbs, pedestrian curb and structural steel.

Longitudinal dimensions are measured horizontally.

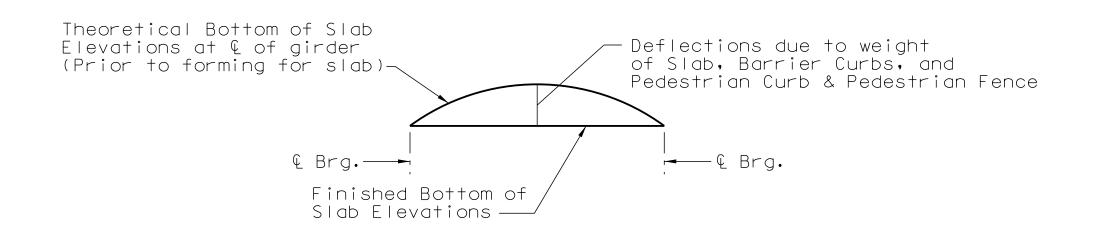
"+" Downward from chord "-" Upward from chord DEAD LOAD DEFLECTION

Note:

15% of dead load deflection is due to the weight of structural steel.

Dead Load deflection includes weight of structural steel, concrete slab, barrier curbs, and pedestrian curb & pedestrian fence.

GIRDER NO.	SPAN LEN	GTHS (& Brg & Brg.)							
GIRDER NO.	Span (1-2)	Span (2-3)	Span (3-4)						
1	′″	′″	'"						
2	′′′	′′	′′′						



*** heoretical Bottom of Slab Elevations at (& of Girder (Prior to forming for slab)
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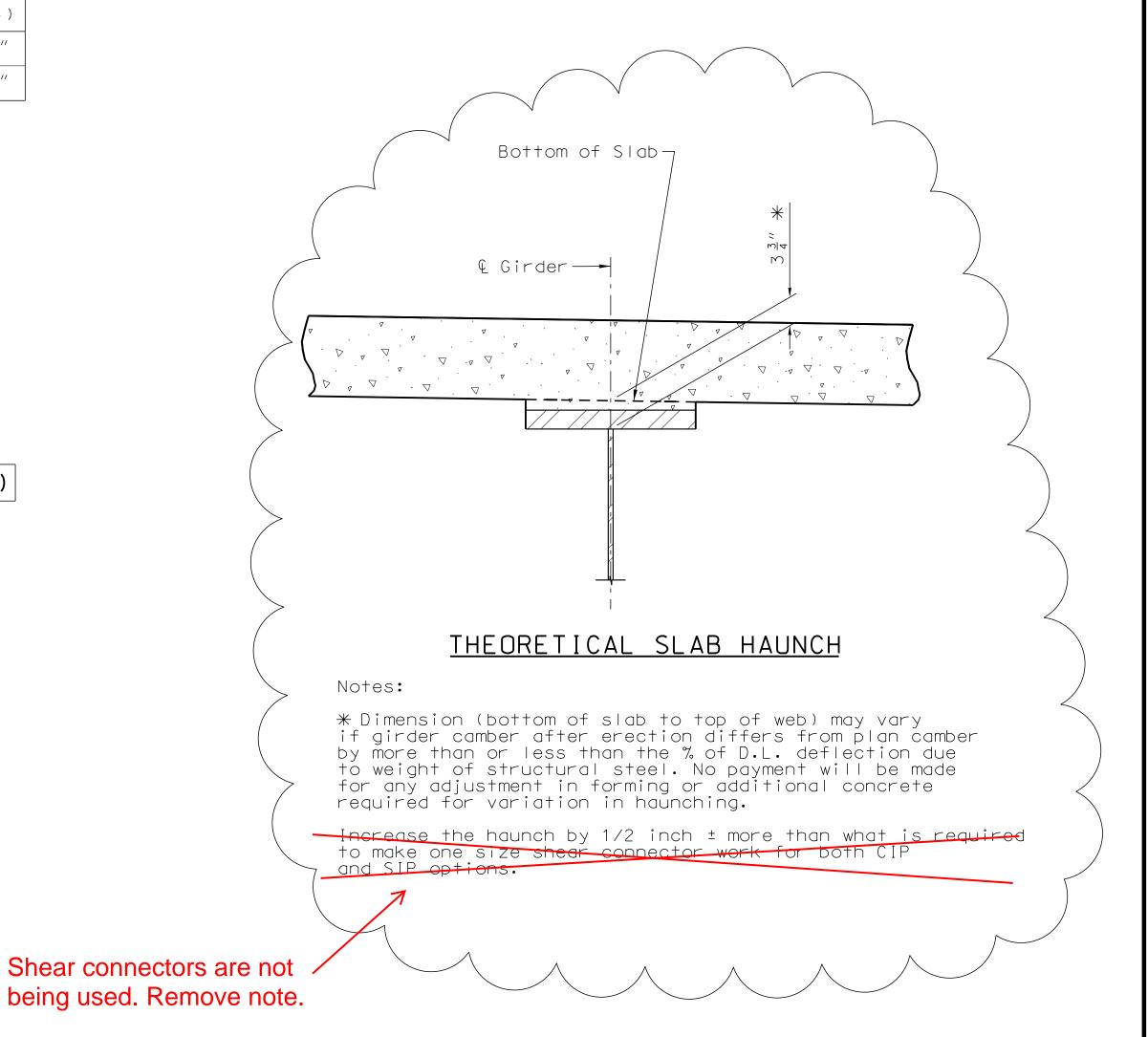
Span 1 (& Brg.-& Brg.)

TYPICAL SLAB ELEVATIONS DIAGRAM

			No.	Ber	it No. 1	.25	.50	.75	Bent No	0. 2		
			1	_	•	•	•	•				
			2	_	•	•	•	•	•			
						Span 2 (€ Brg€	Brg.)				
Gdr. No.	& Brg Bent No. 2	. 1	0	.20	.30	.40	.50	.60	.70	.80	.90	& Brg Bent No. 3
1	•	•		- •	•	•	•	•	•	•	•	•
2	•	•		_•	·	•	•	•	•	•	•	•
						Span 3 (€ Brg€	Brg.)				
			Gdr. No.	€ E Ber	Brg it No. 3	.25	.50	.75	€ Brg Bent No	0. 4		

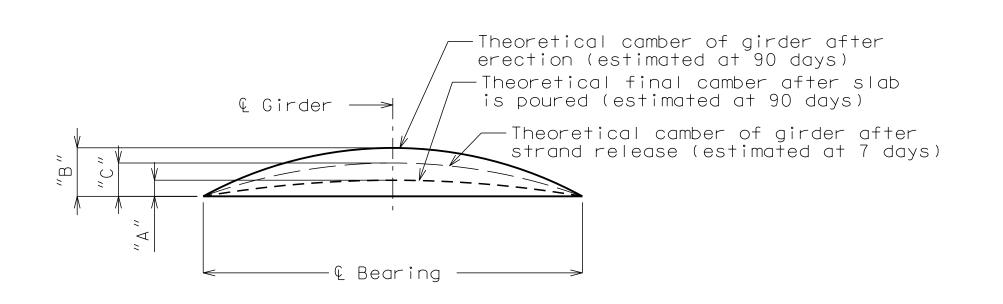
** Elevations are based on a constant slab thickness of $8\frac{1}{2}$ " and include allowance for theoretical dead load deflections due to weight of Slab, Barrier Curbs, and Pedestrian Curb & Pedestrian Fence.

___.



CAMBER, HAUNCHING, & ELEVATIONS (STEEL)

Note: This drawing is not to scale. Follow dimensions.



	S	pan (1-2	2)	S	pan (2-3	3)	Span (3-4)				
	"A"	"B"	"C"	"A"	"B"	"C"	″A ″	"B"	"C"		
Ext. Beam	<u> ''</u>	<u>3</u> //	<u>1</u> "	<u>3</u> //	2 ¼"	1 ½"	<u>5</u> //	1 "	7 ′′		
Int. Beam	<u> "</u> "	8	4	<u>3</u> //	<u> </u>	4	<u>5</u> //	1 2	8		

GIRDER CAMBER DIAGRAM

Conversion factors for girder camber (Estimated at 90 days)

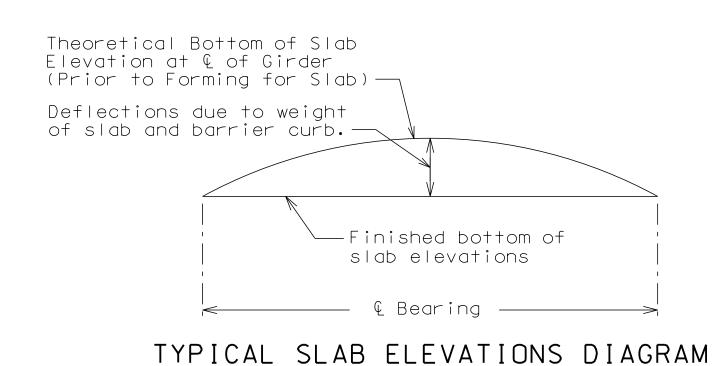
0.1 pt. = 0.314 x 0.5 pt.

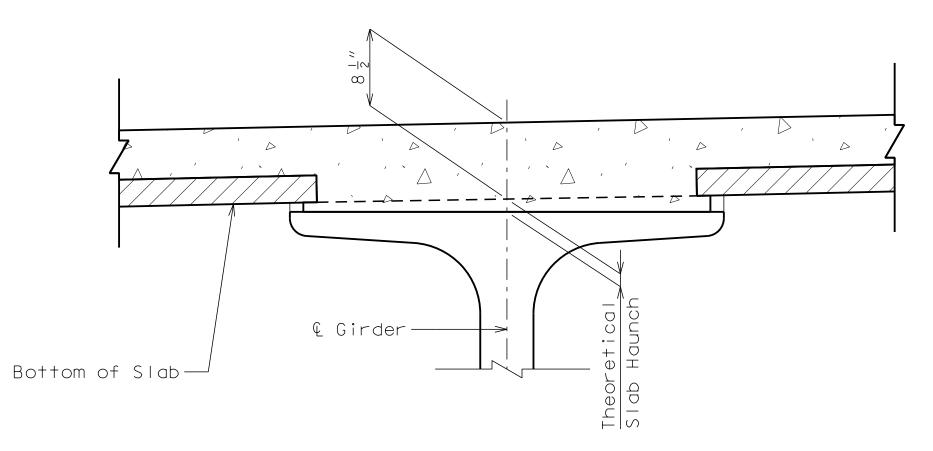
0.2 pt. = 0.593 x 0.5 pt.

0.25 pt. = 0.7125 x 0.5 pt.

0.3 pt. = 0.813 x 0.5 pt.

0.4 pt. = 0.952 x 0.5 pt.





THEORETICAL SLAB HAUNCH

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Girder No. 1			*	•																	
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Girder No. 3	-	_		_		~	\sim	~	<u></u>		_	_			_		_	_		_	_
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Girder No. 4	<u></u>	<u></u>	<u> </u>	<u></u>	<u></u>	<u></u>	<u> </u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	←	<u></u>	<u></u>	<u></u>	_	<u></u>	~
	× 2 2 ×	<u>5</u> //	8 //	8 /	<u> </u>	4 // 4	4 //	\ \ \ \	8 5	8 //	8 //	8 /	8 57 /	% % % % % % % % % % % % % % % % % % %	8 2	8 5 //	4 / /	8 2 /	2 "	22 / 8	<u>≈</u> – ∞
Girder No. 5	<u> </u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	~	<u></u>	~		<u></u>	<u></u>	<u></u>	~	<u></u>		~
	of Slab—, Girder—		<u></u>	<u></u>		\ <u>\</u>			<u> </u>		\ \ \	<u></u>	\	<u></u>	<u></u>			V			
		< 4	equal		<u>S</u>	•	€				equal		es				<	4	equal		>
		<	· & Bear	ring—	>	ŀ	<				€ Bear	ing—				>	=	<	· & Bea	ring-	>
		<	49′-	-5 "	>		€				103′-	10"						=	49′-	-5 "	>
		S	PAN (1	1-2)						•	SPAN (2-3)						S	PAN (3-4)	

THEORETICAL SLAB HAUNCHING DIAGRAM (ESTIMATED AT 90 DAYS)

If girder camber is different from that shown in the camber diagram, in order to maintain minimum slab thickness, an adjustment of the slab haunches, an increase in slab thickness or a raise in grade uniformly throughout the structure shall be necessary. No payment will be made for additional labor or materials required for variation in haunching, slab thickness or grade adjustment.

Concrete in the slab haunches is included in the Estimated Quantities for Slab on Concrete NU Girder.

	Theoretical Bottom of Slab Elevations at Centerline of Girder (Prior to forming for slab) (Estimated at 90 days)																				
	Span	(1-2) (48	8'-4 <u>1</u> " (L	brg – Ę	brg.)				Span ($(2-3) (7^{-3})$	7′-8″ £ t	org – & b	org.)				Span	$(3-4) (6^{-1})$	7′−4″ € 1	brg – & l	org.)
	€ brg.	.25	.50	. 75	€ brg.	€ brg.	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	€ brg.	€ brg.	.25	.50	.75	€ brg.
Girder No. 1	769.64	769.84	770.03	770.19	770.33	770.34	770.47	770.59	770.70	770.80	770.88	770.94	770.99	771.02	771.04	771.05	771.06	771.20	771.28	771.31	771.28
Girder No. 2	769.73	769.94	770.12	770.29	770.43	770.45	770.58	770.71	770.82	770.92	771.00	771.06	771.11	771.15	771.17	771.18	771.19	771.34	771.43	771.46	771.44
Girder No. 3	769.70	769.91	770.10	770.26	770.41	770.43	770.57	770.69	770.81	770.91	771.00	771.06	771.12	771.15	771.18	771.19	771.20	771.36	771.46	771.49	771.50
Girder No. 4	769.45	769.67	769.86	770.03	770.19	770.21	770.34	770.48	770.59	770.70	770.79	770.86	770.91	770.95	770.98	771.00	771.01	771.17	771.27	771.32	771.35
Girder No. 5	769.21	769.43	769.63	769.80	769.96	769.98	770.12	770.25	770.38	770.48	770.57	770.65	770.70	770.75	770.78	770.80	770.81	770.97	771.09	771.14	771.17

Elevations are based on a constant slab thickness of $8\frac{1}{2}''$ and include allowance for theoretical dead load deflections due to weight of slab (including precast panel) and barrier curb.

JJM

DWM

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DESIGN BY:

DRAWN BY:

Paragon Star Development

architects engineers

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"PRELIMINARY

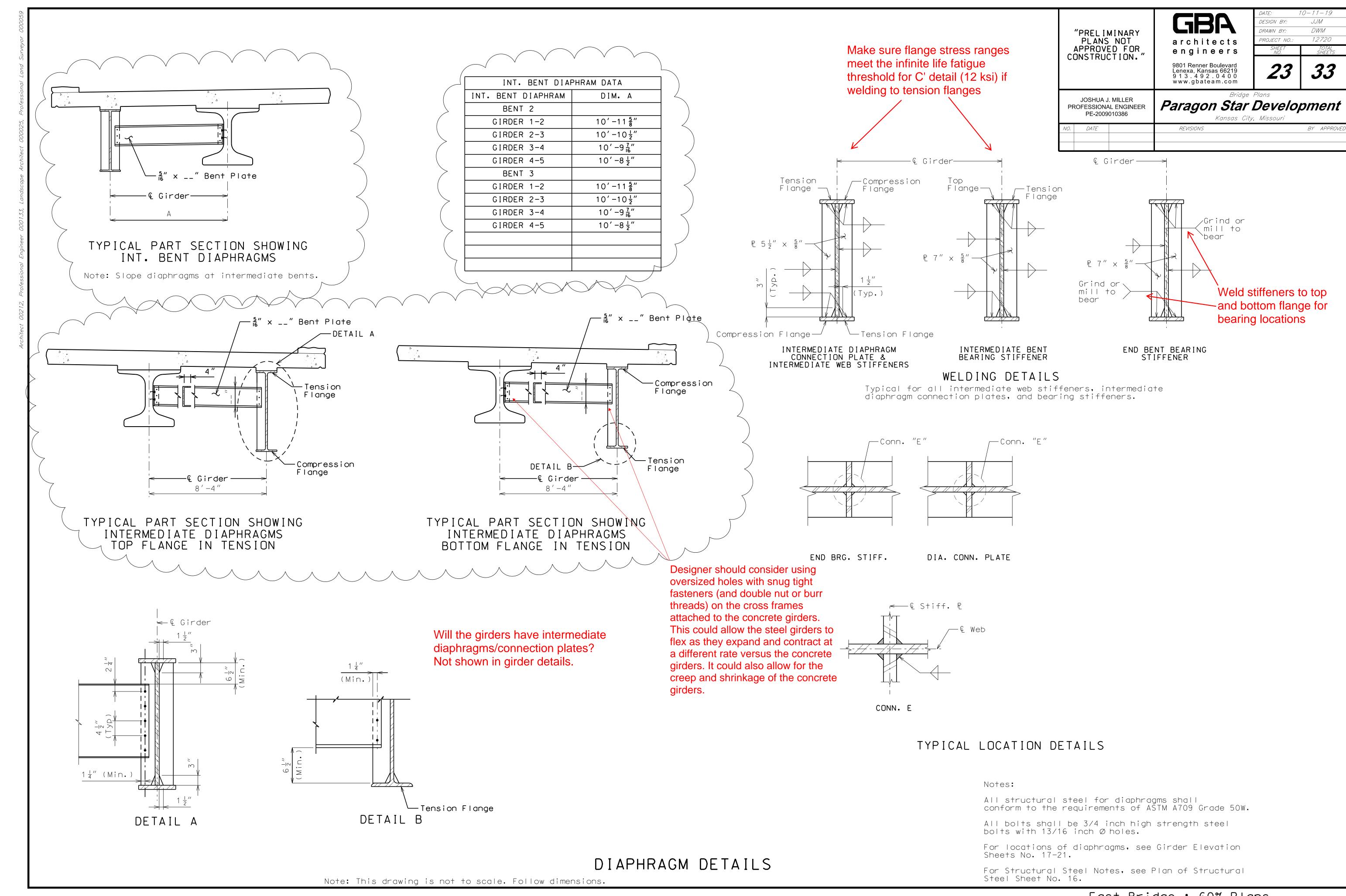
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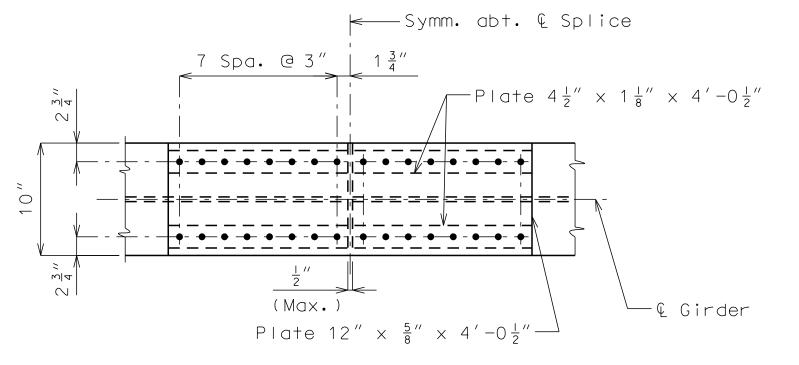
JOSHUA J. MILLER

PROFESSIONAL ENGINEER

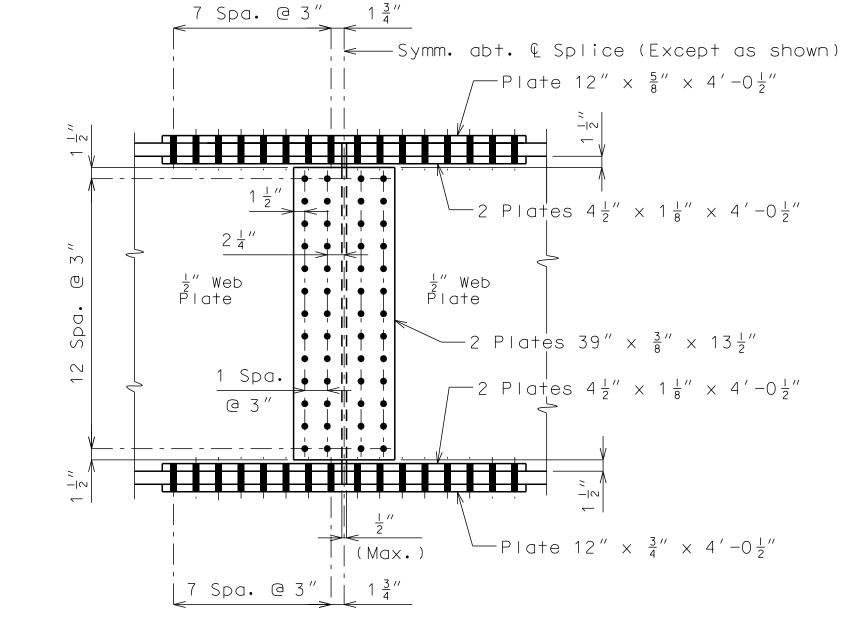
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DATE





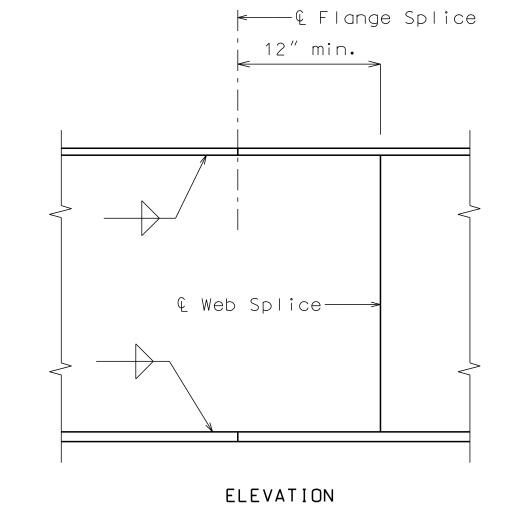
PLAN OF TOP FLANGE SPLICE PLATE



DETAIL OF BOLTED FIELD SPLICE

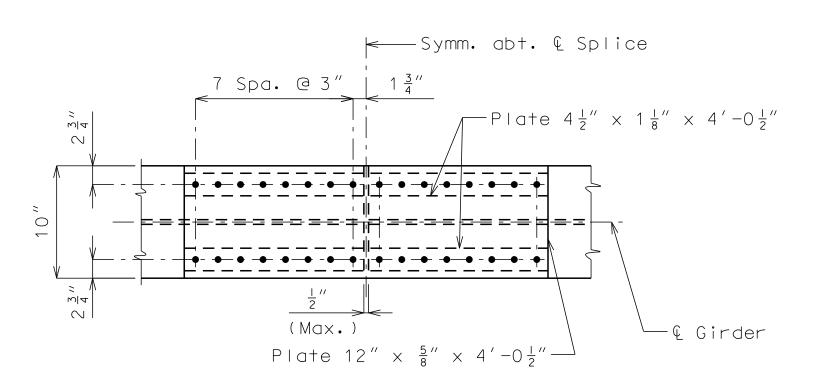
Use 7/8"Ø high strength bolts with 15/16"Ø holes.

Contact surfaces shall be in accordance with Sec 1081 for surface preparation.



WELDED SHOP WEB AND FLANGE SPLICE

Welded shop web and flange splices may be permitted when detailed on the shop drawings and approved by the engineer. No additional payment will be made for optional welded shop web and flange splices.



PLAN OF BOTTOM FLANGE SPLICE PLATE

Splice detail is approximate and subject to change

This will be reviewed with next submittal

SPLICE PLATE DETAILS OF AESTHETIC STEEL GIRDER

GBA

architects

engineers

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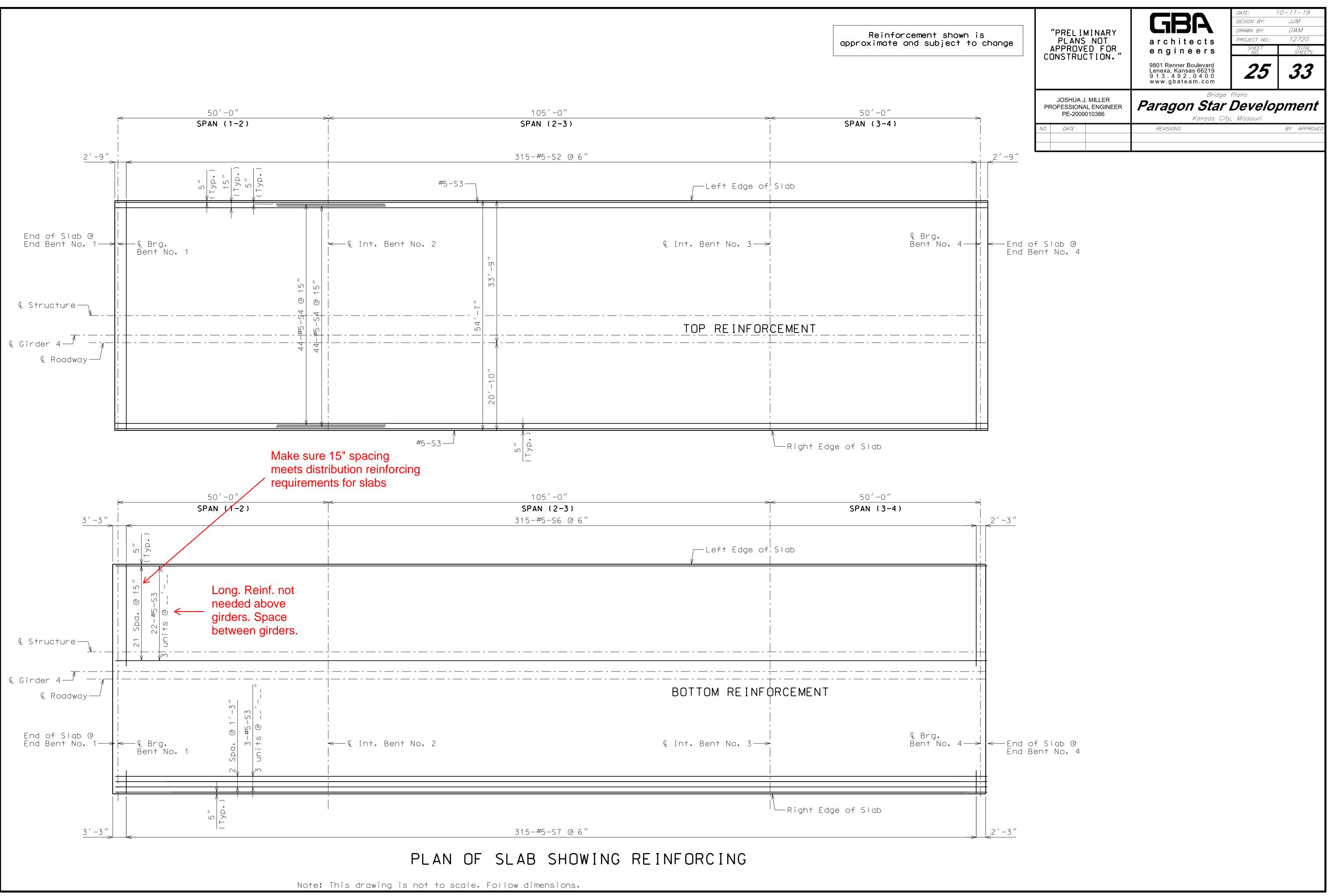
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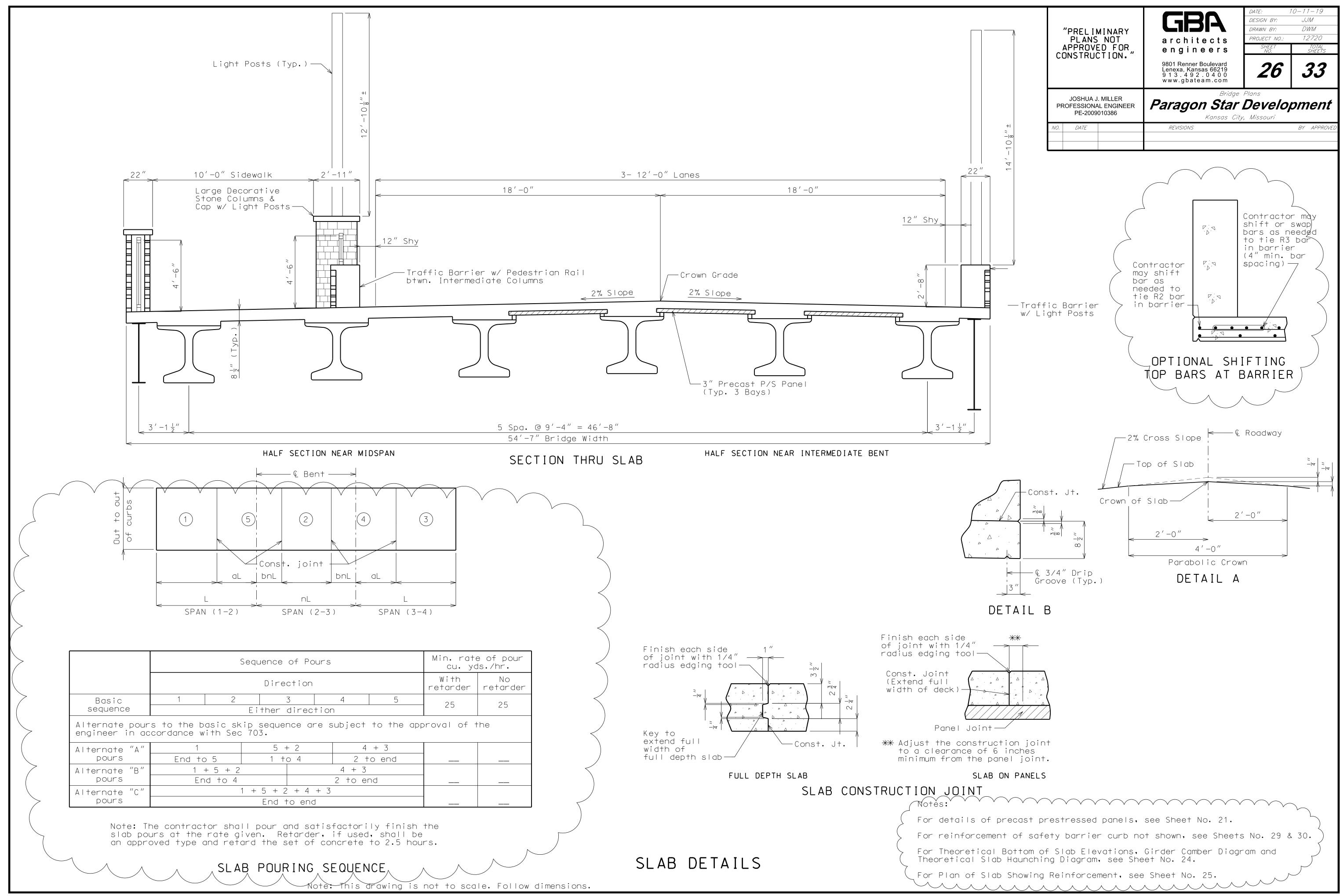
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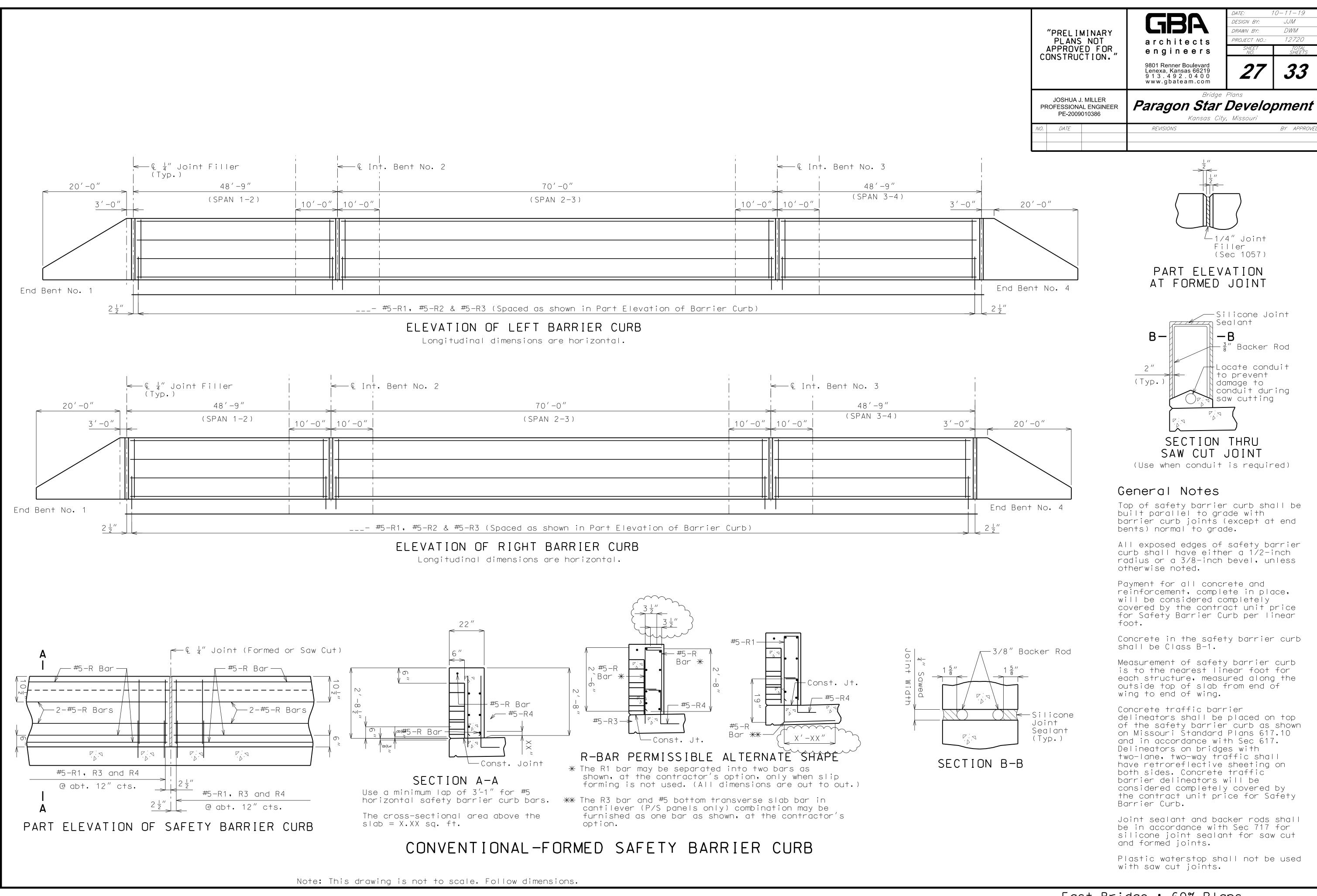
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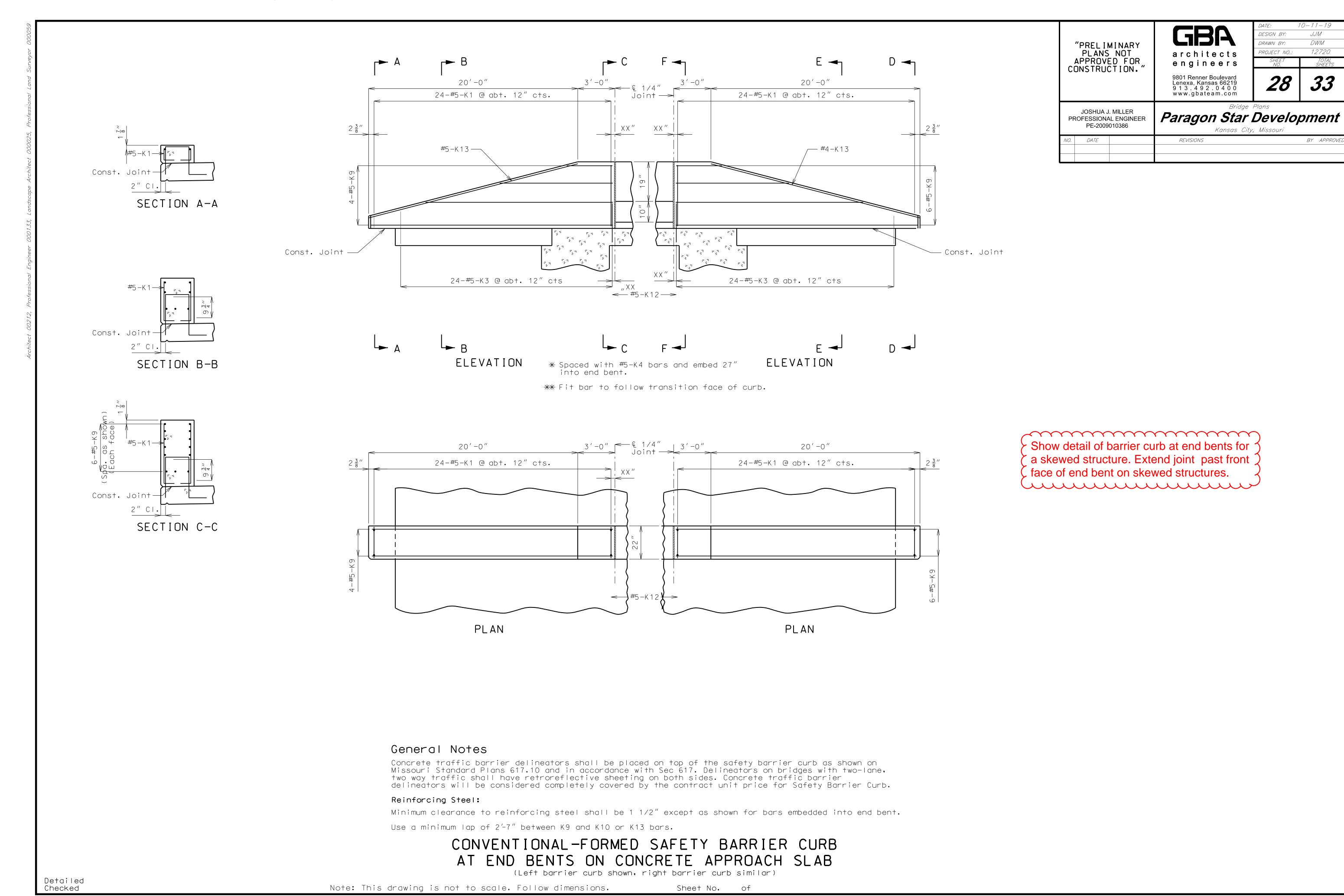
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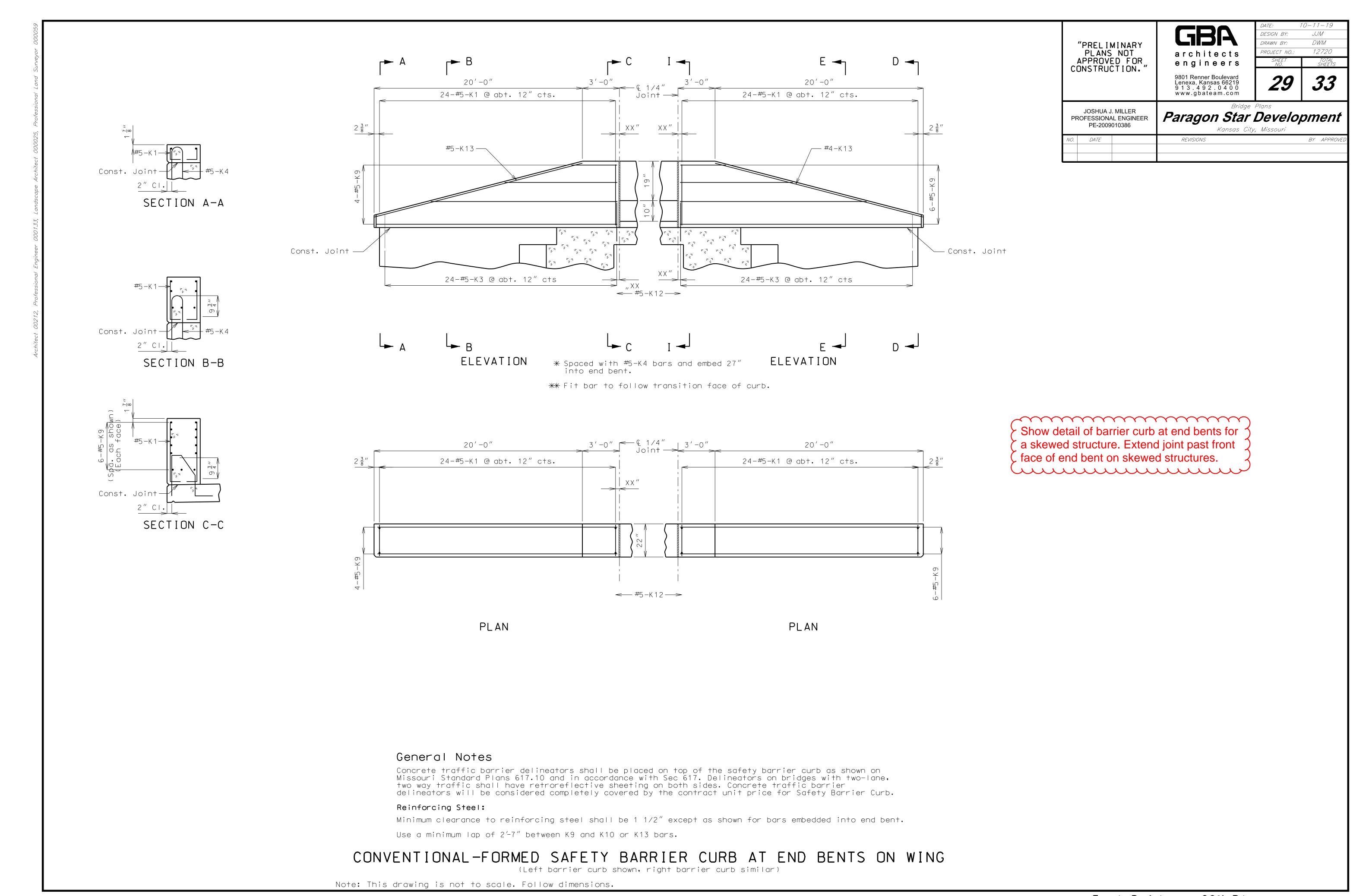
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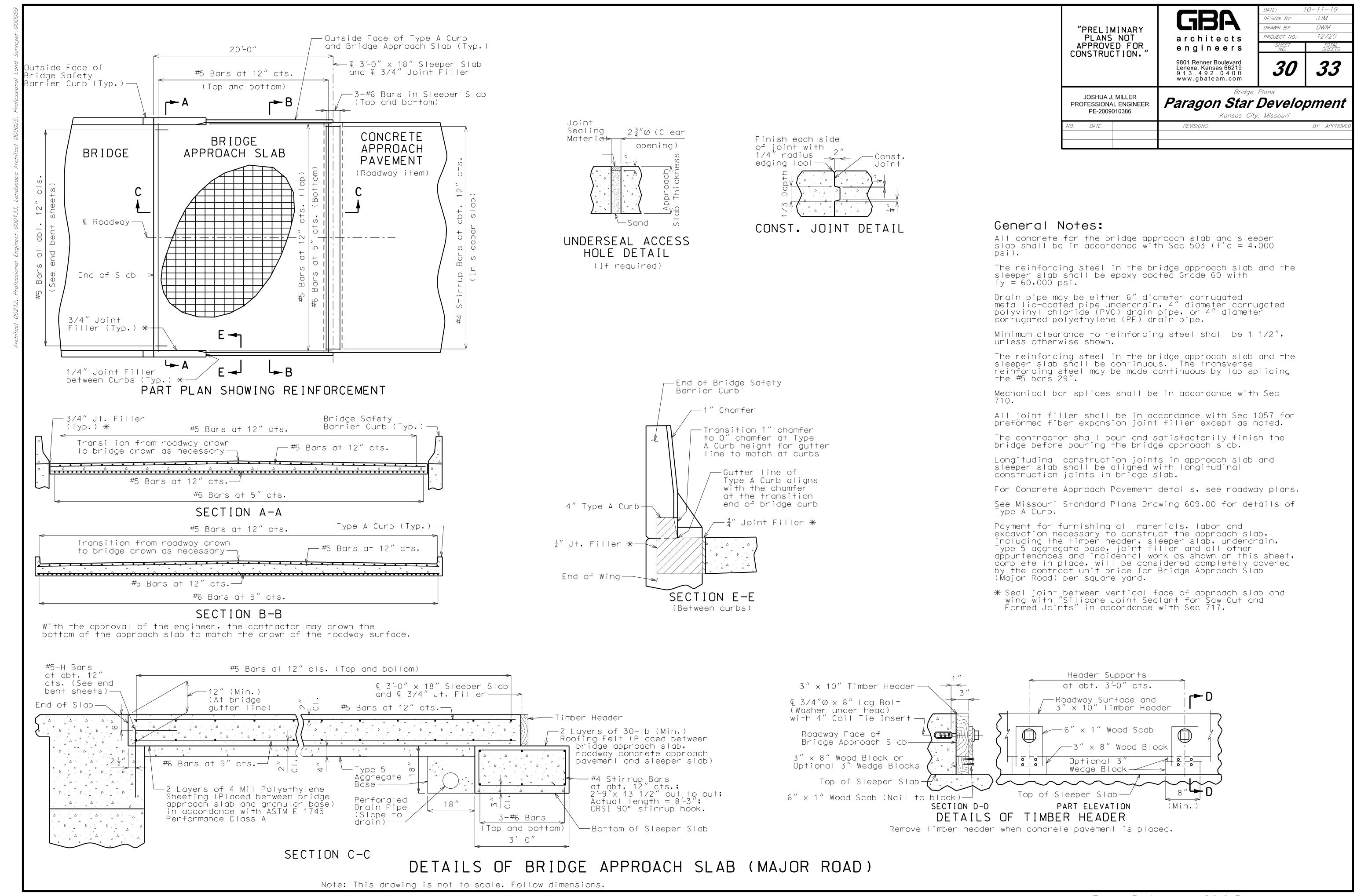
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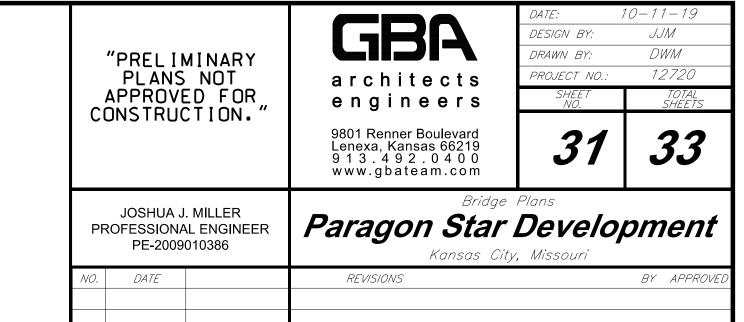
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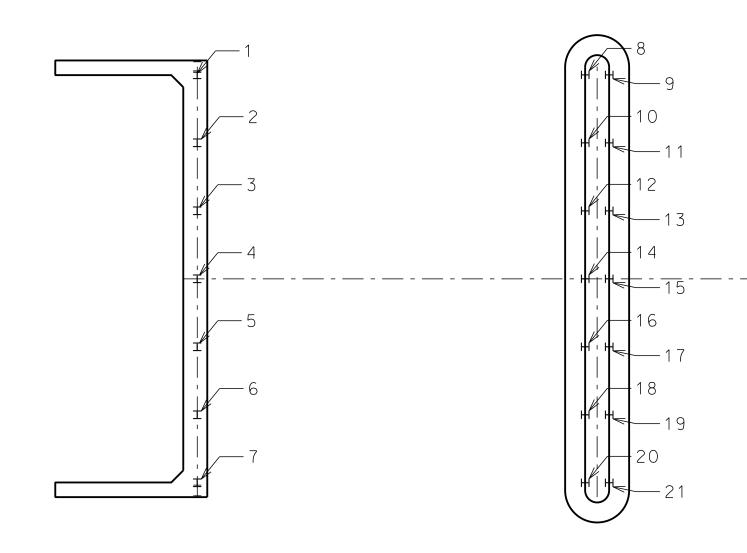
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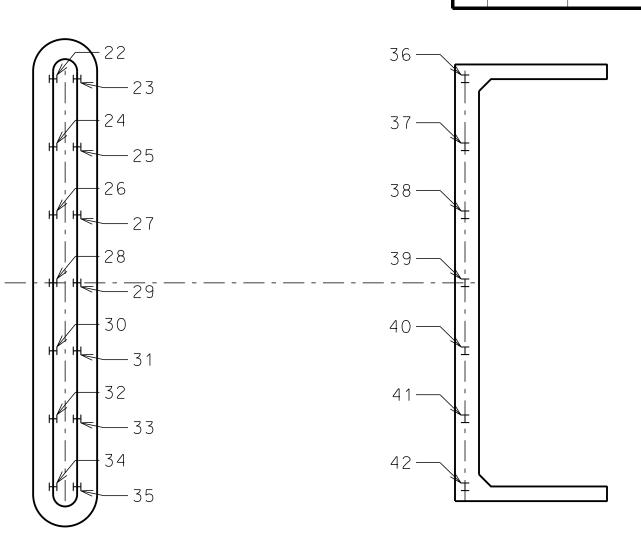
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			As-Built	Pile Do	ata .
Pile No.	Length in Place (ft)	Compressive	PDA End of Drive Blow Count (blows/in.)	Actual End of Drive Blow Count (blows/in.)	Remarks
					END BENT NO. 1
1					
2					
3					
4					
5					
6					
7					
					INT. BENT NO. 2
8					
9					
10					
11					
12					
13					
1 4					
15					
16					
17					
18					
19					
20					
21					

		PDA Nom.	PDA	Actual	
D: La	Length	Axial Compressive Resistance	End of	End of	Remarks
Pile No.	Place	Resistance	Count	Count	Kellidi K3
	(ft)	(kips)	(blows/in.)	(blows/in.)	
					INT. BENT NO. 3
22					
23					
24					
25					
26					
27					
28					
29					
30					
31					
32					
33					
34					
35					
					END BENT NO. 4
36					
37					
38					
39					
40					
41					
42					

Indicate in remarks column:

A. Pile type and grade

B. Batter

C. Driven to practical refusal

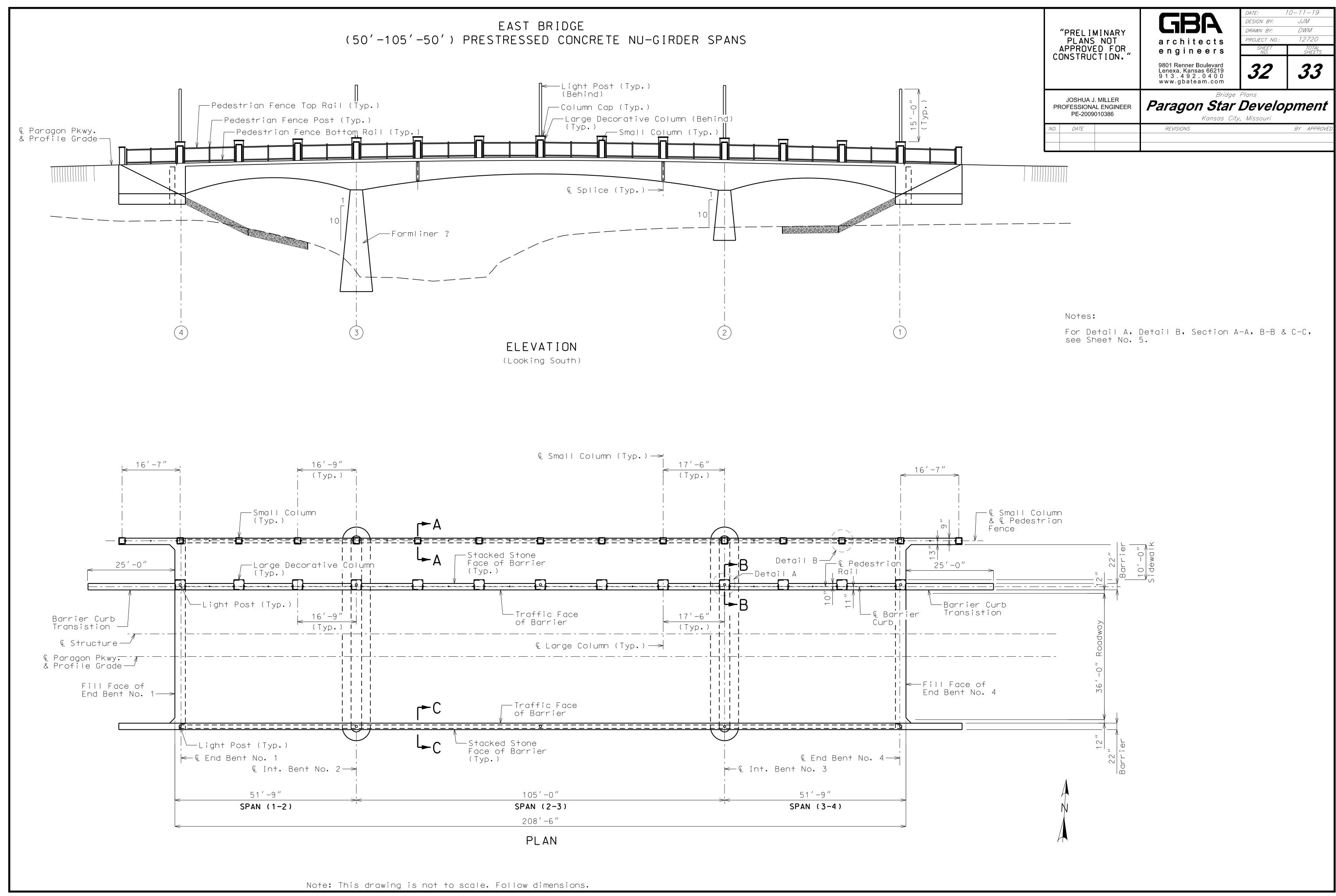
D. PDA test pile

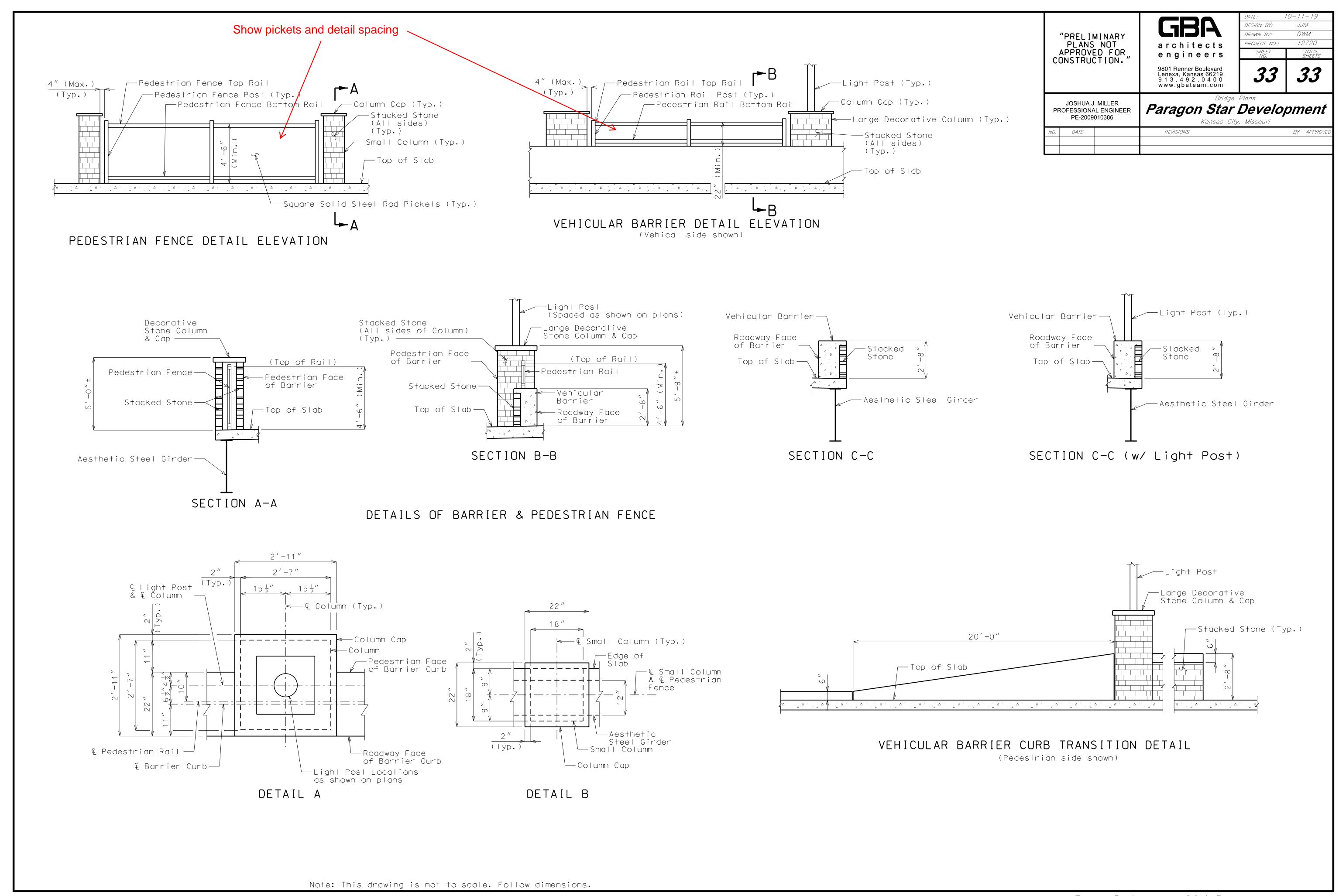
E. Minimum tip elevation controlled

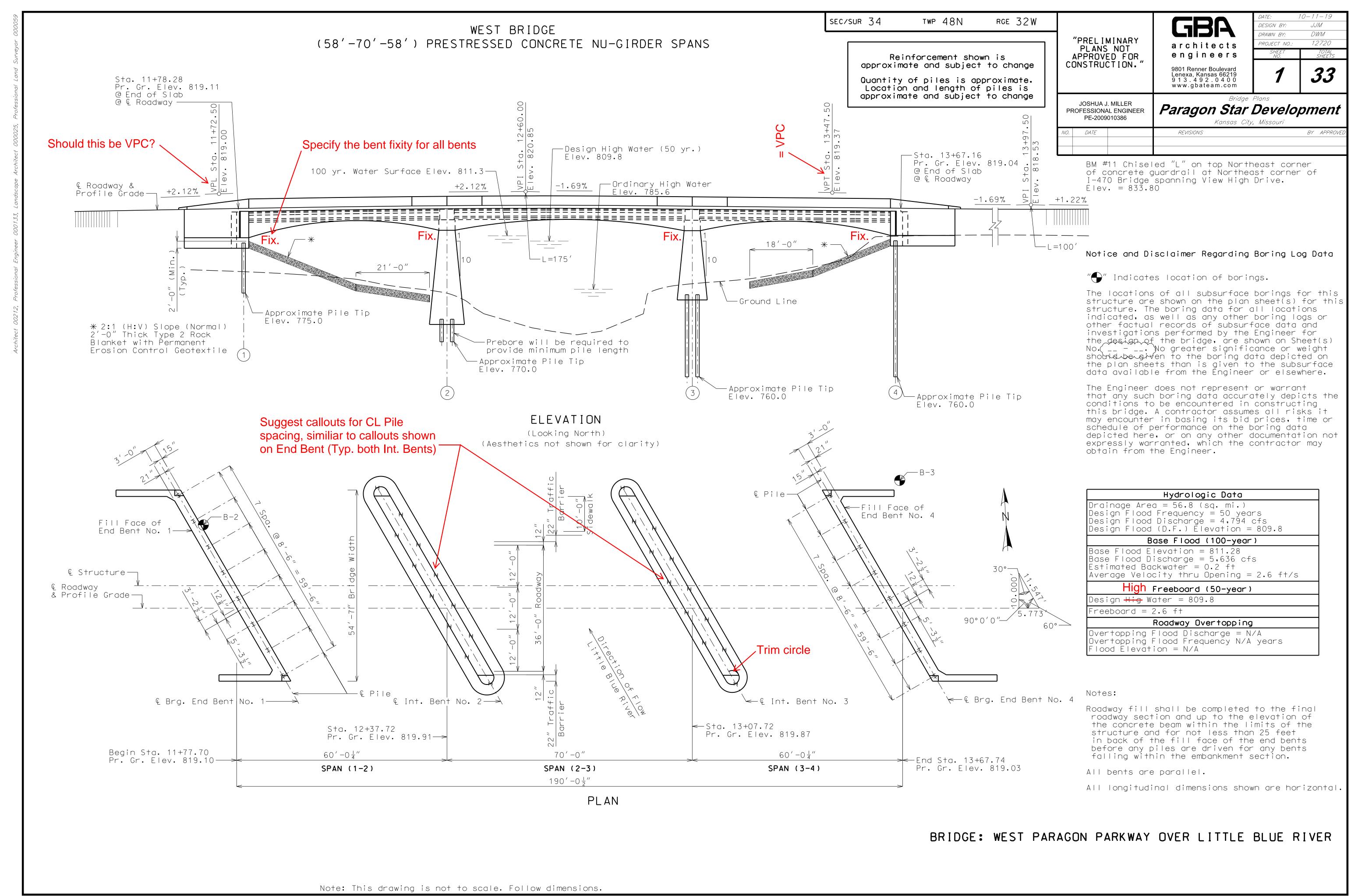
(Use when actual blow count is less than PDA blow count due to minimum tip elevation requirement. A plus sign (+) shall be placed after the PDA nominal axial compressive

resistance value indicating actual value is higher than PDA value.)

This sheet to be completed by MoDOT construction personnel.







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General Notes: Design Specifications: 2012 AASHTO LRFD Bridge Design Specifications (6th Ed.) and 2013 Interim Revisions. Seismic Design Category = A All referenced specifications shall refer to Missouri Standard Specifications for Highway Construction Design Loading: Vehicular = HL-93 Future Wearing Surface = 35 lb/sf Earth = 120 lb/cfEquivalent Fluid Pressure = 45 lb/cf Design Unit Stresses: Class B Concrete (Substructure) f'c = 3,000 psiClass B-1 Concrete (Barrier Curb) f'c = 4,000 psiClass B-2 Concrete (Superstructure except Barrier Curb f'c = 4,000 psify = 60,000 psiReinforcing Steel (Grade 60) Structural Steel HP Pile (ASTM A709 Grade 50S) fy = 50,000 psiFor Precast Prestressed Panel Stresses, see Sheet No. __1. For Prestressed Girder Stresses, See Sheets No. __ & __. Neoprene Pads: Plain and Laminated Neoprene Bearing Pads shall be 60 durometer and shall be in accordance with Sec 716. Joint Filler: All joint filler shall be in accordance with Section 1057 for preformed sponge rubber expansion and partition joint filler, except as noted. Reinforcing Steel: Minimum clearance to reinforcing steel shall be 1 1/2", unless otherwise shown. Minimum clearance between galvanized piles and uncoated (plain) reinforcing steel including bar supports shall be 1 1/2". Nylon, PVC, or other polyethylene spacers shall be used to maintain clearance. Nylon cable ties shall be used to bind the spacers to the reinforcement. Traffic Handling: Structure to be closed during construction. See roadway plans for traffic control. Miscellaneous: City Construction personnel will indicate the type of joint filler option used under the precast panels for this structure: Constant Joint Filler ☐ Variable Joint Filler

	FOUNDATIO	NC	DATA								
TYPE	DESIGN		BENT NUMBER								
'''	DATA		1	2	3	4					
	Pile Type and Size		HP12×53	HP12×53	HP12×53	HP12×53					
	Number	ea	8	- -		8					
	Approximate Length per Each	f+									
l , ,	Pile Point Reinforcement	ea									
Load Bearing	Min. Galvanized Penetration (Elev.)	f†									
Pile											
	Minimum Nominal Axial Compressive Resistance	iр									

DT = Dynamic Testing

Minimum Nominal Axial Compressive Resistance = Maximum Factored Loads/Resistance Factor

HP piles are anticipated to be driven to refusal on rock. Review all borings for depth of rock and restrict driving as appropriate to comply with hard rock driving criteria in accordance with Sec 702.

- All piles shall be galvanized down to the minimum galvanized penetration (elevation).
- Pile point reinforcement need not be galvanized. Shop drawings will not be required for pile point reinforcement.

The contractor shall make every effort to achieve the minimum galvanized penetration (elevation) shown on the plans for all piles. Deviations in penetration less than 5 feet of the minimum will be considered acceptable provided the contractor makes the necessary corrections to ensure the minimum penetration is achieved on subsequent piles.

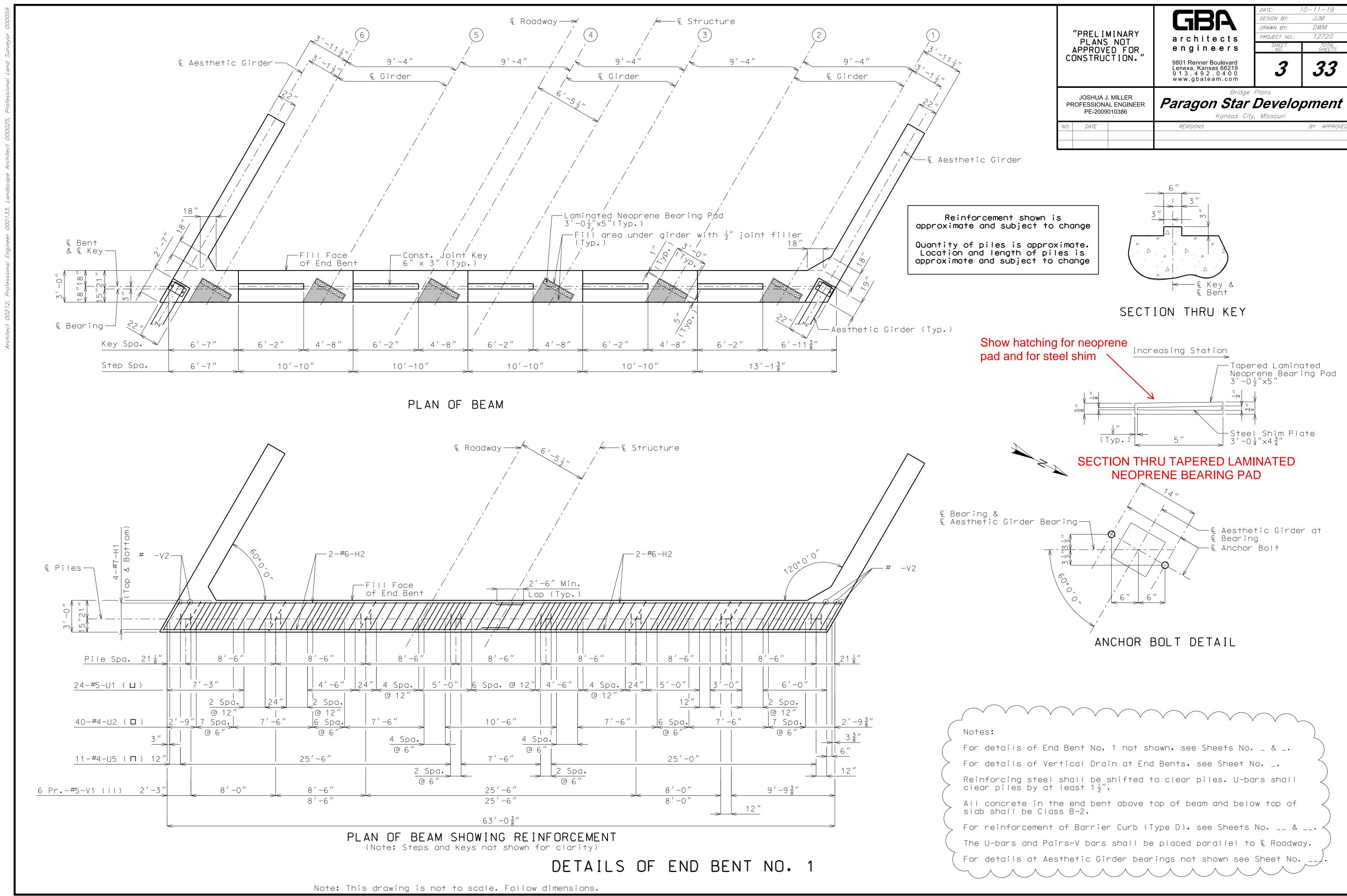
Reinforcement quantity provided is based on _____lbs/cy of concrete.

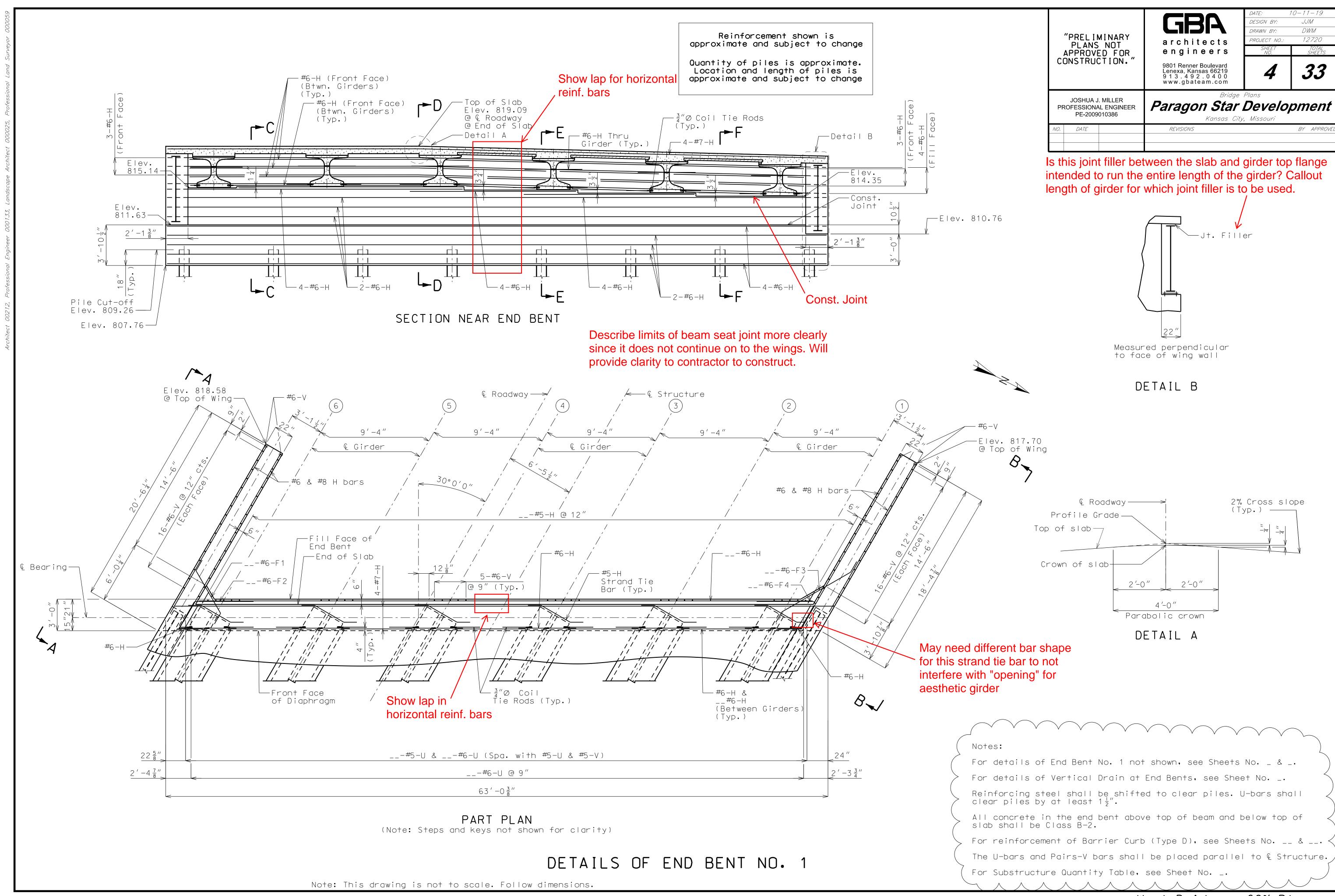
Estimated Quantities		
I tem		Total
Class B-2 Concrete (Superstructure Concrete on NU-Girder)	cu. yard	
Reinforcing Steel (Epoxy Coated)	pound	

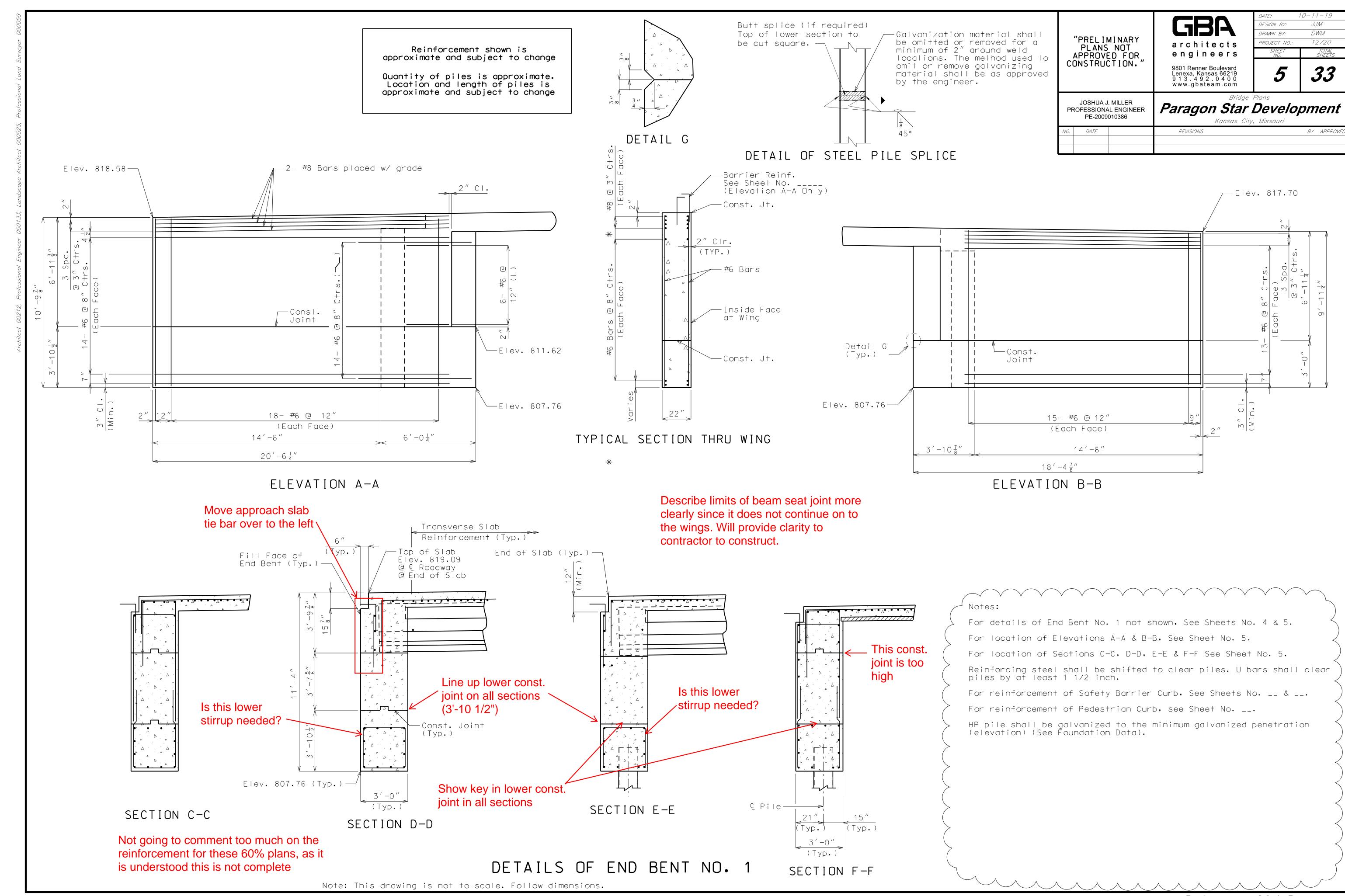
The table of Estimated Quantities represents the quantities used by the Engineer in preparing the cost estimate. Payment for the Bridge will be considered completely covered by the contract Lump sum price. Variations may be encountered in the estimated quantities but the variations cannot be used for adjustment in the contract Lump sum price.

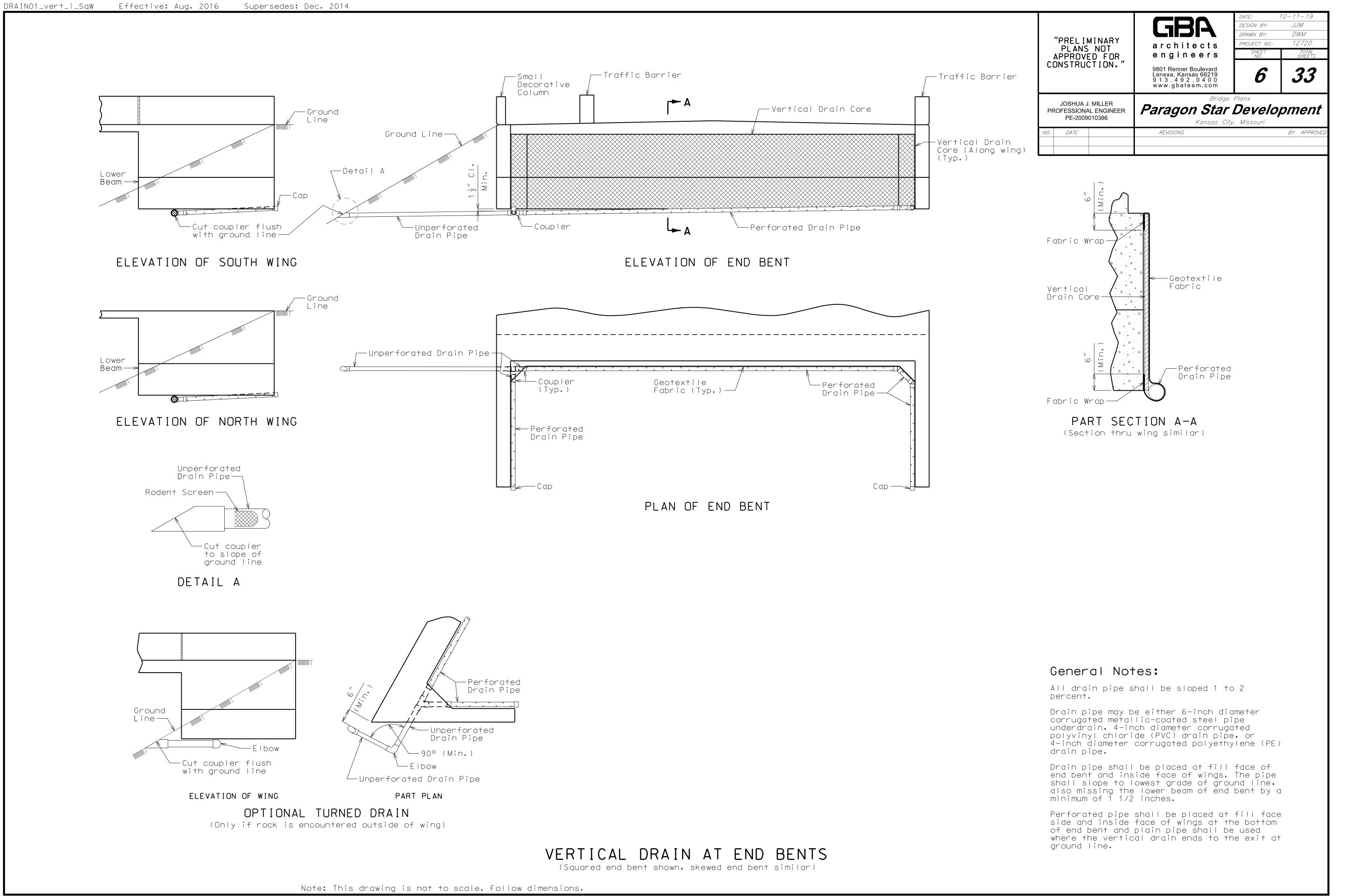
Method of forming the slab shall be as shown on the plans and in accordance with Sec 703. All hardware for forming the slab to be left in place as a permanent part of the structure shall be coated in accordance with ASTM A123 or ASTM B633 with a thickness class SC 4 and a finish type I, II, or III.

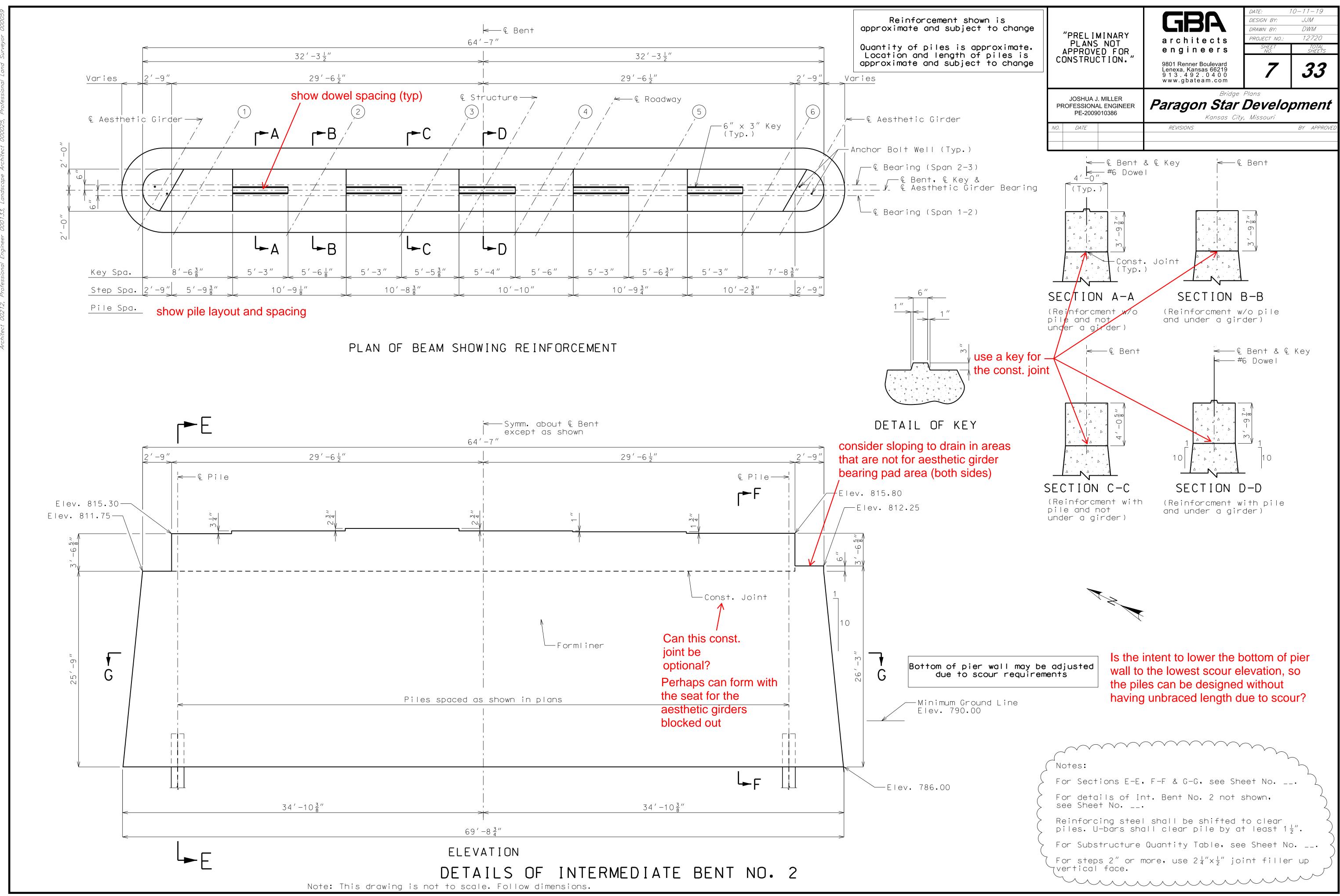
GENERAL NOTES AND QUANTITIES

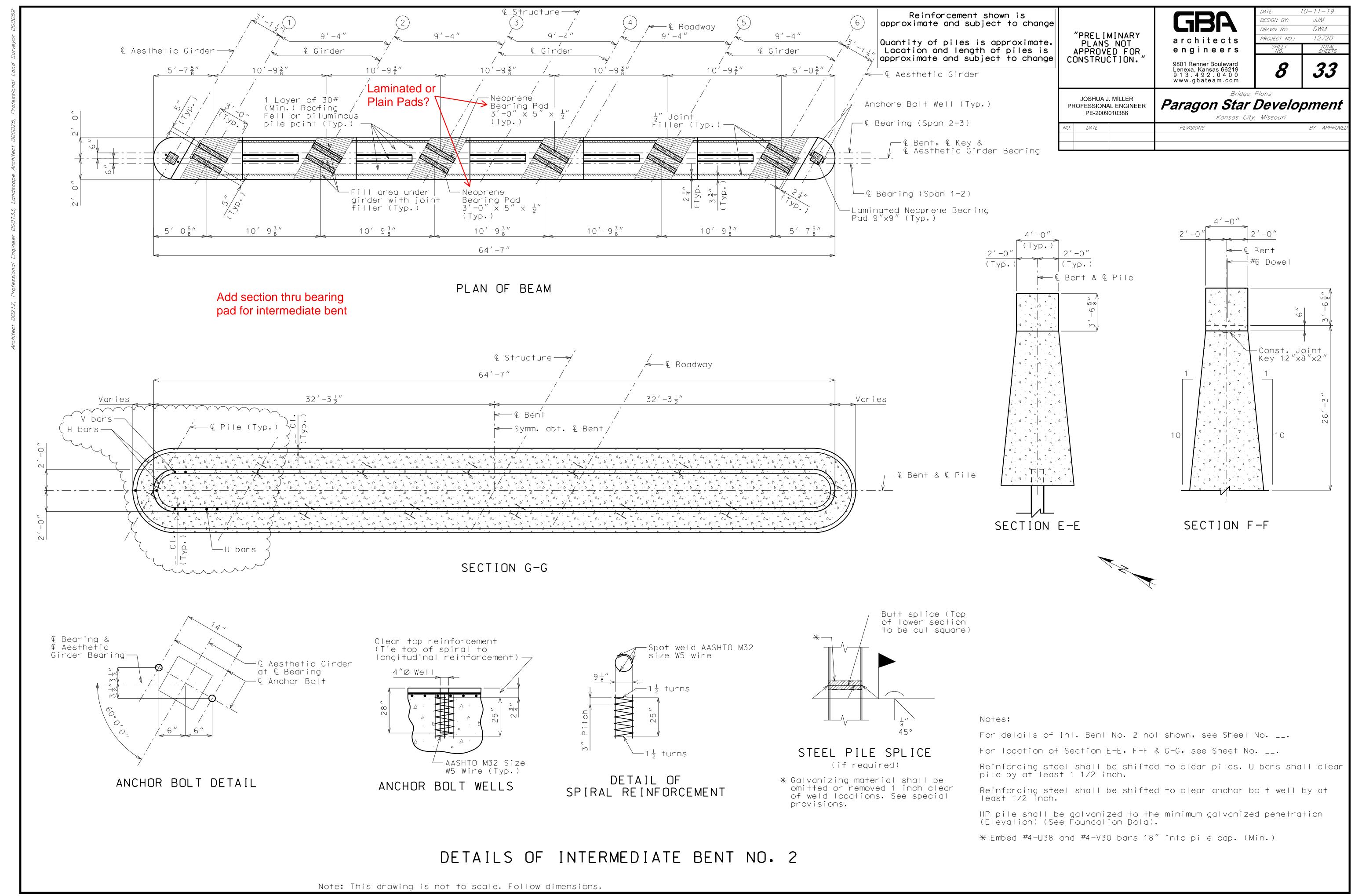


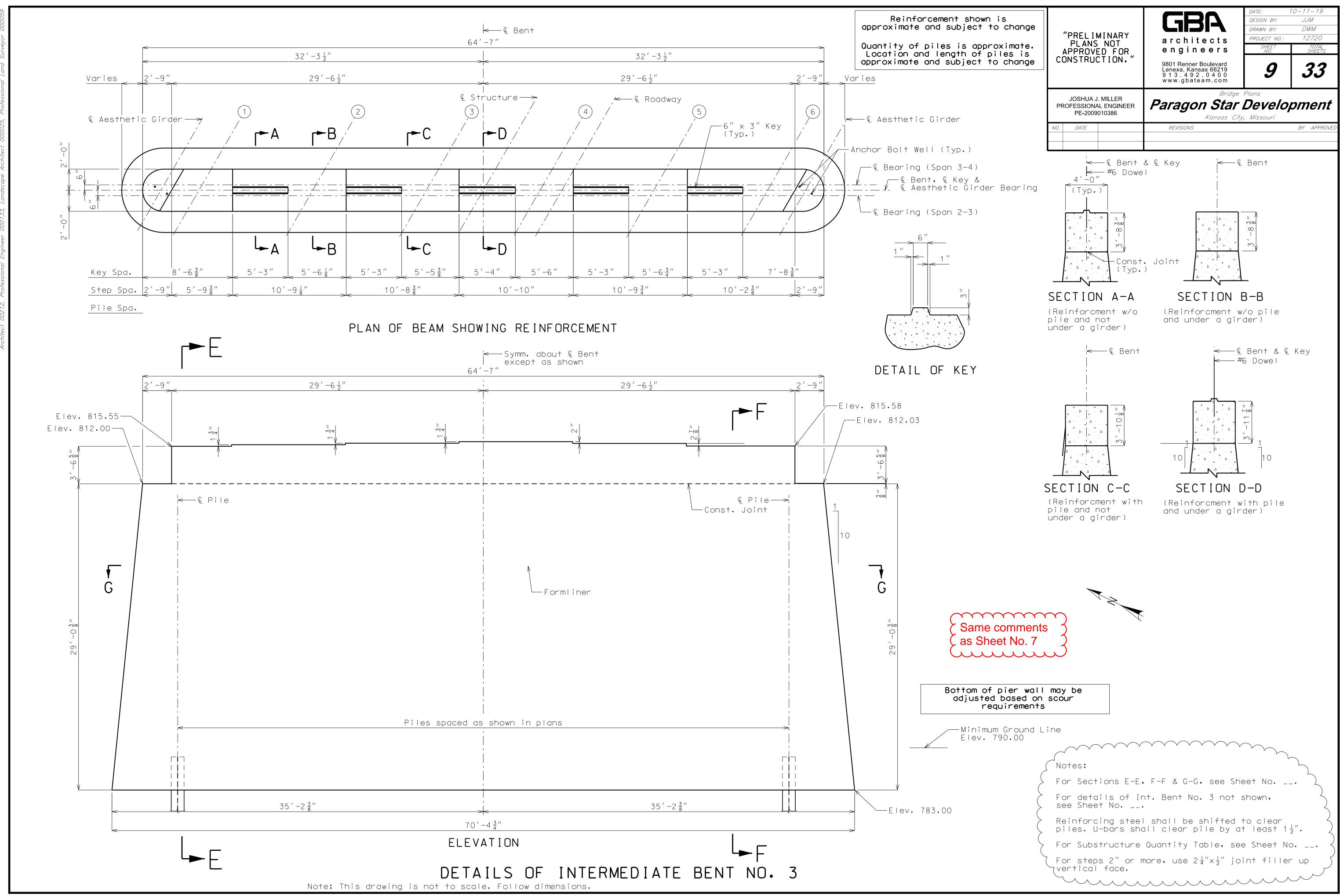


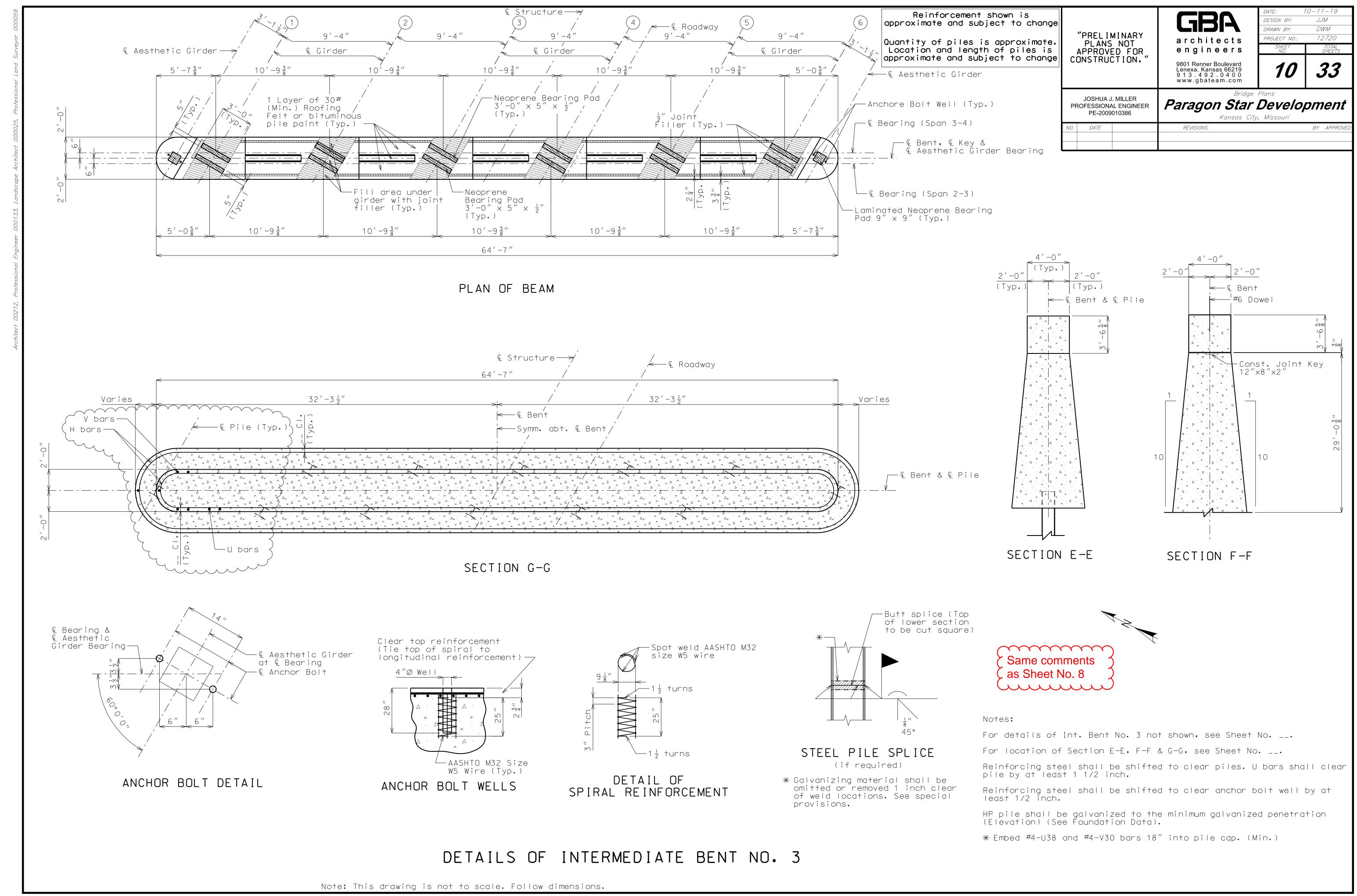


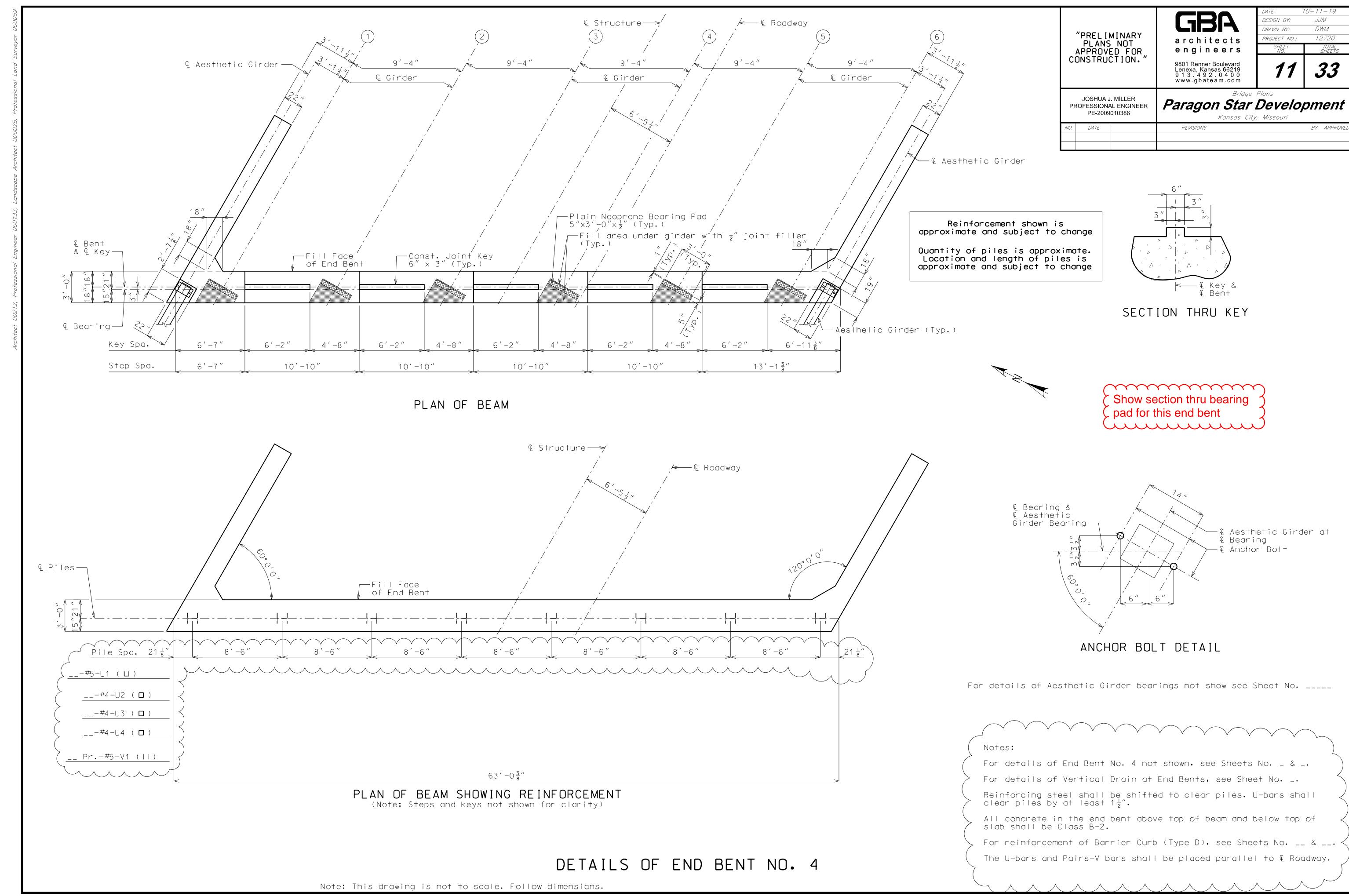


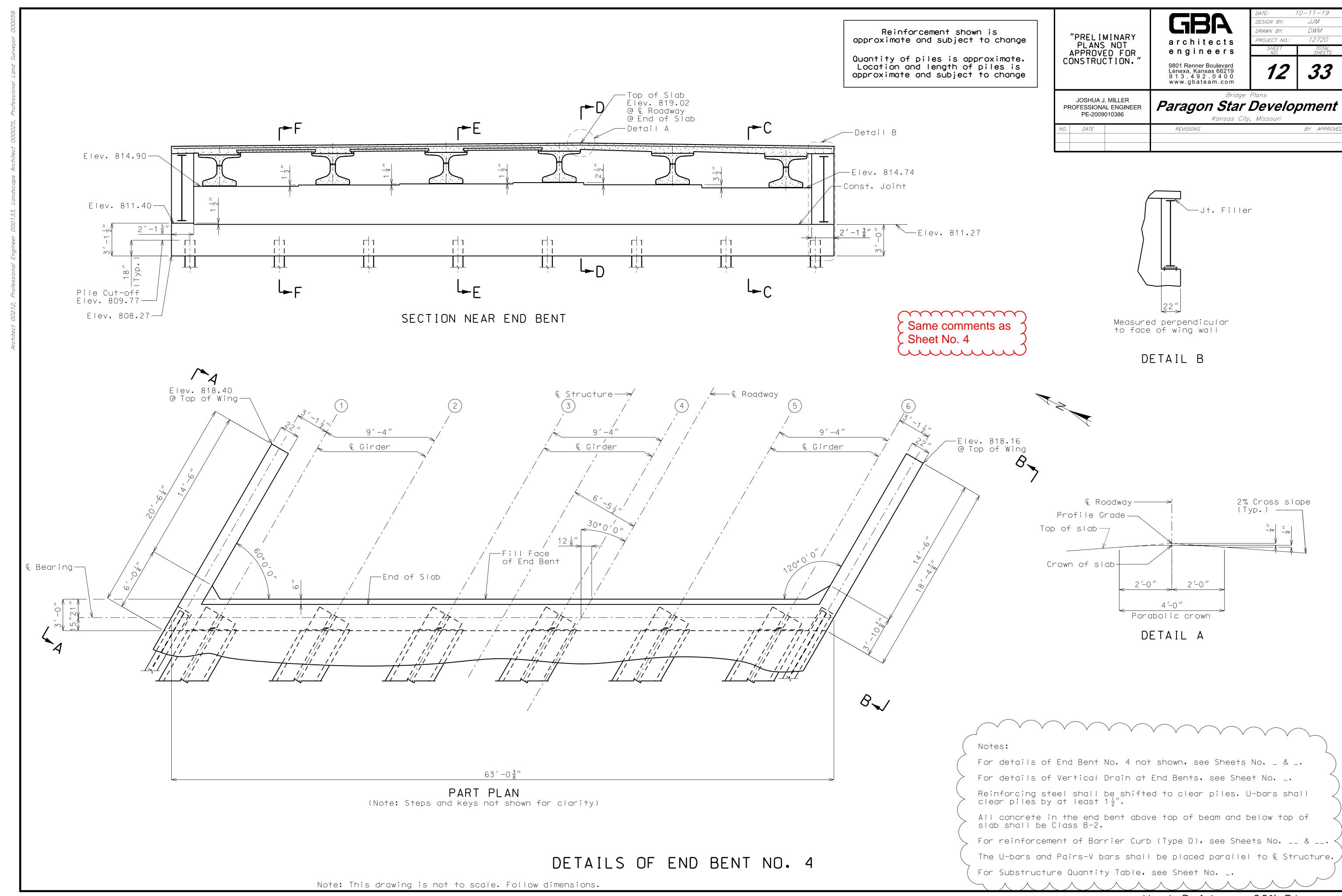


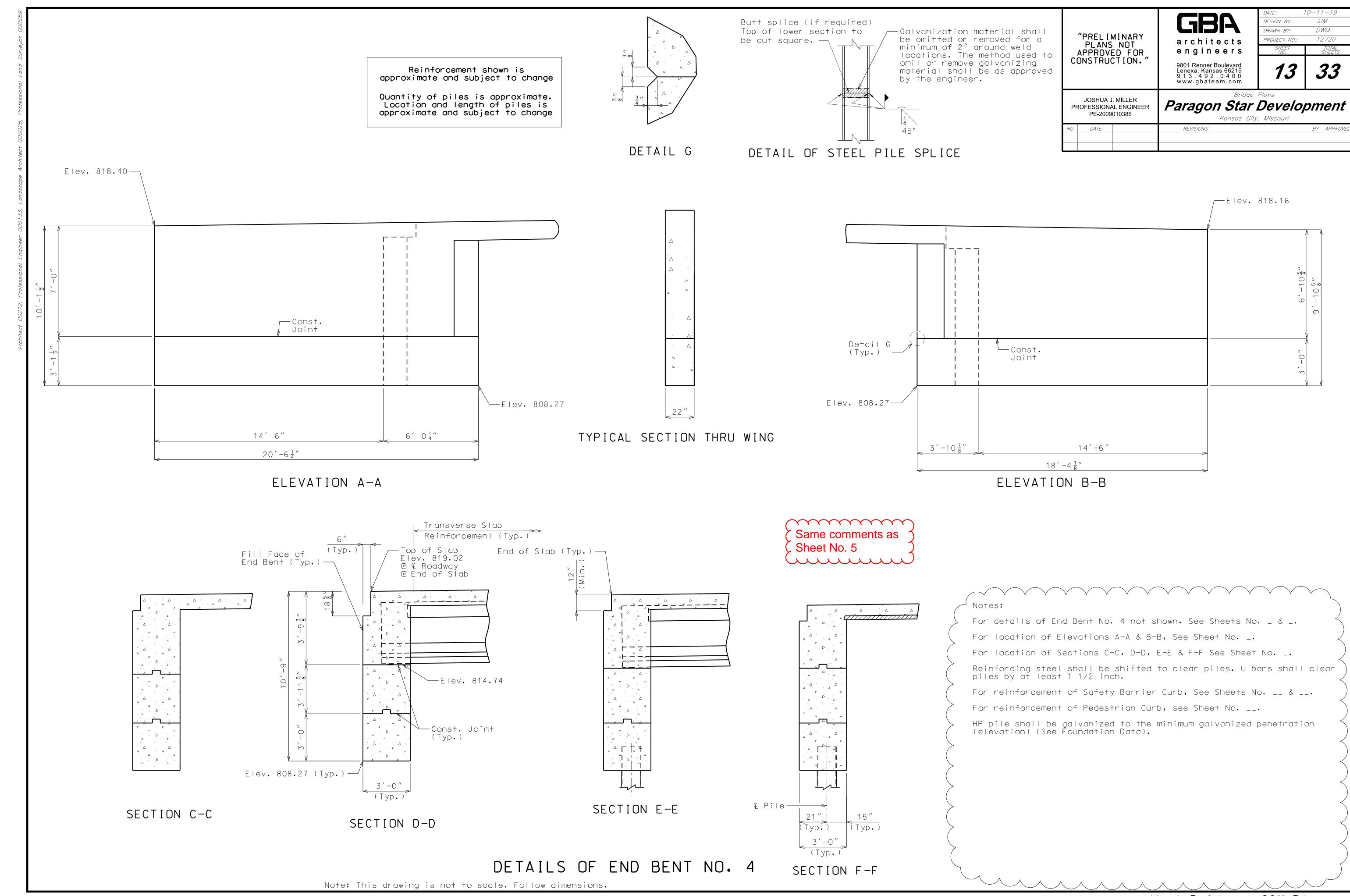














JOSHUA J. MILLER

PROFESSIONAL ENGINEER PE-2009010386

GBA architects engineers

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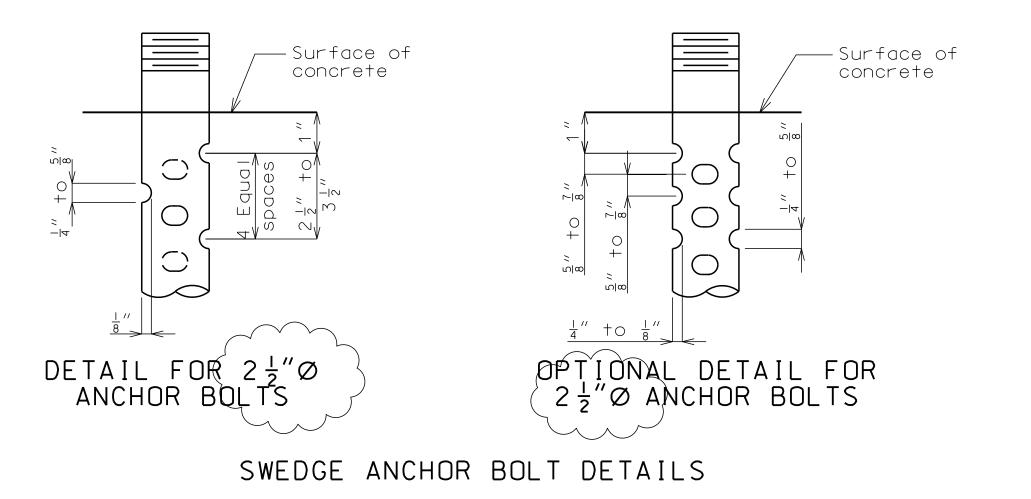
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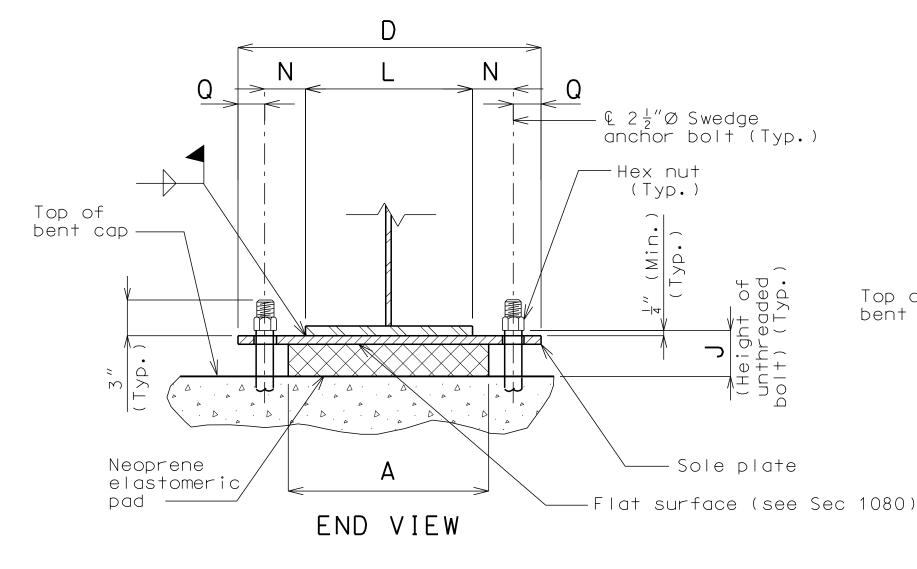
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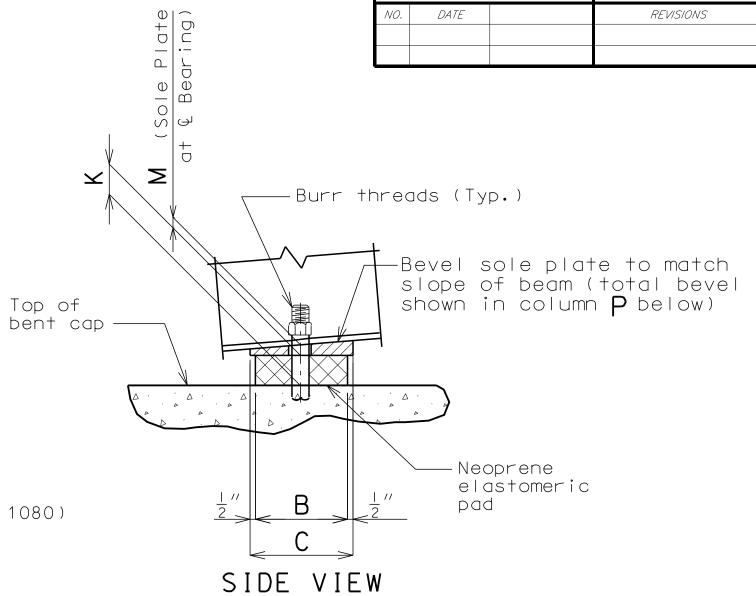
Paragon Star Development

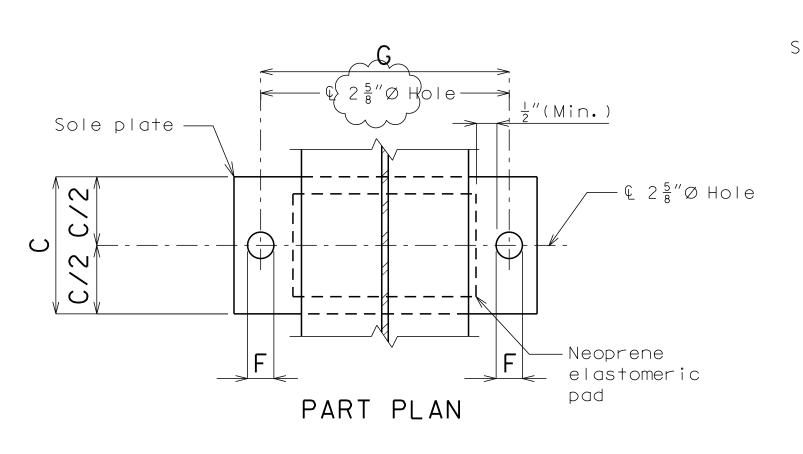
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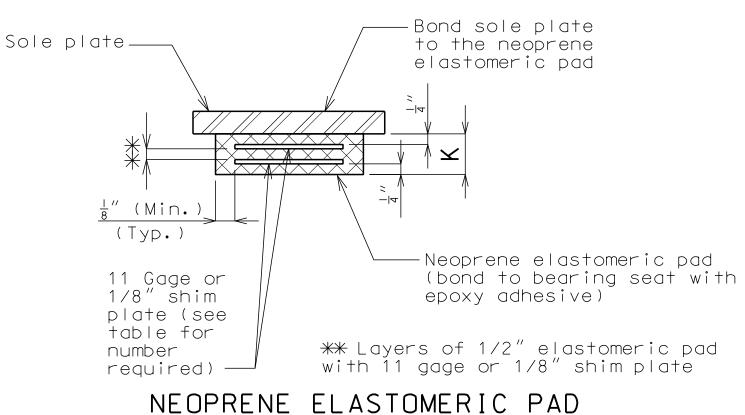


* The required shim plate shall be placed between layers of elastomer and molded together to form an integral unit.









									F	IXE	D BE	ARI	NGS		
`	BENT NO.	А	В	С	D	F	G	J	К	L	М	N	P Q	NUMBER OF SHIM PLATES *	NUMBER REQUIRED
`	1	9 "	9 "	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	" 2 ½"	7	5
> 	2	9 "	9 "	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	" 2 ¼"	7	5
>	3	9 "	9 "	10"	18½"	2 5 "	14"	6 ½"	4 3 "	10"	1 ½"	2 "	" 2 ¼"		
	4	9 "	9 "	10"	18 ½"	2 5 "	14"	6 ½ ′′	4 3 "	10"	1 ½"	2 "	" 2 ½"		

GENERAL NOTES:

Anchor bolts shall be $2\frac{1}{2}$ // ASTM F1554 Grade 55 swedged bolts and shall extend 25" into the concrete with ASTM A563 Grade A Hex or Heavy Hex nuts. Actual manufacturer's certified mill test reports (chemical and mechanical) shall be provided. Swedging shall be 1" less than extension into the concrete.

All structural steel for the anchor bolts and heavy hexagon nuts shall be coated with a minimum of two coats of inorganic zinc primer (5 mils minimum).

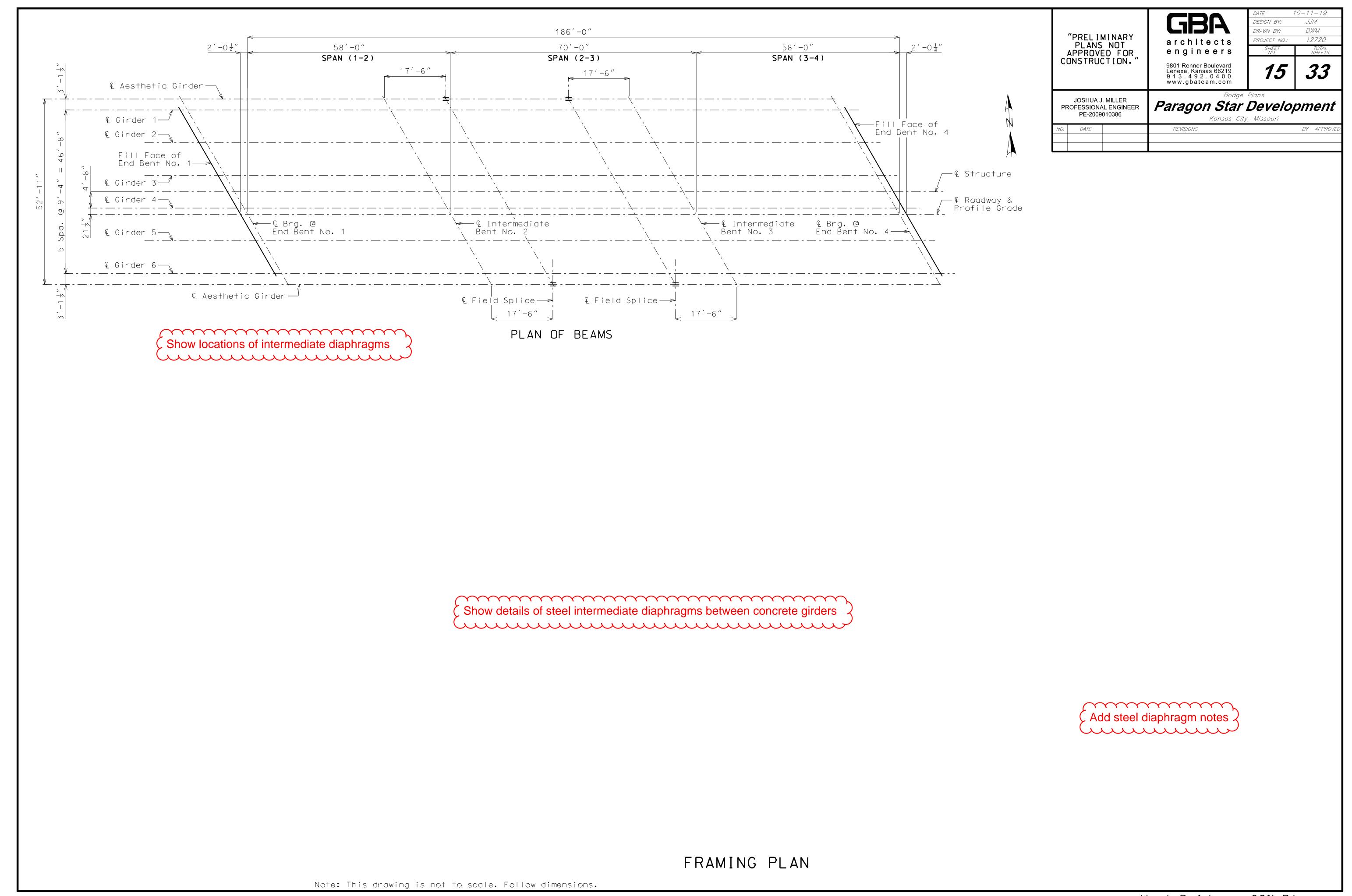
Neoprene Elastomeric Pads shall be 60 Durometer.

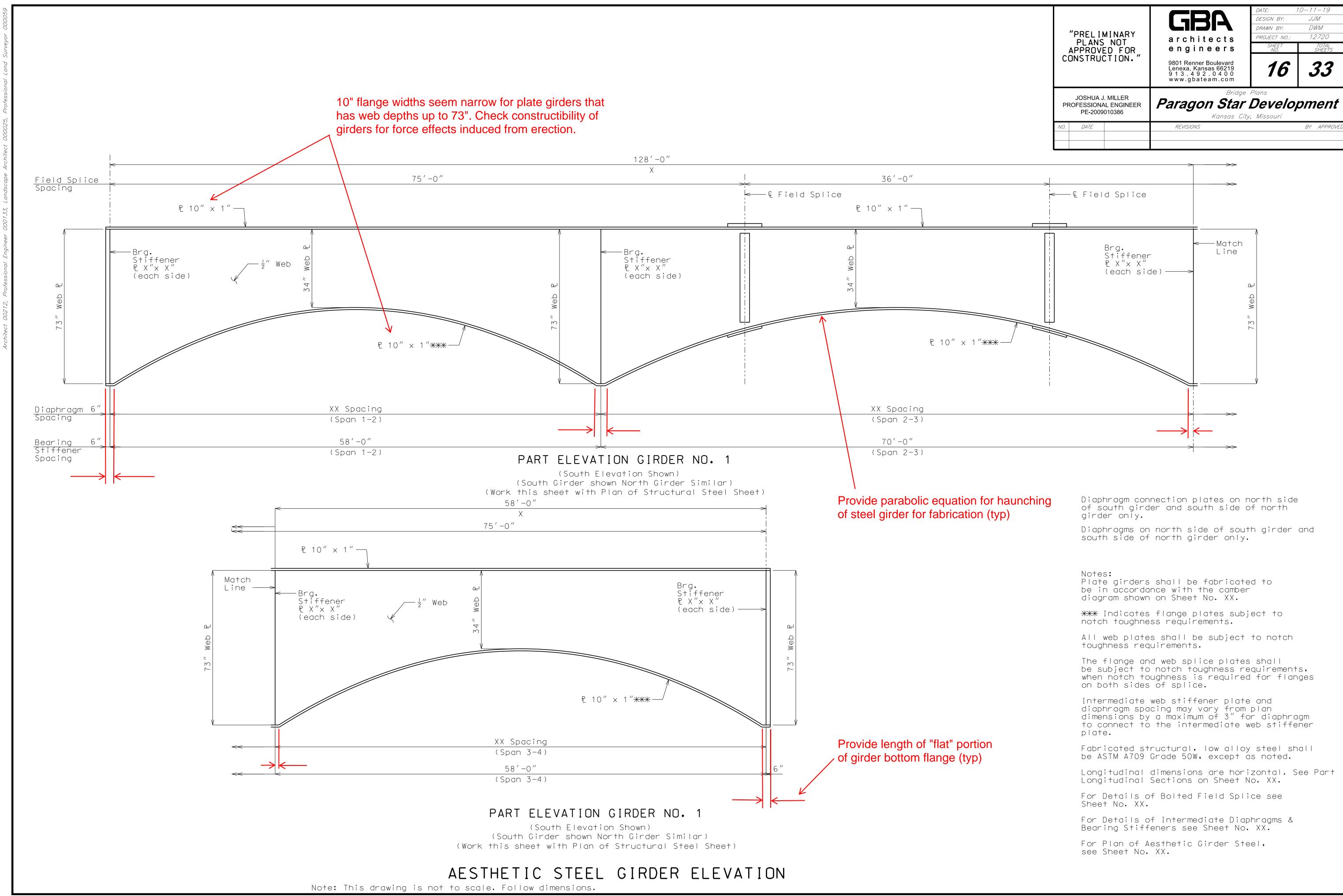
Structural steel for sole plate shall be ASTM A709 Grade 50W. The welds shall have corrosion resistance and weathering characteristics compatible with the base material.

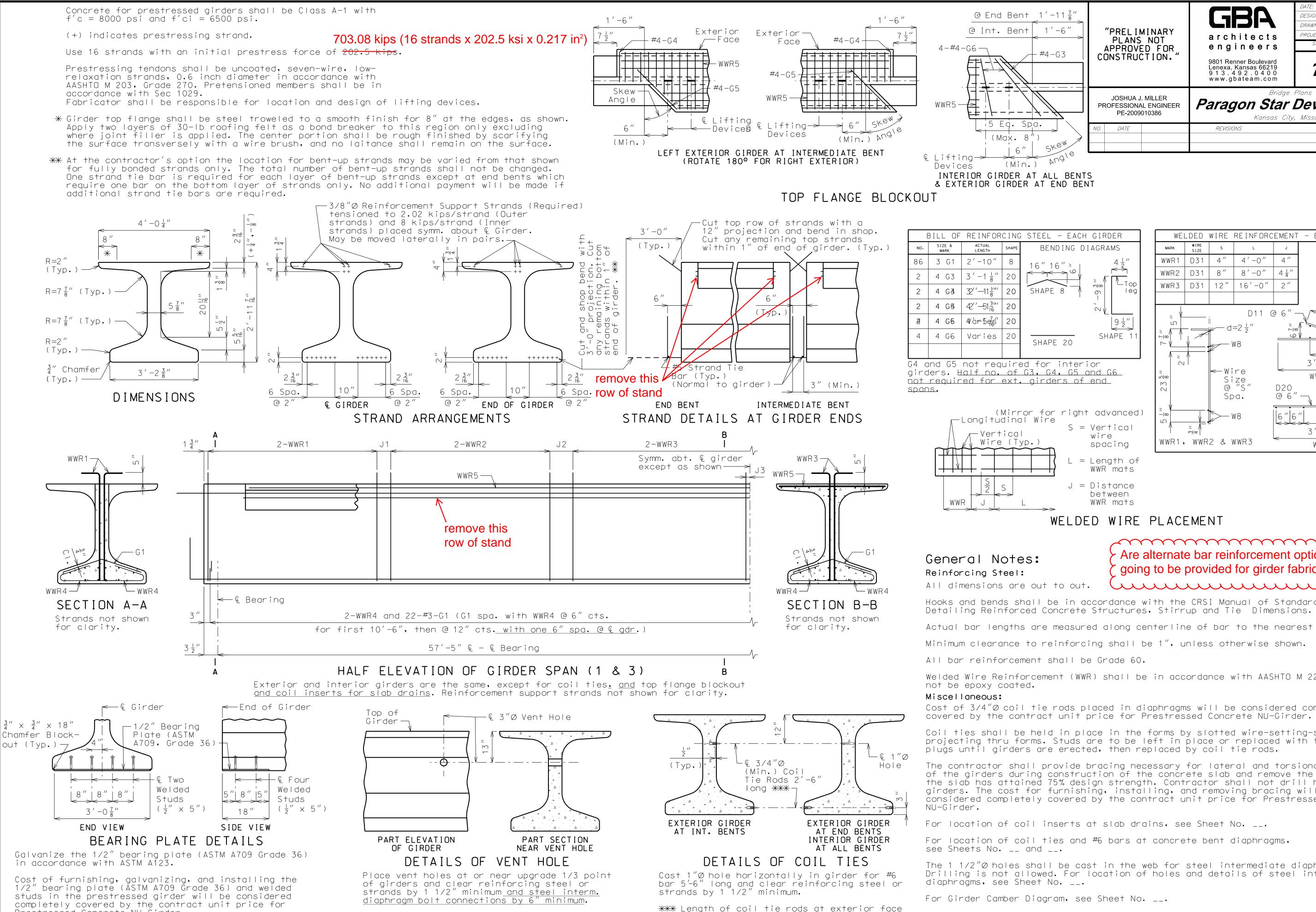
Laminated Neoprene Bearing Pad Assembly shall be in accordance with Sec

DETAILS OF LAMINATED NEOPRENE BEARING PAD ASSEMBLY

TOTAL BEARINGS







Note: This drawing is not to scale. Follow dimensions.

Prestressed Concrete NU-Girder.

BILL OF REINFORCING STEEL - EACH GIRDER WELDED WIRE REINFORCEMENT - EACH GIRDER BENDING DIAGRAMS 4'-0" 4" WWR1 | D31 | 2′-10″ WWR2 | D31 $8' - 0'' \mid 4\frac{1}{4}'$ WWR3 | D31 | 12" | 16'-0" | 2" SHAPE 8 32′ ′--11∦″' D11 @ 6' | War5es" SHAPE 1 Varies SHAPE 20 G4 and G5 not required for interior girders. Half no. of G3, G4, G5 and G6 Size @"S" not required for ext. girders of end

S = Vertical

spacing

WWR mats

L = Length of

J = Distance between WWR mats

(Mirror for right advanced)

1'-6"

#4-G3

5 Eg. Spa.

(Max. 8"

"PREL IMINARY

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PROFESSIONAL ENGINEER PE-2009010386

CONSTRUCTION.

WELDED WIRE PLACEMENT

General Notes: Reinforcing Steel:

Hooks and bends shall be in accordance with the CRSI Manual of Standard Practice for

WWR1, WWR2 & WWR3

Actual bar lengths are measured along centerline of bar to the nearest inch.

Minimum clearance to reinforcing shall be 1", unless otherwise shown.

All bar reinforcement shall be Grade 60.

Welded Wire Reinforcement (WWR) shall be in accordance with AASHTO M 221. WWR shall not be epoxy coated.

Miscellaneous:

of exterior girders at end bents = $_{-}^{\prime}$.

Cost of 3/4"Ø coil tie rods placed in diaphragms will be considered completely covered by the contract unit price for Prestressed Concrete NU-Girder.

Coil ties shall be held in place in the forms by slotted wire-setting-studs projecting thru forms. Studs are to be left in place or replaced with temporary plugs until girders are erected, then replaced by coil tie rods.

The contractor shall provide bracing necessary for lateral and torsional stability of the girders during construction of the concrete slab and remove the bracing after the slab has attained 75% design strength. Contractor shall not drill holes in the girders. The cost for furnishing, installing, and removing bracing will be considered completely covered by the contract unit price for Prestressed Concrete

For location of coil inserts at slab drains, see Sheet No. __.

For location of coil ties and #6 bars at concrete bent diaphragms, see Sheets No. __ and __.

The 1 $1/2''\emptyset$ holes shall be cast in the web for steel intermediate diaphragms. Drilling is not allowed. For location of holes and details of steel intermediate diaphragms, see Sheet No. __.

For Girder Camber Diagram, see Sheet No. __.

Alternate bar reinforcing steel details are provided and may be used. The same type of reinforcing steel shall be used for all girders in all spans.

JJM

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BENDING

DIAGRAMS

 $16\frac{3}{4}''$

(Typ.) —

 $3' - 3\frac{3}{8}''$

20"

 $3'-10\frac{1}{4}''$

WWR4

DESIGN BY

DRAWN BY:

Paragon Star Development

architects

engineers

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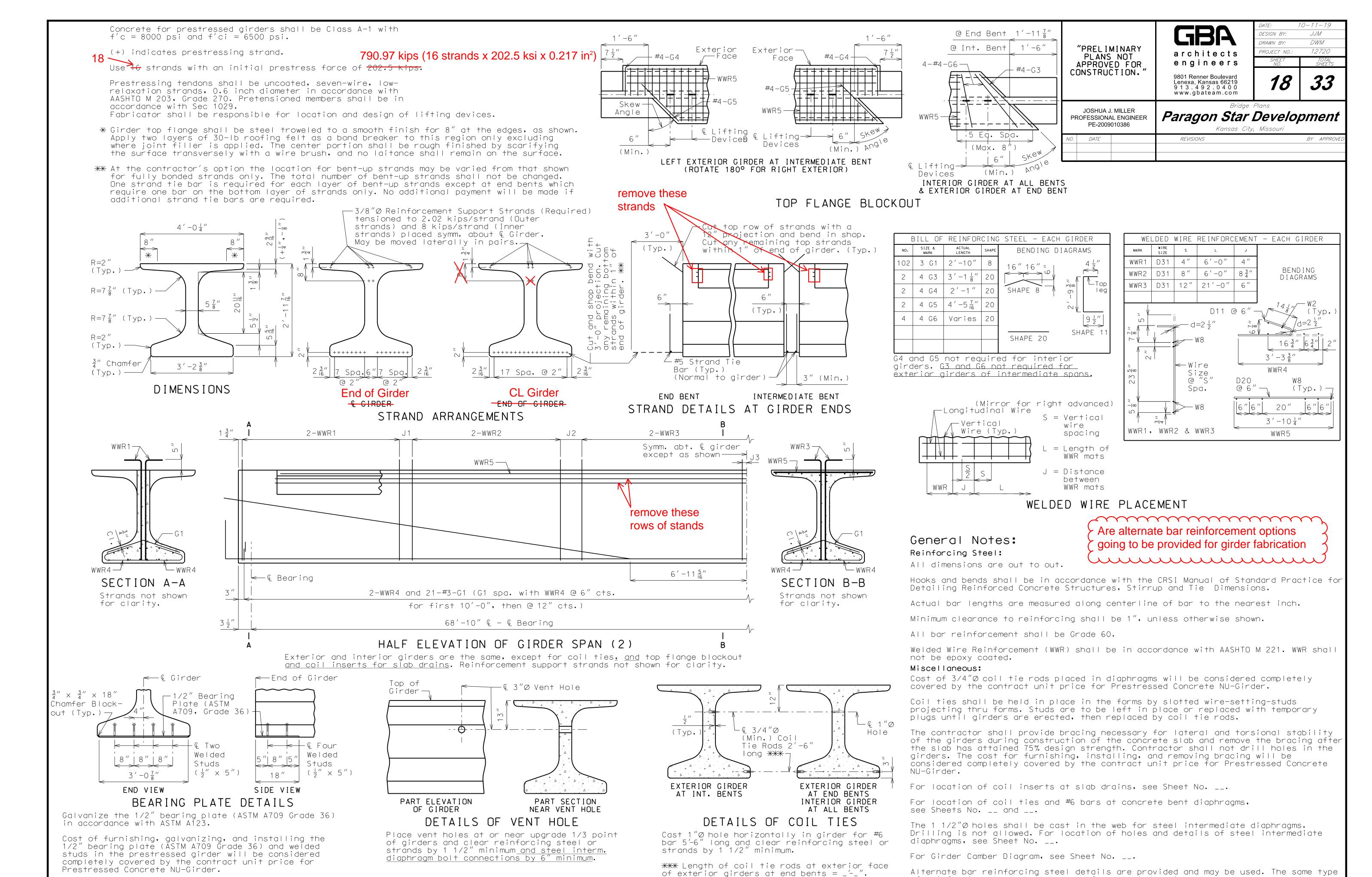
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Are alternate bar reinforcement options

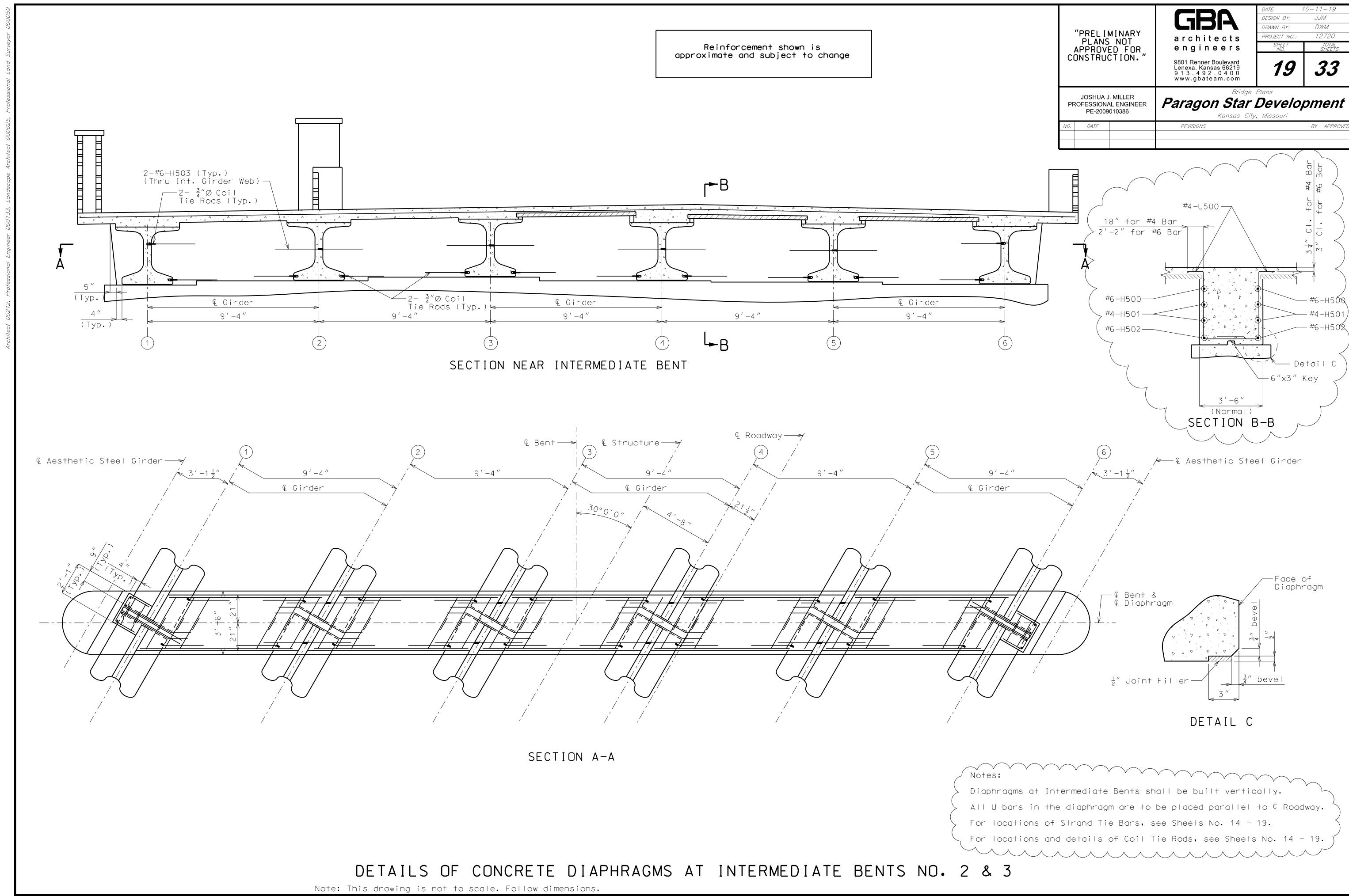
going to be provided for girder fabrication

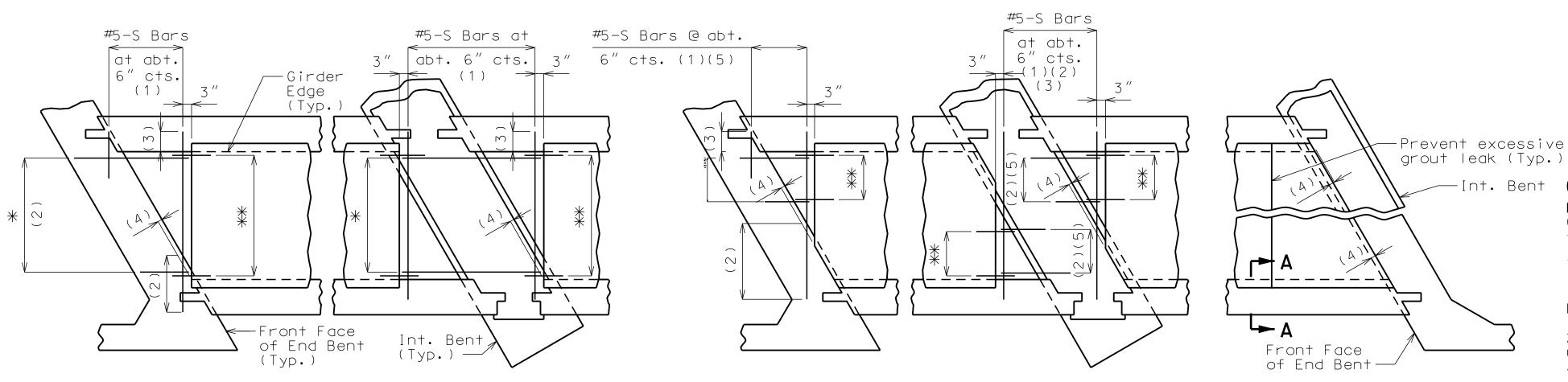


Note: This drawing is not to scale. Follow dimensions.

West Bridge: 60% Plans

of reinforcing steel shall be used for all girders in all spans.





SQUARED END PANELS OR TRUNCATED END PANELS

L/4 : L/4 : L/4 : L/4

© Strand

 $\frac{1}{2}$ " (Min.)

M M X

 ∞ \leftarrow

DW W

 $\frac{1}{2}$ " (Min.)

(Max.)

2/m

BENDING DIAGRAM FOR U1 BAR

U1 Bars may be oriented at right angles to location and spacing shown. U1 Bars shall

#3-P2 at abt.

6" cts. at top

Panel Width

SECTION B-B

(10) —

#3-P2 at abt.

6" cts. at top

Panel Width

*** 3" (Min.), 6" (Max.)

PLAN OF OPTIONAL TRUNCATED END PANEL

be placed between P1 bars.

5-#3-P3 at 6" cts.

between P2 bars (8)

#3-P1 at 12" cts.

at top (6)

3" (Min.)

(Typ.)

3/8″Ø

Strand—

 $1\frac{1}{2}''$ (Min.

3" (Max.)

May be cast

sawn to skew-

× D X

 $\infty \sqrt{}$

 $1\frac{1}{2}''$ (Min.)

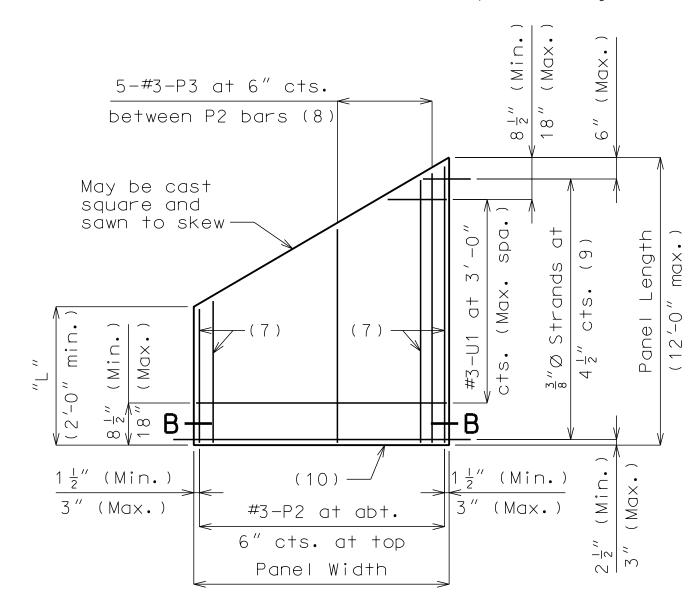
3" (Max.)

B#

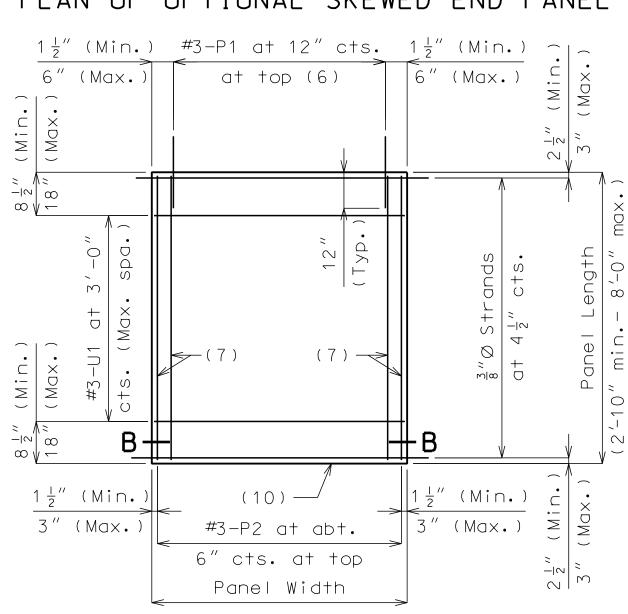
square and

PLAN SHOWING PANELS PLACEMENT

* #5-S Bars at abt. 9" cts. (1)
** #3-P1 at 12" cts. (End panels only)



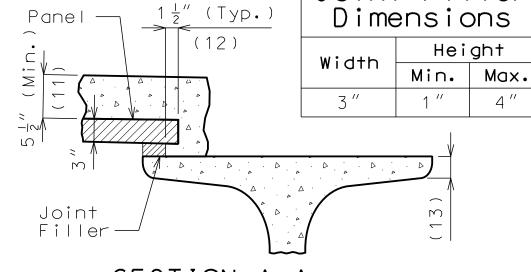
PLAN OF OPTIONAL SKEWED END PANEL



PLAN OF SQUARED PANEL

Joint Filler

SKEWED END PANELS



SECTION A-A

Reference Notes: Plan of Panels Placement:

(1) S-bars shown are bottom steel in slab between panels and used with squared and truncated end panels only.

of end bents and int. bents for squared and truncated end panels only.

(3) Extend S-bars 9 inches beyond edge of girder (Typ.).

(4) End panels shall be dimensioned 1/2" min. to 1 1/2" max. from the inside face of diaphragm.

(5) For truncated end panels, use a min. of #5-S than 2 feet. bars at 6" crossings in openings, or min. $4 \times 4 - W7 \times W7$.

Plans of Panels:

(6) For end panels only, P1 bars shall be 2'-0'' in length and embedded 12". P1 bars will not be

(7) #3-P2 bars near edge of panel at bottom (under strands).

(8) Use #3-P3 bars if panel is skewed 45° or greater.

(9) Any strand 2'-0'' or shorter shall have a #4 reinforcing bar on each side of it, centered between strands. Strands 2'-0" or shorter may then S-bars are not listed in the bill of reinforcing. be debonded at the fabricator's option.

(10) Optional 1/2" x 45° Chamfer one or both sides at bottom.

Section A-A:

(11) Slab thickness over prestressed panels minimum slab thickness, it may be necessary to raise the grade uniformly throughout the labor or materials required for necessary grade

adjustment.

under and between panels.

(13) At the contractor's option, the variation in top of flange. slab thickness over prestressed panels may be eliminated or reduced by increasing and varying the girder top flange thickness. Dimensions shall be shown on the shop drawings.

DETAILS OF PRESTRESSED PANELS

CONSTRUCTION.

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DESIGN BY

JOSHUA J. MILLER

Paragon Star Development

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-Int. Bent General Notes:

Prestressed Panels:

Concrete for prestressed panels shall be Class A-1 with f'c = 6,000 psi, f'ci = 4.000 psi.

The top surface of all panels shall receive a scored finish with a depth of scoring of 1/8" perpendicular to the prestressing strands in the panels.

Prestressing tendons shall be high-tensile strength, uncoated, seven-wire, low-relaxation strands for prestressed concrete in accordance with AASHTO M 203 Grade 270, with nominal diameter of strand = 3/8" and nominal area = 0.085 sq.in. and minimum ultimate strength = 22.95 kips (270 ksi). Larger strands may be used with the same spacing and initial tension.

Initial prestressing force = 17.2 kips/strand.

The method and sequence of releasing the strands shall be shown on the shop drawings.

Suitable anchorage devices for lifting panels may be cast in panels, provided the devices are shown on the shop drawings and approved by the engineer. Panel lengths shall be determined by the contractor and shown on the shop drawings.

When squared end panels are used at skewed bents, the skewed portion shall be cast full depth. No separate payment will be made for additional concrete and reinforcing required.

Support from diaphragm forms is required under the optional skewed end until cast-in-place concrete has reached 3,000 psi compressive strength.

Prestressed panels shall be brought to saturated surface-dry (SSD) condition just prior to the deck pour. There shall be no free standing water on the panels or in the area to

The prestressed panel quantities are not included in the table of estimated quantities for the slab. Reinforcing Steel:

All dimensions are out to out.

Hooks and bends shall be in accordance with the CRSI Manual of Standard Practice for Detailing Reinforced Concrete Structures, Stirrup and Tie Dimensions.

(2) Extend S-bars 18 inches beyond the front face Minimum clearance to reinforcing steel shall be 1 1/2", unless otherwise shown.

If U1 bars interfere with placement of slab steel, U1 loops may be bent over, as necessary, to clear slab steel.

Deformed welded wire reinforcement (WWR) providing a minimum area of reinforcing perpendicular to strands of 0.22 sq in./ft, with spacing parallel to strands sufficien to ensure proper handling, may be used in lieu of the #3-P2 bars shown. Wire diameter shall not be larger than 0.375 inch. The above alternative reinforcement criteria may be used in lieu of the #3-P3 bars, when required, and placed over a width not less

The following reinforcing steel shall be tied securely to the strands with the following maximum spacing in each direction: #3-P2 bars at 16 inches.

WWR at 24 inches.

required for panels at squared integral end bents. The #3-U1 bars shall be tied securely to #3-P2 bars, to WWR or to strands (when placed between P1 bars) at about 3-foot centers.

Minimum reinforcement steel length shall be 2'-0".

All reinforcement other than prestressing strands shall be epoxy coated.

Precast panels may be in contact with stirrup reinforcing in diaphragms.

within the limits noted in the table of Joint Filler Dimensions.

Cost of S-bars will be considered completely covered by the contract unit price for the slab. Joint Filler:

Joint filler shall be preformed fiber expansion joint material in accordance with Sec 1057 or expanded or extruded polystyrene bedding material in accordance with

Sec 1073. varies due to girder camber. In order to maintain Use Slab Haunching Diagram on Sheet No. XX for determining thickness of joint filler

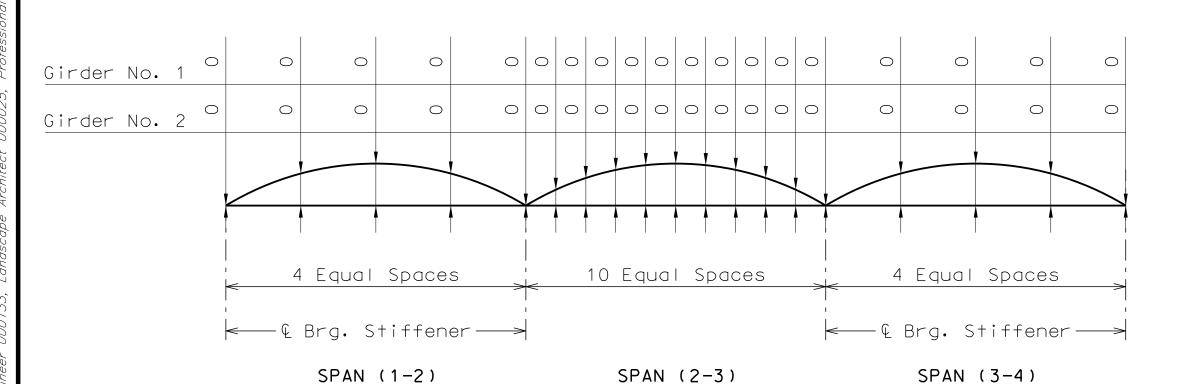
structure. No payment will be made for additional Thicker material may be used on one or both sides of the girder to reduce cast-in-place concrete thickness to within tolerances.

The same thickness of preformed fiber expansion joint material shall be used under any (12) Contractor shall ensure proper consolidation one edge of any panel except at locations where top flange thickness may be stepped. The maximum change in thickness between adjacent panels shall be 1/4 inch. The polystyrene bedding material may be cut with a transition to match haunch height above

> Joint filler shall be glued to the girder. When thickness exceeds 1 1/2 inches, the joint filler shall be glued top and bottom. The glue used shall be the type recommended by the joint filler manufacturer.

Edges of panels shall be uniformly seated on the joint filler before slab reinforcement is placed.

Note: This drawing is not to scale. Follow dimensions.



CAMBER DIAGRAM

Camber includes allowance for vertical curve and for

dead load deflection due to concrete slab, barrier

Longitudinal dimensions are measured horizontally.

curbs, pedestrian curb and structural steel.

Note:

"+" Downward from chord
"-" Upward from chord

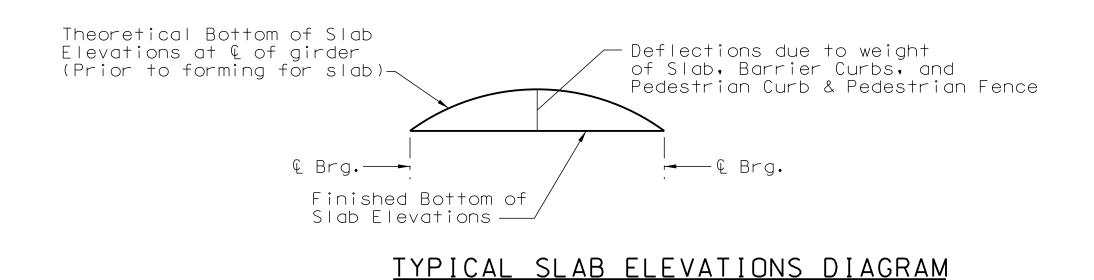
DEAD LOAD DEFLECTION

Note:

15% of dead load deflection is due to the weight of structural steel.

Dead Load deflection includes weight of structural steel, concrete slab, barrier curbs, and pedestrian curb & pedestrian fence.

GIRDER NO.	SPAN LEN	GTHS (& Brg.	- (£ Brg.)
GIRDER NO.	Span (1-2)	Span (2-3)	Span (3-4)
1	′″	′″	'"
2	′″	′″	'"



**Theoretical Bottom of Slab Elevations at & of Girder (Prior to forming for slab)

	S	Span 1 ((ì Brg€	Brg.)	
Gdr. No.	€ Brg Bent No. 1	.25	.50	. 75	& Brg Bent No. 2
1	•	•	•	•	•
2	•	•	•	•	•

				(Span 2 (€ Brg€	Brg.)				
Gdr. No.	& Brg Bent No. 2	.10	.20	.30	.40	.50	.60	.70	.80	.90	& Brg Bent No. 3
1	·	•	•	•	•	•	•	•	•	•	•
2		•	•	•	•	•	•	•		•	

		Span 3 (€ Brg€	Brg.)	
Gdr. No.	& Brg Bent No. 3	.25	.50	.75	& Brg Bent No. 4
1	•	•	•	•	•
2					

** Elevations are based on a constant slab thickness of $8\frac{1}{2}$ " and include allowance for theoretical dead load deflections due to weight of Slab, Barrier Curbs, and Pedestrian Curb & Pedestrian Fence.

Bottom of Slab

© Girder

© Girder

© Market SLAB HAUNCH

Notes:

* Dimension (bottom of slab to top of web) may vary if girder camber after erection differs from plan camber by more than or less than the % of D.L. deflection due to weight of structural steel. No payment will be made for any adjustment in forming or additional concrete required for variation in haunching.

Increase the bounch by 1/2 inch ± more then what is required

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Increase the haunch by 1/2 inch ± more than what is required to make one size shear connector work for both CIP and SIP options.

Shear connectors are not being used. Remove note.

CAMBER, HAUNCHING, & ELEVATIONS (STEEL)

Note: This drawing is not to scale. Follow dimensions.

West Bridge : 60% Plans

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DRAWN BY:

Paragon Star Development

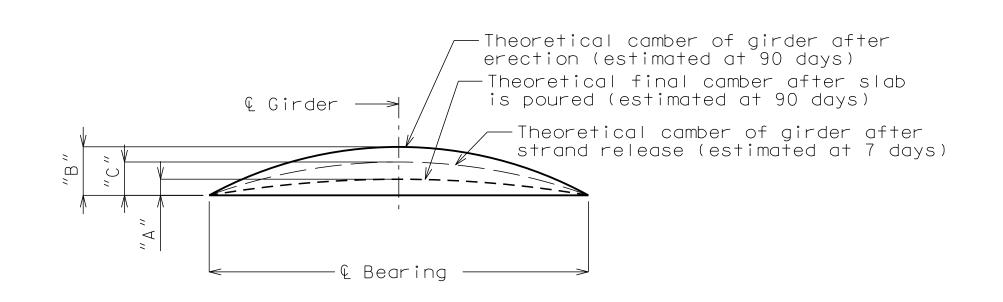
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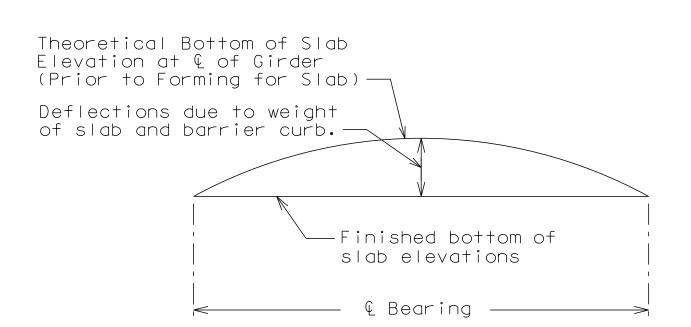
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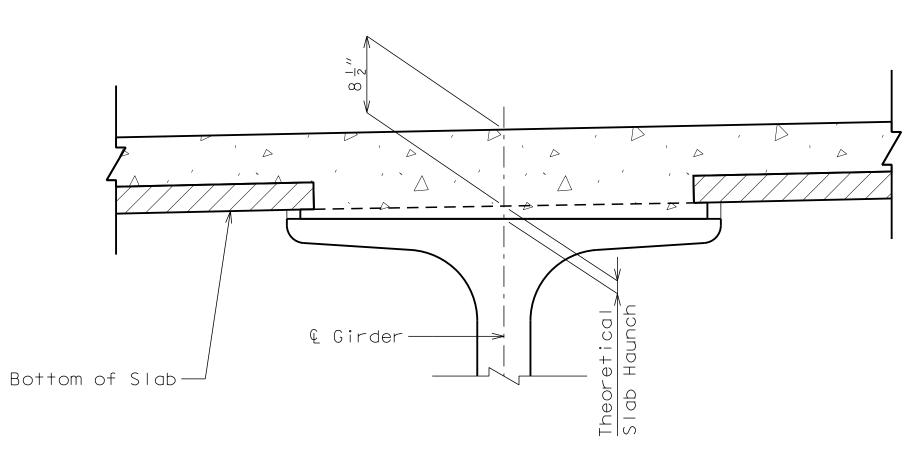
	S	pan (1-2	2)	S	pan (2-3	3)	S	pan (3-4	1)
	"A"	"B"	"C"	"A"	"B"	"C"	″A ″	"B"	"C"
Ext. Beam	"	//	//	"	//	//	"	//	//
Int. Beam	"			"			"		

GIRDER CAMBER DIAGRAM

Conversion factors for girder camber (Estimated at 90 days) $0.1 \text{ pt.} = 0.314 \times 0.5 \text{ pt.}$ $0.2 \text{ pt.} = 0.593 \times 0.5 \text{ pt.}$ $0.25 \text{ pt.} = 0.7125 \times 0.5 \text{ pt.}$ $0.3 \text{ pt.} = 0.813 \times 0.5 \text{ pt.}$ $0.4 pt. = 0.952 \times 0.5 pt.$



TYPICAL SLAB ELEVATIONS DIAGRAM



SPAN (1-2)

THEORETICAL SLAB HAUNCH

	× - 2		& \ & \		×	× 4 × × × × × × × × × × × × × × × × × ×	%	8 8 2	8 8 2	× × × × × × × × × × × × × × × × × × ×	 8 2	×	8 	× × × × × × × × × × × × × × × × × × ×	% 2
Girder No. 1	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	<u></u>	□ 1/10	~	~ \	~	- -	-
Girder No. 2	1 1 // 2	1 5 //	1 5 / 8	1 5 // 8	1 = 1 = 1	1 3 "	1 3 "	1 5 "	1 5 // 8	1 5 //	1 5 "	1 5 / 8	7 %	1 5 //	1 5 //
Girder No. 3	√ 8 5	7 8 12 12	8 5	\ 8 5	2 -	1 × × × × × × × × × × × × × × × × × × ×	۲ 8 ا	1 3 //	8 5	~ \ 8 \	7 8 5 ,	→ 8 57 ,	7 8 5	↑ 8 57 ,	15 / 8
Girder No. 4	15 / 8	1 3 // 4	, '8 	1 2 1	7 / 8	,, 2	, 2	,, 2	/ <u>8</u> /	1 2 1 8	1 3 ′′	1 4 3	1 3 // 4	2 2 2 2 2 2 2 2 2 2 	1 3 //
Girder No. 5	- C	7 8 ,	~ % 22	~ 8 52	2 2	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7 × 4 × × × × × × × × × × × × × × × × ×	7 3 / 4 / /	~ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1 5 %	~ 8 5 ,	√ 8 52 ×	7 8 ,	1 5 %	1 5 // 8
Girder No. 6	7 8 2	1 5 / 8	~ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	~ 8 2 ,	7 2	1 3 1 2 1 2 1	۲ کا کا ''	1 3 //	~ % %	7 8 2	7 8 5,	~ % %	, % 8 %	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7 %
Bottom of SI	ab —	V	V	V	V	V	·	V	V	V	V	V	V	V	V
Top of Girde	er—														
	/								1			N			
		€ 4	equal	space	es >	4	4	equal	space	ss >	•	4	equal	space	S
		<	· (L. Bea		>	•	<	€ Bea		>	<	=	€ Bea		>
			57′-	- //				68′-	4 0 //				57′-	- //	

If girder camber is different from that shown in the camber diagram, in order to maintain minimum slab thickness, an adjustment of the slab haunches, an increase in slab thickness or a raise in grade uniformly throughout the structure shall be necessary. No payment will be made for additional labor or materials required for variation in haunching, slab thickness or grade adjustment.

Concrete in the slab haunches is included in the Estimated Quantities for Slab on Concrete NU Girder.

SPAN (2-3)

THEORETICAL SLAB HAUNCHING DIAGRAM (ESTIMATED AT 90 DAYS)

	T						Elevat slab)						er		
	Span	$(1-2) (5^{\circ}$	7'-5" @ t	org – (į l	org.)	Span	(2-3) (68	3′-10″ €	brg - Q	brg.)	Span	(3-4) (5)	7′-5″ Q	brg – Ę	brg.)
	€ brg.	. 25	• 50	. 75	€ brg.	€ brg.	0.25	0.50	0.75	€ brg.	€ brg.	. 25	•50	. 75	€ brg.
Girder No. 1	769.64	769.84	770.03	770.19	770.33	770.34	770.59	770.88	770.99	771.05	771.06	771.20	771.28	771.31	771.28
Girder No. 2	769.73	769.94	770.12	770.29	770.43	770.45	770.71	771.00	771.11	771.18	771.19	771.34	771.43	771.46	771.44
Girder No. 3	769.70	769.91	770.10	770.26	770.41	770.43	770.69	771.00	771.12	771.19	771.20	771.36	771.46	771.49	771.50
Girder No. 4	769.45	769.67	769.86	770.03	770.19	770.21	770.48	770.79	770.91	771.00	771.01	771.17	771.27	771.32	771.35
Girder No. 5	769.21	769.43	769.63	769.80	769.96	769.98	770.25	770.57	770.70	770.80	770.81	770.97	771.09	771.14	771.17
Girder No. 6	769.45	769.67	769.86	770.03	770.19	770.21	770.48	770.79	770.91	771.00	771.01	771.17	771.27	771.32	771.35

Elevations are based on a constant slab thickness of $8\frac{1}{2}''$ and include allowance for theoretical dead load deflections due to weight of slab (including precast panel) and barrier curb.

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BY APPROVE

DESIGN BY:

DRAWN BY:

Paragon Star Development

architects

engineers

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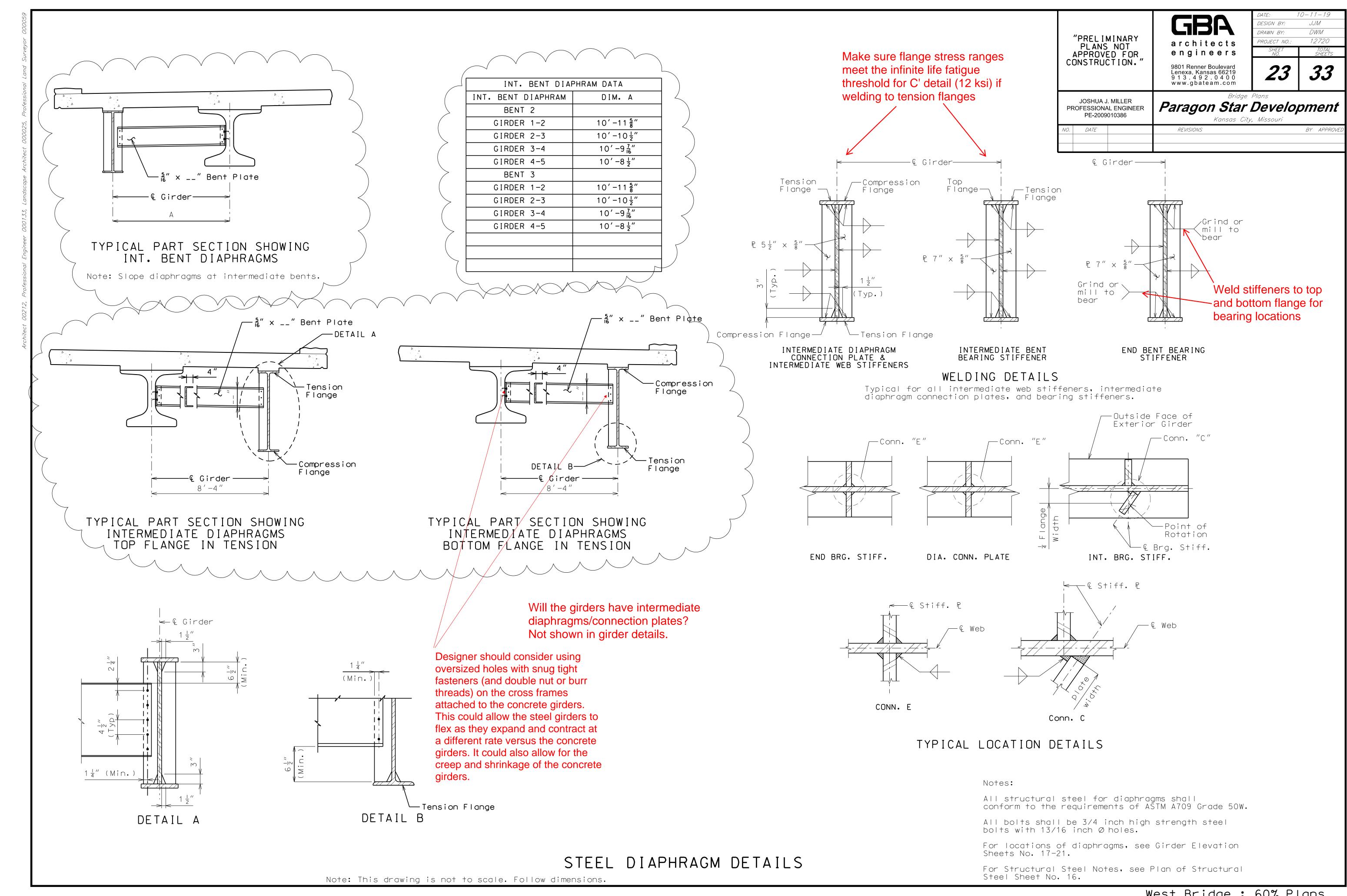
PROFESSIONAL ENGINEER

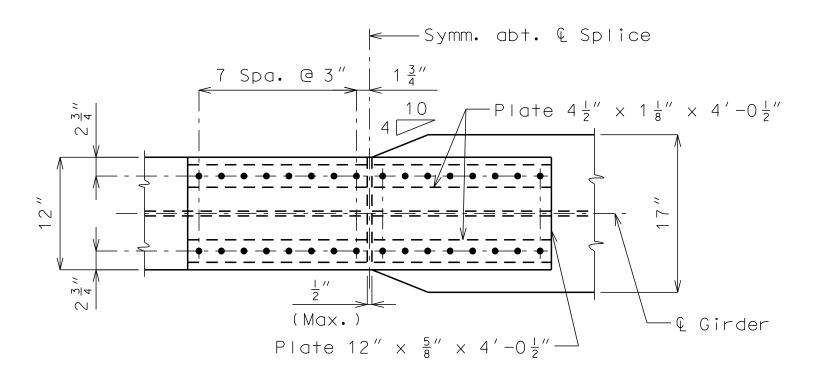
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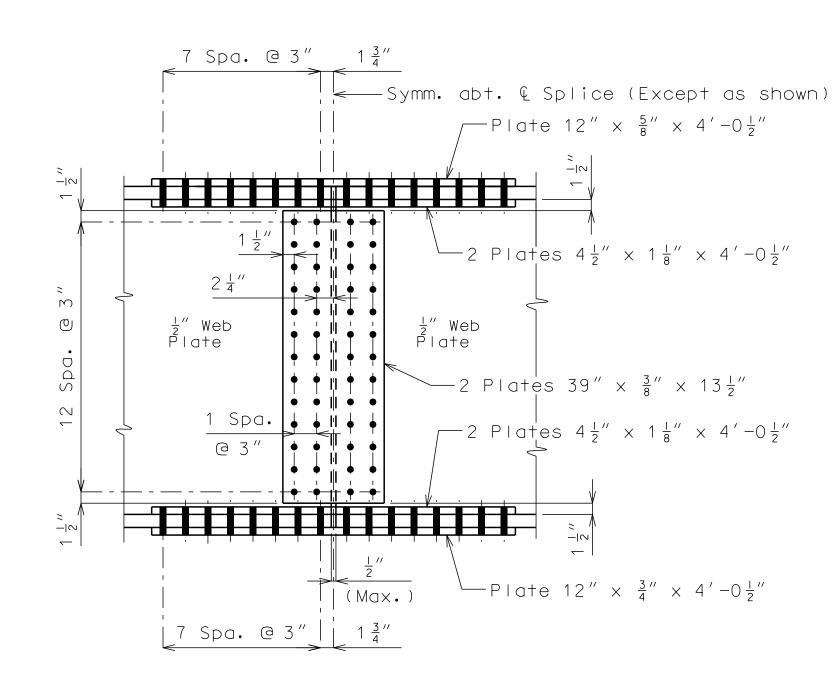
SPAN (3-4)

CONSTRUCTION.





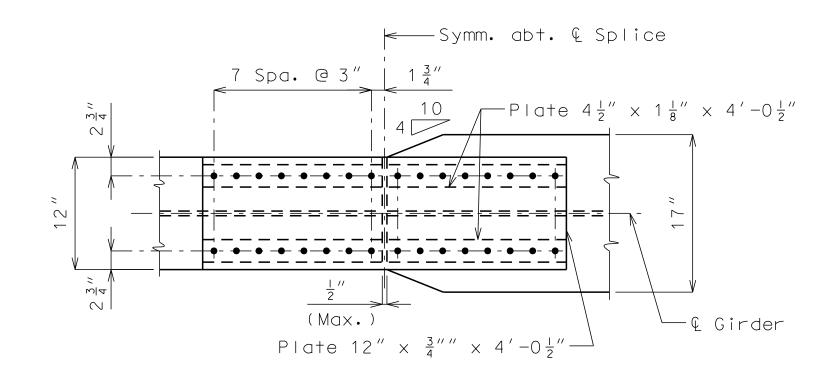
PLAN OF TOP FLANGE SPLICE PLATE



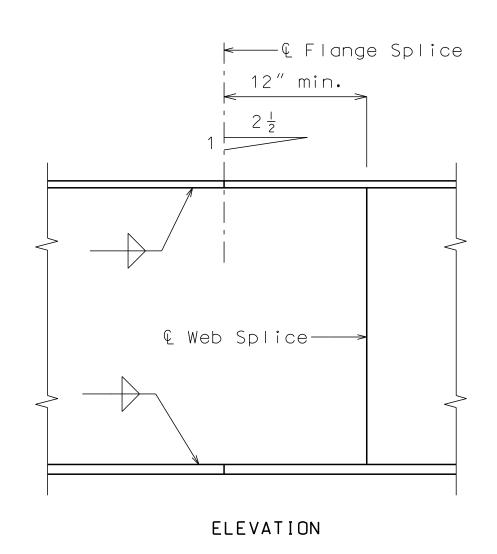
DETAIL OF BOLTED FIELD SPLICE

Use 7/8"Ø high strength bolts with 15/16"Ø holes.

Contact surfaces shall be in accordance with Sec 1081 for surface preparation.



PLAN OF BOTTOM FLANGE SPLICE PLATE



WELDED SHOP WEB AND FLANGE SPLICE

Welded shop web and flange splices may be permitted when detailed on the shop drawings and approved by the engineer. No additional payment will be made for optional welded shop web and flange splices.

Splice detail is approximate and subject to change

This will be reviewed with next submittal

SPLICE PLATE DETAILS OF AESTHETIC STEEL GIRDER

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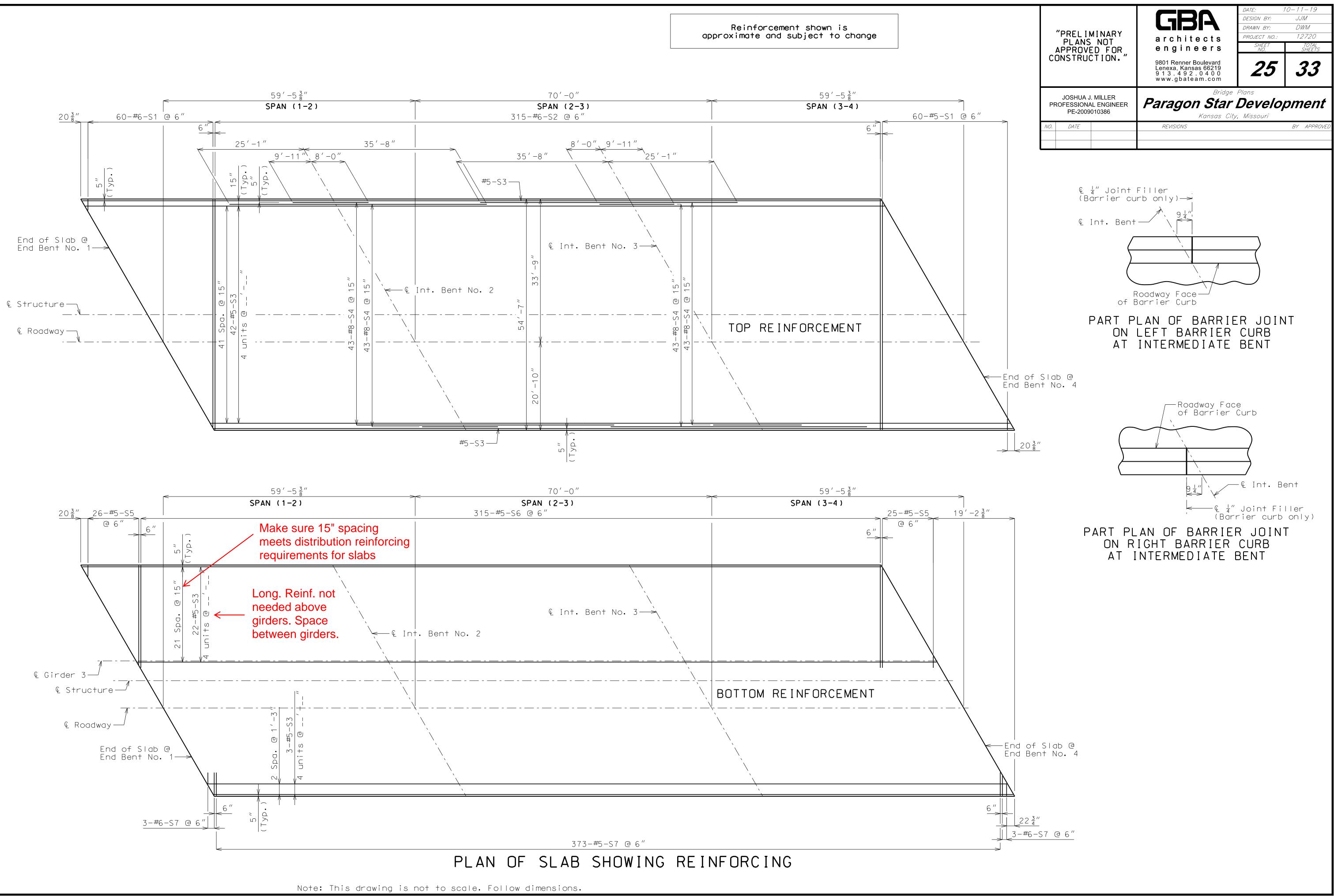
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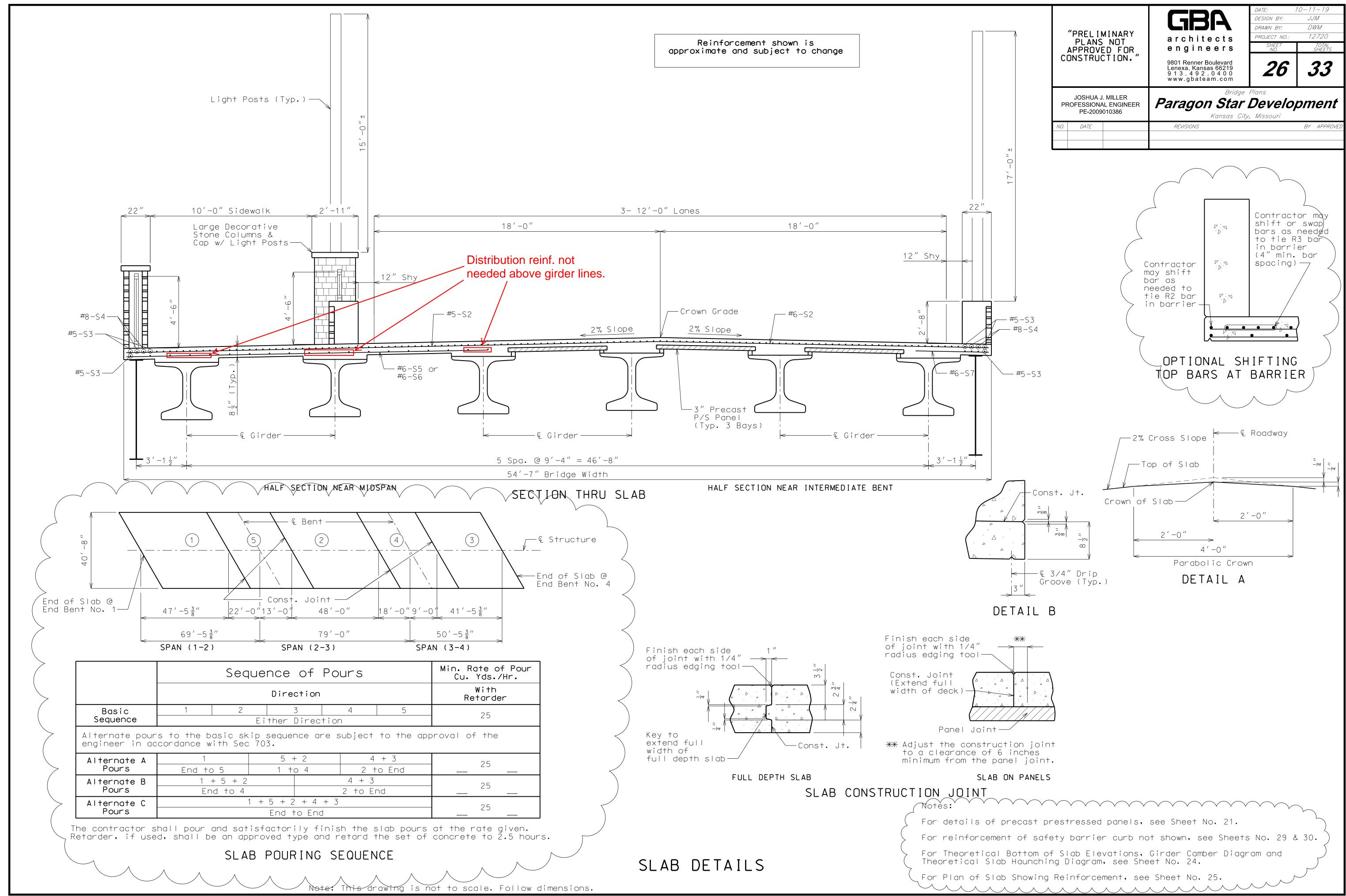
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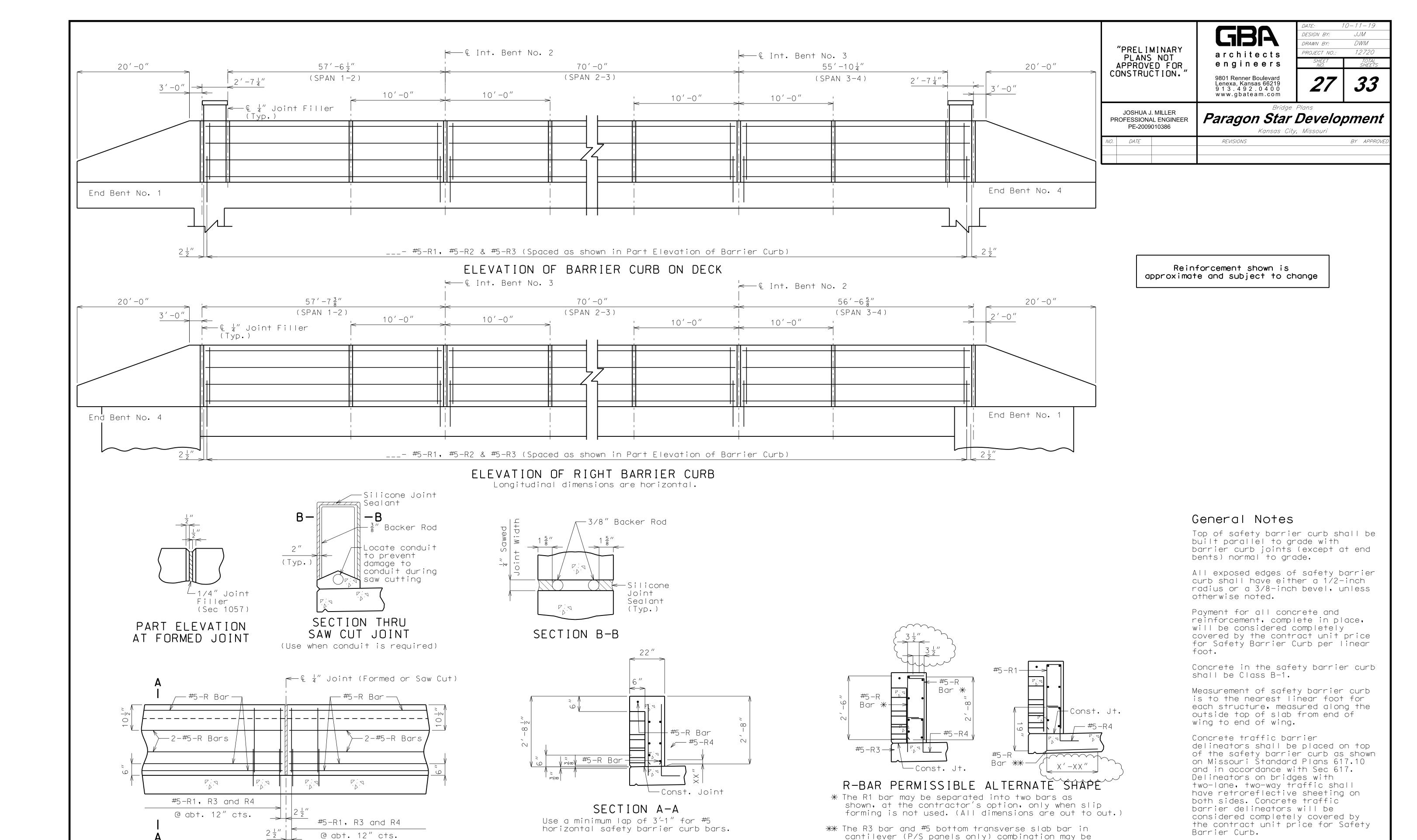
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PROJECT NO.:







The cross-sectional area above the

CONVENTIONAL-FORMED SAFETY BARRIER CURB

slab = X.XX sq. ft.

Note: This drawing is not to scale. Follow dimensions.

PART ELEVATION OF SAFETY BARRIER CURB

Plastic waterstop shall not be used with saw cut joints.

furnished as one bar as shown, at the contractor's

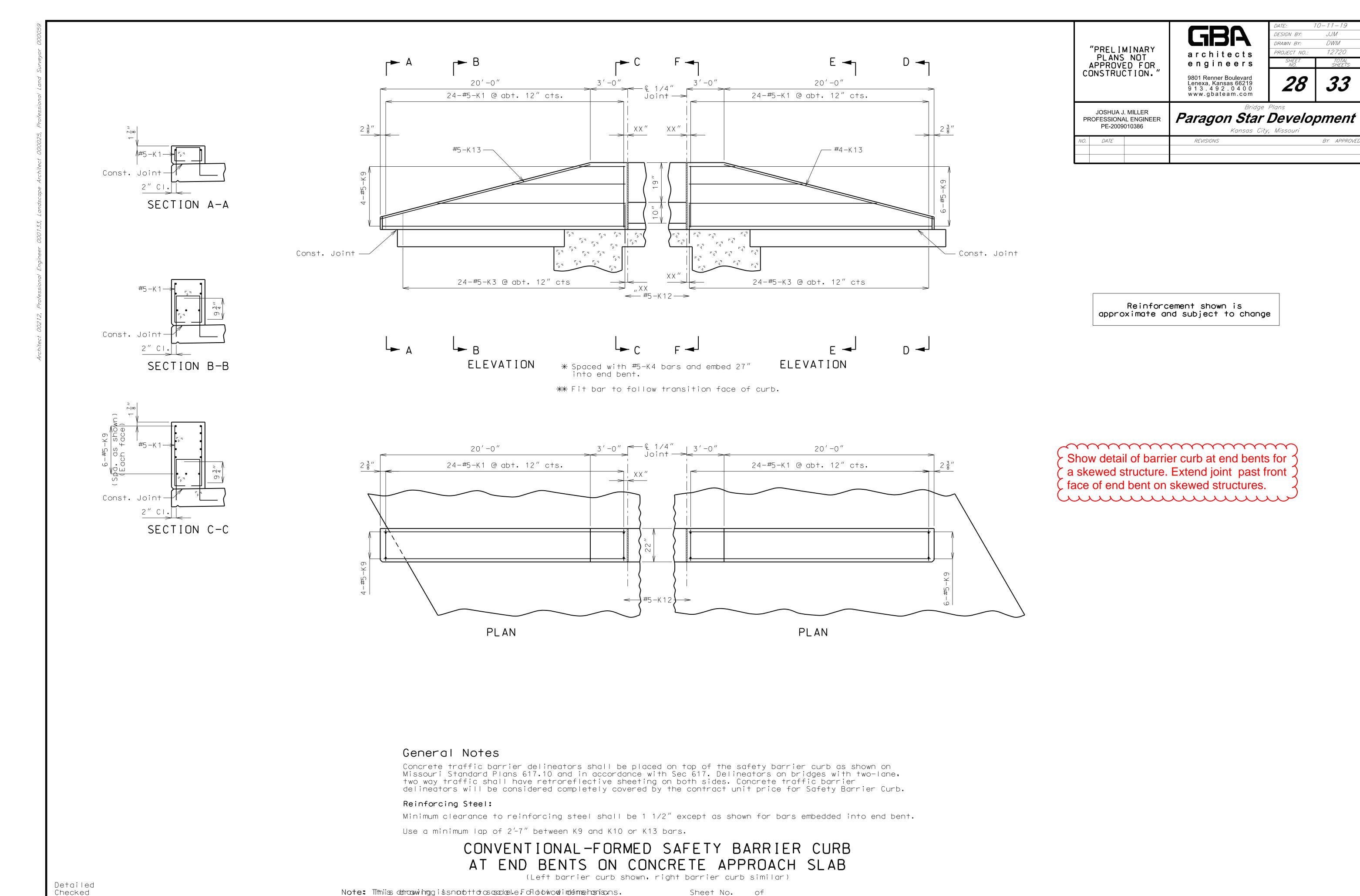
option.

West Bridge : 60% Plans

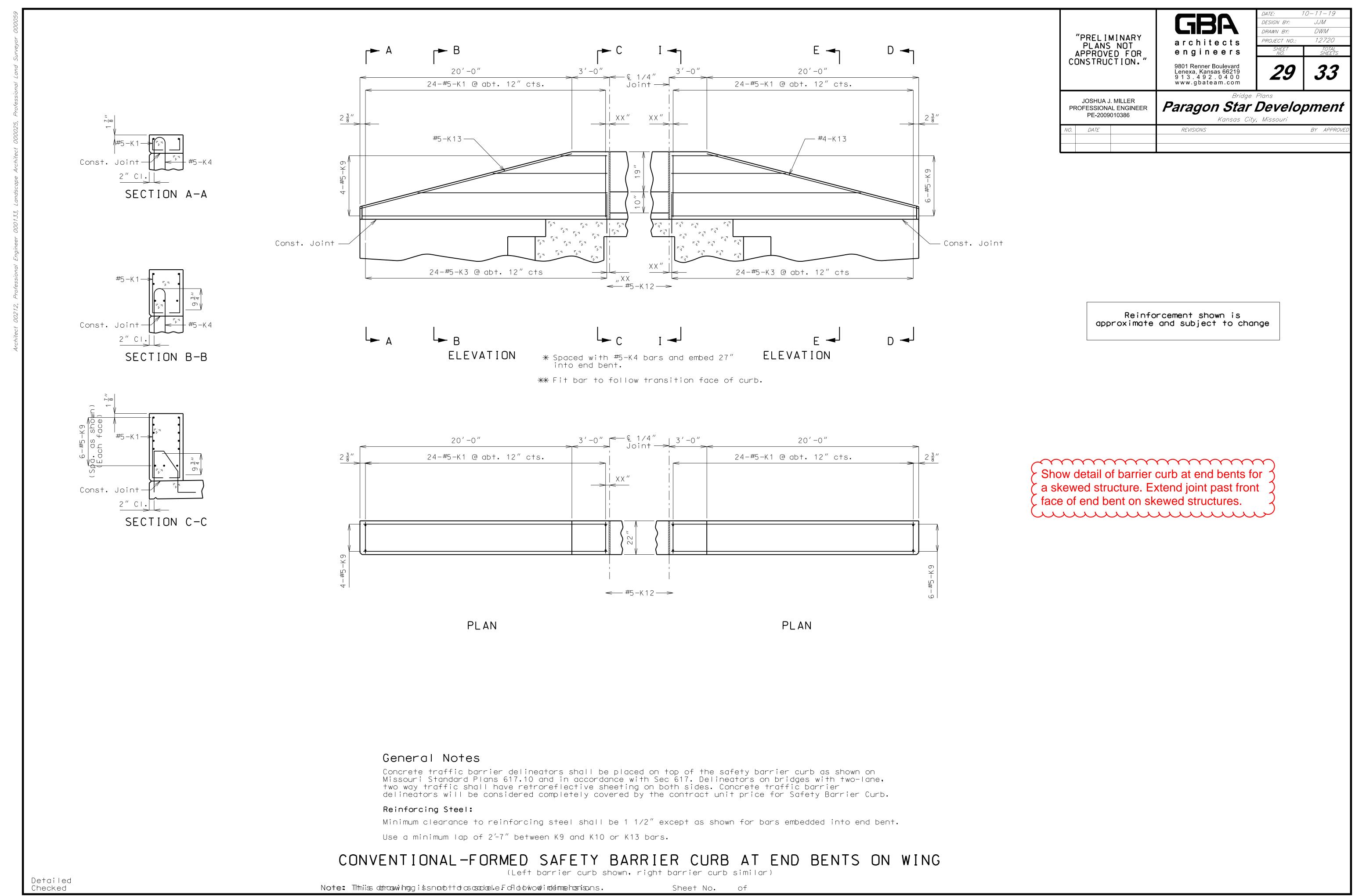
Joint sealant and backer rods shall

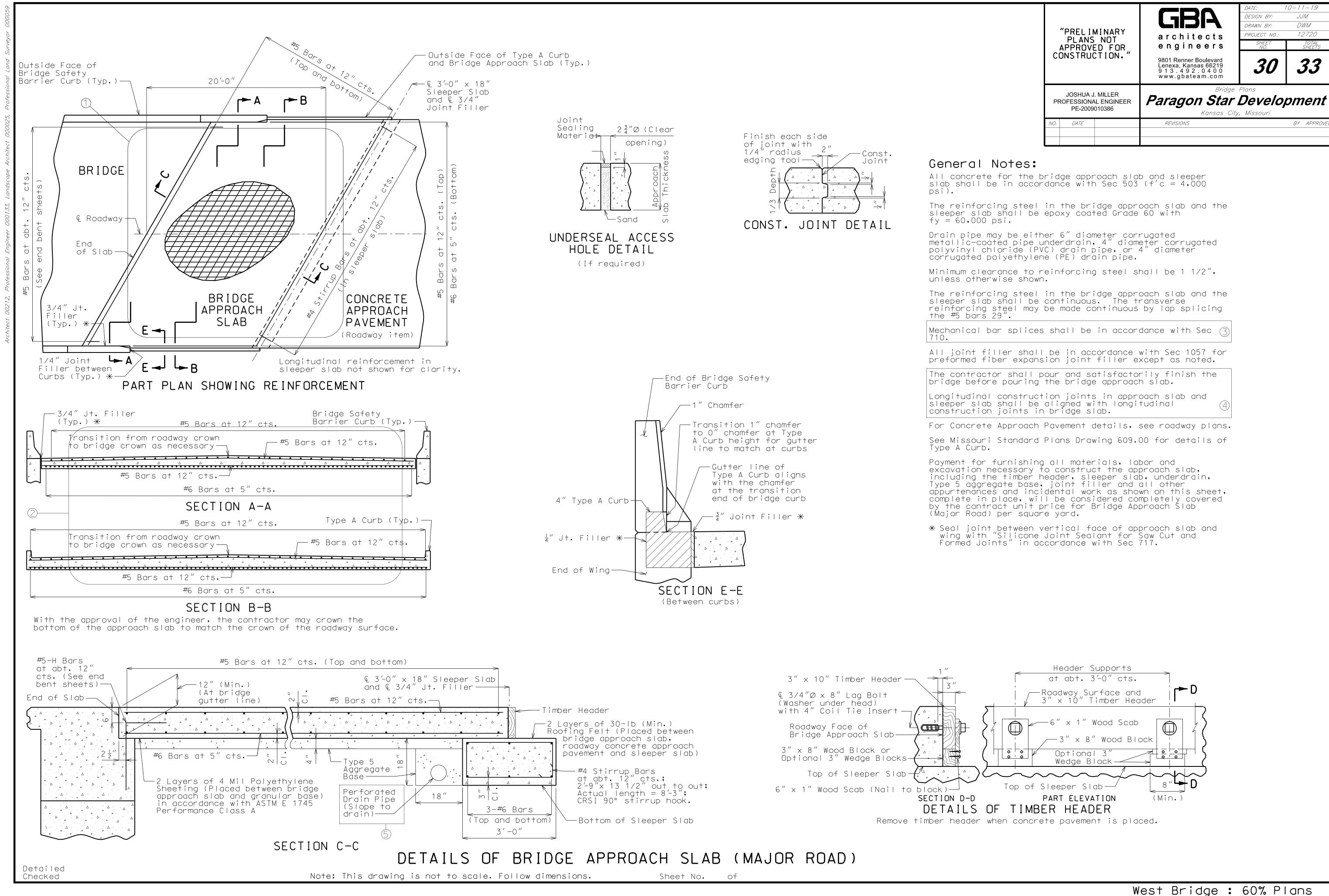
be in accordance with Sec 717 for silicone joint sealant for saw cut

and formed joints.



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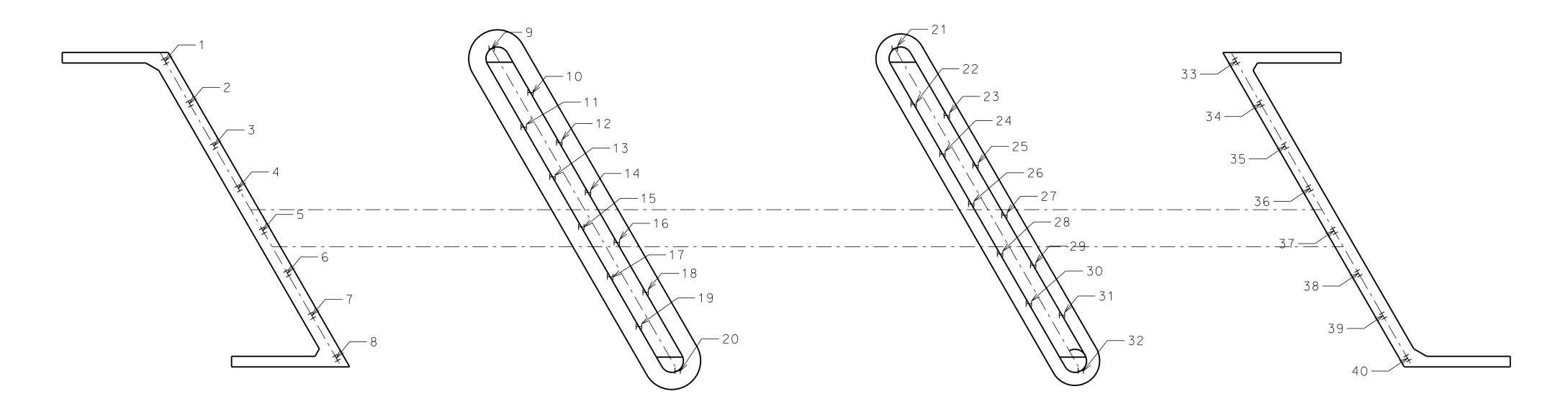
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Bridge Plans

Paragon Star Development

REVISIONS DATE



		,	As-Built	Pile Do	nta
Pile No.	Length in Place (ft)	Compressive	PDA End of Drive Blow Count (blows/in.)	Actual End of Drive Blow Count (blows/in.)	Remarks
					END BENT NO. 1
1					
2					
3					
4					
5					
6					
7					
8					
					THE DENT NO. 0
					INT. BENT NO. 2
9					
10					
11					
13					
14					
15					
16					
17					
18					
19					
20					

		,	As-Built	Pile Do	nta
Pile No.	Length in Place (ft)	Compressive	PDA End of Drive Blow Count (blows/in.)	Drive Blow	Remarks
					INT. BENT NO. 3
21					
22					
23					
24					
25					
26					
27					
28					
29					
30					
31					
32					
					END BENT NO. 4
33					
34					
35					
36					
37					
38					
<u> </u>					
<u> </u>					
70					

Quantity of piles is approximate.

Location and length of piles is approximate and subject to change

Indicate in remarks column:
A. Pile type and grade
B. Batter C. Driven to practical refusal
D. PDA test pile E. Minimum tip elevation controlled (Use when actual blow count is less than PDA blow count due to minimum tip elevation requirement. A plus sign (+) shall be placed after the PDA nominal axial compressive

This sheet to be completed by MoDOT construction personnel.

resistance value indicating actual value is higher than PDA value.)

