

February 28, 2019

Mike Weisenborn Project Manager, Development Center City of Lee's Summit 220 SE Green Street Lee's Summit, MO 64063

Re: 18-0251 Burton Townhomes Sanitary Sewer Impact Statement

Mr. Weisenborn:

Per the requirements provided by the City of Lee's Summit's planning code regarding the preliminary development plan submittal for the proposed Burton Townhomes, a sanitary sewer impact analysis has been conducted. The following is a report of the analysis.

PROJECT DESCRIPTION

The proposed Burton Townhomes development is in the City of Lee's Summit, Jackson County, MO. The project is located on the southwest corner of NW Olive St and NW Orchard Dr and is 3.76 acres in size. A site location map has been provided as Exhibit A. The complex generally consists of nine primary townhomes and associated infrastructure. The entire site is located within the Cedar Creek Watershed. Refer to Exhibit B for a layout of the proposed complex.

METHODOLOGY

Based on the provisions outlined in the Lee's Summit Design and Construction Manual (LS DCM) 6500 for Sanitary Sewers, the peak sanitary sewer flow has been determined. Using as-builts and survey information on the existing sanitary sewer infrastructure, the existing sanitary sewer system has been analyzed to determine if the proposed flows will require any modifications to the existing system.

EXISTING PEAK FLOW

The existing sanitary sewer system services residential housing, two warehouses, a storage facility, a commercial lumber yard, an office building, a church, and a veterinarian complex. The existing residential area and surrounding non-residential developments were analyzed to determine the existing peak flowrate conditions. The LS DCM 6501.C was used to calculate peak sanitary sewer flowrates for the existing system. The peak sanitary sewer flow is the summation of the peak base flow, the peak infiltration, and peak inflow of the existing residential and non-residential developments. Jackson County Incentive Viewer was used to determine lot acreage. An existing sanitary sewer layout was provided by the City of Lee's Summit. Refer to Exhibit C (Existing Site) for a layout of the existing sanitary sewer and lot lines used to determine existing peak flowrates. A summary of the sanitary sewer peak flows calculated for the existing use has been provided in Table 1.



	Table 1. Summary of Existing Sanitary Sewer Peak Flows											
	Contributing			Peak			Peak Inflo	w		Dook	Peak	
Res Nor De	Residential and Non-Residential Developments	Area (Ac.)	EDU	Base Flow (gpd)	Peak Infiltration	Time of Concentration T₅ (min)	Intensity i (iph)	Peak Inflow Q (cfs)	Peak Inflow (gpd)	Flow (gpd)	Flow Rate (cfs)	
	Ex Residential 1	1.33	-	2,000	667	19.96	6.27	0.025	16,209	18,875	0.029	
~	Lumber Yard	0.58	0.1	761	291	16.19	6.98	0.024	15,752	16,804	0.026	
of RF	Ex Residential 2	1.68	-	2523	841	21.16	6.12	0.031	19,957	23,321	0.036	
ast o	Office Building	0.07	0.3	257	33	9.33	8.13	0.003	2,069	2,359	0.004	
ш	Church	0.10	0.5	675	52	10.47	7.84	0.005	3,141	3,867	0.006	
	Animal Hospital	0.21	0.4	1,093	105	12.50	7.58	0.010	6,147	7,345	0.011	
	Ex Residential 3	1.44	-	2,153	718	20.33	6.22	0.054	34,624	37,495	0.058	
	Ex Residential 4	1.81	-	2,716	905	21.56	6.07	0.066	42,616	46,237	0.072	
f RR	Storage Unit Facility	6.72	0.1	8,780	3,359	30.02	4.98	0.201	129,753	141,893	0.220	
est o	Ex Residential 5	1.48	-	2,226	742	20.50	6.02	0.054	34,645	37,613	0.058	
Ň	Warehouse 1	1.03	0.1	1,348	516	18.71	6.43	0.040	25,720	27,584	0.043	
	Warehouse 2	0.68	0.1	889	340	16.84	6.67	0.027	17,590	18,819	0.029	
	Ex Residential 6	2.07	-	3,109	1,036	22.31	5.97	0.074	47,987	52,132	0.081	
	Total	19.2		9,462	9604			0.613	396,210	415,275	0.672	

PROPOSED PEAK FLOW

The proposed sanitary sewer system will service a 3.76 acre of multi-family townhomes along NW Olive St. This residential development was analyzed to determine the proposed peak sanitary sewer flowrate conditions. The LS DCM 6501.C was used to calculate the peak sanitary sewer flow for the proposed multi-family townhomes. The peak sanitary sewer flow is the summation of the peak base flow, the peak infiltration, and the peak inflow of the proposed townhomes as well as existing residential and non-residential developments. A summary of the flows calculated for proposed use and existing use has been provided in Table 2. Refer to Exhibit D (Proposed Site) for details regarding the proposed peak sanitary sewer flow calculations.



	Table 2. Summary of Proposed Sanitary Sewer Peak Flows												
	Contributing			Peak			Peak Inflow	v		Deek	Peak		
	Residential and Non-Residential Developments	Area (Ac.)	EDU	Base Flow (gpd)	Peak Infiltration	Time of Concentration T₀ (min)	Intensity i (iph)	Peak Inflow Q (cfs)	Peak Inflow (gpd)	Flow (gpd)	Flow Rate (cfs)		
	Prop Townhomes	3.76	-	5,280	1,760	25.50	5.56	0.059	37,948	44,988	0.074		
	Ex Residential 1	1.33	-	2,000	667	19.96	6.27	0.025	16,209	18,875	0.029		
RR	Lumber Yard	0.58	0.1	761	291	16.19	6.98	0.024	15,752	16,804	0.026		
st of	Ex Residential 2	1.68	-	2523	841	21.16	6.12	0.031	19,957	23,321	0.036		
Eas	Office Building	0.07	0.3	257	33	9.33	8.13	0.003	2,069	2,359	0.004		
	Church	0.10	0.5	675	52	10.47	7.84	0.005	3,141	3,867	0.006		
	Animal Hospital	0.21	0.4	1,093	105	12.50	7.58	0.010	6,147	7,345	0.011		
	Ex Residential 3	1.44	-	2,153	718	20.33	6.22	0.054	34,624	37,495	0.058		
	Ex Residential 4	1.81	-	2,716	905	21.56	6.07	0.066	42,616	46,237	0.072		
f RR	Storage Unit Facility	6.72	0.1	8,780	3,359	30.02	4.98	0.201	129,753	141,893	0.220		
est o	Ex Residential 5	1.48	-	2,226	742	20.50	6.02	0.054	34,645	37,613	0.058		
We	Warehouse 1	1.03	0.1	1,348	516	18.71	6.43	0.040	25,720	27,584	0.043		
	Warehouse 2	0.68	0.1	889	340	16.84	6.67	0.027	17,590	18,819	0.029		
	Ex Residential 6	2.07	-	3,109	1,036	22.31	5.97	0.074	47,987	52,132	0.081		
	Total	22.7		33,809	11364			0.672	434157	479,331	0.746		

SANITARY IMPACT ANALYSIS

The capacities of the existing sanitary sewer infrastructure have been modeled to verify that the existing infrastructure is adequate to support the estimated peak sanitary sewer flows from the proposed sites. Sanitary flows are conveyed to an existing 4' concrete sanitary sewer manhole north of the proposed site. Table 3 provides a summary of the existing pipes as well as pipe flow capacity in the system based on survey and provided as-built information. Flow capacities were calculated using Manning's Equation. The information for pipe 30-051 was provided via survey. Flowlines and length for pipes 30-068 through 30-009 were not provided by survey nor are reflected in the provided as-built information. Slopes for pipes 30-068 through 30-009 were assumed based on minimum requirements per LS DCM 6500 D.2.d. Pipe size was assumed to be 8" for pipes 30-068 through 30-010, and 10" for pipe 30-009. See Exhibit E for provided as-built information.

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	Pipe ID	Pipe Length (ft)	US Flowline (ft)	DS Flowline (ft)	Pipe Slope (ft/ft)	Manning's n	Pipe Size (in)	Pipe Area (sf)	Flow Capacity (cfs)
	30-051	323.77	1007.25	1005.95	0.004	0.015	8	0.35	0.664
RR	30-031	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
it of	30-014	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
Eas	30-013	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-010	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-047	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-029	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-068	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
ĸ	30-030	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
of RI	30-026	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
/est	30-012	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
S	30-005	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-006	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-007	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-008	N/A	N/A	N/A	0.006	0.015	8	0.35	0.813
	30-009	N/A	N/A	N/A	0.006	0.015	10	0.55	1.475

Table 3. Summary of Existing Sanitary System & Flow Capacities

Table 4 provides a summary of the proposed system as well as pipe flow capacity in the proposed system based on Manning's Equation.

Table 4. Summary of Froposed Samilary System & Flow Capacities										
	Pipe	US	DS	Pipe	Manning's	Pipe	Pipe	Pipe Flow		
Pipe ID	Length	Flowline	Flowline	Slope	n	Size	Area	Capacity		
			/				16711	17-16-1		
	(11)	(11)	(11)	(iuii)		(111)	(31)	(015)		

Table 4. Summary of Proposed Sanitary System & Flow Capacities

The existing peak flow rate was modeled in the existing system to determine current capacity and service conditions. The location of contributing laterals from residential and non-residential developments were assumed based on the existing sanitary sewer layout. Table 5 gives a summary of the existing sanitary sewer impact under existing conditions. See Exhibit C for pipe performance models of the existing sanitary pipes under existing conditions.



	Contributing Residential and Non-Residential Developments	Pipe ID	Pipe Slope (ft/ft)	Pipe Size (in)	Existing Flow Rate (cfs)	Depth (ft)	Accumulative Flow Rate (cfs)	Accumulative Depth (ft)	Pipe Velocity (ft/s)
	Ex Residential South + Lumber	30-051	0.004	8	0.055	0.13	0.055	0.13	1.14
East of RR	Ex Residential North	30-031	0.006	8	0.036	0.10	0.091	0.15	1.53
	Office, Church, Hospital	30-014	0.006	8	0.021	0.08	0.112	0.17	1.58
	N/A	30-013	0.006	8	0.021	0.08	0.112	0.17	1.58
	N/A	30-010	0.006	8	0.021	0.08	0.112	0.17	1.58
	Ex Residential 3	30-047	0.006	8	0.058	0.13	0.058	0.13	1.20
	Ex Residential 4	30-029	0.006	8	0.072	0.14	0.130	0.19	1.57
	Storage Unit Facility	30-068	0.006	8	0.220	0.24	0.220	0.24	1.93
R	Ex Residential 5	30-030	0.006	8	0.058	0.13	0.407	0.34	2.25
of F	Warehouse 1	30-026	0.006	8	0.043	0.11	0.450	0.36	2.32
Nest	Warehouse 2	30-012	0.006	8	0.029	0.09	0.479	0.37	2.39
-	Ex Residential 6	30-005	0.006	8	0.081	0.15	0.081	0.15	1.36
	N/A	30-006	0.006	8	0.081	0.15	0.081	0.15	1.36
	N/A	30-007	0.006	8	0.110	0.17	0.560	0.41	2.47
	N/A	30-008	0.006	8	0.110	0.17	0.560	0.41	2.47
	N/A	30-009	0.006	10	0.131	0.17	0.672	0.40	2.60

Table 5. Outlinding of Existing Outliding impact officer Existing Conditions
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The proposed peak flow rate (along with the existing peak flowrate) was modeled in the existing system to determine if it is adequate to receive and convey the flows from the proposed development. Table 6 gives a summary of the existing sanitary sewer impact under proposed conditions. See Exhibit D for pipe performance models of the existing sanitary pipes under proposed conditions.





	Table 6. Summary of Existing Sanitary impact order Proposed Conditions											
	Contributing Residential and Non-Residential Developments	Pipe ID	Pipe Slop e (ft/ft)	Pipe Size (in)	Existing Flow Rate (cfs)	Depth (ft)	Accumulative Flow Rate (cfs)	Accumulative Depth (ft)	Pipe Velocity (ft/s)			
East of RR	Prop Townhomes	Prop. Pipe	0.006	8	0.070	0.14	0.070	0.14	1.31			
	Ex Residential South + Lumber	30-051	0.004	8	0.055	0.13	0.125	0.20	1.40			
	Ex Residential North	30-031	0.006	8	0.036	0.10	0.161	0.20	1.81			
	Office, Church, Hospital	30-014	0.006	8	0.021	0.08	0.182	0.22	1.79			
	N/A	30-013	0.006	8	0.021	0.08	0.182	0.22	1.79			
	N/A	30-010	0.006	8	0.021	0.08	0.182	0.22	1.79			
	Ex Residential 3	30-047	0.006	8	0.058	0.13	0.058	0.13	1.20			
	Ex Residential 4	30-029	0.006	8	0.072	0.14	0.130	0.19	1.57			
	Storage Unit Facility	30.068	0.006	8	0.220	0.24	0.220	0.24	1.93			
R	Ex Residential 5	30-030	0.006	8	0.058	0.13	0.407	0.34	2.25			
of F	Warehouse 1	30-026	0.006	8	0.043	0.11	0.450	0.36	2.32			
Nest	Warehouse 2	30-012	0.006	8	0.029	0.09	0.479	0.37	2.39			
-	Ex Residential 6	30-005	0.006	8	0.081	0.15	0.081	0.15	1.36			
	N/A	30-006	0.006	8	0.081	0.15	0.081	0.15	1.36			
	N/A	30-007	0.006	8	0.110	0.17	0.560	0.41	2.47			
	N/A	30-008	0.006	8	0.110	0.17	0.560	0.41	2.47			
	N/A	30-009	0.006	10	0.131	0.17	0.742	0.42	2.69			

Summers of Existing Senitors Impact Under Drenead Conditions

SUMMARY

The proposed use identified herein results in an increase in the expected sanitary sewer flows as compared to the existing conditions. The existing infrastructure, however, is still adequate to receive and convey the sanitary sewer peak flows from the proposed townhome development in addition to the existing residential and non-residential developments peak flows. Table 7 provides a summary comparing the proposed system sanitary sewer peak flow rates to the existing sanitary sewer pipe capacities.

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	Contributing Residential and Non-Residential Developments	Pipe ID	Pipe Size (in)	Existing Flow Rate (cfs)	Accumulative Flow Rate (cfs)	Pipe Flow Capacity (cfs)
	Prop Townhomes	Prop. Pipe	8	0.070	0.070	0.813
of RR	Ex Residential South + Lumber	30-051	8	0.055	0.125	0.664
	Ex Residential North	30-031	8	0.036	0.161	0.813
East	Office, Church, Hospital	30-014	8	0.021	0.182	0.813
ш	N/A	30-013	8	0.021	0.182	0.813
	N/A	30-010	8	0.021	0.182	0.813
	Ex Residential 3	30-047	8	0.058	0.058	0.813
	Ex Residential 4	30-029	8	0.072	0.130	0.813
	Storage Unit Facility	30.068	8	0.220	0.220	0.813
2	Ex Residential 5	30-030	8	0.058	0.407	0.813
of RI	Warehouse 1	30-026	8	0.043	0.450	0.813
lest (Warehouse 2	30-012	8	0.029	0.479	0.813
5	Ex Residential 6	30-005	8	0.081	0.081	0.813
	N/A	30-006	8	0.081	0.081	0.813
	N/A	30-007	8	0.110	0.560	0.813
	N/A	30-008	8	0.110	0.560	0.813
	N/A	30-009	10	0.131	0.742	1.475

Table 7. Summary of Sanitary Sewer Flow Rates vs. Pipe Flow Capacities

It is our opinion that no modifications to the existing public sanitary sewer infrastructure will be required to accommodate the sanitary sewer peak flows from the proposed development. If you have any questions or need additional clarification, please do not hesitate to contact us.



RENAISSANCE INFRASTRUCTURE CONSULTING

Guund. Jan Sover

E. Danielle Sandman, E.I. dsandman@ric-consult.com

Exhibit A Site Location Maps



Exhibit B Proposed General Layout



2" APWA Type 3 Asphaltic Concrete Surface Course

4" APWA Type 1 Asphaltic Base Course Proposed Northwest Pond Edge

6" MoDOT Type 5 Crushed Stone Base

6" Chemically Stabilized Subgrade

Asphaltic Pavement Section



6" PCC Surface



PCC Pavement Section

Roll Back Dry Curb & Gutter (Type CG-2 Dry) Straight Back Dry Curb & Gutter (Type CG-1 Dry)



LEGEND Existing Section Line Proposed Right-of-Way _____ Proposed Property Line Existing Right-of-Way Line Existing Lot Line Proposed Lot Line Proposed Easement Existing Easement Line ---------- U/E -Proposed Curb & Gutter Existing Curb & Gutter _____ Proposed Sidewalk Existing Sidewalk 4 Proposed Storm Sewer Existing Storm Sewer _____ Proposed Storm Structure Existing Storm Structure Existing Waterline Proposed Fire Hydrant А —— W/L —— Existing Gas Main Proposed Waterline ____ GAS ____ Proposed Sanitary Sewer **Existing Sanitary Sewer** _____ SS __ _____ SAN _____ Proposed Sanitary Manhole G Existing Sanitary Manhole S Proposed Contour Major Existing Contour Major ____ Proposed Contour Minor Existing Contour Minor

Future Curb & Gutter

Lot Info Lot Area: 3.76AC Units: 36 Units per Acre: 9.57 Unit Size: 1,663 SF Total Floor Area: 66,520 SF Floor Area Ratio: .43 Impervious Area: 68,663 SF (44.8%) Parking Required: 72 (2/Unit) Parking Provided: 136 (3/Unit, & 28 Visitor Parking)

Proposed Asphaltic Pavement

Note:

1) All fencing constructed adjacent to PI zoning districts shall conform to City of Lee's Summit UDO Section 8.890 minimum buffer screen requirements.

Exhibit C Existing Sanitary Sewer



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Pipe 30-031 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.15
		Q (cfs)	= 0.091
		Area (sqft)	= 0.06
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.53
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.66
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.14
		Top Width (ft)	= 0.56
Calculations		EGL (ft)	= 0.19
Compute by:	Known Q		
Known Q (cfs)	= 0.09		



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Pipe 30-014 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.17
		Q (cfs)	= 0.112
		Area (sqft)	= 0.07
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.58
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.71
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.16
		Top Width (ft)	= 0.58
Calculations		EGL (ft)	= 0.21
Compute by:	Known Q		
Known Q (cfs)	= 0.11		



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Pipe 30-051 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.13
		Q (cfs)	= 0.055
		Area (sqft)	= 0.05
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.14
Slope (%)	= 0.40	Wetted Perim (ft)	= 0.61
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.11
		Top Width (ft)	= 0.53
Calculations		EGL (ft)	= 0.15
Compute by:	Known Q		
Known Q (cfs)	= 0.06		



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Pipe 30-009 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.83	Depth (ft)	= 0.40
		Q (cfs)	= 0.672
		Area (sqft)	= 0.26
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.60
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.27
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.37
		Top Width (ft)	= 0.83
Calculations		EGL (ft)	= 0.51
Compute by:	Known Q		
Known Q (cfs)	= 0.67		



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Pipe 30-007 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.41
		Q (cfs)	= 0.560
		Area (sqft)	= 0.23
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.47
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.21
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.35
		Top Width (ft)	= 0.65
Calculations		EGL (ft)	= 0.50
Compute by:	Known Q		
Known Q (cfs)	= 0.56		



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Pipe 30-012 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.37
		Q (cfs)	= 0.479
		Area (sqft)	= 0.20
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.39
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.13
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.33
		Top Width (ft)	= 0.67
Calculations		EGL (ft)	= 0.46
Compute by:	Known Q		
Known Q (cfs)	= 0.48		



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Pipe 30-026 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.36
		Q (cfs)	= 0.450
		Area (sqft)	= 0.19
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.32
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.11
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.32
		Top Width (ft)	= 0.67
Calculations		EGL (ft)	= 0.44
Compute by:	Known Q		
Known Q (cfs)	= 0.45		



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Pipe 30-068 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.24
		Q (cfs)	= 0.220
		Area (sqft)	= 0.11
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.93
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.86
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.22
		Top Width (ft)	= 0.64
Calculations		EGL (ft)	= 0.30
Compute by:	Known Q		
Known Q (cfs)	= 0.22		



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Pipe 30-005 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.15
		Q (cfs)	= 0.081
		Area (sqft)	= 0.06
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.36
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.66
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.13
		Top Width (ft)	= 0.56
Calculations		EGL (ft)	= 0.18
Compute by:	Known Q		
Known Q (cfs)	= 0.08		



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Pipe 30-047 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.13
		Q (cfs)	= 0.058
		Area (sqft)	= 0.05
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.20
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.61
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.11
		Top Width (ft)	= 0.53
Calculations		EGL (ft)	= 0.15
Compute by:	Known Q		
Known Q (cfs)	= 0.06		



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Pipe 30-030 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.34
		Q (cfs)	= 0.407
		Area (sqft)	= 0.18
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.25
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.07
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.30
		Top Width (ft)	= 0.67
Calculations		EGL (ft)	= 0.42
Compute by:	Known Q		
Known Q (cfs)	= 0.41		



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Pipe 30-029 Existing Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.19
		Q (cfs)	= 0.130
		Area (sqft)	= 0.08
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.57
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.75
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.17
		Top Width (ft)	= 0.60
Calculations		EGL (ft)	= 0.23
Compute by:	Known Q		
Known Q (cfs)	= 0.13		



Exhibit D Proposed Sanitary Sewer



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Pipe 30-014 Proposed Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.22
		Q (cfs)	= 0.182
		Area (sqft)	= 0.10
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.79
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.82
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.20
		Top Width (ft)	= 0.63
Calculations		EGL (ft)	= 0.27
Compute by:	Known Q		
Known Q (cfs)	= 0.18		



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Pipe 30-009 Proposed Conditions

Circular		Highlighted	
Diameter (ft)	= 0.83	Depth (ft)	= 0.42
		Q (cfs)	= 0.742
		Area (sqft)	= 0.28
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.69
Slope (%)	= 0.60	Wetted Perim (ft)	= 1.32
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.38
		Top Width (ft)	= 0.83
Calculations		EGL (ft)	= 0.53
Compute by:	Known Q		
Known Q (cfs)	= 0.74		



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Pipe 30-031 Proposed Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.20
		Q (cfs)	= 0.161
		Area (sqft)	= 0.09
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.81
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.78
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.19
		Top Width (ft)	= 0.61
Calculations		EGL (ft)	= 0.25
Compute by:	Known Q		
Known Q (cfs)	= 0.16		



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Prop. Pipe Proposed Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.14
		Q (cfs)	= 0.070
		Area (sqft)	= 0.05
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.31
Slope (%)	= 0.60	Wetted Perim (ft)	= 0.64
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.12
		Top Width (ft)	= 0.54
Calculations		EGL (ft)	= 0.17
Compute by:	Known Q		
Known Q (cfs)	= 0.07		



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Pipe 30-051 Proposed Conditions

Circular		Highlighted	
Diameter (ft)	= 0.67	Depth (ft)	= 0.20
		Q (cfs)	= 0.125
		Area (sqft)	= 0.09
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 1.40
Slope (%)	= 0.40	Wetted Perim (ft)	= 0.78
N-Value	= 0.015	Crit Depth, Yc (ft)	= 0.17
		Top Width (ft)	= 0.61
Calculations		EGL (ft)	= 0.23
Compute by:	Known Q		
Known Q (cfs)	= 0.13		

