

Mid-Continent Public Library East Lee's Summit Branch Final Stormwater Study

BATTERY DRIVE AND SOUTHEAST BLUE PARKWAY LEE'S SUMMIT, MISSOURI

January 25, 2019
Revised February 2019

Prepared for: Mid-Continent Public Libraries (MCPL)

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NUMBER
PE-2018010505
PSIONAL FINANCES

Olsson Project No. B18-0330

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GENERAL INFORMATION

This Stormwater Management Study is being submitted on behalf of the Mid-Continent Public Library (MCPL) for the proposed library facility located at the northeast corner of SE Blue Parkway and Battery Drive.

Project Location and Description

The proposed site is located on Lot 2 of the Magnolia Place at Charleston Park, 1st Plat in the Northeast ¼ of Section 10, Township 47 North, Range 31 West, in Jackson County, Lee's Summit, Missouri and includes approximately 3.8 acres. The site is located at the northeast corner of the SE Blue Parkway and Battery Drive intersection and is generally bounded by Village Cooperative of Lee's Summit to the north, SE Battery Dr to the west, SE Blue Parkway to the south, and an undeveloped lot to the east (See Figure 2). The Church of Jesus Christ of Latter-Day Saints lies east of the undeveloped lot. The proposed development includes a 18,500 S.F. library facility with associated parking lots, landscaping, grading, and utilities. The entirety of the site is located outside of the 100-Year FEMA Floodplain.

Study Purpose

The purpose of this study is to provide a Stormwater Management Plan for the proposed development in accordance with the American Public Works Association (APWA) *Standard Specifications and Design Criteria* Section 5600 "Storm Drainage Systems and Facilities", APWA Manual of Best Management Practices (BMP) for Stormwater Quality, and applicable City of Lee's Summit, Missouri guidelines.

Soils Descriptions

Soil classifications were obtained from the Natural Resource Conservation Service's website by utilizing the Web Soil Survey feature. The site soil composition and classification are listed below:

10082 – Arisburg-Urban Land Complex, 1 to 5 percent slopes – HSG Type C.
 10180 – Udarents-Urban Land-Sampsel Complex, 2 to 5 percent slopes - HSG Type C.

*HSG - Hydrologic Soils Group

See Soils Map in Appendix B.

METHODOLOGY

General Criteria and References

Analytical and design criteria conform to those of Division V - Section 5600 – "Storm Drainage Systems and Facilities" of the Kansas City Metropolitan Chapter of the American Public Works Association's "Standard Specifications and Design Criteria". Based on these criteria, Post-development discharge rates for 2, 10, and 100-year storm events will be limited to provisions in section 5608.4-C1 Performance Criteria – "Comprehensive Control". Post-development discharge rates are limited to 0.5 cfs per acre for the 2-Year event, 2.0 cfs per acre for the 10-year event, and 3.0 cfs per acre for 100-year storm event. Pre and post-development flows from the site are shown below and were calculated using HEC-HMS for the 2, 10 and 100-year storm events. Existing and proposed hydrographs were calculated using the 24-hour SCS Type II rainfall distribution. Given the size of the site, all times of concentration were set a minimum of 5 minutes, the defined minimum per Section 5600.

HYDROLOGIC/HYDRAULIC ANALYSES

Existing Conditions Analysis

The existing site is an undeveloped parcel of land that consist of native vegetation. The site is bounded by SE Battery Drive to the west, The Village Cooperative Apartments to the north, undeveloped property to the east, and SE Blue Parkway to the South. Currently, Blue Parkway lies within MoDOT's US-50 right of way.

The existing drainage for the site is split by a ridge into two outfalls, "A" and "B". The east section drains to outfall "A" and the west section drains to outfall "B". Outfall "A" drains northwest over the curb into the gutter. The gutter drains to an existing public curb inlet on Battery Drive. Outfall "B" drains overland to the northeast. This area drains over the back of the curb to an existing storm structure in the parking lot of the Village Cooperative Apartments.

South of the property there is an existing ditch that lies within US-50 right of way. The ditch drains run-off from Blue Parkway. There is no curb and gutter on Blue Parkway, just a graveled shoulder that allows run-off to drain into the existing ditch. There is an existing 18x24 arch culvert that drains to the ditch from under Battery Drive flows east along the north side of Blue Parkway.

As stated previously, there is an undeveloped lot to the east of the property that is owned by Richard D. Link. Mr. Link is also the person who sold Lot 2, Magnolia place to MCPL. The proposed development did not require all of the property for Lot 2. The east 81' of the property was excluded from the sale and remains the property of Richard D. Link. The proposed drive from the south will be a common access drive that will serve both the MCPL property and the future developed lot to the east. The east half of this drive will be constructed on the undeveloped lot under a mutual understanding with Mr. Link.

This property generally drains to the east to an existing swale away from the library property. None of this area drains to the proposed collection system for the library.

For the purposes of the drainage calculations moving forward this area will be included, therefore the studied area will increase from 3.8 acres to 4.5 acres.

A composite curve number was generated for the site by referencing the Web Soil Survey available in Appendix C, APWA Section 5600 and considered the following factors:

- Existing impervious area
- Existing pervious area
- Hydrologic soil group

The following tables summarize the pre-development composite curve number generation.

Table 1: Pre-Development Curve Number Analysis

| Sub-Area | Area (AC) | Soil Group | Curve Number |
|----------------|--------------|------------|--------------|
| Pasture (Good) | 3.0 | С | 74 |
| Pasture (Good) | 1.5 | С | 74 |

The existing peak discharge rates for the 2-year, 10-year, and 100-year storm events from the site are shown in Table 2 below:

Table 2: Existing Peak Flows

| Sub-Area / Outfall | Area (acres) | Q (2-Year Storm) (cfs) | Q (10-Year Storm) (cfs) | Q (100-Year Storm) (cfs) |
|--------------------|-----------------|---------------------------|-------------------------------|--------------------------------|
| Α | 3 | 7.2 | 11 | 19.2 |
| В | 1.5 | 2.6 | 5.5 | 9.6 |

Proposed Conditions Analysis

The proposed Public Library will include a 18,500 SF library with associated parking lots, landscaping, grading, and utilities. A site plan has been included in Appendix A. The site will generally continue to drain in the same pattern as existing. Drainage from the site will

enter into an enclosed storm sewer system that will be constructed with the development. The proposed system will collect drainage from the parking area and building. The increase in impervious area will increase runoff from the site. To mitigate the increase in runoff, the following strategy will be implemented.

The site will be graded so that Drainage Areas A & B, noted in the Existing Conditions, will drain north and directed into a detention basin. A proposed drainage map is included in Appendix A.

A post-development composite curve number was generated using the same methodology implemented during the pre-development curve number analysis. Table 3 below summarizes the post-development composite curve number generation.

Table 3: Post-Development Curve Number Analysis

| Sub-Area | Area (AC) | Soil Group | Curve Number |
|---------------------------------|--------------|---------------|-----------------|
| Pavement, Buildings, Impervious | 2.0 | С | 98 |
| Turf (Good) | 2.5 | С | 85 |

A peak flow analysis of the post-development site was conducted using HEC-HMS, the composite curve number, and rainfall and distribution information acquired from APWA section 5600. Post-development peak to the outfall are summarized in the Table 4. Detailed reports from HEC-HMS are available in Appendix D

Table 4: Proposed Peak Flows

| Sub-Area / Outfall | Tributary Area | Q (2-Year Storm) | Q (10-Year Storm) | Q (100-Year Storm) |
|--------------------|----------------|------------------|-------------------|--------------------|
| | (acres) | (cfs) | (cfs) | (cfs) |
| Detention Basin | 4.5 | 13.7 | 21.1 | 33.4 |

The existing ditch to the south will remain essentially unchanged. The drainage area, for the ditch, lies within the existing right of way. An embankment will need to be constructed across the ditch for the southern entrance. A culvert will be installed under the entrance to

maintain flow in the ditch. The 30" culvert will receive the flow from the existing 18x24 (24" equivalent) local drainage from Blue Parkway.

Stormwater Detention Requirements

One proposed detention pond will be utilized to mitigate the increase in flow due to an increase in impervious area. The Detention Basin will be located on the northern part of the property. It will collect runoff from the 4.5-acre property. The pond has an outlet pipe that connects to an orifice plate within a junction box structure that will be within the dam.

The outlet for the detention basin will be a flared end section with a trash rack connected by a 15" pipe to a control structure. The control structure will have an internal control plate. The control plate will have a series of 6 - 1" holes arranged in a single vertical row beginning at Elevation 1006.5. There will be a 2.4 foot weir located at Elevation 1008.75.

The series of 1" vertical holes are designed for the water treatment requirements. the water quality volume (WQv) will be controlled by the vertical holes at the bottom of the plate. The 1" holes will release the water quality volume over a 40-hour period to allow pollutants to settle out of this precipitation event.

The weir will be located above the WQv surface elevation and will control the release of the 2, 10 and 100-year storm events. These storms have been analyzed through the control structure and will release below the pre-existing storm events and below the Comprehensive Control release rates defined in APWA section 5600. The dam will have an emergency spillway to control the 100-year overflow should the outlet become blocked.

Table 5 provides the water surface elevations (WSE's) and peak flows for the proposed detention basin.

Table 5: Detention Basin, WSE's and Peak Flows

| | SIII, WSE S dilu Peak Flows |
|----------------------------------|--------------------------------------|
| Description | Statistics |
| Bottom of Basin | 1007 |
| Total Storage Volume | 1.1 ac-ft |
| Emergency Spillway | |
| (IE, 100-Yr WSE) | 1011.12, 1011.75 |
| Top of Dam Elevation | 1012.20 |
| WQv Perf. Plate | |
| (IE Elevation, Perf and Spacing) | 1007.00, 1" Vertical Holes 4" C to C |
| Water Quality Volume | |
| WSE, Storage, Peak Outflow | 1008.95, 0.3 ac-ft, 1.3 cfs |
| 2 nd Stage Weir | |
| (IE, Width) | 1008.75, 2.40 ft |
| 10–Year Storm | |
| WSE, Storage, Peak Outflow | 1009.52, 0.44 ac-ft, 5.8 cfs |
| 100–Year Storm | |
| WSE, Storage, Peak Outflow | 1010.12, 0.67 ac-ft, 13.2 cfs |

Table 6 shows the overall peak flows for the site for both pre and post-construction. In addition, it also shows the allowable Comprehensive control release rate. Note that peak flow for post-construction has been lowered in all storm events.

Table 6: Peak Flow Change Analysis

| Site | Q (2-Year Storm) (cfs) | Q (10-Year Storm) (cfs) | Q (100-Year Storm) (cfs) |
|--|------------------------------|-------------------------------|--------------------------------|
| Pre-Construction | 7.2 | 11 | 19.2 |
| Section 5600 Allowable Comprehensive Release Rate | 2.3 (0.5 cfs per acre) | 9 (2.0 cfs per acre) | 13.5 (3.0 cfs per acre) |
| Post Construction | 2.1 | 5.8 | 13.3 |
| Post Const Less Than Allowable | Yes | Yes | Yes |

STORMWATER TREATMENT REQUIREMENTS

As stated previously, the proposed detention is designed to act an extended dry bottom detention facility will be used to treat stormwater per MARC water quality standards. The orifice plate for the basin will be sized to release the water quality volume (1.37") over a 40-hour period to allow pollutants to settle from runoff before entering the public stormwater system. The maximum storage for the water quality event in the basin will be 0.3 acre-ft reaching a peak water surface of elevation 1008.95 feet.

CLEAN WATER ACT SECTION 404 PERMITTING REQUIREMENTS

No jurisdictional Waters of the United States have been identified on the study site. Therefore, a Section 404 permit is not required.

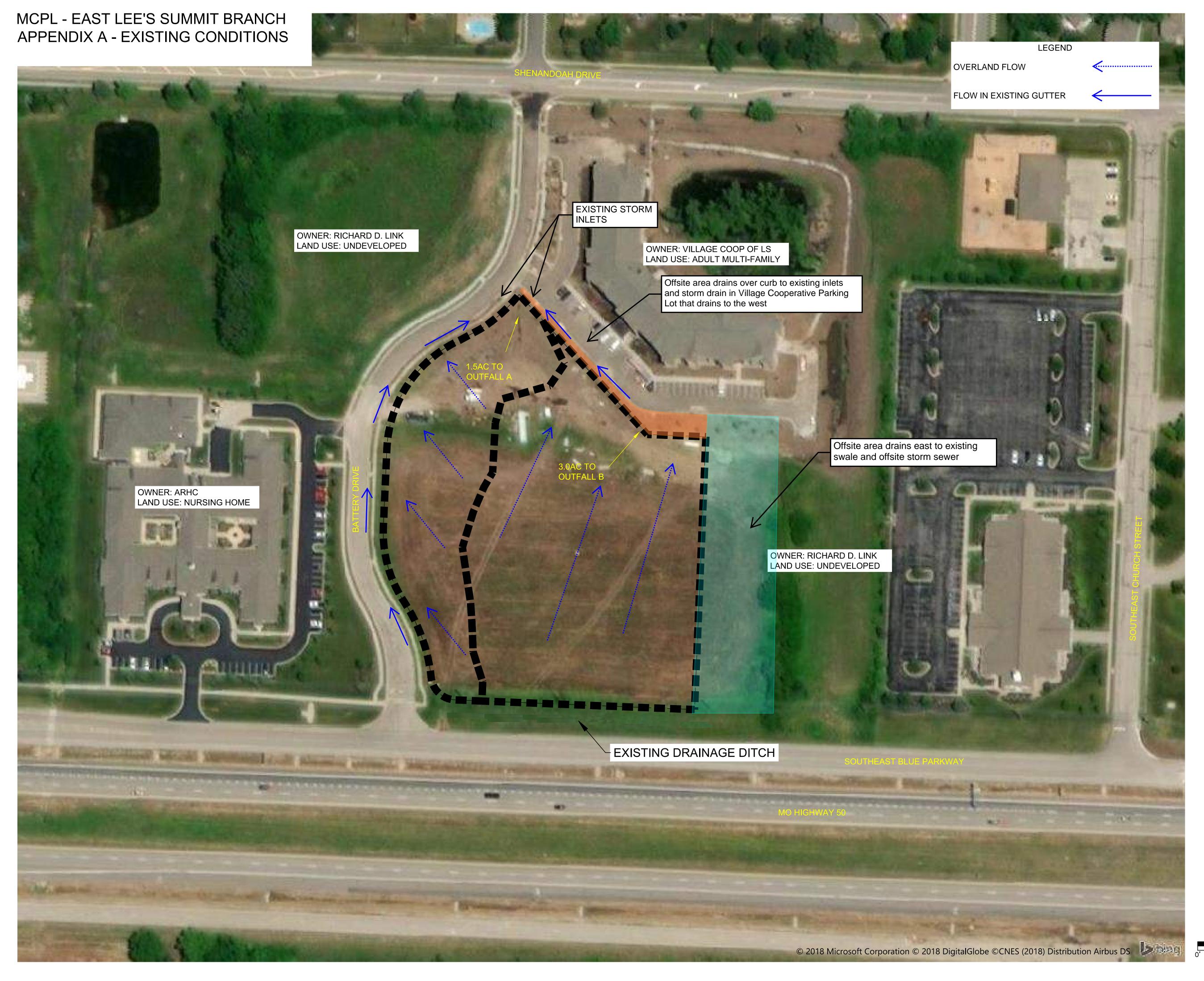
FEMA/DWR PERMIT REQUIREMENTS

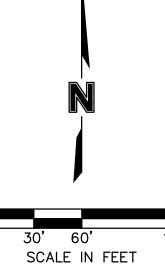
No FEMA permitting or submittals will be required on this site because there are no FEMA delineated floodplains on the site. A copy of the FIRM map for this area has been included in Appendix B.

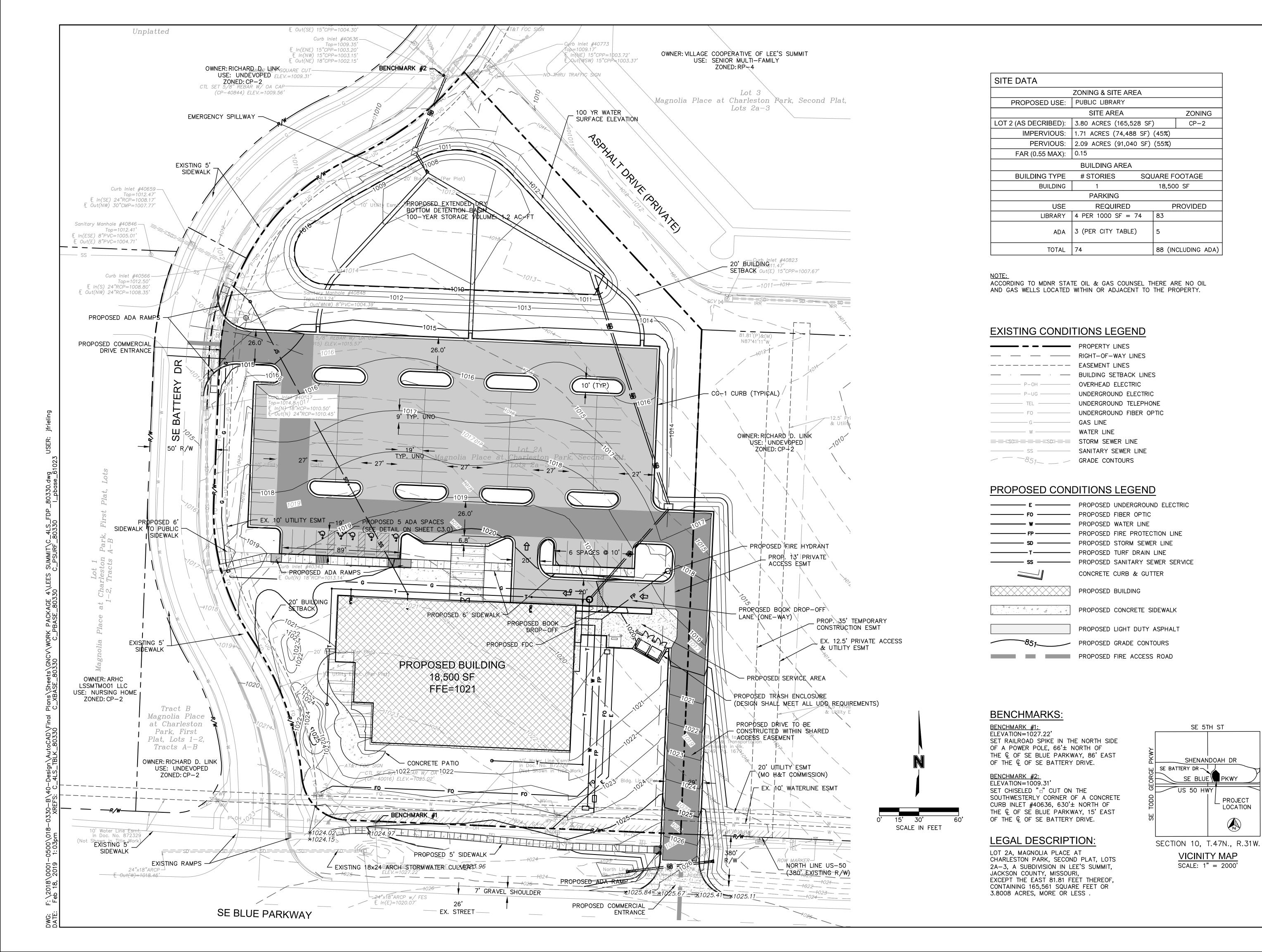
CONCLUSIONS AND RECOMMENDATIONS

As outlined in the preceding report, increased runoff rates in the post-development conditions are mitigated by the detention basins. Drainage patterns on the site remain relatively unchanged. An extended dry detention basin has been designed to maintain or improve storm water quality. Based on these facts and other information provided herein, we request that this stormwater study be approved.

Appendix A Map Exhibits









Sapp Design Associates Architects, P.C. Missouri State Certificate of Authority #000607

Kansas City, MO 64108

816.300.0300

SPECIAL NOTICES

n the event the client consents to, allows, authorizes or approves o nanges to any plans, specifications or other construction design professional, the client recognizes that such changes and the results thereof are not the responsibility of the design professional. herefore, the client agrees to release the design professional from any liability arising from the construction, use or result of such changes. In addition, the client agrees to the fullest extent permitted y law, to indemnify and hold the design professional harmless from ny damage, liability or cost (including reasonable attorney's fees an

osts of defense) arising from such changes. he personal seal of the registered Architect or Engineer shall be the legal equivalent of his signature whenever & wherever used, and the owner of the seal shall authenticate this sheet and the specification sections pertaining to this sheet. Responsibility shall be disclaimed for all other plans, specifications, estimates, reports or other ocuments or instruments relating to or intended to be used for any

art or parts of the architectural project.

BRANC

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Engineer of Record

Terry M Parsons, Engineer MO PE-2018010505

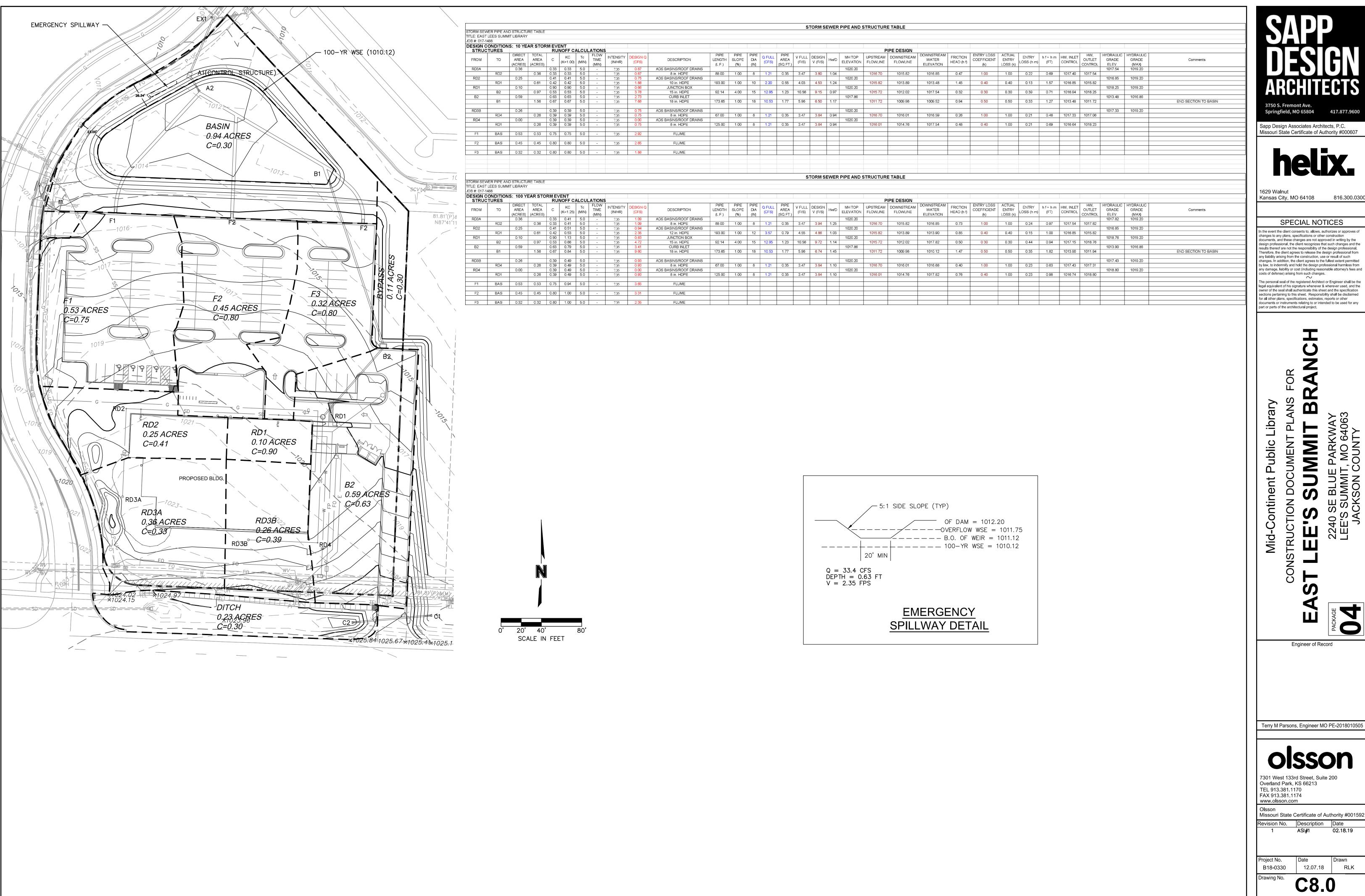
Overland Park, KS 66213 TEL 913.381.1170 FAX 913.381.1174

www.olsson.com Missouri State Certificate of Authority #001592

evision No. Description Date 02.18.19 ASI#1

12.07.18 B18-0330

FINAL DEVELOPMENT PLAN





Sapp Design Associates Architects, P.C. Missouri State Certificate of Authority #000607

1629 Walnut Kansas City, MO 64108

816.300.0300

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he personal seal of the registered Architect or Engineer shall be the legal equivalent of his signature whenever & wherever used, and the owner of the seal shall authenticate this sheet and the specification sections pertaining to this sheet. Responsibility shall be disclaimed cuments or instruments relating to or intended to be used for any rt or parts of the architectural project.

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Missouri State Certificate of Authority #001592 Description Date
ASI#1 02.18.19

B18-0330

12.07.18 C8.0

DRAINAGE PLAN

pyright 2018 - Sapp Design Associates, Architects, P.C.

Appendix B
FEMA Flood Classification Firm

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Soummary of Stillwater Elevations tables contained within the Flood insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-doot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be tulked in conjunction with the FIRM for purposes of construction and/or floodplain management.

Boundaries of the **floodways** were computed at cross sections and interpolic between cross sections. The floodways were based on hydraulic considerations regard to requirements of the National Flood Insurance Program. Floodway wide and other pertinent floodway data are provided in the Flood Insurance Study Rep for this jurisdiction.

The projection used in the preparation of this map was Missouri State Plane West Zone (FIPS zone 2403). The horizontal datum was NAD 83, GRS 1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do no affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same verifical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, with the National Geodetic Survey website a https://www.ngs.noaa.gov or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at https://www.ngs.nosa.gov.

Base map information shown on this FIRM was derived from the

The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the profile baseline, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

Based on updated topographic information, this map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than properties of the configuration of the configu

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels: community map repository addresses; and a Listing of Communities table containing National Flocid Insurance Program dates for each community as well as a listing of the panels on which each community

For information on available products associated with the furnar van tier emp-Service Center (MSC) website at http://mscferna.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the MSC website.

2835000 FT 2840000 FT 94° 20' 37.5" 38" 54" 22 5" Same named to the same. PROJECT LOCATION THE SHIPPERS 384⁰⁰⁰⁷⁹E

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 19% ANNUAL CHANCE FLOOD

The 1% across indexer food (100-year food), also knows as the base flood, is the flood that ha a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the sees subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard Area is flooding that the special Flood Hazard Area is the december of the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, RE, AH, RO, AR, A99, V, and VE. The Bese flood Elevation is the water-surface december of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined

ZONE AE Base Flood Elevations determined. ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determine

Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently describled. Zone All indicates that ferfirmer flood control system is being restored to provide protection from the 1% annual chance or greater flood.

Areas to be protected from 1% annual chance flood by a l'ederal flood protection system under construction; no Base Flood Elevabors determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevation

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations

9111. FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encreachment so that the 1% annual chance flood can, be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 floot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS ZONE X Areas determined to be outside the 0.2% annual chance floodplain. ZONE D

Areas in which flood hazards are undetermined, but possible

7777 COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. 1% Annual Chance Floodplain Boundary

0.2% Annual Chance Floodplain Boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hiszard Area Zones and boundhiding Special Flood Hiszard Areas of different Base Flood El flood depths, or flood velocities.

Base Flood Elevation line and value; elevation in feet* ~~ 513~~

Base Flood Elevation value where uniform within zone; elevation in feet* (EL 987)

(A)- $\overline{\mathbb{A}}$ 23 ---- 23

Geographic coordinates referenced to the North American Datum of 1983 (NAO 83) Western Hemisphere

5000-foot ticks: Missouri State Plane West Zone (FIPS Zone 2403), Transverse Mercator projection Bench mark (see explanation in Notes to Users section of this FIRM panel) 3100000 FT DX5510 X

MAP REPOSITORIES
Refer to Map Repositories list on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP September 29, 2005

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL January 20, 2017 - to change Special Flood Hazard Areas



FIRM

FLOOD INSURANCE RATE MAP JACKSON COUNTY, MISSOURI

PANEL 0439G

PANEL 439 OF 625

AND INCORPORATED AREAS

CONTAINS

NEWLINENULAYIN

m

COMMUNITY
JACKSON COUNTY,
Unincorporated
LEE'S SUMMIT,
CITY OF NUMBER PANEL SUFFIX 290492 0439 G 290174 0438 G

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject



MAP NUMBER 29095C0439G MAP REVISED **JANUARY 20, 2017**

Federal Emergency Management Agency



Appendix C Soil Map

MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

✓ Rock Outcrop✓ Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

LLGLIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot
 Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

+++ Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 18, Sep 16, 2017

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 11, 2017—Sep 22, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|-----------------------------|--|--------------|----------------|
| 10082 | Arisburg-Urban land complex, 1 to 5 percent slopes | 3.3 | 79.5% |
| 10180 | Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes | 0.9 | 20.5% |
| Totals for Area of Interest | ' | 4.2 | 100.0% |

Jackson County, Missouri

10082—Arisburg-Urban land complex, 1 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w7ld Elevation: 750 to 1,130 feet

Mean annual precipitation: 39 to 45 inches Mean annual air temperature: 50 to 55 degrees F

Frost-free period: 177 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Arisburg and similar soils: 61 percent

Urban land: 30 percent Minor components: 9 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Arisburg

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam A - 6 to 13 inches: silt loam

Bt - 13 to 19 inches: silty clay loam

Btg - 19 to 56 inches: silty clay loam

BCg - 56 to 79 inches: silty clay loam

Properties and qualities

Slope: 1 to 5 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high (0.20 to 0.60 in/hr) Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Available water storage in profile: High (about 11.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: Loess Upland Prairie (R107BY007MO)

Hydric soil rating: No

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Minor Components

Sharpsburg

Percent of map unit: 3 percent

Landform: Ridges

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: Loess Upland Prairie (R109XY002MO)

Hydric soil rating: No

Sampsel

Percent of map unit: 3 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Concave

Ecological site: Interbedded Sedimentary Upland Savanna

(R109XY010MO)

Hydric soil rating: Yes

Greenton

Percent of map unit: 3 percent

Landform: Hillslopes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: Loess Upland Prairie (R109XY002MO)

Hydric soil rating: No

Data Source Information

Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 18, Sep 16, 2017

Jackson County, Missouri

10180—Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1n85h

Elevation: 600 to 900 feet

Mean annual precipitation: 33 to 43 inches Mean annual air temperature: 50 to 57 degrees F

Frost-free period: 175 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Udarents and similar soils: 41 percent

Urban land: 39 percent

Sampsel and similar soils: 15 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Udarents

Setting

Landform position (two-dimensional): Summit Landform position (three-dimensional): Crest

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Mine spoil or earthy fill

Typical profile

C1 - 0 to 5 inches: silt loam
C2 - 5 to 80 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.14 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Available water storage in profile: Moderate (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: Deep Loess Upland Prairie (R107BY002MO)

Other vegetative classification: Mixed/Transitional (Mixed Native

Vegetation)

Hydric soil rating: No

Description of Urban Land

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Across-slope shape: Convex

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Description of Sampsel

Setting

Landform: Hillslopes

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Convex

Parent material: Residuum weathered from shale

Typical profile

Ap - 0 to 13 inches: silty clay loam Bt - 13 to 80 inches: silty clay

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 0 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Available water storage in profile: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C/D

Ecological site: Wet Footslope Prairie (R112XY041MO)
Other vegetative classification: Grass/Prairie (Herbaceous

Vegetation)

Appendix D

Drainage and Detention Calculations

MCPL EAST LEE'S SUMMIT - DRAINAGE CALCULATIONS

| | STORM SEWER PIPE AND STRUCTURE TABLE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--------------|--------------------------------------|----------------|-----------|--------|----------------------|------------|--------------|--------------|-----------------------------------|-----------|--------|-----------------|-----------|--------|---------|--------|------------|------------|-------------|--------------------|------------|---------------------------|-----------------|------------|-----------|----------|----------|--------------------|------------------|----------------------|
| STORM SEW | STORM SEWER PIPE AND STRUCTURE TABLE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TITLE: EAST | LEES SUMN | /IT LIBRAR | Y | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| JOB #: 017-1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| DESIGN C | ONDITION | S: 10 YE | AR STOR | N EVEN | | | | | | | | | | | | | | | | | | | | | | | | | | |
| STRUC | | | | | IOFF CALC | ULATIONS | S | | | | | | | | | | | Р | PIPE DESIGN | | | | | | | | | | | |
| | | DIRECT | TOTAL | | KC To | FLOW | INITENIOIT | | | PIPE | PIPE I | PIPE | PIPE | | DEGLOS | | | LIDOTDEALA | BOUNDEDEAN | DOWNSTREAM | EDIOTION | ENTRY LOSS | ACTUAL | ENTRY | 1.6.1 | | HW, | HYDRAULI | HYDRAULIC | |
| FROM | TO | AREA | AREA | С | | TIME | INTENSIT | | DESCRIPTION | LENGTH | | DIA Q FL | | V FULL | | Hw/D | MH TOP | UPSTREAM | | WATER | FRICTION | COEFFICIENT | ENTRY | | h f + h m | HW, INLE | OUTLET | GRADE | GRADE | Comments |
| | | (ACRES) | (ACRES) | | (K=1.00) (MII | N) (MIN) | (IN/HR) | (CFS) | | (L.F.) | | (IN) CF | S) (SQ.F1 | | V (F/S) | | ELEVATION | FLOWLINE | FLOWLINE | ELEVATION | HEAD (h f) | (k) | LOSS (k) | LOSS (h m) | (FT) | CONTROL | CONTROL | | (MAX) | |
| RD3A | | 0.36 | | 0.33 | 0.33 5.0 | 0 - | 7.35 | 0.87 | ADS BASINS/ROOF DRAINS | 1 ` ′ | ` / | ` / | , · · | 1 | | | 1020.20 | | | | | | 1 | | | | | 1017.54 | 1019.20 | |
| - | RD2 | | 0.36 | 0.33 | 0.33 5.0 | 0 - | 7.35 | 0.87 | 8 in. HDPE | 88.00 | 1.00 | 8 1.2 | 1 0.35 | 3.47 | 3.80 | 1.04 | | 1016.70 | 1015.82 | 1016.85 | 0.47 | 1.00 | 1.00 | 0.22 | 0.69 | 1017.40 | 1017.54 | | | |
| RD2 | | 0.25 | | 0.41 | 0.41 5.0 | | 7.35 | 0.75 | ADS BASINS/ROOF DRAINS | | | | 1 | | | 1 | 1020.20 | | | | | | | | | | 1 | 1016.85 | 1019.20 | |
| | RD1 | | 0.61 | 0.42 | 0.42 5.0 | | 7.35 | 1.88 | 10 in, HDPE | 193.00 | 1.00 | 10 2.2 | 0.55 | 4.03 | 4.53 | 1.24 | | 1015.82 | 1013.89 | 1013.48 | 1.45 | 0.40 | 0.40 | 0.13 | 1.57 | 1016.85 | 1015.82 | | | |
| RD1 | | 0.10 | | | 0.90 5.0 | | 7.35 | 0.66 | JUNCTION BOX | | | | | | | | 1020.20 | | | | | | | | | | 10.00.00 | 1018.25 | 1019.20 | |
| | B2 | | 0.97 | | | 0 - | 7,35 | 3.78 | 15 in. HDPE | 92.14 | 4.00 | 15 12. | 95 1.23 | 10.56 | 9.15 | 0.97 | | 1015.72 | 1012.02 | 1017.54 | 0.32 | 0.30 | 0.30 | 0.39 | 0.71 | 1016.94 | 1018.25 | | | |
| B2 | | 0.59 | | | 0.63 5.0 | 0 - | 7.35 | 2.73 | CURB INLET | i i | | | | | | | 1017.86 | | | | | | | | | | | 1013.48 | 1016.86 | |
| | B1 | | 1.56 | | | | 7.35 | 7.68 | 18 in. HDPE | 173.65 | 1.00 | 18 10. | 53 1.77 | 5.96 | 6.50 | 1.17 | | 1011.72 | 1009.98 | 1009.52 | 0.94 | 0.50 | 0.50 | 0.33 | 1.27 | 1013.48 | 1011.72 | | | END SECTION TO BASIN |
| | | | | | | | | | | | | | | 1 | | 1 | | | | | | | | | | T | | | | |
| RD3B | | 0.26 | | 0.39 | 0.39 5.0 | 0 - | 7.35 | 0.75 | ADS BASINS/ROOF DRAINS | † | | | | | | 1 | 1020.20 | i e | | | | | | i i | | | | 1017.33 | 1019.20 | |
| | RD4 | 1 | 0.26 | | 0.39 5.0 | | 7.35 | 0.75 | 8 in. HDPE | 67.00 | 1.00 | 8 1.2 | 1 0.35 | 3.47 | 3.64 | 0.94 | | 1016.70 | 1016.01 | 1016.59 | 0.26 | 1.00 | 1.00 | 0.21 | 0.46 | 1017.33 | 1017.06 | | 10.00.00 | |
| RD4 | | 0.00 | | 0.39 | 0.39 5.0 | | 7.35 | 0.00 | ADS BASINS/ROOF DRAINS | | | | | | | | 1020.20 | | | | | | | | | | | 1 | | <u> </u> |
| | RD1 | 1 | 0.26 | 0.39 | | 0 - | 7.35 | 0.75 | 8 in. HDPE | 125.00 | 1.00 | 8 1.2 | 1 0.35 | 3.47 | 3.64 | 0.94 | | 1016.01 | 1014.76 | 1017.54 | 0.48 | 0.40 | 1.00 | 0.21 | 0.69 | 1016.64 | 1018.23 | 1 | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | | |
| F1 | BAS | 0.53 | 0.53 | 0.75 | 0.75 5.0 | 0 - | 7.35 | 2.92 | FLUME | t i | | | | | 1 | | | İ | | | | | | | | | | 1 | | |
| | | | | | | | | | | i i | | | | | | | | | | | | | | | | | | | | |
| F2 | BAS | 0.45 | 0.45 | 0.80 | 0.80 5.0 | 0 - | 7.35 | 2.65 | FLUME | 1 | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | i i | | | | | | | | | | | | | | | | | | | | |
| F3 | BAS | 0.32 | 0.32 | 0.80 | 0.80 5.0 | 0 - | 7.35 | 1.88 | FLUME | † | | | | | | | | | | | | | | | | | | | | |
| | | | | | | _ | ,,,,,, | | · | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | l l | | | | · · | STORM | SEWED | DIDE AND | STRUCTURE | TARIE | U | · | | II. | | | | · · | | | |
| CTODM CEM | ED DIDE AN | ID CTDLICT | URE TABLE | | | | | | | | | | | | STORW | SEVVEN | C FIFE AND | SIKUCIUKE | IADLE | | | | | | | | | | | |
| TITLE: EAST | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| JOB #: 017-1 | | MII LIBKAK | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| DESIGN C | | C. 400 V | EAD STOP | NA EVE | | | 1 | 1 1 | | 1 | | | | | | 1 | ı | 1 | 1 | | 1 | | | 1 | | | 1 | 1 | - | |
| STRUC | JNUITION | 100 YI | EAK SIUN | IN EVE | IOFF CALC | III ATIONS | e . | | | | | | | | | | | | PIPE DESIGN | | _1 | L | I | | | l | | | | |
| SIRUC | IUKES | DIDECT | TOTAL | KUI | | | | | | PIPE | PIPE I | DIDE | DIDE | | 1 | 1 1 | ı | | | DOWNSTDE ANA | | ENTRYLOSS | ACTUAL | 1 | | 1 | LI\A/ | I HADDVIII I | C HYDRAULIC | |
| FROM | то | DIRECT AREA | AREA | | KC To | FLOW | INTENSITY | | DESCRIPTION | LENGTH | | DIA Q FL | | V FULL | | 1 11/5 | MH TOP | UPSTREAM | DOWNSTREAM | DOWNSTREAM | FRICTION | ENTRY LOSS COEFFICIENT | ACTUAL ENTRY | ENTRY | h f + h m | HW, INLE | | HYDRAULIO GRADE | GRADE | Comments |
| FROM | 10 | (ACRES) | (ACRES) | C | (K=1.25) (MII | N) (MIN) | (IN/HR) | (CFS) | DESCRIPTION | (L.F.) | | (IN) CF | S) AREA | (F/S) | V (F/S) | Hw/D | ELEVATION | FLOWLINE | FLOWLINE | WATER ELEVATION | HEAD (h f) | (k) | LOSS (k) | LOSS (h m) | (FT) | CONTROL | OUTLET | | (MAX) | Comments |
| RD3A | | 0.36 | (ACRES) | | 0.41 5.0 | () | 7.35 | 1.09 | ADS BASINS/ROOF DRAINS | (L.F.) | (%) | (IIN) | (SQ.FI | .) | + ' ' | + | 1020.20 | 1 | | ELEVATION | + | (K) | LUSS (K) | <u> </u> | | | CONTROL | 1017.82 | (MAX) 1019.20 | |
| KDSA | RD2 | 0.36 | 0.26 | | | | 7.35 | | 8 in. HDPE | 88.00 | 1.00 | 0 4 | 1 0.25 | 2 /7 | 2.04 | 1 2F | 1020.20 | 1016.70 | 1015.00 | 1016.05 | 0.72 | 1.00 | 1.00 | 0.24 | 0.07 | 1017 F4 | 1017.82 | | 1019.20 | |
| DD3 | RUZ | 0.25 | 0.30 | 0.33 | 0.41 5.0 0.51 5.0 | | 7.35 | 1.09 0.94 | ADS BASINS/ROOF DRAINS | 00.00 | 1.00 | 0 1.2 | 0.35 | 3.47 | 3.94 | 1.20 | 1020.20 | 1010.70 | 1015.82 | 1016.85 | 0.73 | 1.00 | 1.00 | 0.24 | 0.97 | 1017.54 | 1017.82 | 1016.85 | 1019.20 | |
| RD2 | DD1 | 0.25 | 0.61 | | | - | | | 12 in, HDPE | 102.00 | 1.00 | 12 25 | 7 0.70 | 4.55 | 4.00 | 1.03 | 1020.20 | 1015.00 | 1013.89 | 1013.90 | 0.85 | 0.40 | 0.40 | 0.15 | 1.00 | 1016.05 | 1015.82 | | 1019.20 | - |
| DD4 | RD1 | 0.10 | 0.61 | 0.42 | 1.13 5.0 | 0 - | 7.35 7.35 | 2.35 0.83 | JUNCTION BOX | 193.00 | 1.00 | 12 3.5 | 0.79 | 4.05 | 4.00 | 1.03 | 1000.00 | 1015.82 | 1013.09 | 1013.90 | 0.00 | 0.40 | 0.40 | 0.15 | 1.00 | 1010.85 | 1015.82 | | 1010.00 | |
| RD1 | D2 | 0.10 | 0.07 | | | | | | | 02.14 | 4.00 | 15 10 | 05 100 | 10.50 | 0.72 | 1.14 | 1020.20 | 1015.72 | 1012.02 | 1017.82 | 0.50 | 0.20 | 0.20 | 0.44 | 0.94 | 1017 15 | 1018.76 | 1018.76 | 1019.20 | |
| D2 | B2 | 0.50 | 0.97 | | 0.66 5.0 | | 7.35 | 4.72 | 15 in. HDPE CURB INLET | 92.14 | 4.00 | ιυ 1 <u>2</u> . | 95 1.23 | 10.56 | 9.12 | 1.14 | 1017.86 | 1015.72 | 1012.02 | 1017.02 | 0.50 | 0.30 | 0.30 | 0.44 | 0.94 | 1017.15 | 1010.76 | 1012.00 | 1016.86 | |
| B2 | D4 | 0.59 | 1.50 | | 0.79 5.0 | | 7.35 | 3.41 | | 170 CE | 1.00 | 10 10 | EO 477 | E 00 | 6.74 | 1.45 | 1017.80 | 1011 70 | 1000.00 | 1010.12 | 1.47 | 0.50 | 0.50 | 0.25 | 1.00 | 1012.00 | 1011.01 | 1013.90 | 1070.86 | END SECTION TO DASIN |
| - | B1 | + | 1.56 | 0.67 | 0.84 5.0 | U - | 7.35 | 9.60 | 18 in. HDPE | 173.65 | 1.00 | 18 10. | 1.// | 5.96 | 6.74 | 1.45 | - | 1011.72 | 1009.98 | 1010.12 | 1.47 | 0.50 | 0.50 | 0.35 | 1.82 | 1013.90 | 1011.94 | 1 | - | END SECTION TO BASIN |
| DD2B | | 0.00 | + | 0.20 | 0.40 5 | | 7.25 | 0.02 | ADE DACINE/DOOF DDAING | | | | | | - | + | 1020.20 | 1 | | | + | | 1 | | | | + | 1017.10 | 1010.00 | |
| RD3B | RD4 | 0.26 | 0.26 | | | 0 - | 7.35 7.35 | 0.93 | ADS BASINS/ROOF DRAINS | 67.00 | 1.00 | 0 4 | 1 0.25 | 2 /7 | 2 0 4 | 1.10 | 1020.20 | 1016.70 | 1016.01 | 1016.68 | 0.40 | 1.00 | 1.00 | 0.22 | 0.62 | 1017.42 | 1017.31 | 1017.43 | 1019.20 | |
| DD4 | KU4 | 0.00 | 0.20 | | 0.49 5.0 | | | 0.93 | 8 in. HDPE ADS BASINS/ROOF DRAINS | 67.00 | 1.00 | 0 1.2 | 0.35 | 3.47 | 3.04 | 1.10 | 1020.20 | 1010.70 | 10.0101 | 1010.06 | 0.40 | 1.00 | 1.00 | 0.23 | 0.03 | 1017.43 | 1017.31 | | 1010.00 | |
| RD4 | DD4 | 0.00 | 0.06 | | 0.49 5.0 | | 7.35 | 0.00 | | 105.00 | 1.00 | 0 47 | 1 0.05 | 2.47 | 2.04 | 1.10 | 1020.20 | 1016.04 | 1014.76 | 1017.00 | 0.76 | 0.40 | 1.00 | 0.00 | 0.00 | 1016 74 | 1010.00 | 1018.80 | 1019.20 | |
| - | RD1 | + | 0.26 | 0.39 | 0.49 5.0 | U - | 7.35 | 0.93 | 8 in. HDPE | 125.00 | 1.00 | 8 1.2 | 0.35 | 3.47 | 3.84 | 1.10 | - | 1016.01 | 1014.76 | 1017.82 | 0.76 | 0.40 | 1.00 | 0.23 | 0.98 | 1016.74 | 1018.80 | 1 | + | |
| | D A C | 0.50 | 0.50 | 0.75 | 0.04 | | 7.25 | 2.05 | FILMAT | ├ | | - | | | - | + | | 1 | | | + | | 1 | | | | + | + | + | - |
| F1 | BAS | 0.53 | 0.53 | 0.75 | 0.94 5.0 | υ - | 7.35 | 3.65 | FLUME | | - | | | - | - | - | | 1 | | | + | - | 1 | | | | + | 1 | + | |
| Fo | DAC | 0.45 | 0.45 | 0.00 | 100 5 | | 7.25 | 2.24 | FILIME | | - | | | - | - | - | | 1 | | | + | - | 1 | | | | + | 1 | + | |
| F2 | BAS | 0.45 | 0.45 | 0.80 | 1.00 5.0 | U - | 7.35 | 3.31 | FLUME | l | - | | - | - | - | 1 | | 1 | | | + | 1 | 1 | | | - | 1 | 1 | + | <u> </u> |
| | D 4 0 | 0.00 | 0.00 | 0.00 | 4.00 | _ | 7.35 | 0.05 | FLUME | ļ | | | | | | + | | ļ | | | + | ļ | ! | | | | 1 | + | | |
| l Lo | DAO | 1 0.32 | | | | | | 2.35 | | | | | | | | | | | | | | 1 | | | | | | | | |

MCPL EAST LEE'S SUMMIT - ELEVATION AREA VOLUME TABLE AND STAGE STORAGE DISCHARGE TABLE

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Wednesday, 02 / 13 / 2019

Pond No. 1 - pond

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1006.50 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 1006.50 | 00 | 0 | 0 |
| 1.00 | 1008.00 | 5,120 | 1,706 | 1.706 |
| 2.00 | 1009.00 | 14,880 | 9,575 | 11,282 |
| 3.00 | 1010.00 | 16,9 4 0 | 15,897 | 27,179 |
| 4.00 | 1011.00 | 18,982 | 17,950 | 45,128 |
| 5.00 | 1012.00 | 21,140 | 20,049 | 65,178 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|------|------|----------|----------------|-------------|----------|------|------|
| Rise (in) | Inactive | 0.00 | 0.00 | 1.00 | Crest Len (ft) | = 2.40 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 10.00 | 0.00 | 0.00 | 1.00 | Crest El. (ft) | = 1008.75 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 0 | 0 | 4 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 1009.00 | 0.00 | 0.00 | 1006.50 | Weir Type | = Rect | | | |
| Length (ft) | = 10.00 | 0.00 | 0.00 | 2.00 | Multi-Stage | = No | No | No | No |
| Slope (%) | = 1.00 | 0.00 | 0.00 | n/a | · · | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Contour) | | |
| Multi-Stage | = n/a | No | No | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

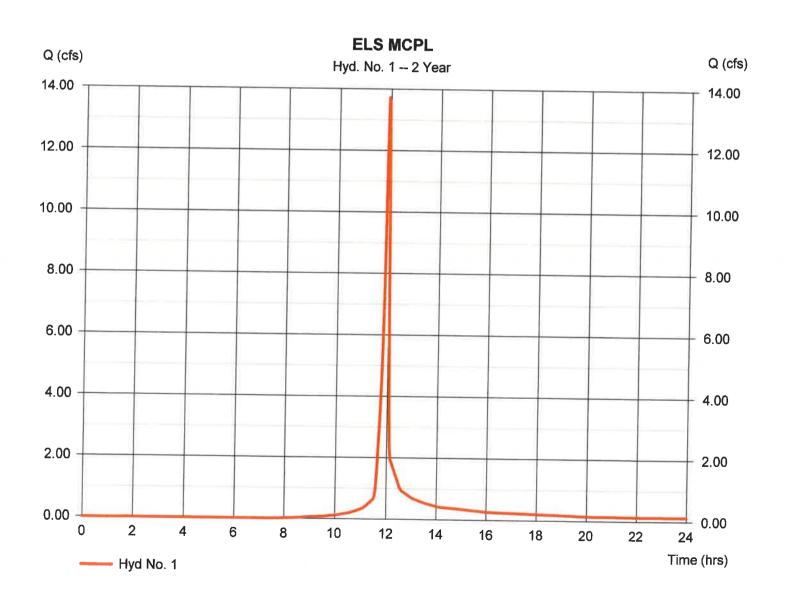
| Stage ft | Storage cuft | Elevation ft | CIv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|--------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 0.00 | 0 | 1006.50 | 0.00 | | | 0.00 | 0.00 | | | | | | 0.000 |
| 1.00 | 1.706 | 1008.00 | 0.00 | | | | | | | | | | 0.000 |
| | - 1 | | | | | 0.14 | 0.00 | | | | | | 0.145 |
| 2.00 | 11,282 | 1009.00 | 0.00 | | | 0.31 | 1.00 | | | | | | 1.310 |
| 3.00 | 27,179 | 1010.00 | 0.00 | | | 0.52 | 11.17 | | | | | | 11.68 |
| 4.00 | 45,128 | 1011.00 | 0.00 | | | 0.75 | 26.97 | | | | | | |
| 5.00 | | | | | | | | | | | | | 27.72 |
| 5.00 | 65,178 | 1012.00 | 0.00 | | | 1.02 | 46.83 | | | | | | 47.84 |

Wednesday, 02 / 13 / 2019

Hyd. No. 1

ELS MCPL

| Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration | = SCS Runoff = 2 yrs = 2 min = 4.500 ac = 0.0 % = User = 3.27 in = 24 hrs | Peak discharge Time to peak Hyd. volume Curve number Hydraulic length Time of conc. (Tc) Distribution Shape factor | = 13.72 cfs = 11.93 hrs = 27,834 cuft = 90 = 0 ft = 5.00 min = Type II = 484 |
|--|--|--|---|
|--|--|--|---|

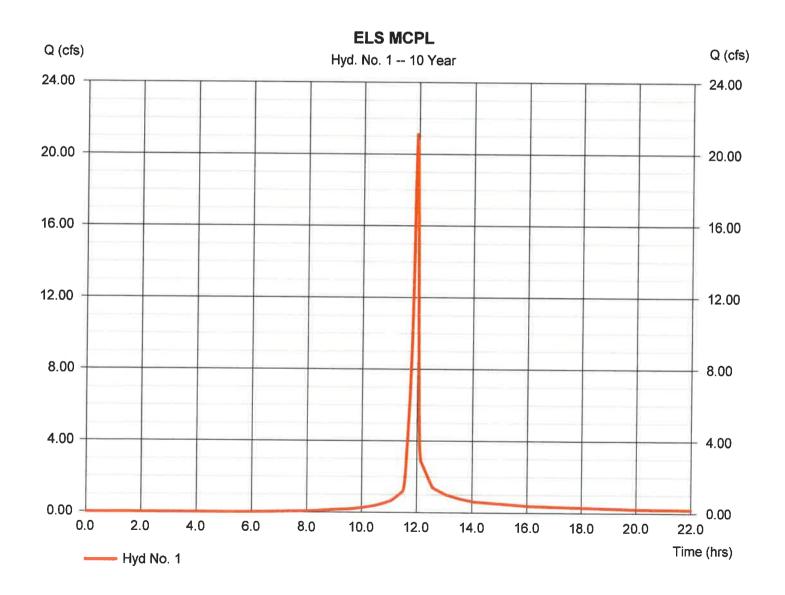


Wednesday, 02 / 13 / 2019

Hyd. No. 1

ELS MCPL

| Hydrograph type | = SCS Runoff | Peak discharge | = 21.11 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 11.93 hrs |
| Time interval | = 2 min | Hyd. volume | = 43,436 cuft |
| Drainage area | = 4.500 ac | Curve number | = 90 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 5.00 min |
| Total precip. | = 4.42 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |
| | | | |

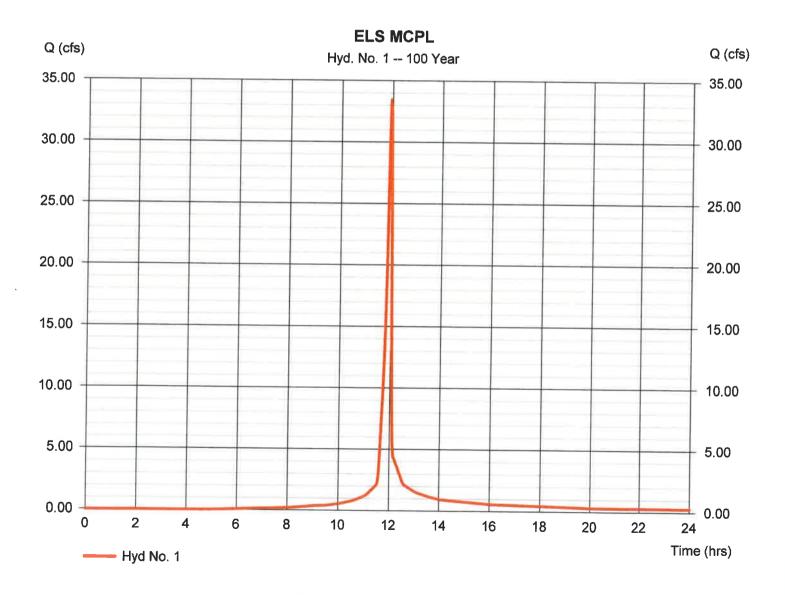


Wednesday, 02 / 13 / 2019

Hyd. No. 1

ELS MCPL

| Hydrograph type = SCS Runoff Storm frequency = 100 yrs Time interval = 2 min Drainage area = 4.500 ac Basin Slope = 0.0 % Tc method = User Total precip. = 6.32 in Storm duration = 24 hrs | Peak discharge Time to peak Hyd. volume Curve number Hydraulic length Time of conc. (Tc) Distribution Shape factor | = 33.45 cfs = 11.93 hrs = 70,523 cuft = 90 = 0 ft = 5.00 min = Type II = 484 |
|--|--|---|
|--|--|---|



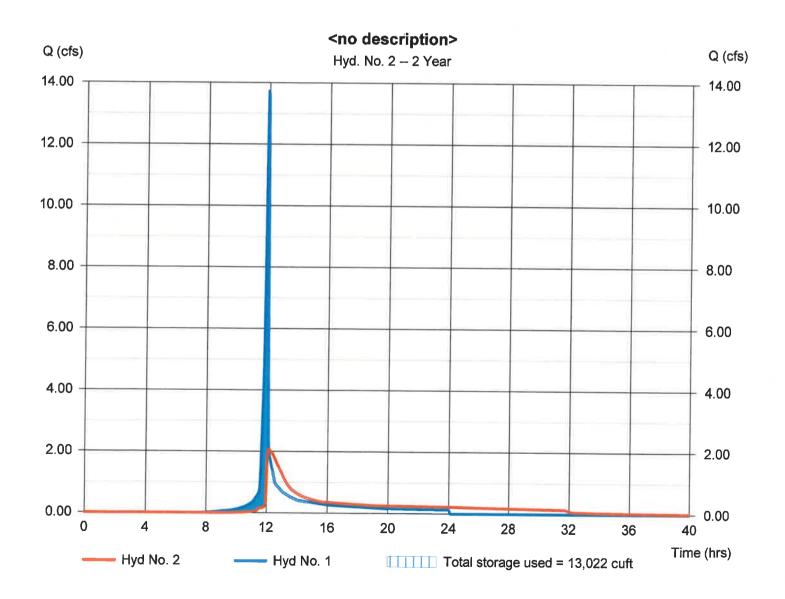
Wednesday, 02 / 13 / 2019

Hyd. No. 2

<no description>

Hydrograph type = Reservoir Peak discharge = 2.058 cfsStorm frequency = 2 yrsTime to peak = 12.13 hrs Time interval = 2 min Hyd. volume = 27.765 cuft Inflow hyd. No. = 1 - ELS MCPL Max. Elevation $= 1009.11 \, \text{ft}$ Reservoir name Max. Storage = pond = 13,022 cuft

Storage Indication method used.



Wednesday, 02 / 13 / 2019

Hyd. No. 2

<no description>

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyd. No. = 1 - FLS MC

Reservoir name = 1 - ELS MCP

= 10 yrs Time to peak
= 2 min Hyd. volume
= 1 - ELS MCPL Max. Elevation

Max. Storage

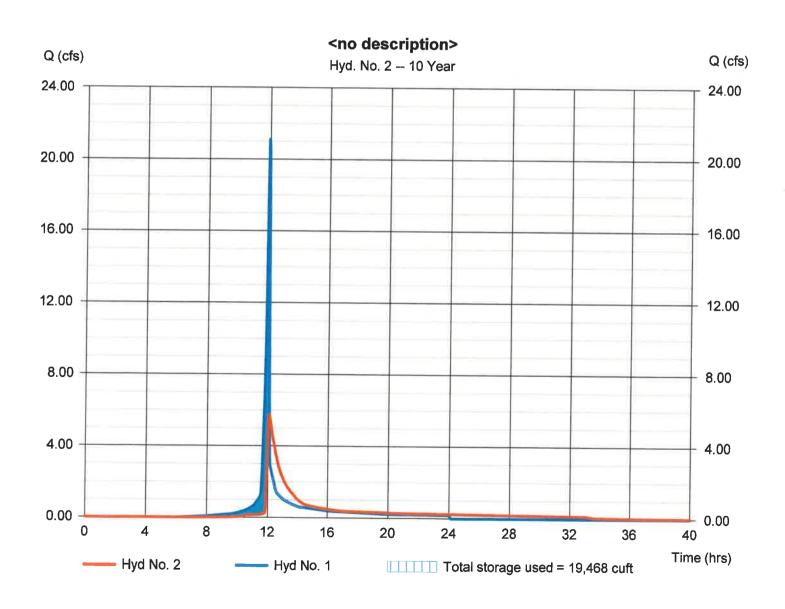
Peak discharge

= 12.07 hrs = 43,368 cuft = 1009.52 ft

= 5.762 cfs

= 19,468 cuft

Storage Indication method used.



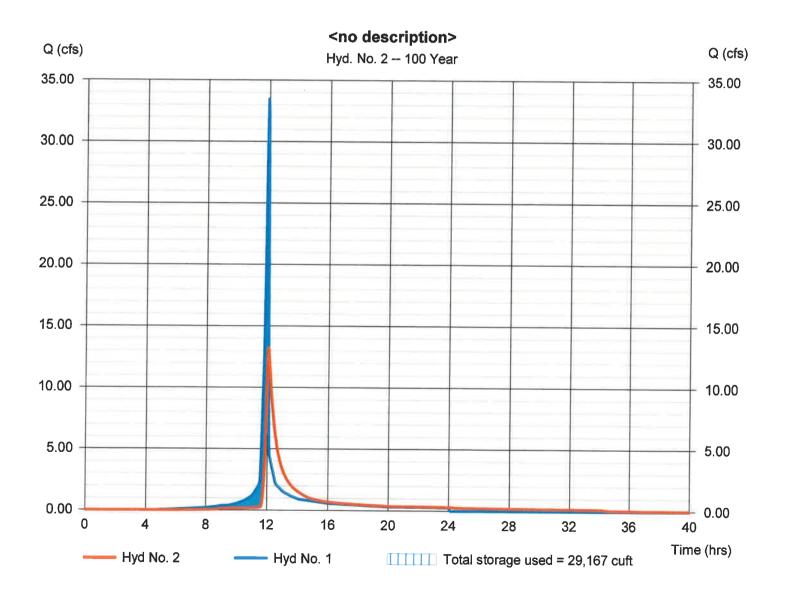
Wednesday, 02 / 13 / 2019

Hyd. No. 2

<no description>

Hydrograph type = Reservoir Peak discharge = 13.23 cfsStorm frequency = 100 yrsTime to peak $= 12.03 \, hrs$ Time interval = 2 min Hyd. volume = 70.455 cuft Inflow hvd. No. = 1 - ELS MCPL Max. Elevation = 1010.12 ft Reservoir name = pond Max. Storage = 29.167 cuft

Storage Indication method used.



Wednesday, 02 / 13 / 2019

Pond No. 1 - pond

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1006.50 ft

Stage / Storage Table

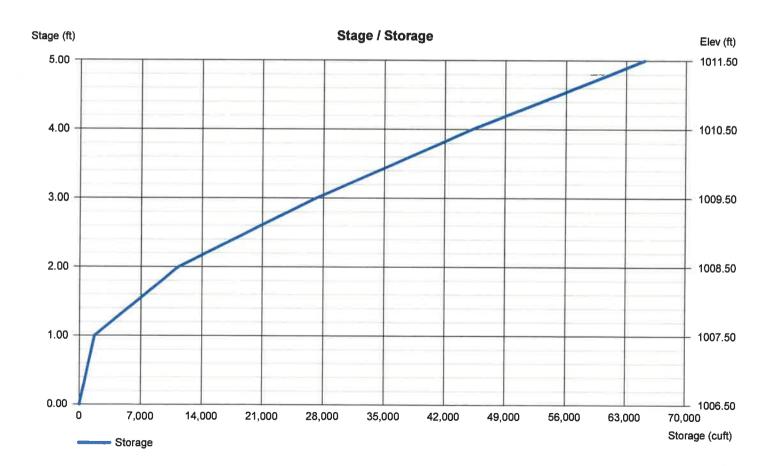
| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 1006.50 | 00 | 0 | 0 |
| 1.00 | 1008.00 | 5,120 | 1,706 | 1.706 |
| 2.00 | 1009.00 | 14,880 | 9.575 | 11,282 |
| 3.00 | 1010.00 | 16,940 | 15,897 | 27,179 |
| 4.00 | 1011.00 | 18,982 | 17,950 | 45,128 |
| 5.00 | 1012.00 | 21,140 | 20,049 | 65,178 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|------|------|----------|----------------|-------------|----------|------|------|
| Rise (in) | Inactive | 0.00 | 0.00 | 1.50 | Crest Len (ft) | = 2.40 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 10.00 | 0.00 | 0.00 | 1.50 | Crest El. (ft) | = 1008.75 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 0 | 0 | 4 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 1009.00 | 0.00 | 0.00 | 1006.50 | Weir Type | = Rect | | | |
| Length (ft) | = 10.00 | 0.00 | 0.00 | 2.00 | Multi-Stage | = No | No | No | No |
| Slope (%) | = 1.00 | 0.00 | 0.00 | n/a | | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Contour) | | |
| Multi-Stage | = n/a | No | No | No | TW Elev. (ft) | = 0.00 | , | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Wednesday, 02 / 13 / 2019

Pond No. 1 - pond

Pond Data

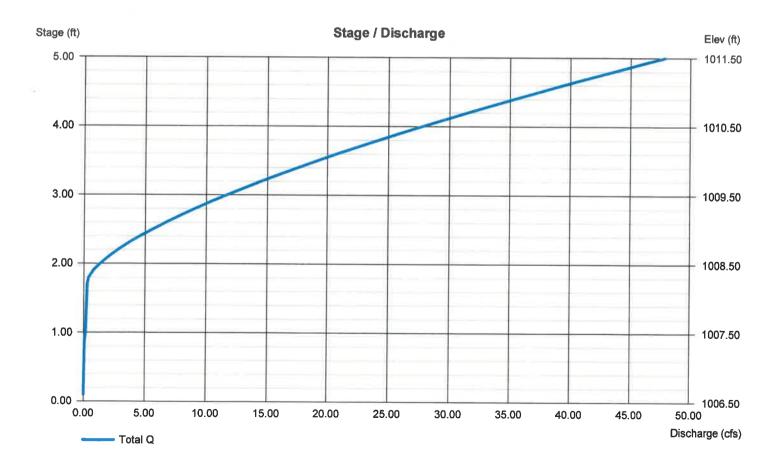
Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 1006.50 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 1006.50 | 00 | 0 | 0 |
| 1.00 | 1008.00 | 5,120 | 1,706 | 1,706 |
| 2.00 | 1009.00 | 14,880 | 9,575 | 11.282 |
| 3.00 | 1010.00 | 16,940 | 15,897 | 27,179 |
| 4.00 | 1011.00 | 18,982 | 17,950 | 45,128 |
| 5.00 | 1012.00 | 21,140 | 20,049 | 65,178 |

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] Rise (in) Inactive 0.00 0.00 1.50 = 2.40 0.00 Crest Len (ft) 0.00 0.00 Span (in) = 10.000.00 0.00 1.50 Crest El. (ft) = 1008.75 0.00 0.00 0.00 No. Barrels = 1 0 Weir Coeff. = 3.33 3.33 3.33 3.33 Invert El. (ft) = 1009.000.00 0.00 1006.50 Weir Type = Rect Length (ft) = 10.00 0.00 0.00 2.00 Multi-Stage = No No No No Slope (%) = 1.00 0.00 0.00 n/a N-Value = .013 .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Contour) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Feb 18 2019

<Name>

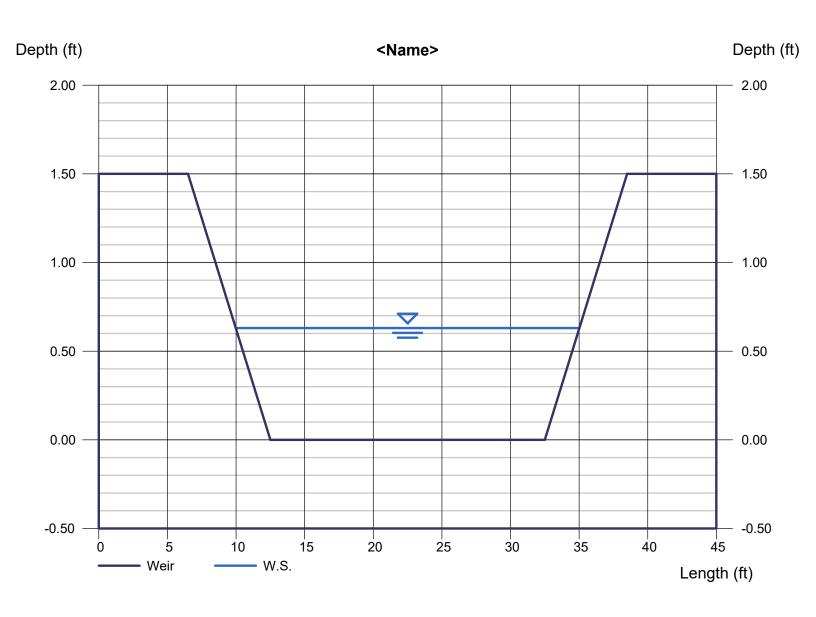
| Trapezoidal Weir | | |
|--------------------|---|-------|
| Crest | = | Broad |
| Bottom Length (ft) | = | 20.00 |
| Total Depth (ft) | = | 1.50 |
| Side Slope (z:1) | = | 5.00 |

Calculations

Weir Coeff. Cw = 3.10 Compute by: Known Q Known Q (cfs) = 33.40

Highlighted Depth (ft) = 0.63 Q (cfs) = 33.40

Area (sqft) = 14.19 Velocity (ft/s) = 2.35 Top Width (ft) = 25.04



| Depth | Q | Area |
|-------|--------|--------|
| (ft) | (cfs) | (sqft) |
| 0.15 | 3.688 | 3.09 |
| 0.30 | 10.68 | 6.36 |
| 0.45 | 20.06 | 9.81 |
| 0.60 | 31.58 | 13.44 |
| 0.75 | 45.10 | 17.25 |
| 0.90 | 60.56 | 21.24 |
| 1.05 | 77.91 | 25.41 |
| 1.20 | 97.15 | 29.76 |
| 1.35 | 118.26 | 34.29 |
| 1.50 | 141.24 | 39.00 |

Appendix D

Drainage and Detention Calculations

Appendix E
Water Treatment Calculations

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet - EDD-1

Project: MCPL East Lee's Summit Date: 01/18/2019

Location: Lee's Summit Company: Olsson

Designer: TMP Checked: LWM

I. Basin Water Quality Volume

- Step 1: Tributary area to EDDB, A_T (ac.) A_T (ac) = 4.50
- Step 2: Calculate WQ_V using methodology in Section 6 WQ_V (ac-ft) = 0.29
- Step 3: Add 20 percent to account for silt and sediment depositation in the basin V_{DESIGN} (ac-ft) = 0.34

14911.83

Ila. Water Quality Outlet Type

Step 1: Set water quality outlet type:

Outlet Type = 2

Type 1 = Single Orifice

Type 2 = Perforated Riser or Plate

Type 3 = V-Notch Weir

Step 2: Proceed to part IIb, IIc, or IId based on water quality outlet type selected

Ilb. Water Quality Pool Outlet, Single Orifice

- Step 1: Depth of water quality volume at outlet, Z_{WQ} (ft) Z_{WQ} (ft) = 2.40
- Step 2: Average head of water quality volume over invert of orifice, H_{WQ} (ft) H_{WQ} (ft) = 1.20 $H_{WQ} = 0.5 * Z_{WQ}$
- Step 3: Average water quality outflow rate, Q_{WQ} (cfs) Q_{WQ} (cfs) = 0.09 $Q_{WQ} = (WQ_V * 43,560) / (40*3,600)$
- Step 4: Set value of orifice discharge coefficient, C_0 $C_0 = 0.66$

 C_O = 0.66 when thickness of riser/weir plate is = or < orifice diameter C_O = 0.80 when thickness of riser/weir plate is > orifice diameter

- Step 5: Water quality outlet orifice diameter (minimum of 1/2 inch), D_O (in) D_O (
- Step 6: To size outlet orifice for EDDB with an irregular stage-volume relationship use the Single Orifice Worksheet

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet

| Project: | MCPL East Lee's Summit | Date: 01/18/2 | 019 | |
|----------|---|--|-------------------------------|----------------|
| | Lee's Summit | Company: Olsson | | |
| esigner | TMP | Checked: <u>LWM</u> | | |
| c. Wate | r Quality Outlet, Peforated Riser (Continu | ued) | | |
| Step 1: | Depth of water quality volume at outlet, Z_W | Q (ft) | Z_{WQ} (ft) = | 2.40 |
| Step 2: | Recommended maximum outlet area per r $A_O = WQ_V / (0.013 * Z_{WQ}^2 + 0.22 * Z_{WQ}^2)$ | | A_{O} (in ²) = | 0.57 |
| Step 3: | Circular perforation diameter per row assur | ming a single column, D _I (| (in) D _I (in) = | 1.00 |
| tep 4: | Numbers of columns, n _c | | $n_c = $ | Use 1" 1.00 |
| tep 5: | Design circular perforation diameter (from | 1 to 2 inches), D _{Perf} (in) | D _{Perf} (in) = | 1.00 |
| tep 6: | Horizontal perforation column spacing when If D_{Perf} is not > or = 1, S_c = 4 | $n_c > 1$, center to center, | $S_c = $ | NA |
| tep 7: | Number of rows, 4" vertical spacing between | en perforations, center to | center, $n_r = $ | 7 |
| c. Wate | r Quality Outlet, V-Notch Weir | | | |
| step 1: | Depth of water quality volume above perm | anent pool, Z _{WQ} (ft) | Z_{WQ} (ft) = | NA |
| itep 2: | Average head of water quality pool volume $H_{WQ} = 0.5 * Z_{WQ}$ | over invert of v-notch H _W | H_{WQ} (ft) H_{WQ} (ft) = | NA |
| tep 3: | Average water quality pool outflow rate, Q_V $Q_{WQ} = (WQ_V * 43,560) / (40*3,600)$ | | Q _{WQ} (cfs) = | NA |
| tep 4 | V-notch weir coefficient, C_{ν} | | C _v = | NA |
| tep 5: | V-notch weir angle, q (deg) θ = 2 *(180/ π)*arctan(Q _{WQ} / (C _v * | H _{wQ} ^{5.2})) | q (deg) = | NA |
| | V-notch angle should be at least 2 20 degrees if calculated angle is si | • | | |
| Step 6: | V-notch weir top width, W_v (ft) $W_v = 2^* Z_{WQ} * TAN(\theta/2)$ | | W _v (ft) = | NA |
| ton 7: | T | - inna malamaka masa ka | alatina di Santa di | |

Step 7: To calculate v-notch angle for EDW with an irregular stage-volume relationship, use th V-notch Weir Worksheet

Design Procedure Form: Extended Dry Detention Basin (EDDB) Main Worksheet

| Project: | MCPL East Lee's Summit | Date: | 01/18/2019 |
|-----------|------------------------|----------|------------|
| Location: | Lee's Summit | Company: | Olsson |
| Designer | ТМР | Checked: | LWM |

III. Flood Control

Refer to APWA Specifications Section 5608

IV. Trash Racks

Step 1: Total outlet area, A_{ot} (in²)

 A_{ot} (in²) = 5.46

Step 2: Required trash rack open area, A_t (in²)

 $A_t (in^2) = 60.83$

 $A_t = A_{ot} * 77 * e^{(-0.124 * D)}$ for single orifice outlet

 $A_t = (A_{ot} / 2) * 77 * e^{(-0.124*D)}$ for orifice plate or perforated riser outlet

At = 4 * Aot for v-notch weir outlet

V. Basin Shape

| Sten 1: | Length to width ratio should be at least 3:1 (| 1 ·W) wherever | practicable (| (L:W) = | 10:1 Plus |
|---------|--|------------------|---------------|-------------|-----------|
| Otop 1. | Longin to width ratio should be at least 5.1 (| L.VV) WITCH CVCI | practicable (| (L. V V) — | 10.11143 |

Step 2: Low flow channel side lining Concrete: Yes

Soil/Riprap: NA
No low flow channel: NA

 V_{BS} (ac-ft) =

1.03

Step 3: Top stage floor drainage slope (toward low flow channel), S_{TS} (%) S_{TS} (%) = 0.00 Top stage depth, D_{TS} (ft) 0.00 0

Bottom stage volume, V_{BS} (ac-ft) V_{BS} (% of WQ_{V}) = 0.33

VI. Forebay (Optional)

Step 4:

Step 1: Volume should be greater than 10% of WQ_V Min Vol_{FB} (ac-ft) = NA

Step 2: Forebay depth, Z_{FB} (ft) Z_{FB} (ft) = NA

Step 3: Forebay surface area, A_{FB} (ac) A_{FB} (ac) = NA

Step 2: Paved/hard bottom and sides?