

PRELIMINARY STORM WATER DRAINAGE REPORT

LOT 1B

DOUGLAS CORNERS

LEE'S SUMMIT, MISSOURI

100 NE TUDOR ROAD

PREPARED FOR

THOMPSON PROPERTIES, LLC

PREPARED BY

HG CONSULT, INC.

August 6, 2018

This section is to address the Lee's Summit checklist for inclusion. **Response will be in bold.**

1. Preliminary Development Drainage Area Map:
(including Locations of all points of discharge from each sub-drainage area)
2. Post Development Drainage Area Map:
(including Locations of all points of discharge from each sub-drainage area)
3. Undetained Areas:
(as shown on Preliminary Development Drainage Area Map and Post Development Drainage Area Map)
4. Soil analysis, showing the soil type(s) predominant on the site:
(Attached soil analysis from USDA Natural Resources Conservation Web Soil Survey)
5. Time of concentration calculations:
(Time of concentration was assumed to be 5 minutes)
6. Curve number assumptions:
(Curve number assumed to be 87 for existing condition and 89 for proposed condition)
7. Floodplain issues (if any):
No Floodplain issues are on this site.
8. Wetland and USCOE issues:
No Wetland or USCOE issues are on this site.
9. Methodology used in the preparation of this report:
General methodology of report was prepared using Bentley PondPack V8i to determine the storm events, the rainfall amounts and the detention pond requirements.
10. Existing Conditions:
The existing conditions for this site includes a 33,640 SF office building with adjacent parking and a drive aisle access to the north with the existing drive on Lot 1A and Lot 1B. The site to the south (Schlotzky's Restaurant) was previously included in site development for the sizing of the existing detention pond with a 3,330 SF building and parking lot. There was an undersized detention pond for the entire development including the partially developed Lot 1B in the existing condition drawing. Lot 1B included a parking pad and original garage area space.
11. Proposed Conditions:
The proposed condition site includes the existing condition plus the addition of a 7,972 SF office building with an additional 4,496 SF of apartments on the second floor. The proposed condition site includes the improvement of the existing detention pond to accommodate the existing office building, restaurant and all existing parking and drive aisles.
12. Future development:
No future development is planned at this time.
13. A discussion of the method used to comply with the water quality standard set forth in Section 5600 (i.e., 40 hour extended detention, or volumetric reduction credit, or combination thereof).
APWA 5608.4 requires a 40-hour extended release of the water quality storm event (1.37"/24-hour rainfall) per Section 8.10 of the BMP Manual. The detention facility will release the water quality event over a 40-hour period. The Time vs. Volume graph is attached.

14. The Time vs. Volume graph:
(See attached).

15. A discussion of all conclusions, including any waivers necessary to comply with the Design and Construction Manual.

All design is in compliance with the Design and Construction Manual. No variance requested.

16. Explanation of the accounting procedure used to calculate the allowable release rate at key points shown on the drainage maps. In essence, if off-site contributors to drainage area are present in the existing condition drainage area map, then a percentage of their existing peak flow rate can be added to the allowable peak flow rate to the various drainage points of discharge.

No off-site areas are included in this report.

17. A table showing how these drainage areas were accounted in the calculation of the allowable peak flow rate at the various drainage points of discharge.

All drainage areas discharge at the detention pond as shown and accounted for.

18. Final Report - Inflow hydrographs for the 2, 10, and 100 year storm events (please keep in mind that this information will be required to run the preliminary model, but not necessarily required in the preliminary report).

The 2, 10 and 100 year storm events are included in this report.

19. The maximum water surface elevation within the basin (normally the 100 year event).

The maximum water surface elevation within the basin are included in this report (1016.74).

20. Final Report: Stage-discharge-rating curves/data tables for each emergency spillway, primary outlet works and combined outlets and overflows.

Stage-storage rating curves included in Douglas Spillway Report.

21. Final Report: Routing curves for all design storms with time plotted as the abscissa, and the following plotted as ordinates:

- a. Cumulative inflow volume
- b. Cumulative discharge
- c. Stage elevation
- d. Cumulative storage

Routing curves to be submitted with Final Report as requested.

Project Overview

The proposed project is a speculative retail/apartment building. The building will be contained in a 7,972 square foot building footprint with retail on the bottom floor and 4,496 square foot apartments on the second floor. This project is contained on a 1.73 acre site. The site is construction ready. The storm sewer system and detention pond will need additional improvements to allow for proper drainage from site.

The topography of the site is a gentle slope north west to the east. The existing storm sewer detention system is in place on the east side of the site on the east side of NE Douglas Street and the north side of Tudor Road. The overall existing storm sewer system serves all of Douglas Corners. An additional amount of detention will be required to accommodate the entire developed area which is provided with this project.

Drainage Assessment of the Project Site

Due to the slope of the site and the need for a flat slab, the bench and fill grading method was used for the site along with the need to have positive drainage away from the building, drainage areas directing storm water into new storm sewer catchments that forces storm water into the detention pond. The remainder of the site grading directs pervious areas and impervious areas away from the building and drainage to the proposed detention pond. Design requirements call for a piping system with a minimum capacity for the 10 year event, with the 100 year storm event being routed overland in an above grade manner such as swales and gutters. To insure that higher frequency storms would not cause any ponding problems or inundation of parked vehicles, the structures and piping system have been designed to the 100 year event flows. With the relatively small drainage areas, these flows are low and pipe sizes are 18 inch draining to the detention pond and a 18" discharge pipe from the detention pond to an existing catch basin off-site.

Conveyance Design

As shown on the Drainage plan for the site, all areas drain to the detention pond by sheet flow over the parking and drive aisle area and by existing piping system. This system generates a 10 year flow of 38.69 cfs and a 100 year flow of 59.35 cfs pre-developed. After development and routing through the detention pond, 10 year flows have been reduced to 11.18 cfs and 100 year flows have been reduced to 15.28 cfs. All areas within drainage area drain towards the proposed detention pond.

Temporary Erosion and Sediment Control

During construction and prior to paving, it will be necessary to control erosion and sediment from the site during storms with in the construction timeframe. To insure that sediment does not enter the existing storm system or runs off to the existing street, perimeter containment is controlled by silt fence installation, inlet protection and an engineered detention release structure. To keep construction traffic from tracking mud onto the adjacent city street, a stabilized rock construction entrance will need to be installed. These erosion control devices, and their maintenance throughout the construction timeframe, are required by ordinance and the details for them are referenced by the City's Design and Construction Manual and shown on Detail Sheets 10 thru 13.

Post development water quality will be addressed through the use a water quality detention release structure. The owner will need to have a routine maintenance policy for the cleaning, repair and replacement of the detention release structure.

Design Calculations

See the attached for drainage area calculations, flows, pipe sizing, inlet sizing and water quality calculations as requested.

AASHTO Group Index—Jackson County, Missouri
(DOUGLAS CORNERS)



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

8/6/2018
Page 1 of 5

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

Soil Rating Polygons

-  <= 14
-  > 14 and <= 25
-  Not rated or not available

Soil Rating Lines

-  <= 14
-  > 14 and <= 25
-  Not rated or not available

Soil Rating Points

-  <= 14
-  > 14 and <= 25
-  Not rated or not available

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri

Survey Area Data: Version 18, Sep 16, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 11, 2017—Sep 22, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



AASHTO Group Index

Map unit symbol	Map unit name	Rating (none)	Acres in AOI	Percent of AOI
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	25	3.2	98.2%
10180	Udarents-Urban land-Sampsel complex, 2 to 5 percent slopes	14	0.1	1.8%
Totals for Area of Interest			3.2	100.0%



Description

The AASHTO Group Index is a refinement to the seven major groups of the AASHTO soil classification system. According to

this system, soil is classified into seven major groups: A -I through A-7. Soils classified into groups A-1, A-2, and A-3 are granular materials of which 35% or less of the particles pass through the No. 200 sieve. Soils of which more than 35% pass through the No. 200 sieve are classified into groups A-4, A-5, A-6, and A-7. These soils are mostly silt and clay-type materials.

The classifications system is based on the following criteria:

1. Grain size
 - a. Gravel ; fraction passing the 75-mm(3-in.) sieve and retained on the No. 10 (2-mm) U.S. sieve
 - b. sand: fraction passing the No. 10 (2-mm) U.S. sieve and retained on the No.200 (0.075-mm) U.S. sieve
 - c. Silt and clay: fraction passing the No. 200 U.S. sieve
2. Plasticity The term silty is applied when the fine fractions of the soil have a plasticity index of 10 or less. The term clayey is applied when the fine fractions have a plasticity index of 11 or more.
3. If cobbles and boulders (size larger than 75 mm) are encountered, they are excluded from the portion of the soil sample from which classification is made.

To evaluate the quality of a soil as a highway subgrade material, one must also incorporate a number called the group index (GI) with the groups and subgroups of the soil. This index is written in parentheses after the group or subgroup designation.

The group index is given by the equation:

$$GI = (F200-35)[0.2 + 0.005(LL- 40)] + 0.01(.F200-15)(PI- 10)$$

where:

F200 = percentage passing through the No. 200 sieve

LL — liquid limit

PI : plasticity index

The group index is used typically to refine an AASHTO class but in the soil survey database is often used as a standalone soil attribute.

For each soil layer, this attribute is actually recorded as three separate values in the database. A low value and a high value indicate the range of this attribute for the soil component. A "representative" value indicates the expected value of this attribute for the component. For this soil property, only the representative value is used.



Rating Options

Units of Measure: none

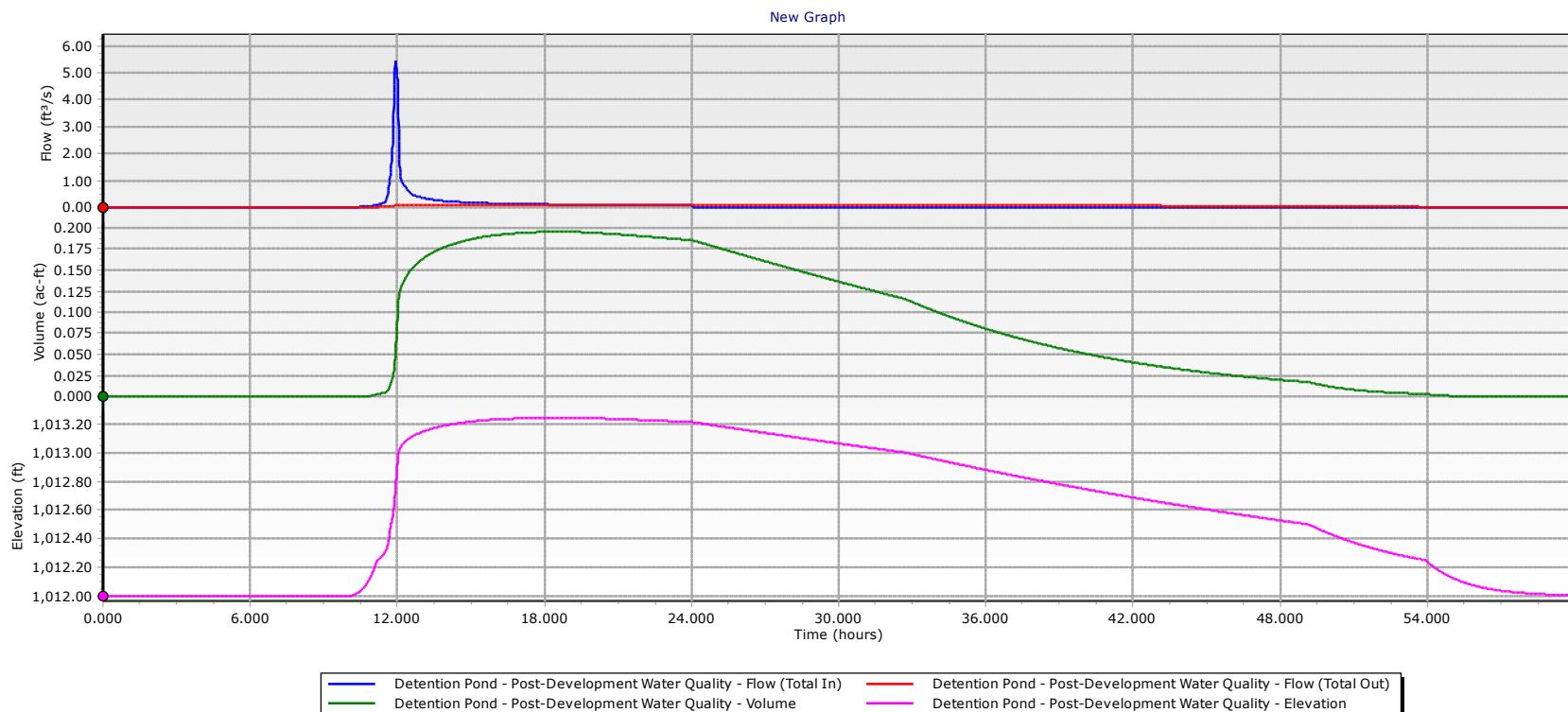
Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

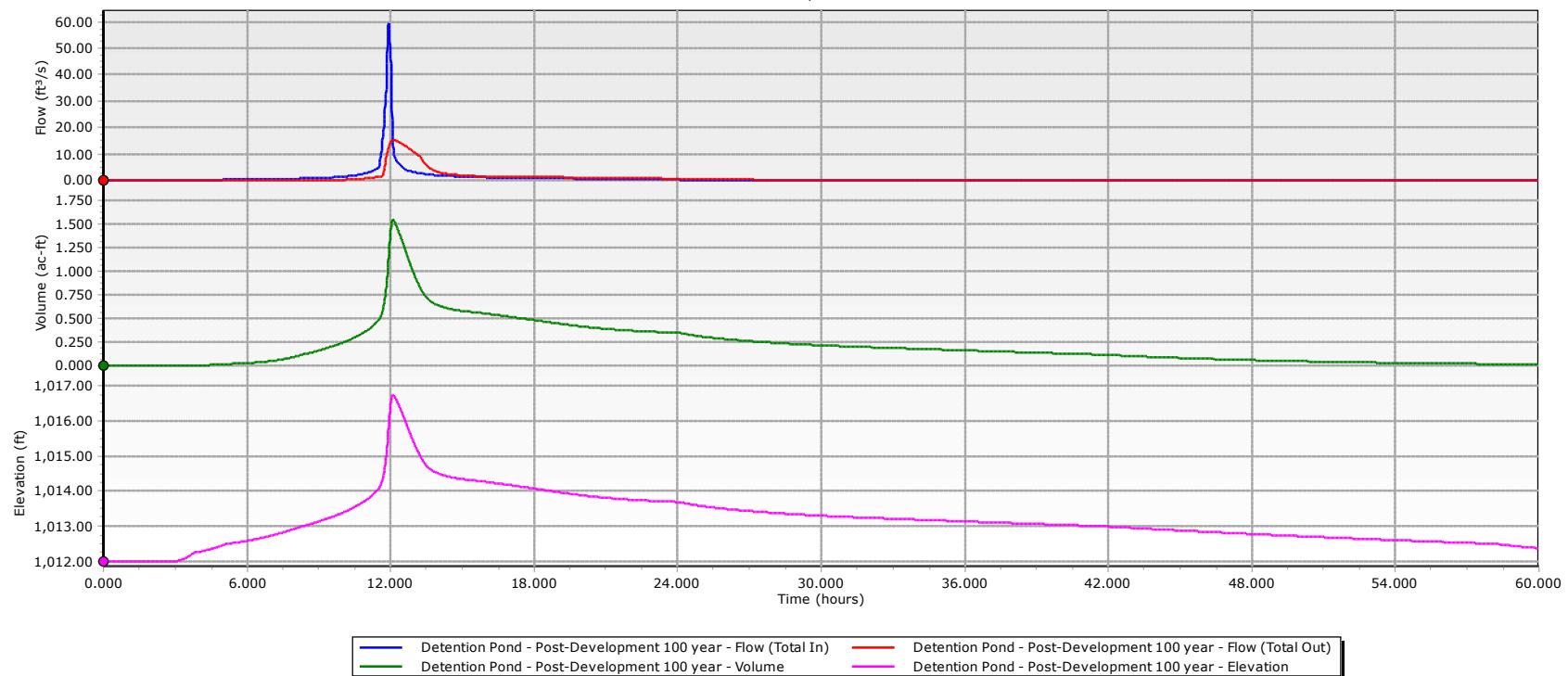
Tie-break Rule: Higher

Interpret Nulls as Zero: No

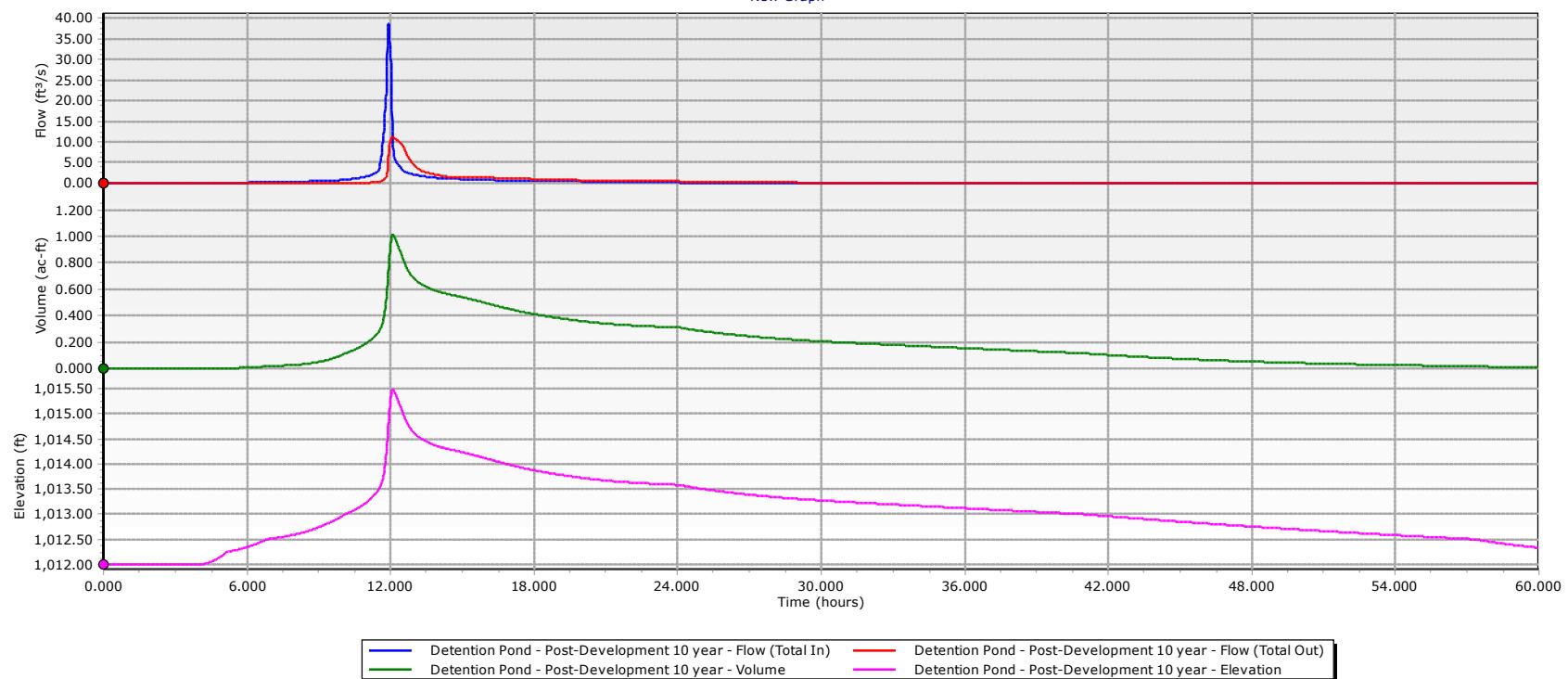
Layer Options (Horizon Aggregation Method): All Layers (Weighted Average)



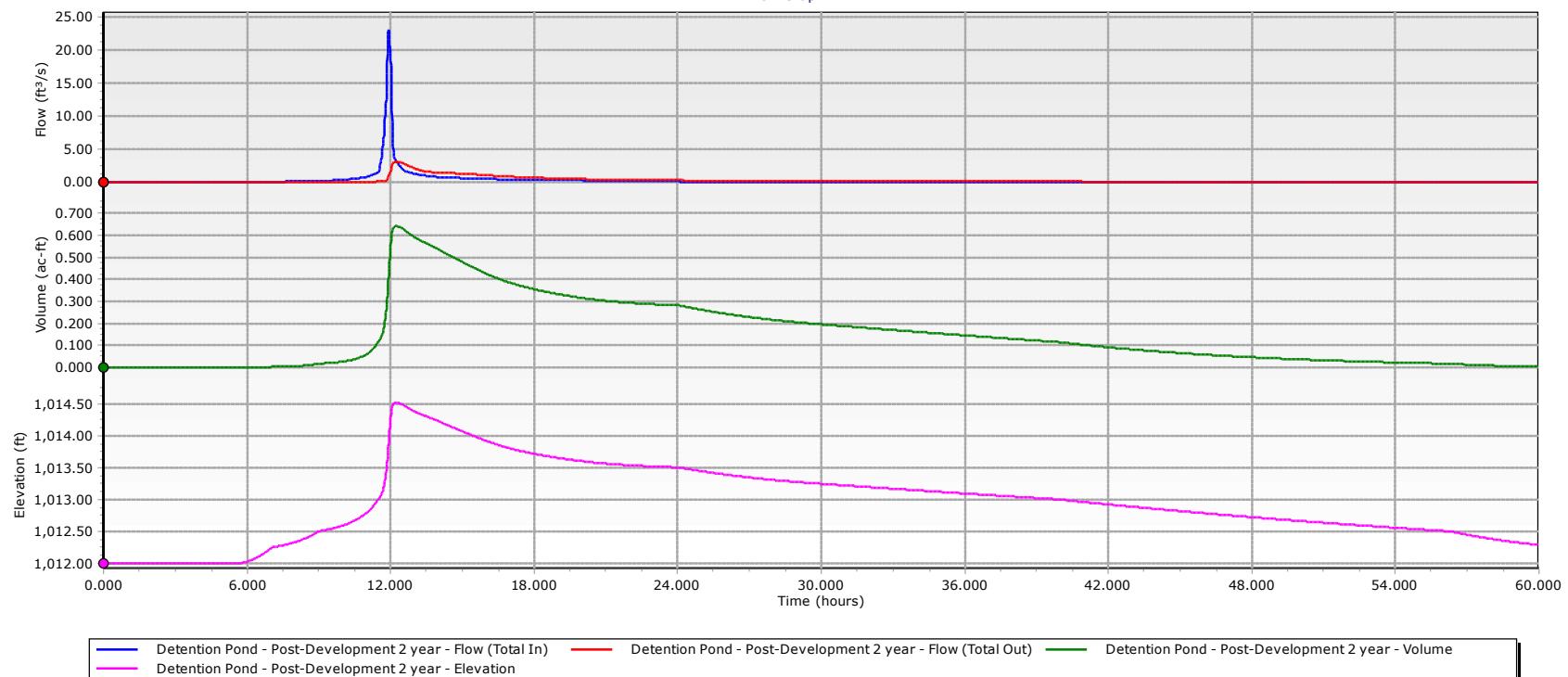
New Graph



New Graph



New Graph



Composite Outlet Structure Detailed Report: Primary Outlet Structure

Element Details			
Label	Primary Outlet Structure	Notes	
Headwater Range			
Headwater Type	Use Pond for Headwater Range	Maximum (Headwater)	1,018.50 ft
Pond	Detention Pond	Increment (Headwater)	0.50 ft
Minimum (Headwater)	1,012.00 ft		
SpotElevation (ft)			
Tailwater Setup			
Tailwater Type	Free Outfall		
Tailwater Tolerances			
Maximum Iterations	30	Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft	Flow Tolerance (Minimum)	0.001 ft³/s
Headwater Tolerance (Maximum)	0.50 ft	Flow Tolerance (Maximum)	10.000 ft³/s
Tailwater Tolerance (Minimum)	0.01 ft		
Outlet Structure			
Outlet Structure Type	Culvert	Culvert Type	Circular
Outlet Structure (IDs and Direction)			
Outlet ID	Culvert - 1	Downstream ID	Tailwater
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Culvert Data			
Number of Barrels	1	Downstream Invert	1,010.82 ft
Length	118.00 ft	Diameter	18.0 in
Upstream Invert	1,012.00 ft		
Unsubmerged->Submerged			
Specify Transitions	False	Compute Inlet Control Only	False

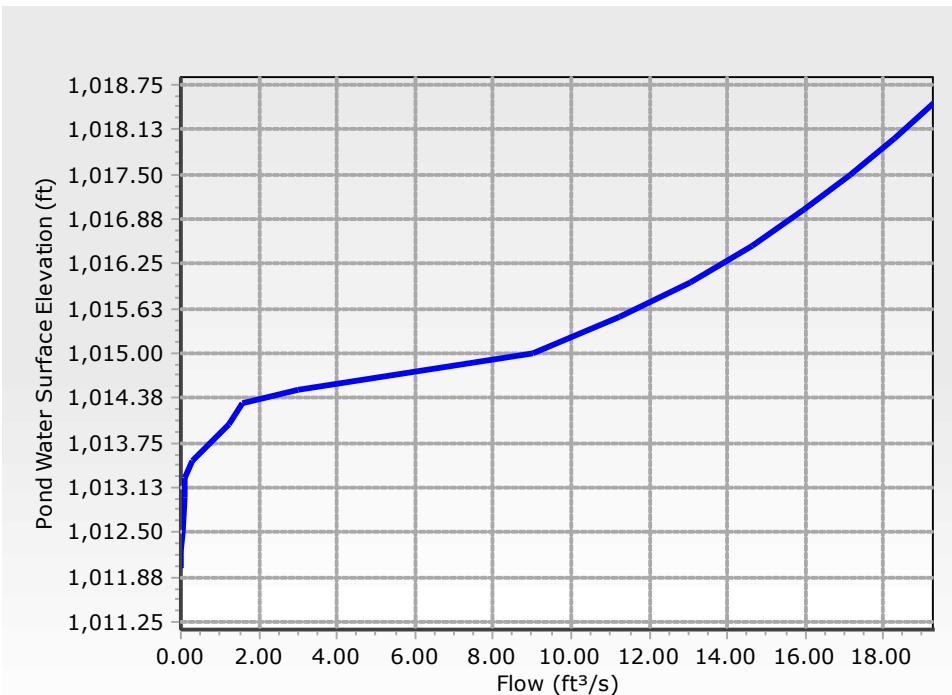
Composite Outlet Structure Detailed Report: Primary Outlet Structure

Culvert Coefficients

Inlet Description	Concrete - Groove end projecting	C	0.0317
Chart	Chart 1	Y	0.6900
Nomograph	Nomograph 3	Manning's n	0.011
Equation Form	Form 1	Ke	0.200
K	0.0045	Kr	0.000
M	2.0000	Slope Correction Factor	-0.500

Culvert (Advanced)

Convergence Tolerance	0.00 ft	Specify Number of Backwater Sections	False
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RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 13.35 ft³/s
 Upstream ID = Orifice - 2, Orifice - 3, Riser - 1, Orifice - 1
 Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,012.00	0.00	0.00	0.00	Free Outfall
1,012.25	0.02	1,012.07	Free Outfall	Free Outfall

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 13.35 ft³/s
 Upstream ID = Orifice - 2, Orifice - 3, Riser - 1, Orifice - 1
 Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,012.50	0.06	1,012.12	Free Outfall	Free Outfall
1,013.00	0.09	1,012.16	Free Outfall	Free Outfall
1,013.25	0.11	1,012.17	Free Outfall	Free Outfall
1,013.50	0.28	1,012.27	Free Outfall	Free Outfall
1,014.00	1.21	1,012.59	Free Outfall	Free Outfall
1,014.30	1.55	1,012.67	Free Outfall	Free Outfall
1,014.50	3.00	1,012.96	Free Outfall	Free Outfall
1,015.00	9.01	1,013.86	Free Outfall	Free Outfall
1,015.50	11.25	1,014.31	Free Outfall	Free Outfall
1,016.00	13.07	1,014.76	Free Outfall	Free Outfall
1,016.50	14.64	1,015.20	Free Outfall	Free Outfall
1,017.00	15.96	1,015.76	Free Outfall	Free Outfall
1,017.50	17.15	1,016.31	Free Outfall	Free Outfall
1,018.00	18.27	1,016.85	Free Outfall	Free Outfall
1,018.50	19.31	1,017.39	Free Outfall	Free Outfall
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	
0.00	0.01	(N/A)	0.00	

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL Vh=.018ft
 Dcr=.053ft CRIT.DEPTH Hev=.00ft

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 13.35 ft³/s
Upstream ID = Orifice - 2, Orifice - 3, Riser - 1, Orifice - 1
Downstream ID = Tailwater (Pond Outfall)

Message	
CRIT.DEPTH CONTROL	Vh= .029ft
Dcr= .086ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .038ft
Dcr= .111ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .040ft
Dcr= .119ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .067ft
Dcr= .194ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .147ft
Dcr= .411ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .169ft
Dcr= .468ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .251ft
Dcr= .658ft	CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL	Vh= .586ft
Dcr= 1.162ft	CRIT.DEPTH Hev= .00ft
INLET CONTROL...	Submerged: HW =2.31
INLET CONTROL...	Submerged: HW =2.76
INLET CONTROL...	Submerged: HW =3.20
FULL FLOW...Lfull=112.82ft	
Vh=1.267ft	HL=3.384ft Hev= .00ft
FULL FLOW...Lfull=115.54ft	
Vh=1.464ft	HL=3.963ft Hev= .00ft
FULL FLOW...Lfull=116.79ft	
Vh=1.660ft	HL=4.521ft Hev= .00ft
FULL FLOW...Lfull=117.01ft	
Vh=1.855ft	HL=5.057ft Hev= .00ft

Outlet Structure

Outlet Structure Type	Riser

Outlet Structure (IDs and Direction)

Outlet ID	Riser - 1	Downstream ID	Culvert - 1
Flow Direction	Forward Flow Only	Notes	

Outlet Structure (Advanced)

Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft

Outlet Structure (Riser)

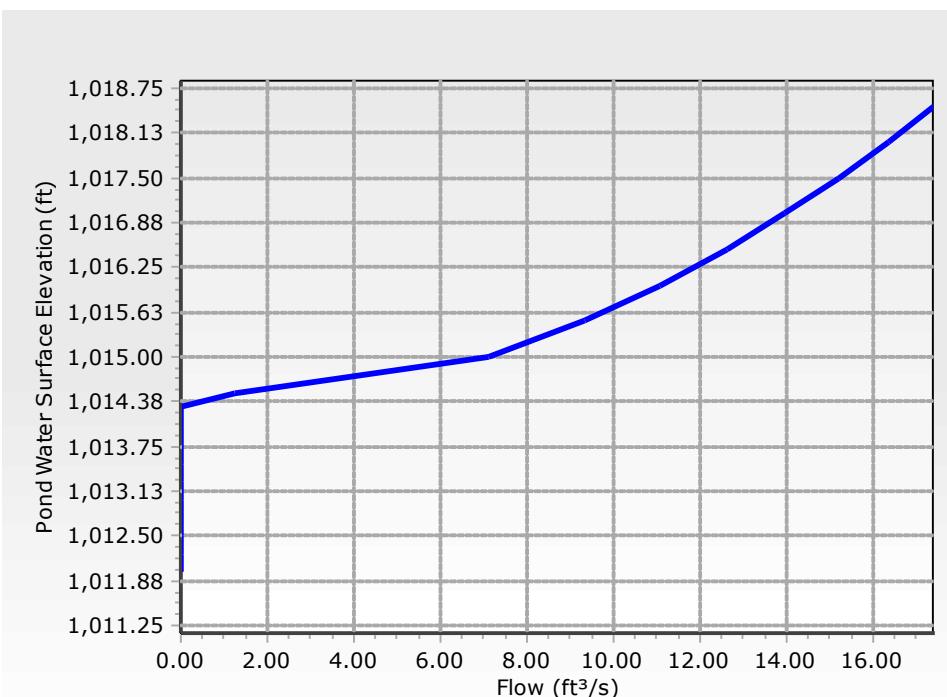
DOUGLAS.ppc 8/6/2018	Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666	Bentley PondPack V8i [08.11.01.56] Page 4 of 16
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Composite Outlet Structure Detailed Report: Primary Outlet Structure

Outlet Structure (Riser)			
Riser	Stand Pipe	Transition Elevation	0.00 ft
Diameter	18.0 in	Transition Height	0.00 ft
Weir Coefficient	3.00 (ft ^{0.5} /s)	K Reverse	1.000
Orifice Coefficient	0.600		

Outlet Structure (Common)			
Elevation	1,014.30 ft		

Outlet Structure (Riser, Advanced)			
Use Orifice Depth to Crest?	True	Use Submerged Weir Equation?	False



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,012.00	0.00	0.00	0.00	0.00
1,012.25	0.00	0.00	0.00	1,012.07
1,012.50	0.00	0.00	0.00	1,012.12

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.
WS below an invert; no flow.

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

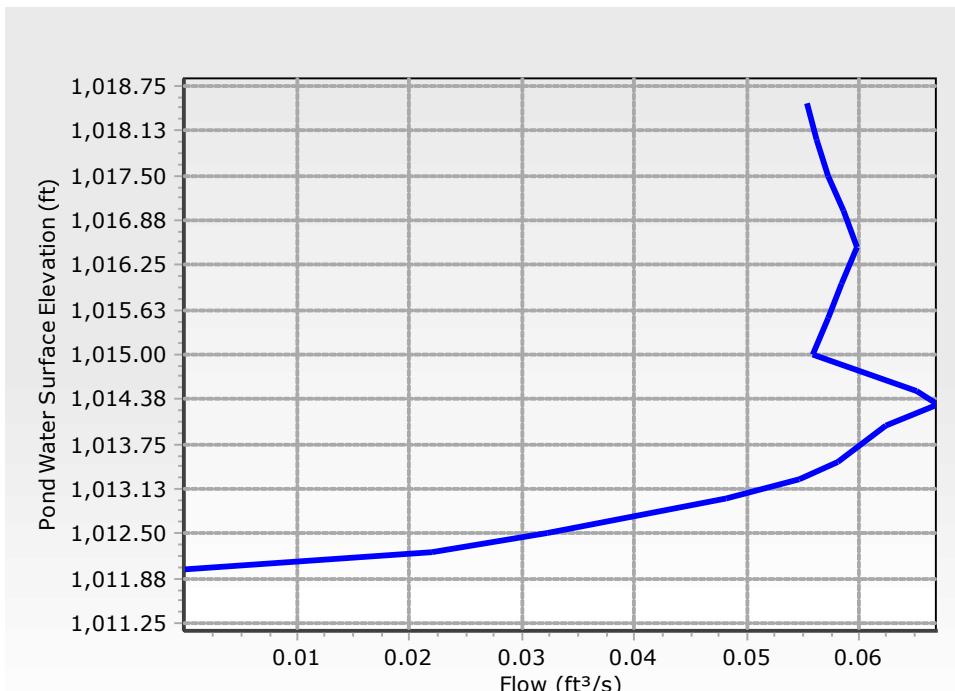
Message

WS below an invert; no flow.
WS below an invert; no flow.
WS below an invert; no flow.
Weir: H =0.2ft
Orifice: H =.70; Riser orifice equation controlling.
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=1.20
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=1.70
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=2.20
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=2.70
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=3.20
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=3.70
FULLY CHARGED RISER: Orifice Equation Control to Crest; H=4.20

Outlet Structure

Outlet Structure Type	Orifice		
Outlet Structure (IDs and Direction)			
Outlet ID	Orifice - 1	Downstream ID	Culvert - 1
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Circular Orifice	Orifice Coefficient	0.600
Number of Openings	2	Orifice Diameter	1.0 in
Outlet Structure (Common)			
Elevation	1,012.00 ft		

Composite Outlet Structure Detailed Report: Primary Outlet Structure



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,012.00	0.00	0.00	0.00	0.00
1,012.25	0.02	1,012.25	1,012.07	1,012.07
1,012.50	0.03	1,012.50	1,012.12	1,012.12
1,013.00	0.05	1,013.00	1,012.16	1,012.16
1,013.25	0.05	1,013.25	1,012.17	1,012.17
1,013.50	0.06	1,013.50	1,012.27	1,012.27
1,014.00	0.06	1,014.00	1,012.59	1,012.59
1,014.30	0.07	1,014.30	1,012.67	1,012.67
1,014.50	0.07	1,014.50	1,012.96	1,012.96
1,015.00	0.06	1,015.00	1,013.86	1,013.86
1,015.50	0.06	1,015.50	1,014.31	1,014.31
1,016.00	0.06	1,016.00	1,014.76	1,014.76
1,016.50	0.06	1,016.50	1,015.20	1,015.20
1,017.00	0.06	1,017.00	1,015.76	1,015.76
1,017.50	0.06	1,017.50	1,016.31	1,016.31
1,018.00	0.06	1,018.00	1,016.85	1,016.85
1,018.50	0.06	1,018.50	1,017.39	1,017.39

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

H = .18

H = .38

H = .84

H = 1.08

H = 1.23

H = 1.41

H = 1.63

H = 1.54

H = 1.14

H-1.19

H = 1.24

H = 1.21

II -1.50

II -1.24

II -1.15

H = 1.15

$$H = 1.11$$

Outlet S

Outlet 6

Outlet Structure

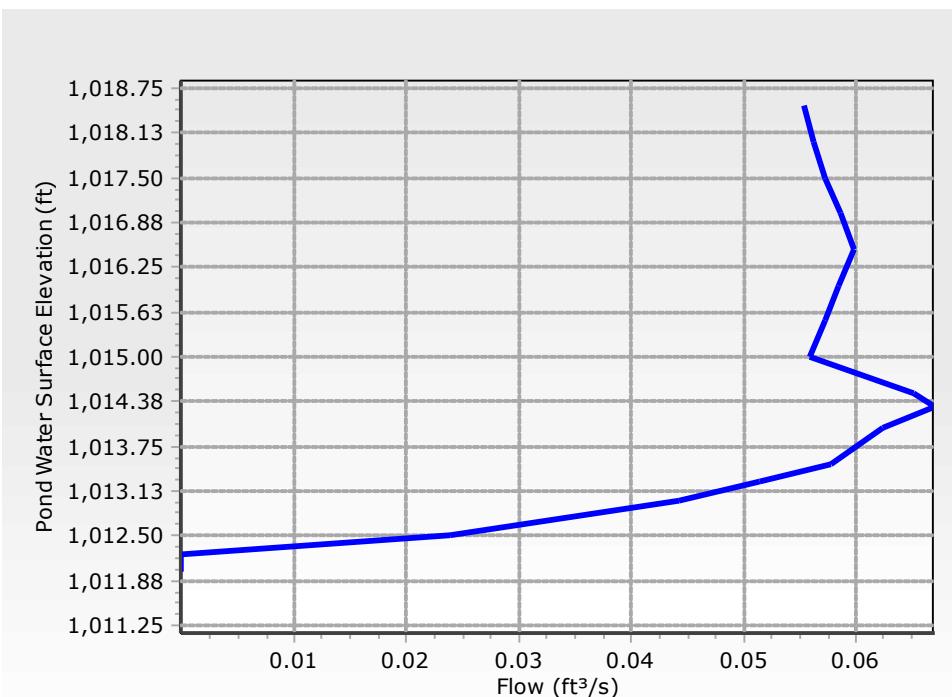
Outlet Structure Type

Orifice

Outlet Structure (IDs and Direction)

Composite Outlet Structure Detailed Report: Primary Outlet Structure

Outlet Structure (IDs and Direction)			
Outlet ID Flow Direction	Orifice - 2 Forward Flow Only	Downstream ID Notes	Culvert - 1
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Circular Orifice	Orifice Coefficient	0.600
Number of Openings	2	Orifice Diameter	1.0 in
Outlet Structure (Common)			
Elevation	1,012.25 ft		



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

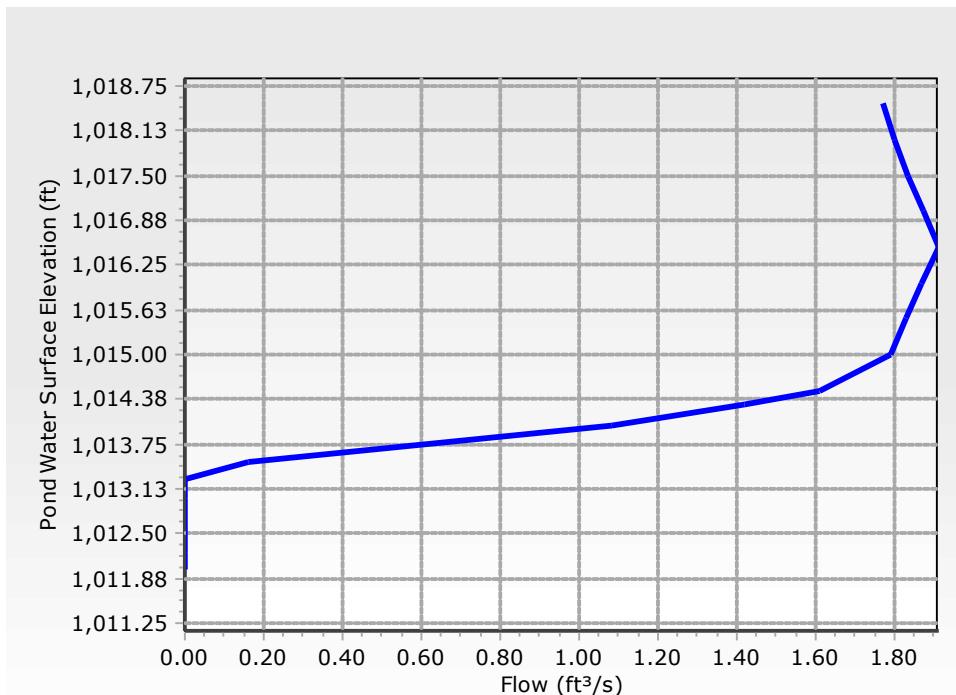
Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message			
H = .21			
H = .71			
H = .96			
H = 1.21			
H = 1.41			
H = 1.63			
H = 1.54			
H = 1.14			
H = 1.19			
H = 1.24			
H = 1.30			
H = 1.24			
H = 1.19			
H = 1.15			
H = 1.11			
Outlet Structure			
Outlet Structure Type	Orifice		
Outlet Structure (IDs and Direction)			
Outlet ID	Orifice - 3	Downstream ID	Culvert - 1
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Circular Orifice	Orifice Coefficient	0.600
Number of Openings	1	Orifice Diameter	8.0 in
Outlet Structure (Common)			
Elevation	1,013.25 ft		

Composite Outlet Structure Detailed Report: Primary Outlet Structure



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 3 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,012.00	0.00	0.00	0.00	0.00
1,012.25	0.00	0.00	0.00	1,012.07
1,012.50	0.00	0.00	0.00	1,012.12
1,013.00	0.00	0.00	0.00	1,012.16
1,013.25	0.00	0.00	0.00	1,012.17
1,013.50	0.16	1,013.50	Free Outfall	1,012.27
1,014.00	1.08	1,014.00	Free Outfall	1,012.59
1,014.30	1.42	1,014.30	Free Outfall	1,012.67
1,014.50	1.61	1,014.50	Free Outfall	1,012.96
1,015.00	1.79	1,015.00	1,013.86	1,013.86
1,015.50	1.83	1,015.50	1,014.31	1,014.31
1,016.00	1.87	1,016.00	1,014.76	1,014.76
1,016.50	1.91	1,016.50	1,015.20	1,015.20
1,017.00	1.87	1,017.00	1,015.76	1,015.76
1,017.50	1.83	1,017.50	1,016.31	1,016.31
1,018.00	1.80	1,018.00	1,016.85	1,016.85
1,018.50	1.77	1,018.50	1,017.39	1,017.39

Composite Outlet Structure Detailed Report: Primary Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 3 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.
CRIT.DEPTH CONTROL Vh=.066ft
Dcr=.184ft CRIT.DEPTH Hev=.00ft
H=.42
H=.72
H=.92
H=1.14
H=1.19
H=1.24
H=1.30
H=1.24
H=1.19
H=1.15
H=1.11

Composite Outlet Structure Detailed Report: Primary Outlet Structure

Composite Rating Table

Tailwater Elevation = Free Outfall (Primary Outlet Structure)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,012.00	0.00	(N/A)	0.00
1,012.25	0.02	(N/A)	0.00
1,012.50	0.06	(N/A)	0.00
1,013.00	0.09	(N/A)	0.00
1,013.25	0.11	(N/A)	0.00
1,013.50	0.28	(N/A)	0.00
1,014.00	1.21	(N/A)	0.00
1,014.30	1.55	(N/A)	0.00
1,014.50	3.00	(N/A)	0.00
1,015.00	9.01	(N/A)	0.00
1,015.50	11.25	(N/A)	0.00
1,016.00	13.07	(N/A)	0.00
1,016.50	14.64	(N/A)	0.00
1,017.00	15.96	(N/A)	0.00
1,017.50	17.15	(N/A)	0.00
1,018.00	18.27	(N/A)	0.00
1,018.50	19.31	(N/A)	0.00

Contributing Structures

(no Q: Orifice - 2,Orifice - 3,Riser - 1,Orifice - 1,Culvert - 1)
Orifice - 1,Culvert - 1
(no Q: Orifice - 2,Orifice - 3,Riser - 1)
Orifice - 2,Orifice - 1,Culvert - 1 (no Q: Orifice - 3,Riser - 1)
Orifice - 2,Orifice - 1,Culvert - 1 (no Q: Orifice - 3,Riser - 1)
Orifice - 2,Orifice - 1,Culvert - 1 (no Q: Orifice - 3,Riser - 1)
Orifice - 2,Orifice - 1,Culvert - 1 (no Q: Orifice - 3,Riser - 1)
Orifice - 2,Orifice - 3,Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 2,Orifice - 3,Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 2,Orifice - 3,Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 2,Orifice - 3,Riser - 1,Orifice - 1,Culvert - 1
Orifice - 2,Orifice - 3,Riser - 1,Orifice - 1,Culvert - 1

Composite Outlet Structure Detailed Report: Primary Outlet Structure

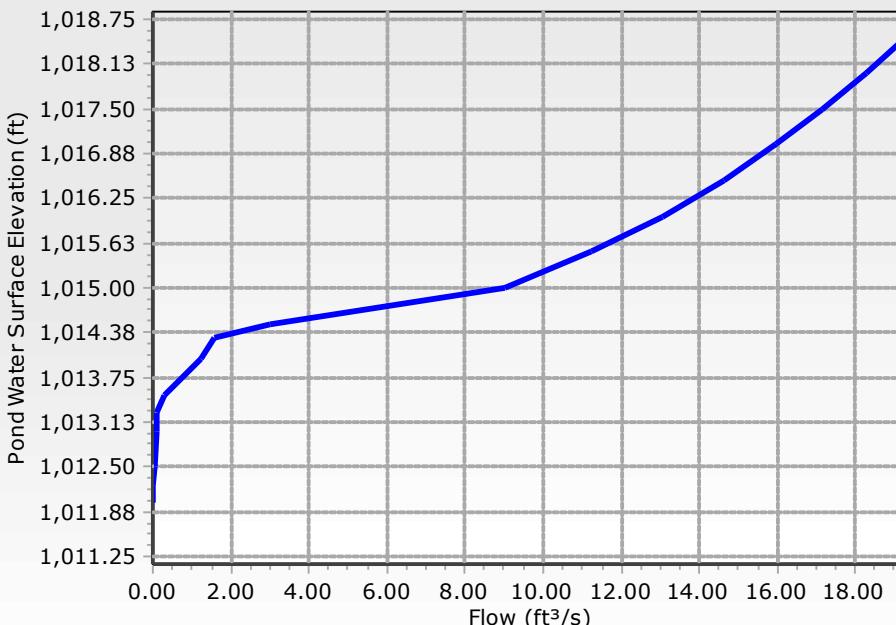
Composite Rating Table

Tailwater Elevation = Free Outfall (Primary Outlet Structure)

Contributing Structures

Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1
Orifice - 2,Orifice -
3,Riser - 1,Orifice -
1,Culvert - 1

Rating Curve



Composite Outlet Structure Detailed Report: Emergency Spillway

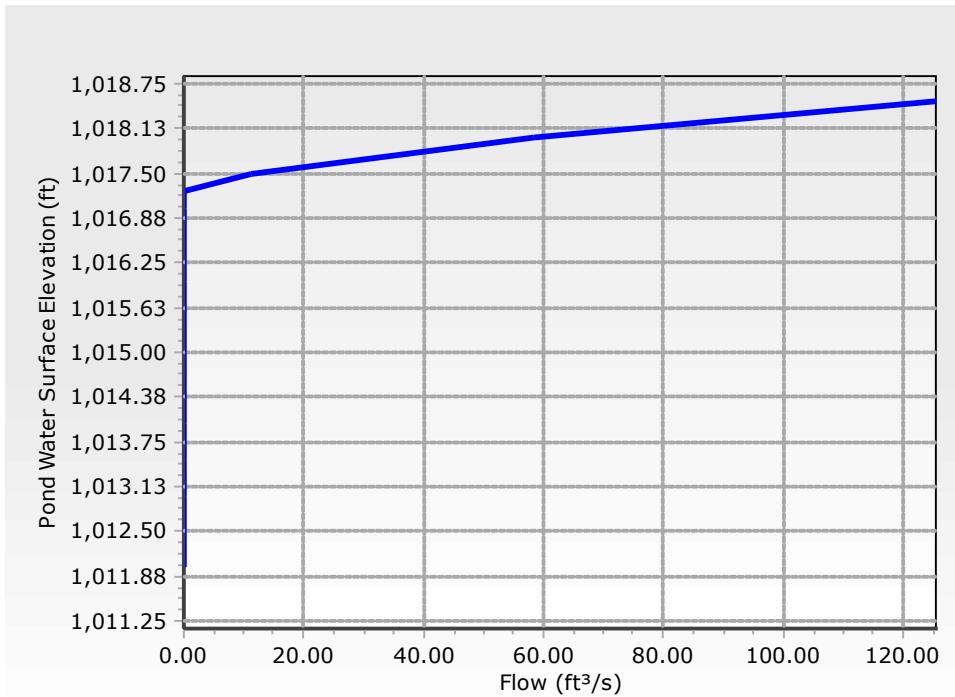
Element Details			
Label	Emergency Spillway	Notes	
Headwater Range			
Headwater Type	Use Pond for Headwater Range	Maximum (Headwater)	1,018.50 ft
Pond	Detention Pond	Increment (Headwater)	0.50 ft
Minimum (Headwater)	1,012.00 ft		
SpotElevation (ft)			
Tailwater Setup			
Tailwater Type	Free Outfall		
Tailwater Tolerances			
Maximum Iterations	30	Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft	Flow Tolerance (Minimum)	0.001 ft ³ /s
Headwater Tolerance (Maximum)	0.50 ft	Flow Tolerance (Maximum)	10.000 ft ³ /s
Tailwater Tolerance (Minimum)	0.01 ft		
Outlet Structure			
Outlet Structure Type	Weir		
Outlet Structure (IDs and Direction)			
Outlet ID	Weir	Downstream ID	Tailwater
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Weir)			
Weir	Rectangular Weir	Rectangular Weir	Suppressed
Vary Coefficient with Depth	False	Weir Length	30.00 ft
Weir Coefficient	3.00 (ft ^{0.5})/s		
Outlet Structure (Common)			
Elevation	1,017.25 ft		

Composite Outlet Structure Detailed Report: Emergency Spillway

Outlet Structure (Weir, Advanced)

User Defined Table

False



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft³/s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,012.00	0.00	(N/A)	0.00
1,012.50	0.00	(N/A)	0.00
1,013.00	0.00	(N/A)	0.00
1,013.50	0.00	(N/A)	0.00
1,014.00	0.00	(N/A)	0.00
1,014.50	0.00	(N/A)	0.00
1,015.00	0.00	(N/A)	0.00
1,015.50	0.00	(N/A)	0.00
1,016.00	0.00	(N/A)	0.00
1,016.50	0.00	(N/A)	0.00
1,017.00	0.00	(N/A)	0.00
1,017.25	0.00	(N/A)	0.00
1,017.50	11.25	(N/A)	0.00
1,018.00	58.46	(N/A)	0.00

Composite Outlet Structure Detailed Report: Emergency Spillway

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft³/s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,018.50	125.78	(N/A)	0.00

Computation Messages

```
HW & TW below
Inv.El.=1017.250
H=.00; Htw=.00;
Qfree=.00;
H=.25; Htw=.00;
Qfree=11.25;
H=.75; Htw=.00;
Qfree=58.46;
H=1.25; Htw=.00;
Qfree=125.78;
```

Composite Outlet Structure Detailed Report: Emergency Spillway

Composite Rating Table

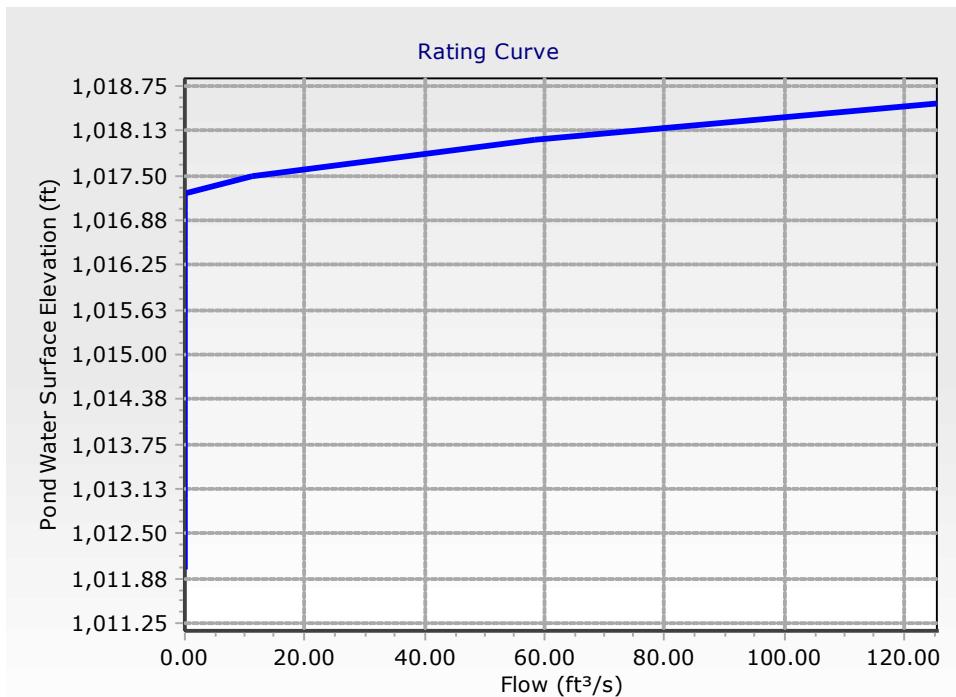
Tailwater Elevation = Free Outfall (Emergency Spillway)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,012.00	0.00	(N/A)	0.00
1,012.50	0.00	(N/A)	0.00
1,013.00	0.00	(N/A)	0.00
1,013.50	0.00	(N/A)	0.00
1,014.00	0.00	(N/A)	0.00
1,014.50	0.00	(N/A)	0.00
1,015.00	0.00	(N/A)	0.00
1,015.50	0.00	(N/A)	0.00
1,016.00	0.00	(N/A)	0.00
1,016.50	0.00	(N/A)	0.00
1,017.00	0.00	(N/A)	0.00
1,017.25	0.00	(N/A)	0.00
1,017.50	11.25	(N/A)	0.00
1,018.00	58.46	(N/A)	0.00
1,018.50	125.78	(N/A)	0.00

Contributing Structures

None Contributing
Weir - 1

Composite Outlet Structure Detailed Report: Emergency Spillway

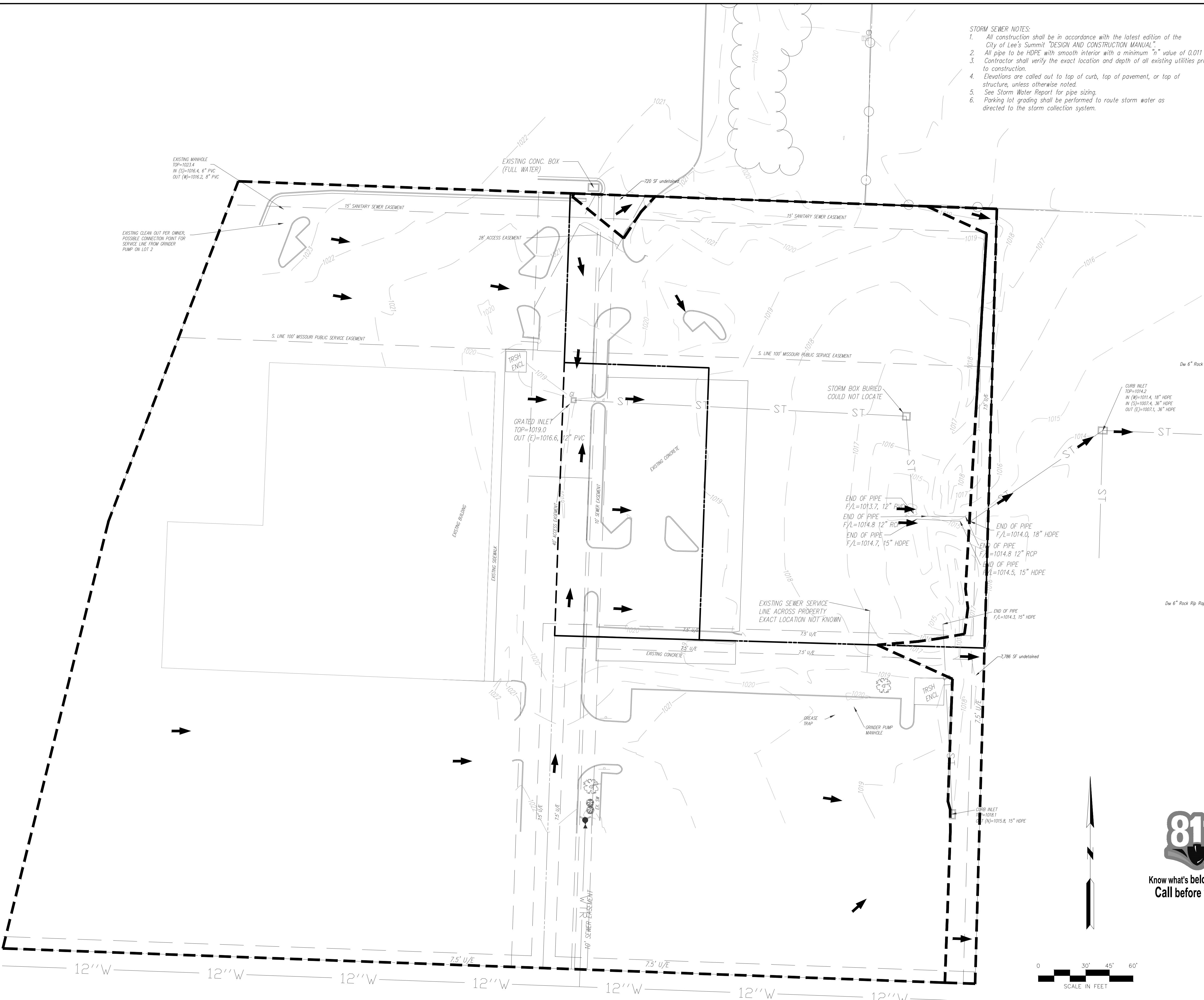


Consult Inc engineers planners

CORPORATE LICENSE No. E201005973

PRELIMINARY DEVELOPMENT DRAINAGE AREA MAP

DOUGLAS CORNERS BUILDING
LEE'S SUMMIT - JACKSON COUNTY - MISSOURI



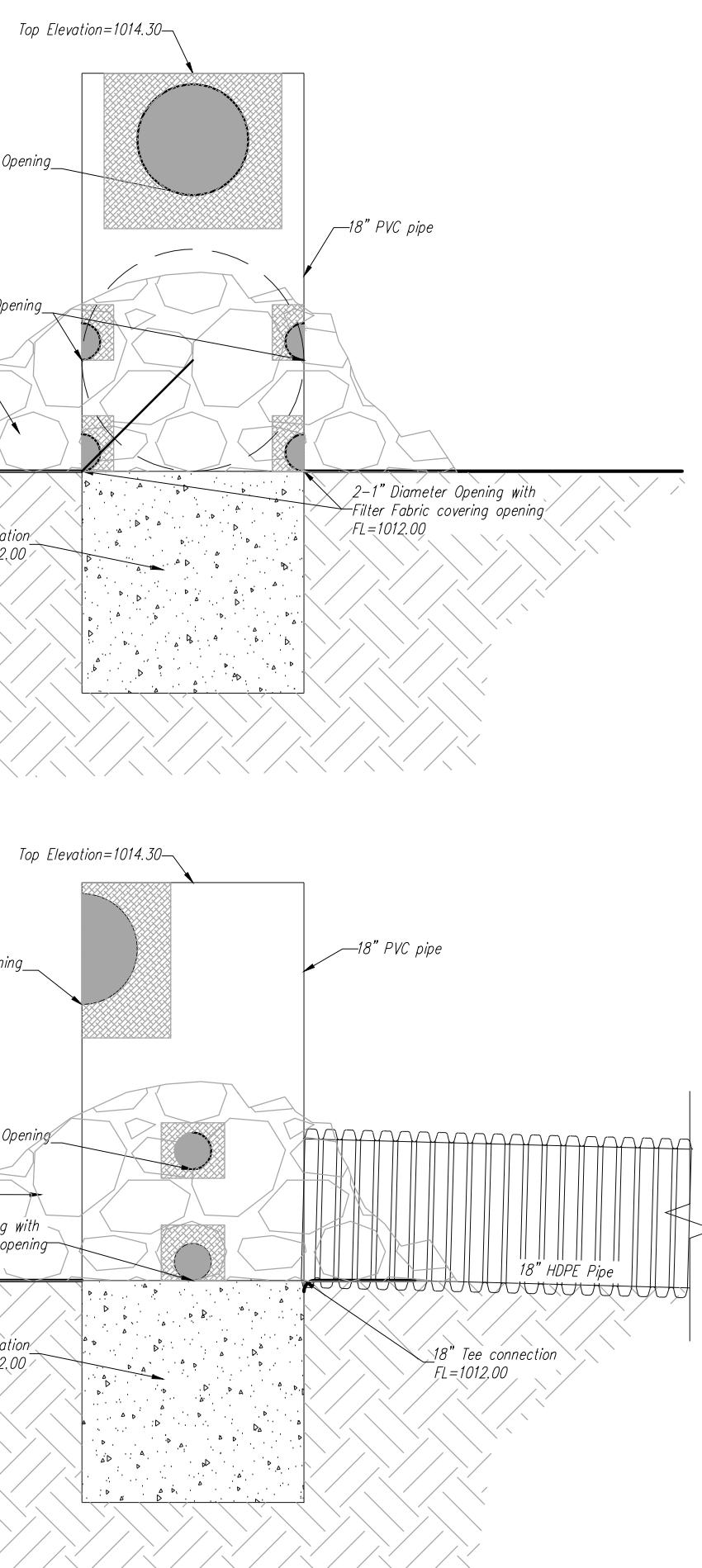
Detention Pond Details:

No.	By	CK/APP
1012	52	0
1013	14,200	7,127
1014	15,477	21,965
1015	16,796	38,102
1016	18,158	55,580
1016.74	19,193	69,731 (100 year storage)
1017	19,577	74,448

Detention release was sized by Bentley PondPACK V8i and is sized to release the 100-year storm event over the proposed rip rap lined channel.

The APWA 5600 allowable minimum releases for 6.3 acres are:

2 year - 3.15 cfs
10 year - 12.60 cfs
100 year - 18.90 cfs



Detention Release Structure
NTS

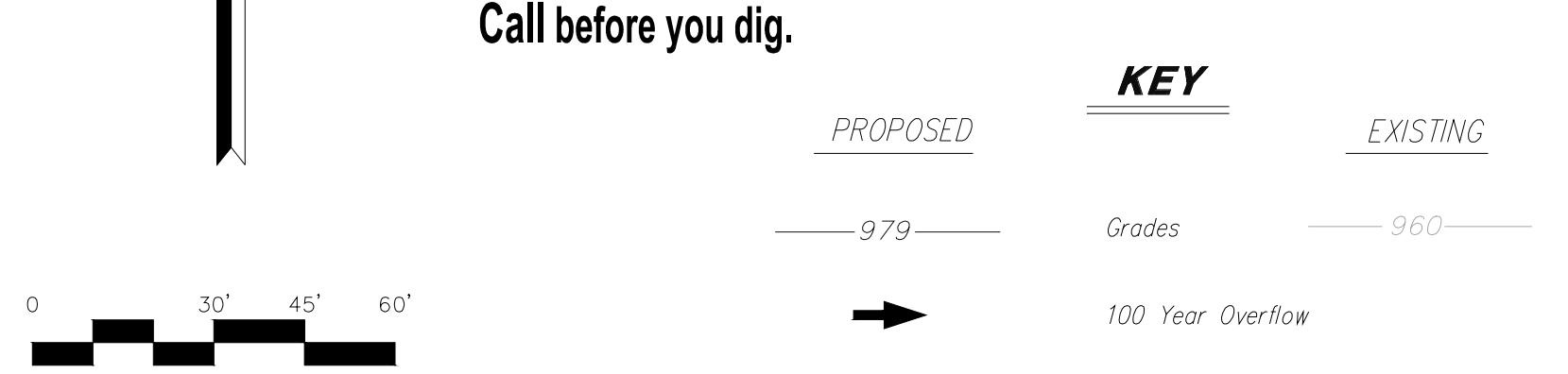
Contractor to verify all invert elevations for existing sewer connections. Contact civil engineer if conflict arises.

PROJECT BENCHMARK:

#1 Iron bar at north west corner of property.
N 1006947.3760
E 2823375.6230
TOP ELEV. 1021.42



Know what's below.
Call before you dig.



Contractor to verify all invert elevations for existing sewer connections. Contact civil engineer if conflict arises.

X-REF NO.	18109B
DRAWING NO.	18007
DATE	JUNE 12, 2018
JOB NO.	18007
SHEET OF	13

