

132 Abbie Ave. Kansas City, KS 66103 P: 913.317.9500 ric-consult.com

April 13, 2018

Mike Weisenborn Project Manager, Development Center City of Lee's Summit 220 SE Green Street Lee's Summit, MO 64063

Re: 18-0129 Northpoint Summit Square II Apartments Water Demand Statement

Mr. Weisenborn:

Per the requirements provided by the City of Lee's Summit's planning code regarding the final development plan submittal for the proposed Summit Square II Apartments, a water use demand analysis has been conducted. The following is a report of the analysis.

PROJECT DESCRIPTION

An approximately 12.8-acre multi-family complex is currently being proposed at the southeast corner of NW Ward Road and NE Tudor Road in Lee's Summit, MO. A site location map has been provided as Exhibit A. The complex generally consists of five primary 4/5-story buildings, a courtyard, and associated parking facilities. The proposed complex will consist of 35 studios, 165 1-bedroom units, and 123 2-bedroom units, for a total unit count of 323. Refer to Exhibit B for a layout of the proposed complex.

METHODOLOGY

Based on the provisions outlined in the Lee's Summit Design and Construction Manual (LS DCM) 6900 for Water Mains, the water demand has been estimated. Required fire flow capacity has been determined using the provisions outlined in the LS DCM 6900, the American Water Works Association (AWWA), and the International Fire Code (IFC) published in 2012.

According to the LS DCM, the water distribution system shall adequately supply "the peak hour demand and maximum day demand (estimated at 0.67 gpm/customer) ... while maintaining a pressure of not less than 40 psi at all points of delivery". In addition, the system must meet the fire flow requirements set forth in the currently adopted IFC for residential buildings greater than 3600 square feet.

DETERMINATION OF PEAK HOUR DEMAND

The peak hour demand has been estimated using the criteria outlined in 6901.C of the LS DCM. Given the proposed unit count of 323, the maximum daily water demand (M) for the proposed use is 224,485 gpd, yielding a peak hour demand (P) of 448,970 gpd (or <u>311.78 gpm</u>). The calculations for the determination of peak hour demand have been provided as Exhibit C.

DETERMINATION OF FIRE FLOW REQUIREMENTS

From Exhibit B of the IFC, fire flow requirements for residential buildings greater than 3600 square feet are based on building types outlined in the International Building Code. The proposed buildings will be sprinklered and have been designated as Type V-A buildings. The total floor area considered in the estimation of fire flow requirements is 395,000 square feet. Based on table B105.1 in the IFC, the required fire flow in gallons per minute for 395,000 square feet of fire flow area is 8,000 gpm. According to the IFC, a reduction of 50% is allowed for approved buildings equipped with automatic sprinkler systems. Therefore, the required fire flow for the development has been estimated at 50% of 8,000 gpm or <u>4,000 gpm</u>.



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WATER DEMAND ANALYSIS

The water demand for the proposed development is the sum of the peak hour demand and the minimum fire flow requirement determined in the previous sections for a total flow requirement of <u>4311.78 gpm</u>.

Three fire hydrants immediately surrounding the development have recently been tested. A map of the fire hydrants giving their numeric designations has been provided by the City of Lee's Summit and is enclosed in this report as part of Exhibit D. The fire hydrants tested were 023-141 located South of NE Tudor Road, and 023-141 and 023-145 located north of Donovan Road. Based on the results from the fire flow tests, the hydrant located on NE Tudor Road (hydrant 023-141) is projected to have an available hydrant flow of 8967 gpm. The hydrants located on Donovan Road are projected to have an available hydrant flow of 5614 gpm each. The total projected available fire flow provided by the existing hydrants surrounding the site has been taken as the sum of the projected available fire flow provided by each hydrant for a total of approximately <u>20,195 gpm</u>. Please refer to Exhibit D for details regarding the information obtained during the fire hydrant flow tests and the expected performance of these fire hydrants based on the test results.

SUMMARY

Due to the results from the fire hydrant flow tests and the proximity of the City's water tanks and pumping facility, it is our opinion that the existing water mains will provide adequate capacity for the proposed use.

If you have any questions or need additional clarification, please do not hesitate to contact us.

Sincerely,

Mick E. Slutter, P.E. mslutter@ric-consult.com Kelsey L. Fitzpatrick, E.I. <u>kfitzpatrick@ric-consult.com</u>

RENAISSANCE INFRASTRUCTURE CONSULTING

April 2018

Exhibit A Site Location Map



	Sheet Exhibit A	
	Water Demand Statement	18-0129 Northpoint Summit Fair II Apartments
		Site Location Map
		ORIGINAL SUBMITTAL REVISION
	Renaissance	AVENUE TY, KANSAS 66103 WWW.RIC-CONSULT.COM MO MO MO MO MO MO MO MO MO MO MO MO M
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Exhibit B Proposed General Layout



Exhibit C

Estimated Water Demand Calculations

N (Residential Population) = Number of Dwelling Units * 2.78 ^{people}/dwelling unit N = 323 * 2.78 = 897.94 people

 $\begin{array}{l} R \ (Avg. Daily \ Water \ Demand \ of \ Residential \ Population) = N * 125 \ gallons/person \\ R = 897.94 * 125 = 112,242.50 \ gpd \end{array}$

A (Average Daily Water Demand) = R + C + SA = 112242.50 + 0 + 0 = 112,242.50 gpd

M (Maximum Daily Water Demand) = A * Y(Maximum Day to Average Day Ratio) M = 112242.50 * 2.1 = 224,485 gpd

> P(Peak Hour Demand) = 2 * M P = 2 * 224,485 = 448,970 gpd $P (gpm) = \frac{448970}{1440} = 311.78 gpm$

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Exhibit D Existing Fire Hydrant Flow Test

Infrastructure Map



EXISTING FIRE HYDRANT FLOW TEST RESULTS:

Fire Hydrant 023-141

Pressure Static (PSI)	82
Pressure Residual (PSI)	80
Pressure Pitot (PSI)	70
Coefficient	0.9
GPM	1404
Test Time (min.)	5
Nozzle Size	2.5

Fire Hydrants 023-142 & 023-145

82
78
58
0.9
1278
5
2.5

Fire Hydrant Flow Calculator - Hydrant 023-141

Static:	82	psi before flowing
Residual:	80	psi while flowing
Pitot:	70	pitot gage reading
Diameter:	2.5	size of opening tested
This hydrant is flowing:	1404	GPM from the test outlet
Projected available hydrant flow:	8967	GPM Note 1
2nd Static:	0	secondary psi before flowing
2nd Residual:	0	secondary psi while flowing
The main can be expected to flow about:	NaN	GPM

Notes:

- 1. Projected available flows calculated at 20 psi residual, or ½ the static pressure for low pressure hydrants having static pressures of less than 40 psi.
- 2. This calculator is based on established Hazen-Williams formulas and is provided for convenience and estimation purposes only. The author and FireHydrant.org express no warranty for its suitability for any particular purpose.
- 3. Fire flows have been calculated using FireHydrant.org flow calculator.

Fire Hydrant Flow Calculator - Hydrants 023-142 and 023-145

Static:	82	psi before flowing
Residual:	78	psi while flowing
Pitot:	58	pitot gage reading
Diameter:	2.5	size of opening tested
This hydrant is flowing:	1278	GPM from the test outlet
Projected available hydrant flow:	5614	GPM Note 1
2nd Static:	0	secondary psi before flowing
2nd Residual:	0	secondary psi while flowing
The main can be expected to flow about:	NaN	GPM

Notes:

- 1. Projected available flows calculated at 20 psi residual, or ½ the static pressure for low pressure hydrants having static pressures of less than 40 psi.
- 2. This calculator is based on established Hazen-Williams formulas and is provided for convenience and estimation purposes only. The author and FireHydrant.org express no warranty for its suitability for any particular purpose.
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