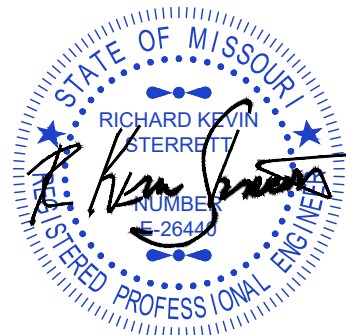


Final Stormwater Management Study

Colton's Crossing 1st Plat
Prepared for Hamblen Road Project, LLC
229 SE Douglas Street
Lee's Summit, MO 64063

HG Consult Project No. 25.018

Prepared by Richard Michael
June 11, 2025



June 11, 2025

I. Table of Contents

| | | |
|------|---------------------------------------------------------------------------------------|----|
| II. | General Information | 3 |
| A. | Description of Existing Site, Location, and Proposed Use | 3 |
| B. | General Overview of Drainage Patterns | 4 |
| C. | FEMA Classification / Floodplain Issues | 5 |
| D. | Wetland and USACE Issues | 6 |
| E. | Soil Classification | 7 |
| III. | Methodology | 7 |
| A. | Unit Hydrograph Modeling Methods | 7 |
| B. | Computation Methods for Runoff Determinations | 7 |
| C. | Design Storm Events Used and Source of Rainfall Data | 7 |
| IV. | Existing Conditions Analysis | 8 |
| A. | Summary of Comprehensive Control Requirements | 8 |
| B. | Existing Drainage Area Map | 8 |
| C. | Description of Each Drainage Area | 8 |
| D. | Table Summarizing Input Data | 8 |
| E. | Table Summarizing Peak Runoff Rates | 9 |
| V. | Proposed Conditions Analysis | 9 |
| A. | Proposed Drainage Area Map | 9 |
| B. | Narrative Description of All Proposed Drainage Areas | 9 |
| C. | Table Summarizing Input Data | 9 |
| D. | Table Summarizing Peak Runoff Rates | 9 |
| E. | Table Summarizing Pre-Developed, APWA Allowable, and Proposed Peak Runoff Rates | 10 |
| F. | Tables Summarizing Detention/Retention Input Data and Results | 11 |
| G. | Undetained Drainage Areas | 11 |
| H. | Water Quality Requirements | 11 |
| I. | Water Quality Summary | 12 |
| VI. | Conclusions and Recommendations | 12 |
| A. | Overview of the Report | 12 |
| B. | List of Requested Waivers | 13 |
| VII. | Appendix - Figures / Maps / Exhibits / Supporting Calculations | 13 |

II. General Information

A. Description of Existing Site, Location, and Proposed Use

Colton's Crossing 1st Plat will consist of the development of a parcel approximately 14.68 acres. The subject property is currently zoned RP-3 (Planned Residential Mixed Use) and is located along SE Hamblen Road directly Northeast of Shamrock Hills Golf Club. The site is currently vacant and being used as farmland. The proposed land use of this phase will be single family residences. The site will also include a detention basin, road & sidewalks, and the necessary utilities to serve the development.

Figure II.A.1 – Aerial Photo of the project site



Figure II.A.2 – Aerial Photo of the project site

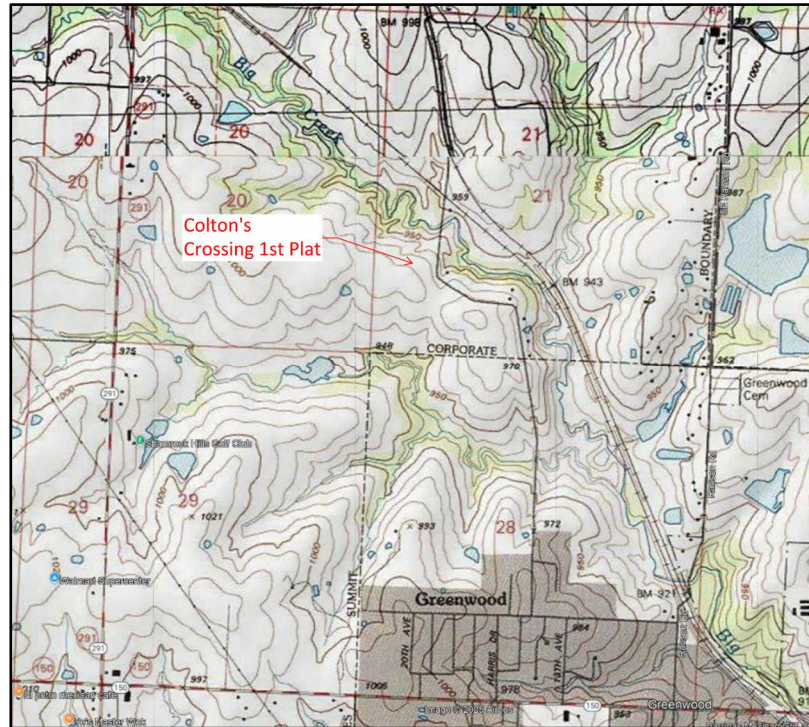


B. General Overview of Drainage Patterns

The project site is divided into 2 different drainage areas as shown on the Pre-Developed Drainage Area Map.

The reason for delineating the areas separately is to clearly distinguish between on-site and off-site. The subject property discharges north/northeast to Big Creek, immediately north of the property.

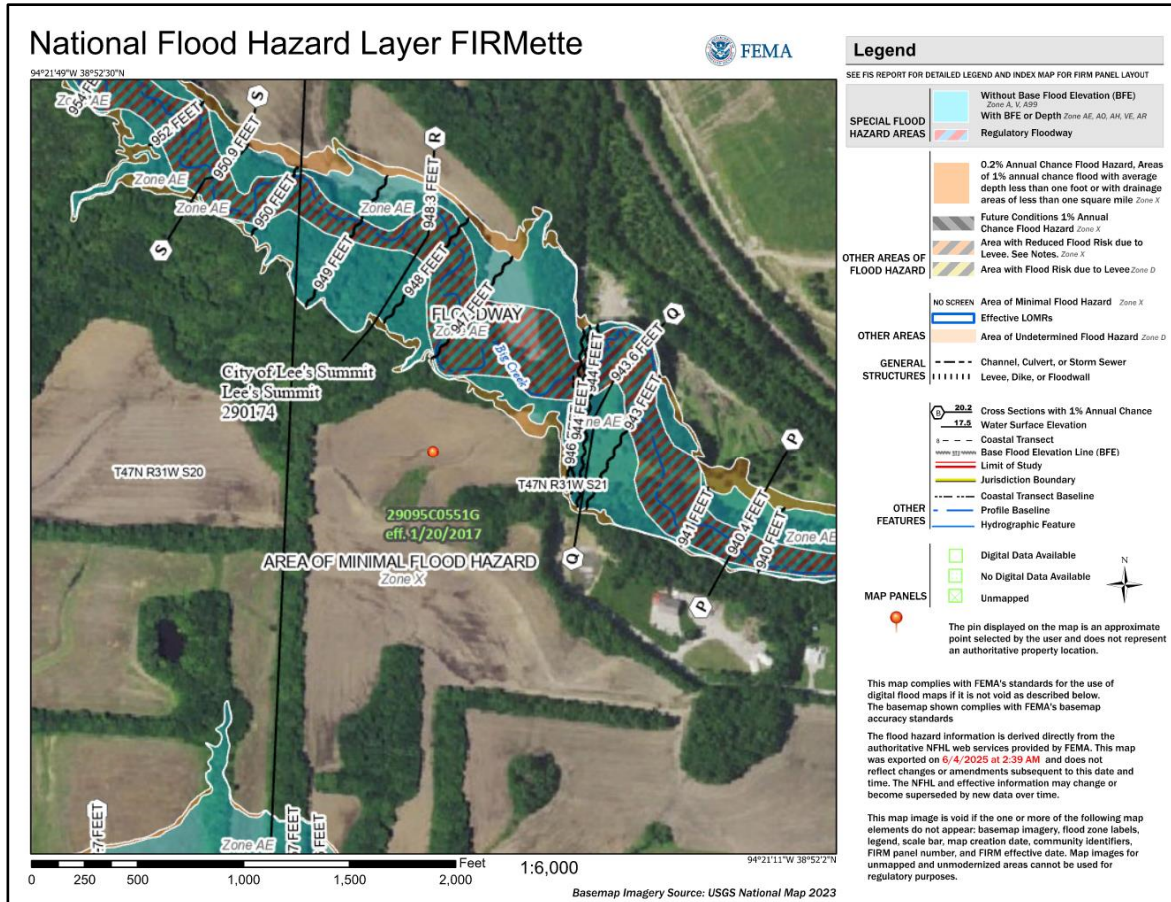
Figure II.B.1 – USGS Quad Map



C. FEMA Classification / Floodplain Issues

The project site is located primarily within Zone X (area of minimal flood hazard), with a small portion being located within Zone AE as represented in the NE. There are no floodplain boundaries being altered and therefore a Flood Study is not required. See Figure II.C.1 for Firm Panel. Included as Figure J of this report is a Stream Buffer Evaluation.

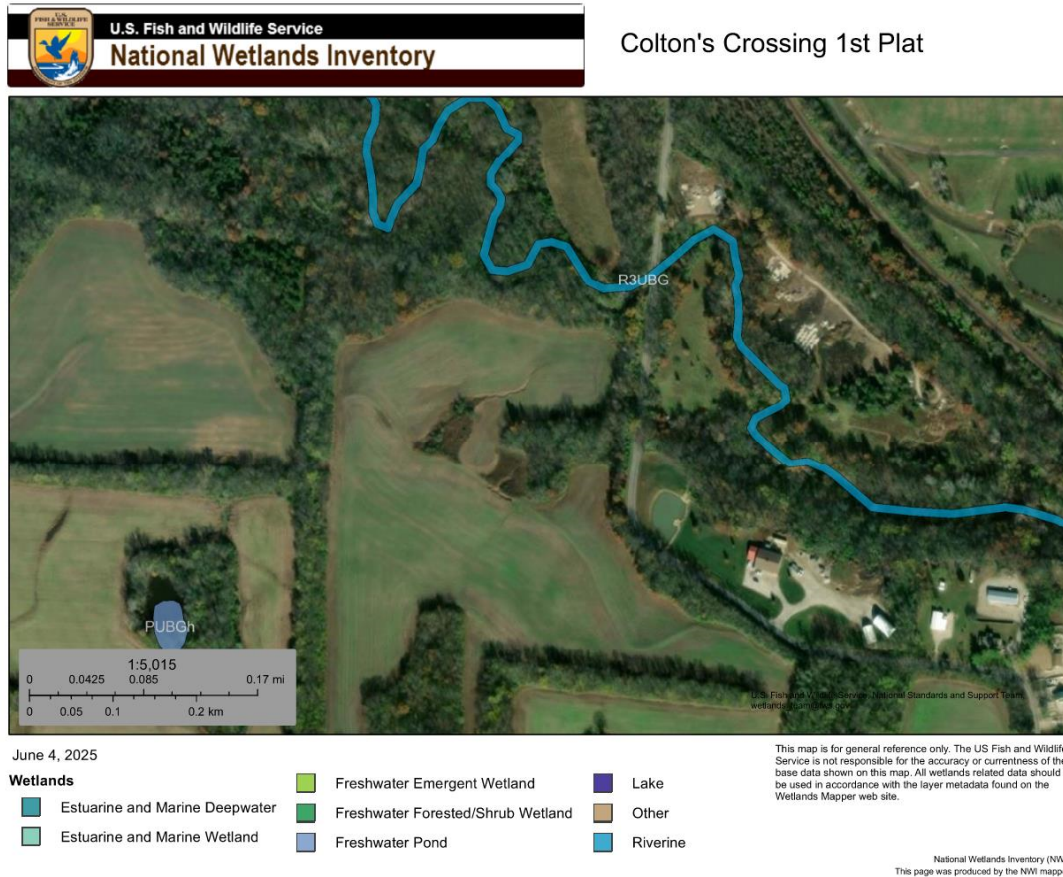
Figure II.C.1 – FEMA FIRM Panel #29095C0551G Eff. 1/20/2017



D. Wetland and USACE Issues

There are no wetlands or Waters of the US being disturbed by this project and therefore no permits are required from the Corps of Engineers for the development of this site. See figure II.D.1 for US Fish and Wildlife Wetland Inventory Map.

Figure II.D.1 – US Fish and Wildlife National Wetland Inventory



E. Soil Classification

NRCS Web Soil Survey categorizes the soils for this project below. See the appendix for additional information.

Table II.E.1 – Soil Classification

| Symbol | Name | Slopes | HSG |
|--------|-------------------------|--------|-----|
| 10000 | Arisburg silt loam | 1-5% | C |
| 10113 | Oska silty clay loam | 5-9% | D |
| 10116 | Sampsel silty clay loam | 2-5% | C/D |
| 10117 | Sampsel silty clay loam | 5-9% | C/D |
| 13629 | Colo silt loam | 1-4% | C/D |

For this analysis, Soil group C was considered for the project. Curve Numbers were used in accordance with APWA Section 5602.3.

III. Methodology

A. Unit Hydrograph Modeling Methods

The method for evaluating this project was with the use of PondPack Connect Edition. Both Pre-Development and Post-Development conditions were considered. The unit hydrograph method used was SCS TR-55.

B. Computation Methods for Runoff Determinations

The computation methods used for runoff determinations are as follows:

- AMC II Soil Moisture conditions
- 24-Hour SCS Type II Rainfall Distribution
- SCS Runoff Curve Numbers per TR-55
- Time of Concentration developed per TR-55

C. Design Storm Events Used and Source of Rainfall Data

The design storms that were considered include the 2, 10, 100, and subsequent 100-Year storms. The rainfall data was gathered from NRCS utilizing curves for a Type II 24-hour rainfall.

Table III.C.1 – Methodology and Rainfall Data

| Methods and Rainfall Data | |
|---------------------------------|---------------------------|
| Pond Routing | Pondpack using SCS Method |
| Existing CN | 74, Group C soils |
| T _c | 5 minutes |
| Water Quality, Type II, 24-hr | 1.4 inch |
| 2-yr rainfall, Type II, 24-hr | 3.5 inch |
| 10-yr rainfall, Type II, 24-hr | 5.3 inch |
| 100-yr rainfall, Type II, 24-hr | 7.7 inch |

IV. Existing Conditions Analysis

A. Summary of Comprehensive Control Requirements

As mentioned previously the soils on-site consist of primarily those with a hydrologic group of C. The site is undeveloped. The APWA default strategy was used to provide comprehensive protection. The APWA default strategy reads as follows:

“Under this strategy, peak runoff control is provided for the 1%, 10% and 50% chance storms and volumetric and/or extended detention control of the 90% mean annual event storm for broad protection of the receiving system, including channel erosion protection and flood peak reductions over a range of return periods. This strategy shall be the default strategy unless otherwise designated or approved by the local authority. Performance standards and sizing criteria are provided in Section 5608.”

B. Existing Drainage Area Map

See the appendix (Pre-Developed Drainage Area Map) for all drainage areas and outfall locations. See Table IV.B.1 for a summary of the drainage areas.

Table IV.B.1 – Pre-Developed Drainage Areas

| Drainage Area | Total Area (acres) |
|---------------|--------------------|
| E-1 | 14.68 |
| E-1 OFF | 3.76 |

C. Description of Each Drainage Area

E-1: This area represents the on-site area that discharges north into Big Creek (located off site). An SCS curve number of 74 has been applied to this area.

E-1 OFF: This area represents the off-site area that discharges to E-1. An SCS curve number of 74 has been applied to this area.

D. Table Summarizing Input Data

Table IV.D.1 – Pre-Developed Input Area Data

| Sub-Area Name | Area | CN | TOC (minutes) |
|---------------|-------|----|---------------|
| E-1 | 14.68 | 74 | 5.00 |
| E-1 OFF | 3.76 | 74 | 5.00 |

E. Table Summarizing Peak Runoff Rates

Table IV.E.1 – Pre-Developed Peak Runoff Rate

| Sub-Area Name | 2-Year (cfs) | 10-Year (cfs) | 100-Year (cfs) |
|---------------|--------------|---------------|----------------|
| E-1 | 27.95 | 60.13 | 107.22 |
| E-1 OFF | 7.16 | 15.40 | 27.46 |
| POI E-1 | 35.11 | 75.53 | 134.68 |

V. Proposed Conditions Analysis

A. Proposed Drainage Area Map

See the appendix (Post-Developed Drainage Area Map) for all drainage areas and outfall locations. See Table V.A.1 for a summary of the drainage areas.

Table V.A.1 – Post-Developed Drainage Areas

| Drainage Area | Total Area (acres) |
|---------------|--------------------|
| P-1 A | 11.67 |
| P-1 B | 3.01 |

B. Narrative Description of All Proposed Drainage Areas

P-1 A: This area represents the on-site area that discharges into the proposed basin. An SCS composite curve number of 83 has been applied to this area.

P-1 B: This area represents the on-site area that does not discharge into the proposed basin due to existing topography and vertical constraints. An SCS curve number of 76 has been applied to this area.

C. Table Summarizing Input Data

Table V.C.1 – Post-Developed Input Area Data

| Sub-Area Name | Area | CN | TOC (minutes) |
|---------------|-------|----|---------------|
| P-1 A | 11.67 | 83 | 5.00 |
| P-1 B | 3.01 | 76 | 5.00 |

D. Table Summarizing Peak Runoff Rates

Table V.D.1 – Post-Developed Peak Runoff Rate

| Sub-Area Name | 2-Year (cfs) | 10-Year (cfs) | 100-Year (cfs) |
|---------------|--------------|---------------|----------------|
| P-1 A | 34.14 | 62.68 | 101.36 |
| P-1 B | 6.38 | 13.19 | 22.97 |
| POI P-1 | 6.87 | 20.73 | 41.91 |

E. Table Summarizing Pre-Developed, APWA Allowable, and Proposed Peak Runoff Rates

Table V.E.3 – Post-Developed Allowable Peak Runoff Rate based on 2011 APWA 5608.4 C

| Post-Developed | | | | Pre-Developed | | | Pre-Developed Rates | | | APWA Allowable Rates | | | | | | Proposed Rates | | |
|----------------|-----------|--------------------|-------|---------------|-----------|-------|---------------------|-------------|--------------|----------------------|------------|-----------------------|-------------|------------------------|--------------|----------------|-------------|--------------|
| POI | Area Name | Status | Area | POI | Area Name | Area | 2-Yr (cfs) | 10-Yr (cfs) | 100-Yr (cfs) | 2-Yr Rate (cfs/acre) | 2-Yr (cfs) | 10-Yr Rate (cfs/acre) | 10-Yr (cfs) | 100-Yr Rate (cfs/acre) | 100-Yr (cfs) | 2-Yr (cfs) | 10-Yr (cfs) | 100-Yr (cfs) |
| POI P-1 | P-1 A | On Site-Detained | 11.67 | POI E-1 | E-1 | 14.68 | 27.95 | 60.13 | 107.22 | 0.5 | 7.34 | 2.0 | 29.36 | 3.0 | 44.04 | 34.14 | 62.68 | 101.36 |
| POI P-1 | P-1 B | On Site-Undetained | 3.01 | | | | | | | | | | | | | 6.38 | 13.19 | 22.97 |
| n/a | n/a | n/a | n/a | POI E-1 | E-1 OFF | 3.76 | 7.16 | 15.40 | 27.46 | n/a | n/a | n/a | n/a | n/a | n/a | n/a | n/a | n/a |
| POI P-1 | | | | POI E-1 | | | 35.11 | 75.53 | 134.68 | 7.34 | | 29.36 | | 44.04 | | 6.87 | 20.73 | 41.91 |

Comprehensive values utilizing 0.5 cfs (2-YR), 2 cfs (10-YR), and 3 cfs (100-YR) per site-acre applied to pre-developed on-site drainage areas only. The release rates in RED are the rates that were used as the maximums for each POI.

F. Tables Summarizing Detention/Retention Input Data and Results

Table V.F.1 –Detention Basin Input Data

| | ELEV |
|-------------------------------|--------|
| 24" Culvert (Upstream Invert) | 945.90 |
| 2" Dia. Orifice (WQ) | 946.00 |
| 4" Dia. Orifice (2YR) | 948.10 |
| 0.5'x4' Orifice (10YR) | 949.80 |
| 4'x4' Riser (100YR) | 952.40 |
| 20' Overflow Weir (100YR*) | 953.50 |
| Top of Basin | 956.00 |

**Assumes zero flow through primary outlet with subsequent 1% storm event*

Table V.F.2 – Detention Basin Results

| | 2-Year | 10-Year | 100-Year | 100-Year* |
|------------------|-------------|-------------|-------------|-------------|
| Basin (IN) | 34.14 | 62.68 | 101.36 | 101.36 |
| Basin (OUT) | 1.85 | 11.38 | 30.78 | 85.59 |
| Basin WSE | 949.88 | 950.99 | 952.86 | 954.75 |
| Freeboard | 6.12 | 5.01 | 3.14 | 1.25 |

**Assumes zero flow through primary outlet with subsequent 1% storm event*

G. Undetained Drainage Areas

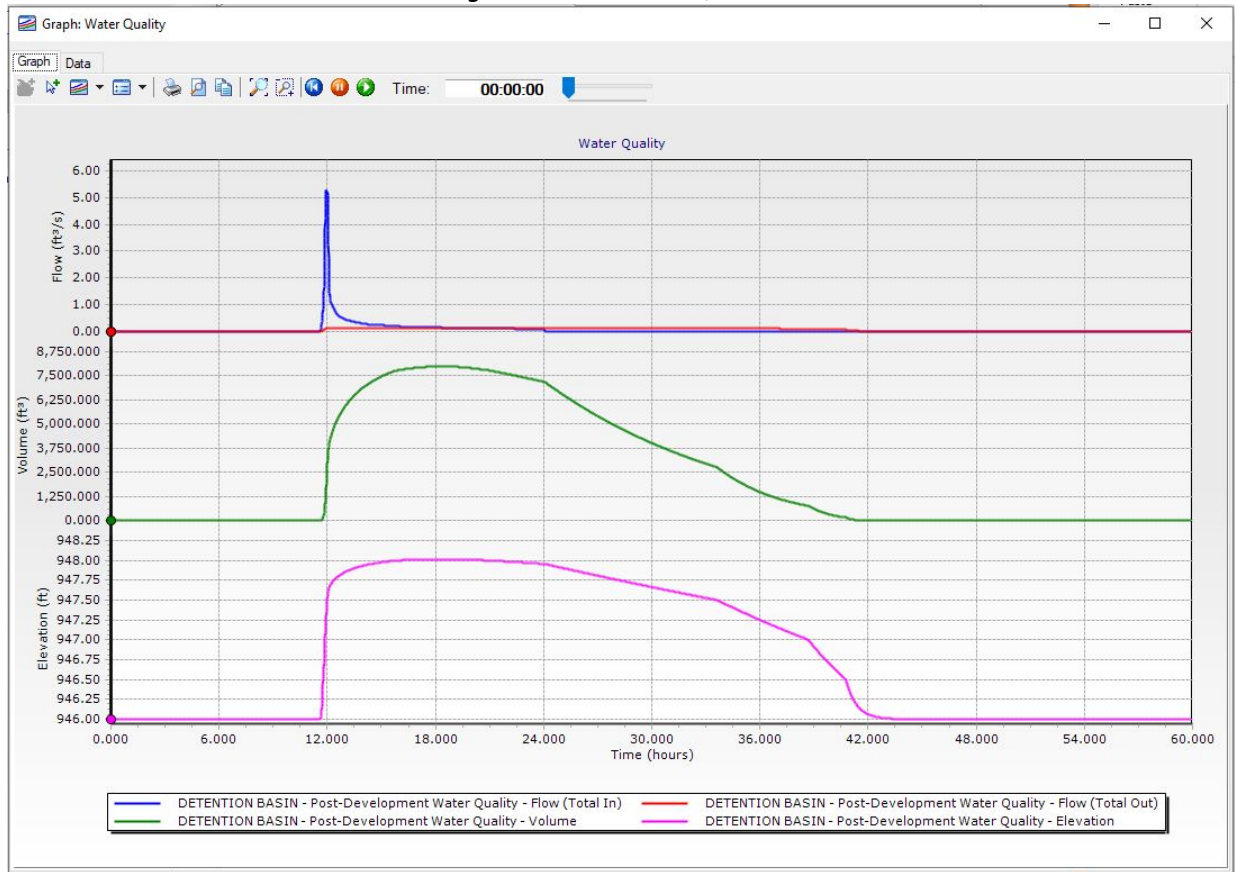
There is one area within this development which is undetained: P-1B. This fringe area is undetained due to elevation and grading constraints.

H. Water Quality Requirements

The proposed development is providing stormwater treatment per APWA 5608.4 and Chapter 6 of the MARC/APWA BMP Manual. As indicated in this study the proposed stormwater treatment is a wet detention basin with a 1.37" storm release over a 40-hour period.

I. Water Quality Summary

Figure V.I.1 – Basin WQ Results



VI. Conclusions and Recommendations

A. Overview of the Report

The proposed development will provide comprehensive control for the developed site via a dry detention basin that discharges to the north, matching the existing topography. The detention basin will treat the 2, 10, 100, and subsequent 100-year events.

The proposed detention releases the WQ event (1.37" of rainfall) over a 40-hour duration. To achieve this, an orifice size of 2" diameter was used. The 2" diameter works well with the proposed pipe guard grate because the openings are less than 1" diameter, meaning that the pipe guard grate will still screen/filter particulates before entering the 2" diameter orifice. When clogged, the pipe guard grate is easily maintained to remove debris. The subsequent 100-year storm event will flow through a 20' long weir acting as the emergency spillway. The elevation of the spillway is greater

than 0.5' above the 100-year WSE (providing 0.64'), meeting APWA criteria. There is greater than 1 foot of freeboard from the subsequent 100-year event WSE to the top of the dam (providing 1.25'), meeting APWA criteria.

Drainage area P-1B is not detained due to elevation and grading constraints.

B. List of Requested Waivers

P-1B – Waiver requested. See section V.G. Undetained Drainage Areas in this report.

VII. Appendix - Figures / Maps / Exhibits / Supporting Calculations

Figure A – Detention Basin Construction Plans

Figure B – Pre-Developed Drainage Area Map

Figure C – Post-Developed Drainage Area Map

Figure D – Detention Basin Volume Results

Figure E – Inflow Hydrographs

Figure F – Stage-Discharge Rating Curves & Input Data Per Basin Outlet

Figure G – Routing Curves for all Design Storms

Figure H – Pondpack Reports (Pre-Developed and Post-Developed)

Figure I – Web Soil Survey

Figure J – Stream Buffer Evaluation

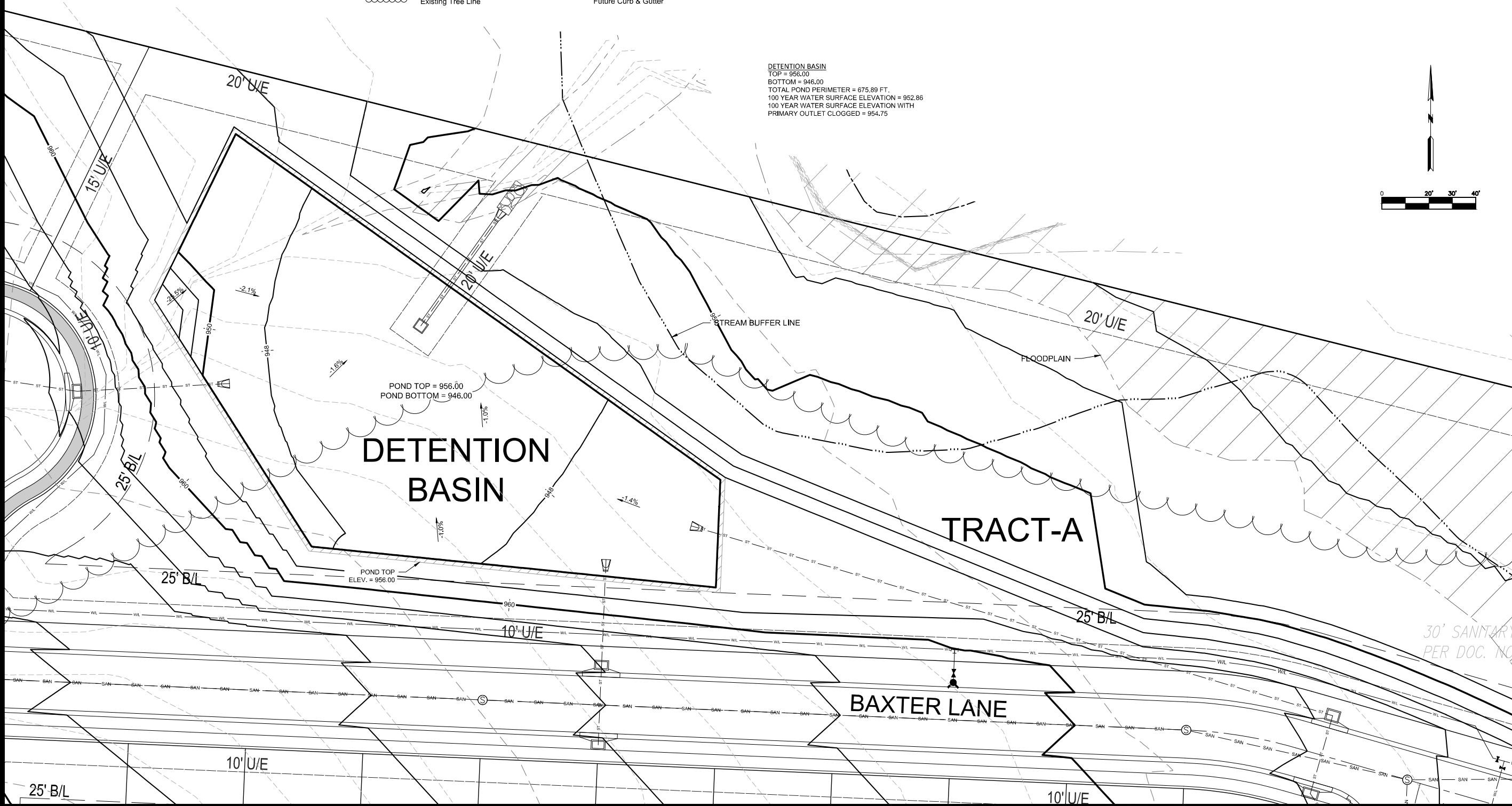


Know what's below.
Call before you dig.

LEGEND

- | | |
|----------------------------|---------------------------|
| Existing Section Line | Proposed Right-of-Way |
| Existing Right-of-Way Line | Proposed Property Line |
| Existing Lot Line | Proposed Lot Line |
| Existing Easement Line | Proposed Easement |
| Existing Curb & Gutter | Proposed Curb & Gutter |
| Existing Sidewalk | Proposed Sidewalk |
| Existing Storm Sewer | Proposed Storm Sewer |
| Existing Storm Structure | Proposed Storm Structure |
| Existing Waterline | Proposed Fire Hydrant |
| Existing Gas Main | Proposed Waterline |
| Existing Sanitary Sewer | Proposed Sanitary Sewer |
| Existing Sanitary Manhole | Proposed Sanitary Manhole |
| Existing Contour Major | Proposed Contour Major |
| Existing Contour Minor | Proposed Contour Minor |
| Existing Tree Line | Future Curb & Gutter |

Figure A - Detention Basin Construction Plans



STORM SEWER PLANS
DETENTION BASIN PLAN
COLTON'S CROSSING
1ST PLAT
CITY OF LEE'S SUMMIT, JACKSON COUNTY, MISSOURI

| |
|-----------------------|
| X-REF NO. 25.018 |
| DRAWING NO. 25.018 |
| DATE JUNE 4, 2025 |
| JOB NO. 25.018 |

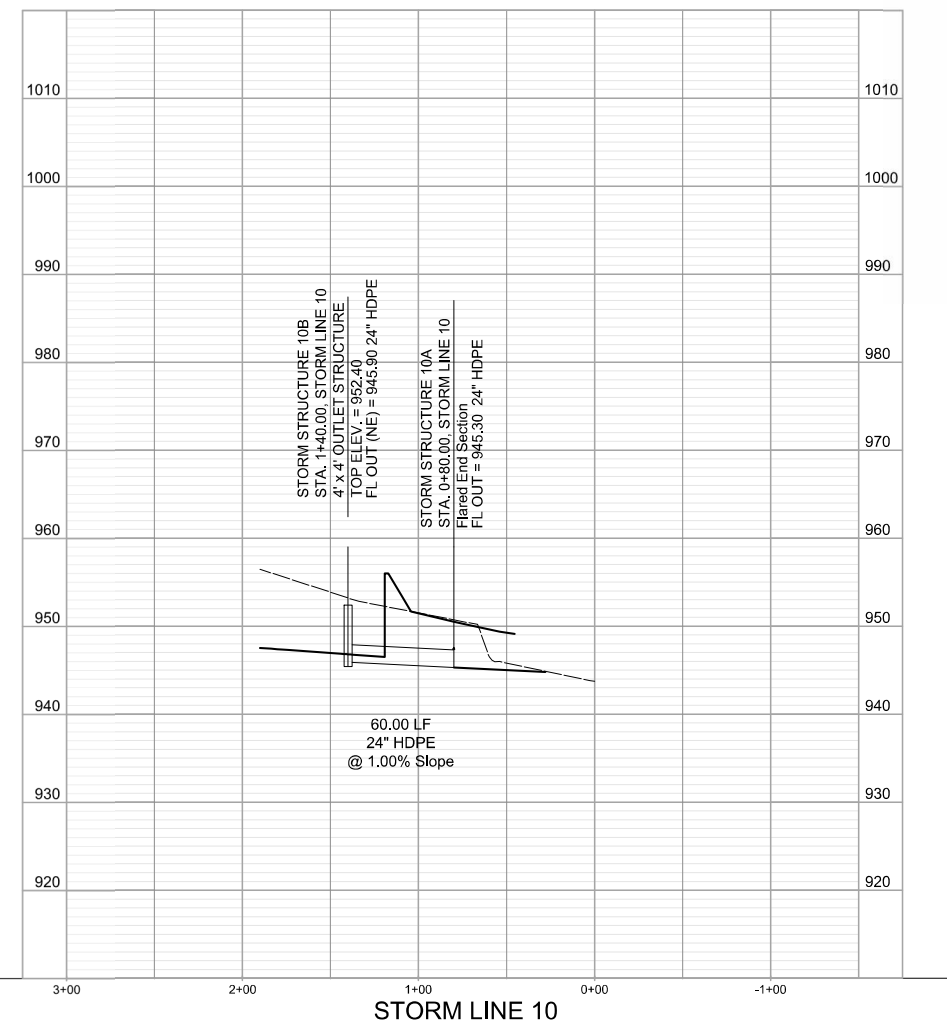
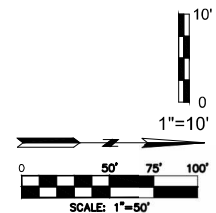
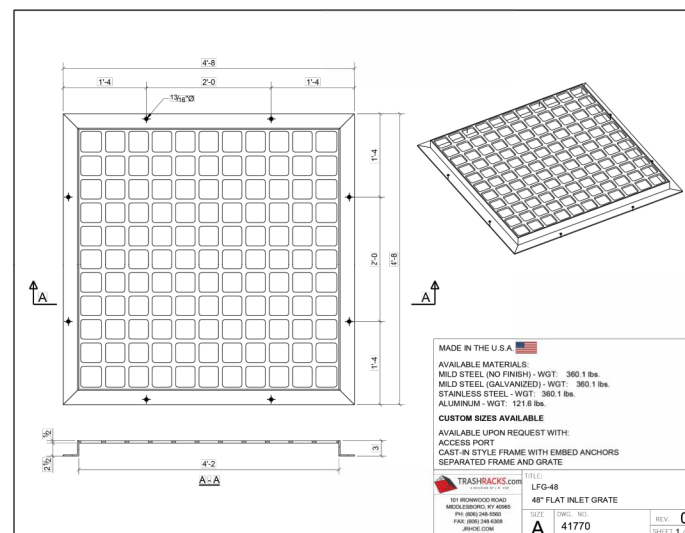
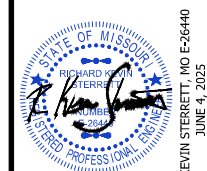


1. ALL REBAR SHOWN IS #5 @ 12' MAX. SPACNG. REBAR SHALL HAVE 2" MIN. CLEAR COVER ON THE SIDE WALLS AND 3" MIN. CLEAR COVER ON THE BASE.



DETENTION BASIN OUTLET STRUCTURE

NOT TO SCALE

[illegible]

R. KEVIN STERRETT, MO E-26440
JUNE 4, 2025



1533 Locust Street, Kansas City, Missouri 64108
CORPORATE LICENSE No. E201000573 (MO.) / E-1736 (KS.) / LS 2019005467

STORM SEWER PLANS
LINE 10 & OUTLET STRUCTURE

COLTON'S CROSSING
1ST PLAT

CITY OF LEE'S SUMMIT; JACKSON COUNTY, MISSOURI

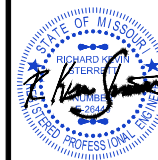
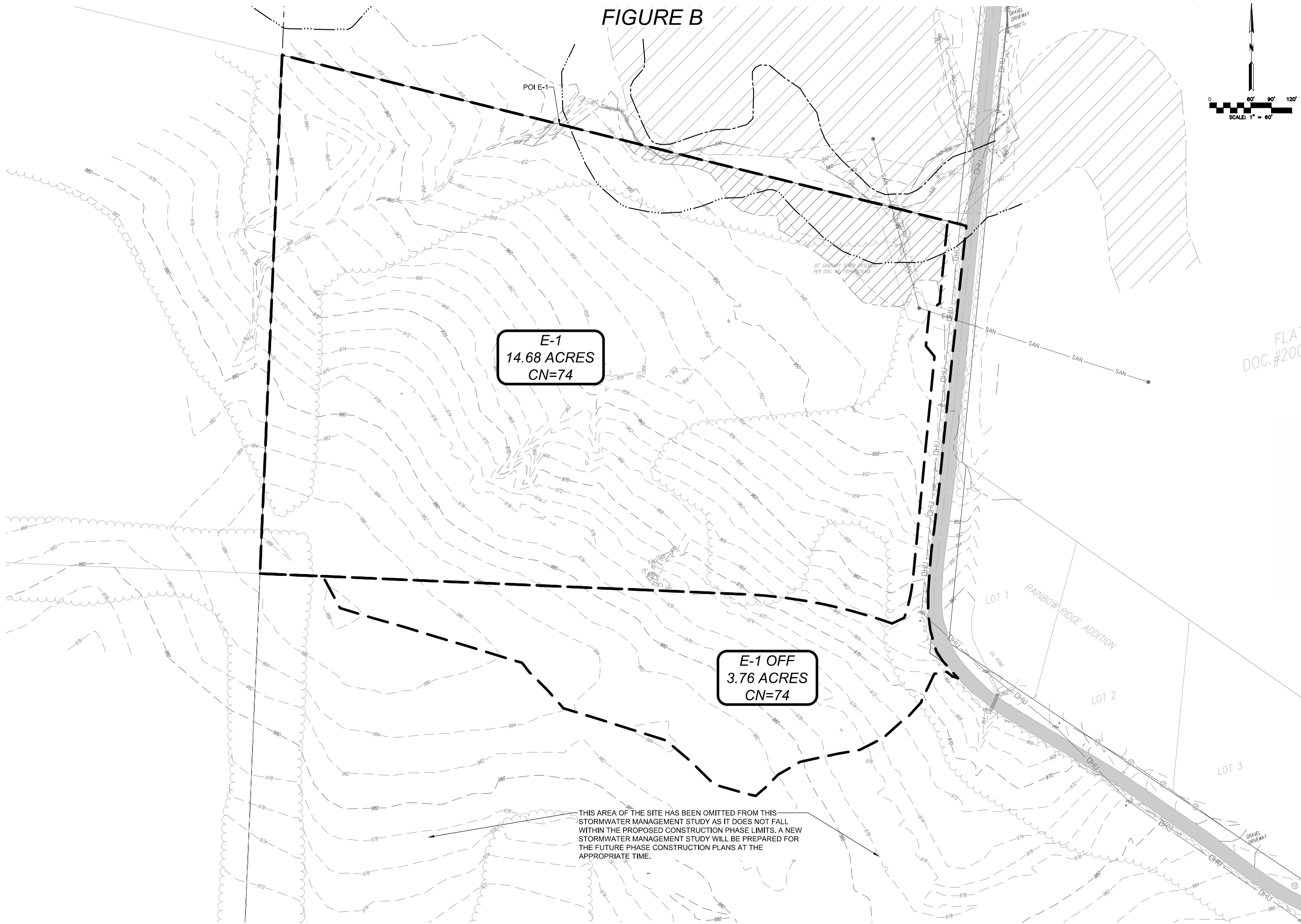
| | |
|-------------|--------------|
| X-REF NO. | 25.018 |
| DRAWING NO. | 25.018 |
| DATE | JUNE 4, 2025 |
| JOB NO. | 25.018 |

7 SHEET OF 12



Know what's below.
Call before you dig.

FIGURE B



R. KEVIN STERRETT, MO E-26440



1533 Locust Street, Kansas City, Missouri 64108

STORM SEWER PLANS PRE-DEVELOPED DRAINAGE AREA MAP

COLTON'S CROSSING

1ST PLAT

CITY OF LEE'S SUMMIT, JACKSON COUNTY, MISSOURI

X-REF NO.
25.018

DRAWING NO.
25.018

DATE
JUNE 4, 20

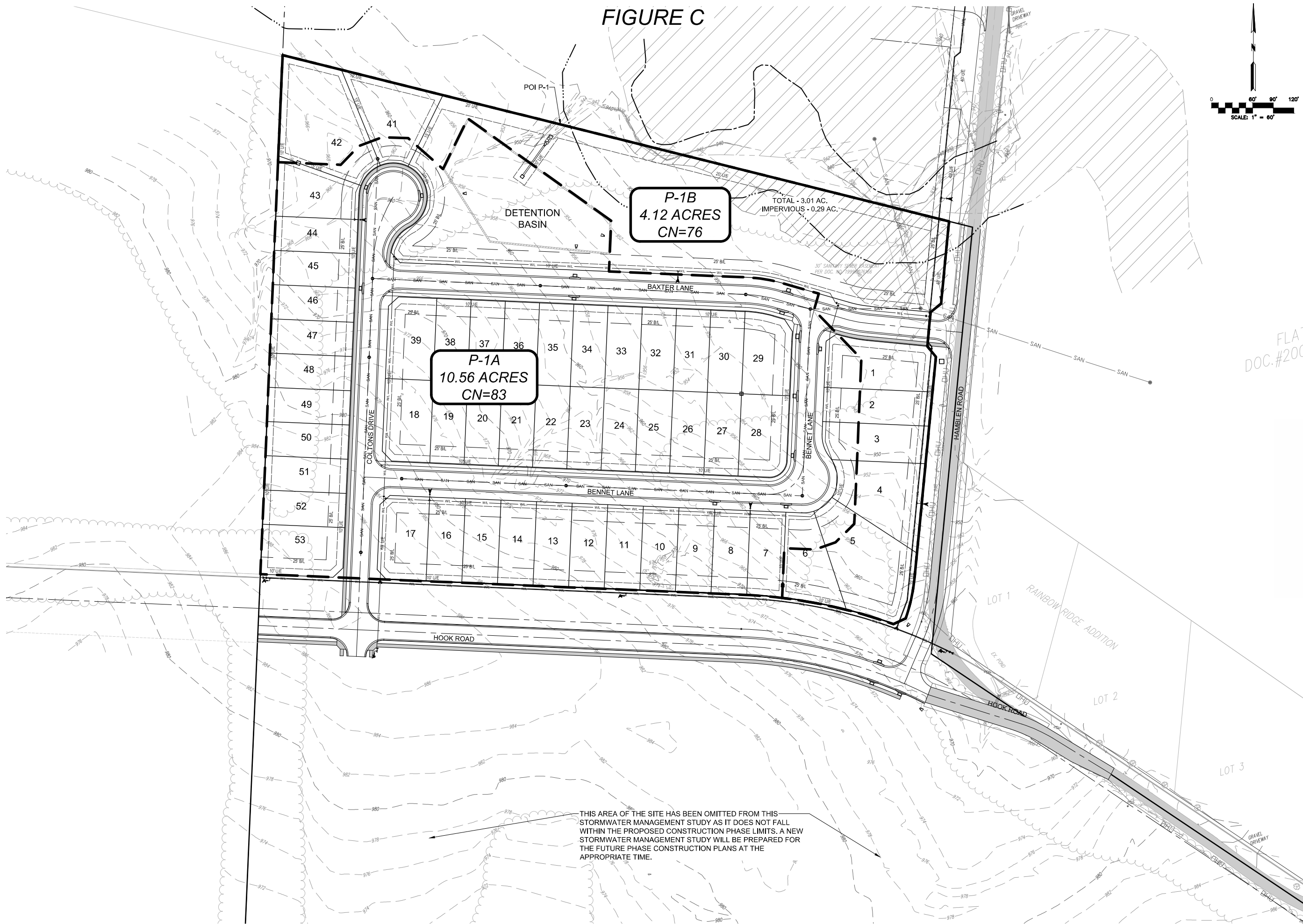
JOB NO.
25.018

C

SHEET
OF

12

FIGURE C



R. KEVIN STERRETT, MO E-26440
JUNE 4, 2025



1533 Locust Street, Kansas City, Missouri 64108
CORPORATE LICENSE No. E201000573 (MO.) / E-1736 (KS.) / L52019005467

**STORM SEWER PLANS
POST - DEVELOPED
DRAINAGE AREA MAP**

COLTON'S CROSSING

1ST PLAT

CITY OF LEE'S SUMMIT, JACKSON COUNTY, MISSOURI

| | |
|-------------|------------|
| X-REF NO. | 25.018 |
| DRAWING NO. | 25.018 |
| DATE | JUNE 4, 20 |
| JOB NO. | 25.018 |

DRAWING NO.
25.018

DATE _____
LINE 4 20

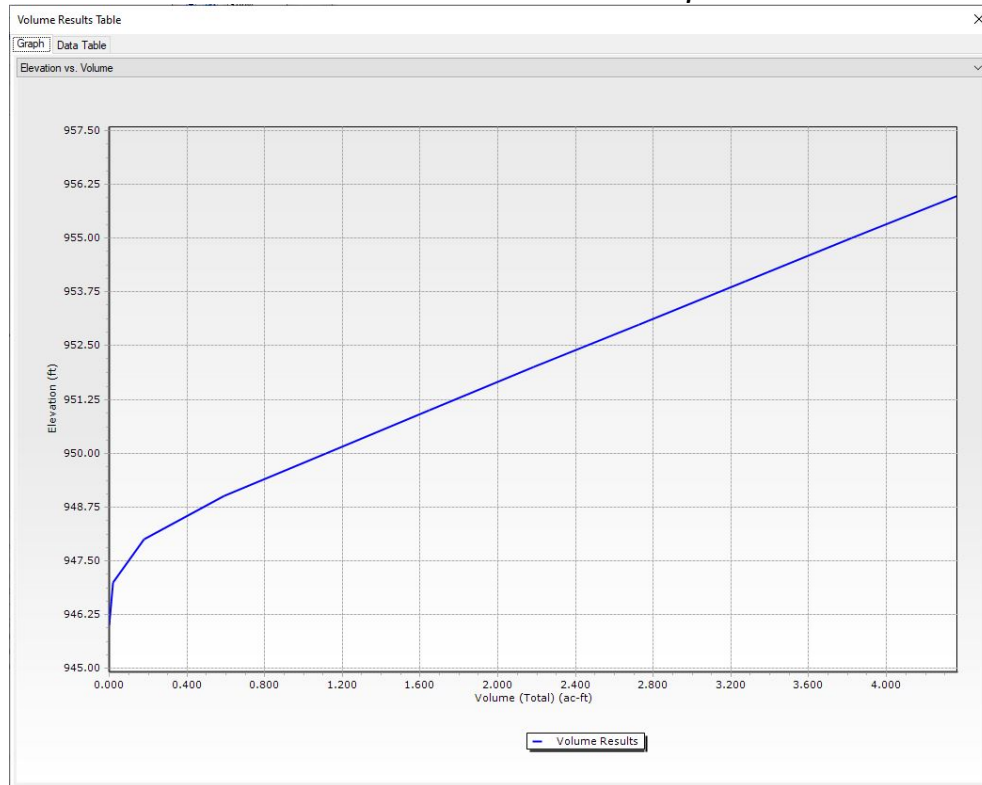
JOB NO.

25.018

10 SHEET OF 12

Figure D – Detention Basin Volume Results

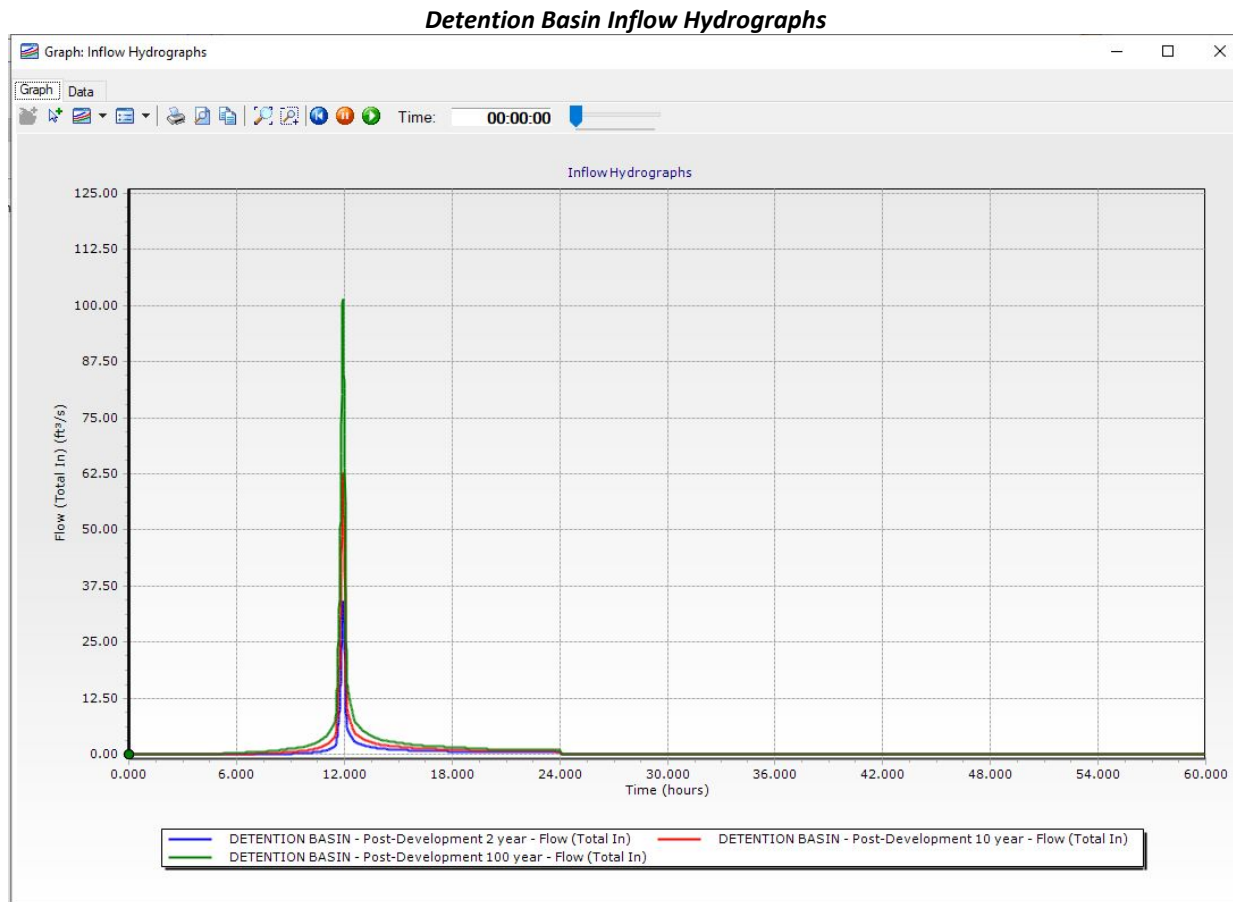
Detention Basin Volume Results Graph



Detention Basin Volume Results Table

| | Elevation (ft) | Planimeter (ft ²) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|----|----------------|-------------------------------|--------------|---------------------------|----------------|------------------------|
| 1 | 946.00 | 0.00 | 0.00 | 0.00 | 0.000 | 0.000 |
| 2 | 947.00 | 0.00 | 0.04 | 0.05 | 0.017 | 0.017 |
| 3 | 948.00 | 0.00 | 0.32 | 0.48 | 0.162 | 0.179 |
| 4 | 949.00 | 0.00 | 0.51 | 1.24 | 0.412 | 0.591 |
| 5 | 950.00 | 0.00 | 0.53 | 1.56 | 0.521 | 1.112 |
| 6 | 951.00 | 0.00 | 0.54 | 1.61 | 0.535 | 1.647 |
| 7 | 952.00 | 0.00 | 0.54 | 1.62 | 0.539 | 2.186 |
| 8 | 953.00 | 0.00 | 0.54 | 1.63 | 0.542 | 2.728 |
| 9 | 954.00 | 0.00 | 0.55 | 1.63 | 0.545 | 3.273 |
| 10 | 955.00 | 0.00 | 0.55 | 1.64 | 0.547 | 3.820 |
| 11 | 956.00 | 0.00 | 0.55 | 1.65 | 0.548 | 4.368 |

Figure E – Inflow Hydrographs



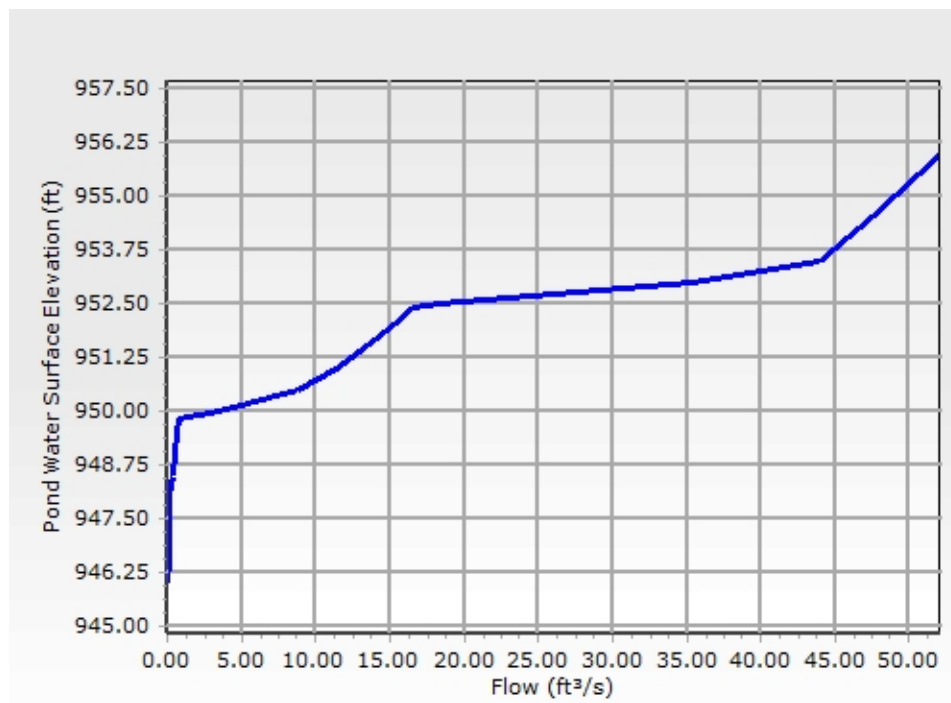
**Figure F –
Stage-Discharge Rating Curves
& Input Data Per Basin Outlet**

Composite Outlet Structure Detailed Report: Composite Outlet Structure

| Element Details | | | |
|--------------------------------------|------------------------------|-------------------------------|--------------|
| Label | Composite Outlet Structure | Notes | |
| Headwater Range | | | |
| Headwater Type | Use Pond for Headwater Range | Maximum (Headwater) | 956.00 ft |
| Pond | DETENTION BASIN | Increment (Headwater) | 0.50 ft |
| Minimum (Headwater) | 946.00 ft | | |
| SpotElevation (ft) | | | |
| Tailwater Setup | | | |
| Tailwater Type | Free Outfall | | |
| Tailwater Tolerances | | | |
| Maximum Iterations | 30 | Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft | Flow Tolerance (Minimum) | 0.001 ft³/s |
| Headwater Tolerance (Maximum) | 0.50 ft | Flow Tolerance (Maximum) | 10.000 ft³/s |
| Tailwater Tolerance (Minimum) | 0.01 ft | | |
| Outlet Structure | | | |
| Outlet Structure Type | Culvert | Culvert Type | Circular |
| Outlet Structure (IDs and Direction) | | | |
| Outlet ID | CULVERT | Downstream ID | Tailwater |
| Flow Direction | Forward Flow Only | Notes | |
| Outlet Structure (Advanced) | | | |
| Elevation (On) | 0.00 ft | Elevation (Off) | 0.00 ft |
| Culvert Data | | | |
| Number of Barrels | 1 | Downstream Invert | 945.32 ft |
| Length | 58.50 ft | Diameter | 24.0 in |
| Upstream Invert | 945.90 ft | | |
| Unsubmerged->Submerged | | | |
| Specify Transitions | False | Compute Inlet Control Only | False |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

| Culvert Coefficients | | | |
|-----------------------|----------------------------------|--------------------------------------|--------|
| Inlet Description | Concrete - Groove end projecting | C | 0.0317 |
| Chart | Chart 1 | Y | 0.6900 |
| Nomograph | Nomograph 3 | Manning's n | 0.012 |
| Equation Form | Form 1 | Ke | 0.200 |
| K | 0.0045 | Kr | 0.200 |
| M | 2.0000 | Slope Correction Factor | -0.500 |
| Culvert (Advanced) | | | |
| Convergence Tolerance | 0.00 ft | Specify Number of Backwater Sections | False |



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = CULVERT (Culvert-Circular)

Mannings open channel maximum capacity: 26.25 ft³/s

Upstream ID = 2YR, 10YR, 4'X4' RISER, WQ

Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|------------------------------|---------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
|------------------------------|---------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = CULVERT (Culvert-Circular)

Mannings open channel maximum capacity: 26.25 ft³/s

Upstream ID = 2YR, 10YR, 4'X4' RISER, WQ

Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|--------------------------------------------|----------------------------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
| 946.00 | 0.00 | 0.00 | 0.00 | Free Outfall |
| 946.50 | 0.07 | 946.02 | Free Outfall | Free Outfall |
| 947.00 | 0.10 | 0.00 | Free Outfall | Free Outfall |
| 947.50 | 0.12 | 0.00 | Free Outfall | Free Outfall |
| 948.00 | 0.15 | 946.08 | Free Outfall | Free Outfall |
| 948.10 | 0.15 | 0.00 | Free Outfall | Free Outfall |
| 948.50 | 0.36 | 946.19 | Free Outfall | Free Outfall |
| 949.00 | 0.53 | 946.25 | Free Outfall | Free Outfall |
| 949.50 | 0.66 | 946.29 | Free Outfall | Free Outfall |
| 949.80 | 0.72 | 946.31 | Free Outfall | Free Outfall |
| 950.00 | 3.46 | 946.83 | Free Outfall | Free Outfall |
| 950.50 | 8.86 | 947.47 | Free Outfall | Free Outfall |
| 951.00 | 11.43 | 947.73 | Free Outfall | Free Outfall |
| 951.50 | 13.50 | 947.92 | Free Outfall | Free Outfall |
| 952.00 | 15.29 | 948.09 | Free Outfall | Free Outfall |
| 952.40 | 16.59 | 948.21 | Free Outfall | Free Outfall |
| 952.50 | 18.39 | 948.37 | Free Outfall | Free Outfall |
| 953.00 | 35.49 | 951.32 | Free Outfall | Free Outfall |
| 953.50 | 44.04 | 953.50 | Free Outfall | Free Outfall |
| 954.00 | 45.78 | 954.00 | Free Outfall | Free Outfall |
| 954.50 | 47.45 | 954.50 | Free Outfall | Free Outfall |
| 955.00 | 49.05 | 955.00 | Free Outfall | Free Outfall |
| 955.50 | 50.62 | 955.50 | Free Outfall | Free Outfall |
| 956.00 | 52.14 | 956.00 | Free Outfall | Free Outfall |
| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = CULVERT (Culvert-Circular)

Mannings open channel maximum capacity: 26.25 ft³/s

Upstream ID = 2YR, 10YR, 4'X4' RISER, WQ

Downstream ID = Tailwater (Pond Outfall)

| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|--------------------------------------------------|-------------------------------------------|-----------------------------------------|-------------------------|
| 0.00 | 0.01 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.01 | (N/A) | 0.00 |
| 0.00 | 0.01 | (N/A) | 0.00 |
| 0.00 | 0.01 | (N/A) | 0.00 |
| 0.00 | 0.02 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 11.34 | (N/A) | 0.00 |
| 0.00 | 51.37 | (N/A) | 0.00 |
| 0.00 | 64.15 | (N/A) | 0.00 |
| 0.00 | 75.12 | (N/A) | 0.00 |
| 0.00 | 84.97 | (N/A) | 0.00 |
| 0.00 | 93.98 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL Vh= .030ft
 Dcr= .088ft CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL Vh= .036ft
 Dcr= .106ft CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL Vh= .041ft
 Dcr= .120ft CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL Vh= .044ft
 Dcr= .130ft CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL Vh= .044ft
 Dcr= .130ft CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO
 UPSTREAM CONTROLLING
 STRUCTURE
 CRIT.DEPTH CONTROL Vh= .086ft
 Dcr= .250ft CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO
 UPSTREAM CONTROLLING
 STRUCTURE
 CRIT.DEPTH CONTROL Vh= .100ft
 Dcr= .291ft CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO
 UPSTREAM CONTROLLING
 STRUCTURE
 CRIT.DEPTH CONTROL Vh= .425ft
 Dcr= 1.062ft CRIT.DEPTH Hev= .00ft

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = CULVERT (Culvert-Circular)

Mannings open channel maximum capacity: 26.25 ft³/s

Upstream ID = 2YR, 10YR, 4'X4' RISER, WQ

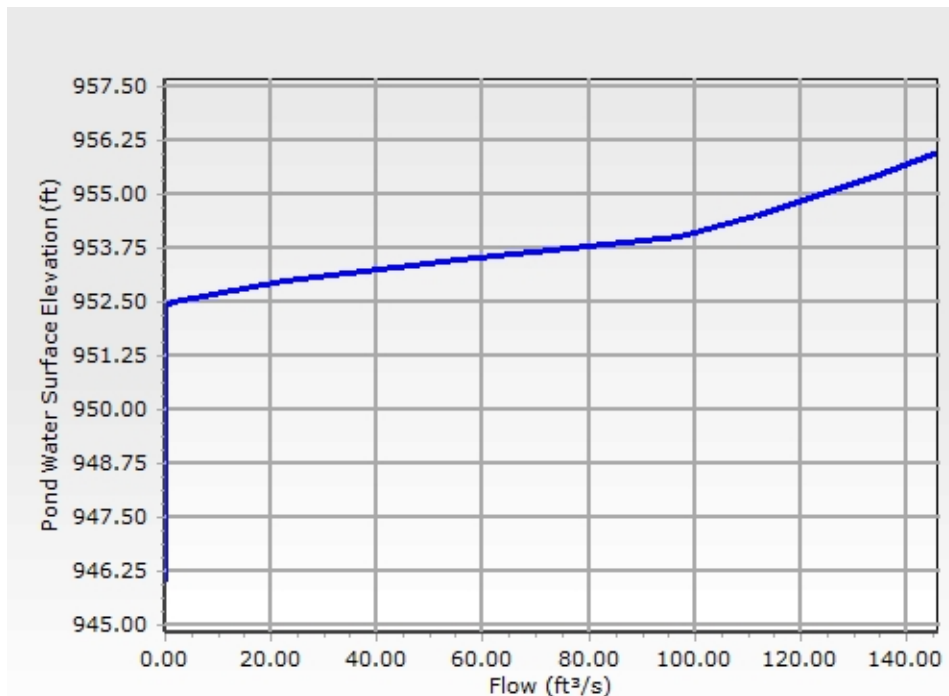
Downstream ID = Tailwater (Pond Outfall)

| Message | | | |
|---------------------------------------------------------------------|--|--|--|
| CRIT.DEPTH CONTROL Vh= .510ft Dcr= 1.214ft CRIT.DEPTH Hev= .00ft | | | |
| CRIT.DEPTH CONTROL Vh= .582ft Dcr= 1.323ft CRIT.DEPTH Hev= .00ft | | | |
| CRIT.DEPTH CONTROL Vh= .649ft Dcr= 1.410ft CRIT.DEPTH Hev= .00ft | | | |
| CRIT.DEPTH CONTROL Vh= .699ft Dcr= 1.468ft CRIT.DEPTH Hev= .00ft | | | |
| CRIT.DEPTH CONTROL Vh= .776ft Dcr= 1.544ft CRIT.DEPTH Hev= .00ft | | | |
| INLET CONTROL... Submerged: HW =5.42 | | | |
| INLET CONTROL... Submerged: HW =7.60 | | | |
| INLET CONTROL... Submerged: HW =8.10 | | | |
| INLET CONTROL... Submerged: HW =8.60 | | | |
| INLET CONTROL... Submerged: HW =9.10 | | | |
| INLET CONTROL... Submerged: HW =9.60 | | | |
| INLET CONTROL... Submerged: HW =10.10 | | | |

| Outlet Structure | | | |
|------------------------------------------------|-------------------|---------------------------------|--------------------------|
| Outlet Structure Type | | Riser | |
| Outlet Structure (IDs and Direction) | | | |
| Outlet ID | 4'X4' RISER | Downstream ID | CULVERT |
| Flow Direction | Forward Flow Only | Notes | |
| Outlet Structure (Advanced) | | | |
| Elevation (On) | 0.00 ft | Elevation (Off) | 0.00 ft |
| Outlet Structure (Riser) | | | |
| Riser | Inlet Box | Orifice Area | 16.00 ft² |
| Weir Length | 16.00 ft | Transition Elevation | 0.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s | Transition Height | 0.00 ft |
| Orifice Coefficient | 0.600 | K Reverse | 1.000 |
| Bentley Systems, Inc. | | Haestad Methods Solution Center | PondPack CONNECT Edition |
| Coltons Crossing 1st Plat Post-Development.ppc | | [10.02.00.01] | |
| 6/4/2025 | | Page 5 of 22 | |
| 27 Siemon Company Drive Suite 200 W | | | |
| Watertown, CT 06795 USA +1-203-755-1666 | | | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

| | | | |
|------------------------------------|-----------|------------------------------|-------|
| Outlet Structure (Riser) | | | |
| | | | |
| Outlet Structure (Common) | | | |
| Elevation | 952.40 ft | | |
| | | | |
| Outlet Structure (Riser, Advanced) | | | |
| Use Orifice Depth to Crest? | True | Use Submerged Weir Equation? | False |



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 4'X4' RISER (Inlet Box)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|------------------------------|---------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
| 946.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 946.50 | 0.00 | 0.00 | 0.00 | 946.02 |
| 947.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 947.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 948.00 | 0.00 | 0.00 | 0.00 | 946.08 |
| 948.10 | 0.00 | 0.00 | 0.00 | 0.00 |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 4'X4' RISER (Inlet Box)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|--------------------------------------------------|-------------------------------------------|--------------------------------------------------|-----------------------------------------------------|-------------------------------------------------|
| 948.50 | 0.00 | 0.00 | 0.00 | 946.19 |
| 949.00 | 0.00 | 0.00 | 0.00 | 946.25 |
| 949.50 | 0.00 | 0.00 | 0.00 | 946.29 |
| 949.80 | 0.00 | 0.00 | 0.00 | 946.31 |
| 950.00 | 0.00 | 0.00 | 0.00 | 946.83 |
| 950.50 | 0.00 | 0.00 | 0.00 | 947.47 |
| 951.00 | 0.00 | 0.00 | 0.00 | 947.73 |
| 951.50 | 0.00 | 0.00 | 0.00 | 947.92 |
| 952.00 | 0.00 | 0.00 | 0.00 | 948.09 |
| 952.40 | 0.00 | 0.00 | 0.00 | 948.21 |
| 952.50 | 1.52 | 952.50 | Free Outfall | 948.37 |
| 953.00 | 22.31 | 953.00 | Free Outfall | 951.32 |
| 953.50 | 55.38 | 953.50 | 953.50 | 953.50 |
| 954.00 | 97.15 | 954.00 | 954.00 | 954.00 |
| 954.50 | 111.60 | 954.50 | 954.50 | 954.50 |
| 955.00 | 124.17 | 955.00 | 955.00 | 955.00 |
| 955.50 | 135.59 | 955.50 | 955.50 | 955.50 |
| 956.00 | 146.11 | 956.00 | 956.00 | 956.00 |
| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 4'X4' RISER (Inlet Box)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|--------------------------------------------------|-------------------------------------------|-----------------------------------------|-------------------------|
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 Weir: H =0.1ft
 Weir: H =0.6ft
 FULLY CHARGED RISER: ADJUSTED TO
 WEIR: H =1.1ft
 FULLY CHARGED RISER,
 DOWNSTREAM CONTROL: Kev=0.
 Hev=0.000
 FULLY CHARGED RISER,
 DOWNSTREAM CONTROL: Kev=0.
 Hev=0.000
 FULLY CHARGED RISER,
 DOWNSTREAM CONTROL: Kev=0.
 Hev=0.000
 FULLY CHARGED RISER,
 DOWNSTREAM CONTROL: Kev=0.
 Hev=0.000

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

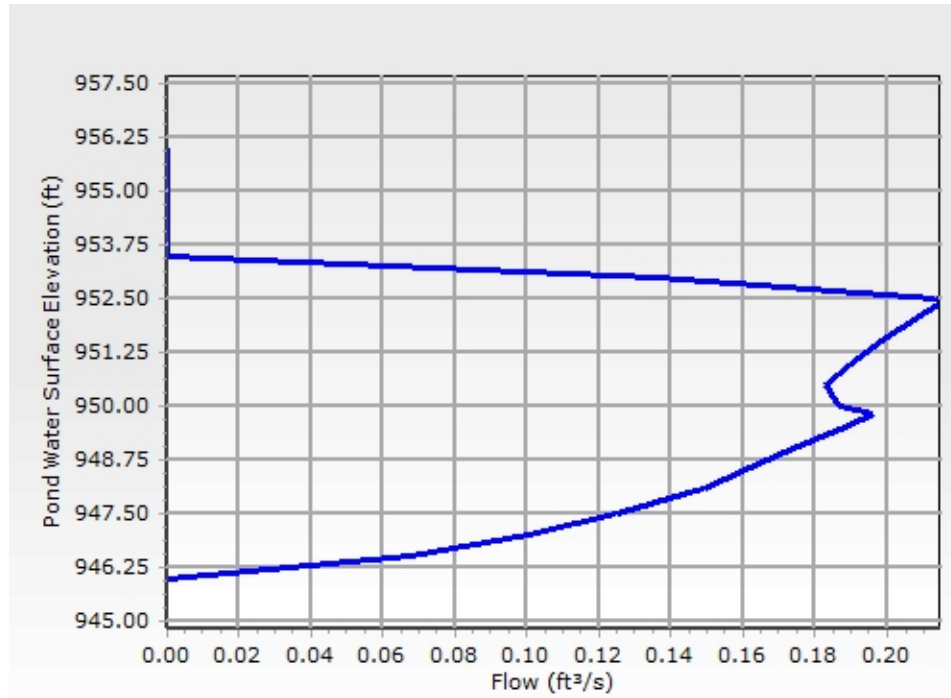
Structure ID = 4'X4' RISER (Inlet Box)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Message | | | |
|-----------------------------------------------------------------|-------------------|---------------------|---------|
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 | | | |
| Outlet Structure | | | |
| Outlet Structure Type | | Orifice | |
| Outlet Structure (IDs and Direction) | | | |
| Outlet ID | WQ | Downstream ID | CULVERT |
| Flow Direction | Forward Flow Only | Notes | |
| Outlet Structure (Advanced) | | | |
| Elevation (On) | 0.00 ft | Elevation (Off) | 0.00 ft |
| Outlet Structure (Orifice) | | | |
| Orifice | Circular Orifice | Orifice Coefficient | 0.600 |
| Number of Openings | 1 | Orifice Diameter | 2.0 in |
| Outlet Structure (Common) | | | |
| Elevation | 946.00 ft | | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = WQ (Orifice-Circular)

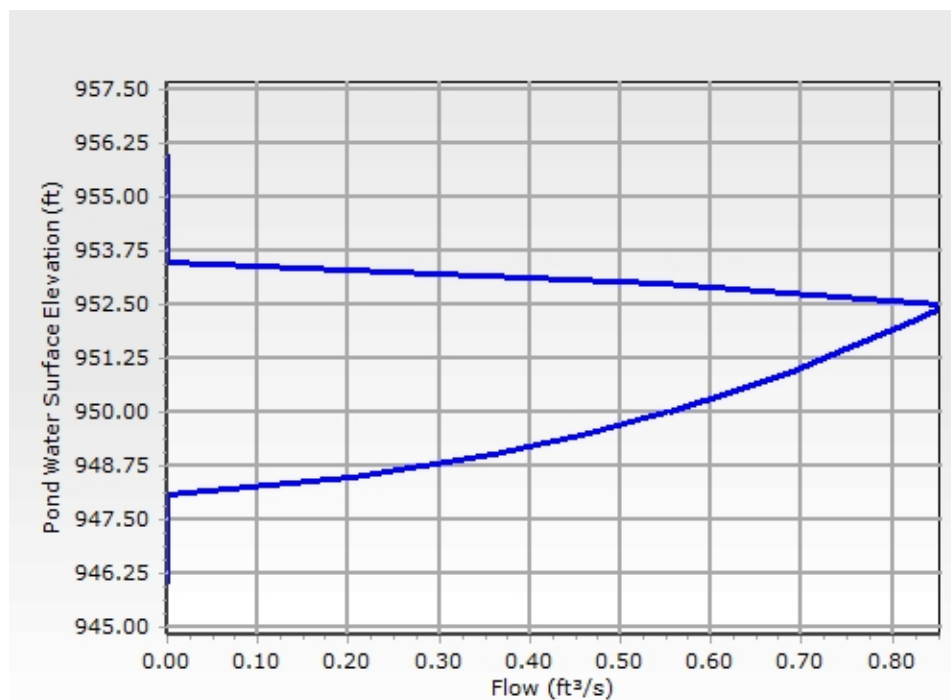
Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|------------------------------|---------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
| 946.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 946.50 | 0.07 | 946.50 | 946.02 | 946.02 |
| 947.00 | 0.10 | 947.00 | 946.05 | 0.00 |
| 947.50 | 0.12 | 947.50 | 946.07 | 0.00 |
| 948.00 | 0.15 | 948.00 | 946.08 | 946.08 |
| 948.10 | 0.15 | 948.10 | Free Outfall | 0.00 |
| 948.50 | 0.16 | 948.50 | 946.19 | 946.19 |
| 949.00 | 0.17 | 949.00 | 946.25 | 946.25 |
| 949.50 | 0.19 | 949.50 | 946.29 | 946.29 |
| 949.80 | 0.20 | 949.80 | 946.31 | 946.31 |
| 950.00 | 0.19 | 950.00 | 946.83 | 946.83 |
| 950.50 | 0.18 | 950.50 | 947.47 | 947.47 |
| 951.00 | 0.19 | 951.00 | 947.73 | 947.73 |
| 951.50 | 0.20 | 951.50 | 947.92 | 947.92 |
| 952.00 | 0.21 | 952.00 | 948.09 | 948.09 |
| 952.40 | 0.22 | 952.40 | 948.21 | 948.21 |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

| | | | |
|-----------------------------|------------------|---------------------|---------|
| Outlet Structure (Advanced) | | | |
| Elevation (On) | 0.00 ft | Elevation (Off) | 0.00 ft |
| Outlet Structure (Orifice) | | | |
| Orifice | Circular Orifice | Orifice Coefficient | 0.600 |
| Number of Openings | 1 | Orifice Diameter | 4.0 in |
| Outlet Structure (Common) | | | |
| Elevation | 948.10 ft | | |



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 2YR (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|------------------------------|----------------------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
| 946.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 946.50 | 0.00 | 0.00 | 0.00 | 946.02 |
| 947.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 947.50 | 0.00 | 0.00 | 0.00 | 0.00 |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 2YR (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|--------------------------------------------------|-------------------------------------------|--------------------------------------------------|-----------------------------------------------------|-------------------------------------------------|
| 948.00 | 0.00 | 0.00 | 0.00 | 946.08 |
| 948.10 | 0.00 | 0.00 | 0.00 | 0.00 |
| 948.50 | 0.20 | 948.50 | Free Outfall | 946.19 |
| 949.00 | 0.36 | 949.00 | Free Outfall | 946.25 |
| 949.50 | 0.47 | 949.50 | Free Outfall | 946.29 |
| 949.80 | 0.52 | 949.80 | Free Outfall | 946.31 |
| 950.00 | 0.55 | 950.00 | Free Outfall | 946.83 |
| 950.50 | 0.63 | 950.50 | Free Outfall | 947.47 |
| 951.00 | 0.69 | 951.00 | Free Outfall | 947.73 |
| 951.50 | 0.76 | 951.50 | Free Outfall | 947.92 |
| 952.00 | 0.81 | 952.00 | Free Outfall | 948.09 |
| 952.40 | 0.85 | 952.40 | 948.21 | 948.21 |
| 952.50 | 0.85 | 952.50 | 948.37 | 948.37 |
| 953.00 | 0.55 | 953.00 | 951.32 | 951.32 |
| 953.50 | 0.00 | 953.50 | 953.50 | 953.50 |
| 954.00 | 0.00 | 954.00 | 954.00 | 954.00 |
| 954.50 | 0.00 | 954.50 | 954.50 | 954.50 |
| 955.00 | 0.00 | 955.00 | 955.00 | 955.00 |
| 955.50 | 0.00 | 955.50 | 955.50 | 955.50 |
| 956.00 | 0.00 | 956.00 | 956.00 | 956.00 |
| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |
| 0.00 | 0.00 | (N/A) | 0.00 | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 2YR (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|--------------------------------------------------|-------------------------------------------|-----------------------------------------|-------------------------|
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |
| 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 H =.23
 H =.73
 H =1.23
 H =1.53
 H =1.73
 H =2.23
 H =2.73
 H =3.23
 H =3.73
 H =4.13
 H =4.13
 H =1.68
 FLOW PRECEDENCE SET TO
 DOWNSTREAM CONTROLLING
 STRUCTURE
 FLOW PRECEDENCE SET TO
 DOWNSTREAM CONTROLLING
 STRUCTURE
 FLOW PRECEDENCE SET TO
 DOWNSTREAM CONTROLLING
 STRUCTURE
 FLOW PRECEDENCE SET TO
 DOWNSTREAM CONTROLLING
 STRUCTURE

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

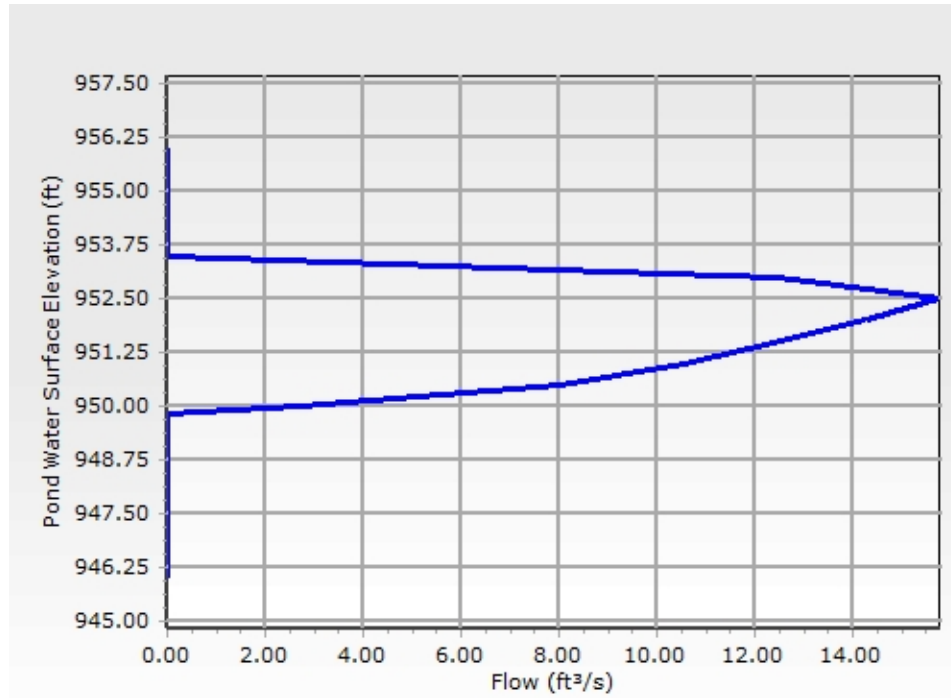
Structure ID = 2YR (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Message | | | |
|---------------------------------------------------------------|----------------------|---------------------|--------------------------|
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE | | | |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE | | | |
| Outlet Structure | | | |
| Outlet Structure Type | | Orifice | |
| Outlet Structure (IDs and Direction) | | | |
| Outlet ID | 10YR | Downstream ID | CULVERT |
| Flow Direction | Forward Flow Only | Notes | |
| Outlet Structure (Advanced) | | | |
| Elevation (On) | 0.00 ft | Elevation (Off) | 0.00 ft |
| Outlet Structure (Orifice) | | | |
| Orifice | Area Orifice | Orifice Orientation | Perpendicular Orifice |
| Number of Openings | 1 | Datum Elevation | 949.80 ft |
| Orifice Coefficient | 0.600 | Top Elevation | 950.30 ft |
| Orifice Area | 2.00 ft² | | |
| Outlet Structure (Common) | | | |
| Elevation | 949.80 ft | | |

Composite Outlet Structure Detailed Report: Composite Outlet Structure



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 10YR (Orifice-Area)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) |
|------------------------------|---------------------|--------------------------------------------|-----------------------------------------------|-------------------------------------------|
| 946.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 946.50 | 0.00 | 0.00 | 0.00 | 946.02 |
| 947.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 947.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 948.00 | 0.00 | 0.00 | 0.00 | 946.08 |
| 948.10 | 0.00 | 0.00 | 0.00 | 0.00 |
| 948.50 | 0.00 | 0.00 | 0.00 | 946.19 |
| 949.00 | 0.00 | 0.00 | 0.00 | 946.25 |
| 949.50 | 0.00 | 0.00 | 0.00 | 946.29 |
| 949.80 | 0.00 | 0.00 | 0.00 | 946.31 |
| 950.00 | 2.72 | 950.00 | Free Outfall | 946.83 |
| 950.50 | 8.05 | 950.50 | Free Outfall | 947.47 |
| 951.00 | 10.54 | 951.00 | Free Outfall | 947.73 |
| 951.50 | 12.55 | 951.50 | Free Outfall | 947.92 |
| 952.00 | 14.28 | 952.00 | Free Outfall | 948.09 |
| 952.40 | 15.52 | 952.40 | Free Outfall | 948.21 |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = 10YR (Orifice-Area)

Upstream ID = (Pond Water Surface)

Downstream ID = CULVERT (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

WS below an invert; no flow.

WS below an invert; no flow.

WS below an invert; no flow.

WS below an invert; no flow.

WS below an invert; no flow.

Hi=.20; Ht=.50; Qt=6.81

H =.70

H =1.20

H =1.70

H =2.20

H =2.60

H =2.70

H =1.68

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

FLOW PRECEDENCE SET TO
DOWNSTREAM CONTROLLING
STRUCTURE

Composite Outlet Structure Detailed Report: Composite Outlet Structure

Composite Rating Table

Tailwater Elevation = Free Outfall (Composite Outlet Structure)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------|---------------------------|--------------------------|------------------------|
| 946.00 | 0.00 | (N/A) | 0.00 |
| 946.50 | 0.07 | (N/A) | 0.00 |
| 947.00 | 0.10 | (N/A) | 0.00 |
| 947.50 | 0.12 | (N/A) | 0.00 |
| 948.00 | 0.15 | (N/A) | 0.00 |
| 948.10 | 0.15 | (N/A) | 0.00 |
| 948.50 | 0.36 | (N/A) | 0.00 |
| 949.00 | 0.53 | (N/A) | 0.00 |
| 949.50 | 0.65 | (N/A) | 0.00 |
| 949.80 | 0.72 | (N/A) | 0.00 |
| 950.00 | 3.46 | (N/A) | 0.00 |
| 950.50 | 8.86 | (N/A) | 0.00 |
| 951.00 | 11.43 | (N/A) | 0.00 |
| 951.50 | 13.50 | (N/A) | 0.00 |
| 952.00 | 15.29 | (N/A) | 0.00 |
| 952.40 | 16.59 | (N/A) | 0.00 |
| 952.50 | 18.39 | (N/A) | 0.00 |
| 953.00 | 35.49 | (N/A) | 0.00 |
| 953.50 | 44.04 | (N/A) | 0.00 |
| 954.00 | 45.78 | (N/A) | 0.00 |
| 954.50 | 47.45 | (N/A) | 0.00 |
| 955.00 | 49.05 | (N/A) | 0.00 |
| 955.50 | 50.62 | (N/A) | 0.00 |
| 956.00 | 52.14 | (N/A) | 0.00 |

Contributing Structures

(no Q: 2YR,10YR,4'X4' RISER,WQ,CULVERT)
 WQ,CULVERT (no Q: 2YR,10YR,4'X4' RISER)
 WQ,CULVERT (no Q: 2YR,10YR,4'X4' RISER)
 WQ,CULVERT (no Q: 2YR,10YR,4'X4' RISER)
 WQ,CULVERT (no Q: 2YR,10YR,4'X4' RISER)
 WQ,CULVERT (no Q: 2YR,10YR,4'X4' RISER)
 2YR,WQ,CULVERT (no Q: 10YR,4'X4' RISER)
 2YR,WQ,CULVERT (no Q: 10YR,4'X4' RISER)
 2YR,WQ,CULVERT (no Q: 10YR,4'X4' RISER)
 2YR,WQ,CULVERT (no Q: 10YR,4'X4' RISER)

Composite Outlet Structure Detailed Report: Composite Outlet Structure

Composite Rating Table

Tailwater Elevation = Free Outfall (Composite Outlet Structure)

| Contributing Structures |
|--------------------------------------------|
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,WQ,CULVERT (no Q: 4'X4' RISER) |
| 2YR,10YR,4'X4' RISER,WQ,CULVERT |
| 2YR,10YR,4'X4' RISER,WQ,CULVERT |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |
| 4'X4' RISER,CULVERT (no Q: 2YR,10YR,WQ) |

Composite Outlet Structure Detailed Report: Composite Outlet Structure

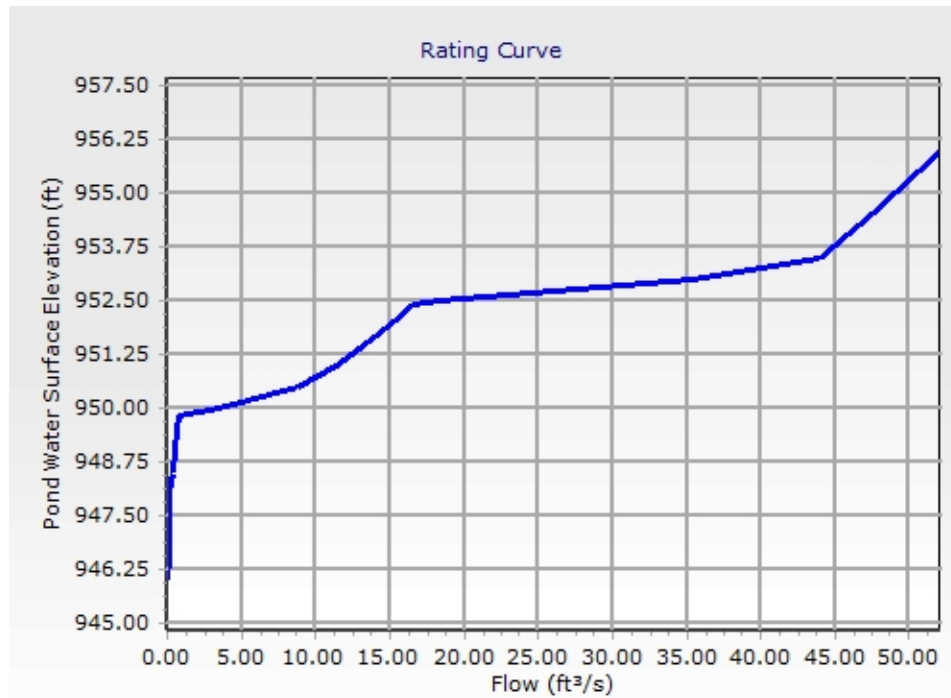
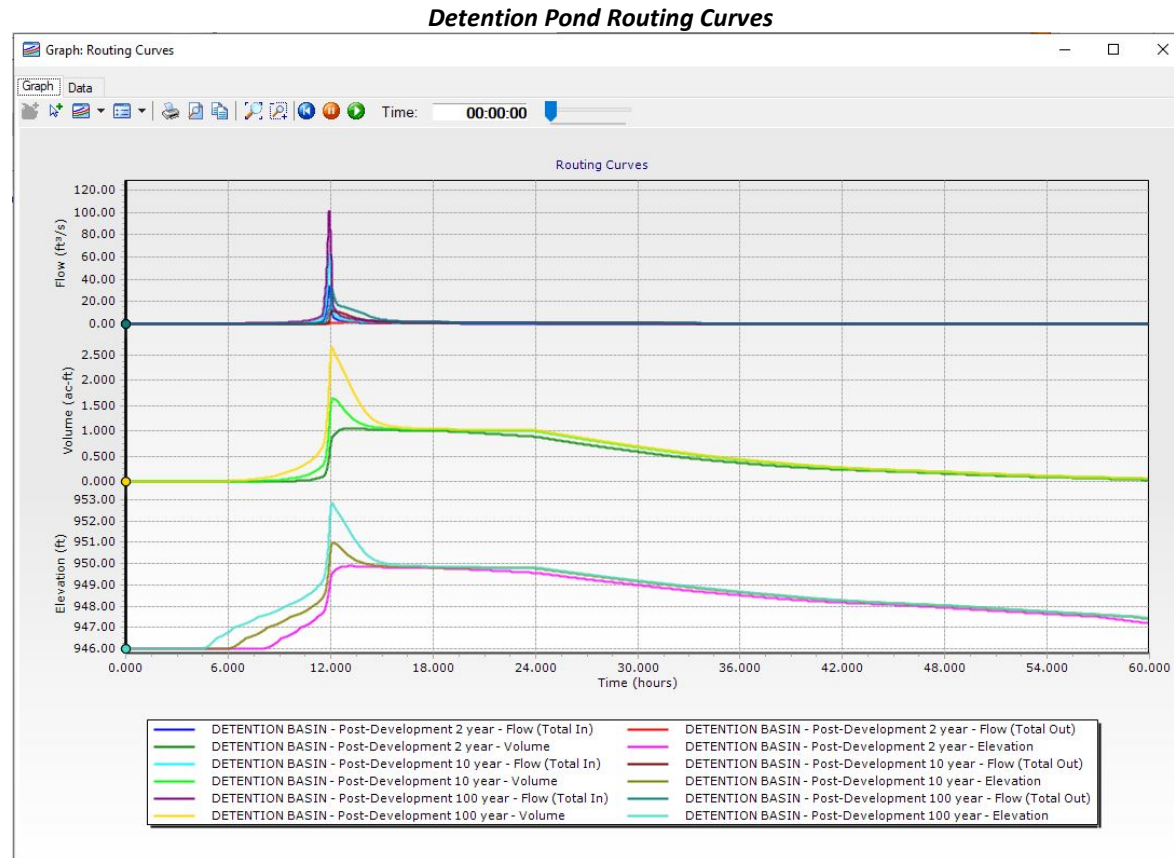
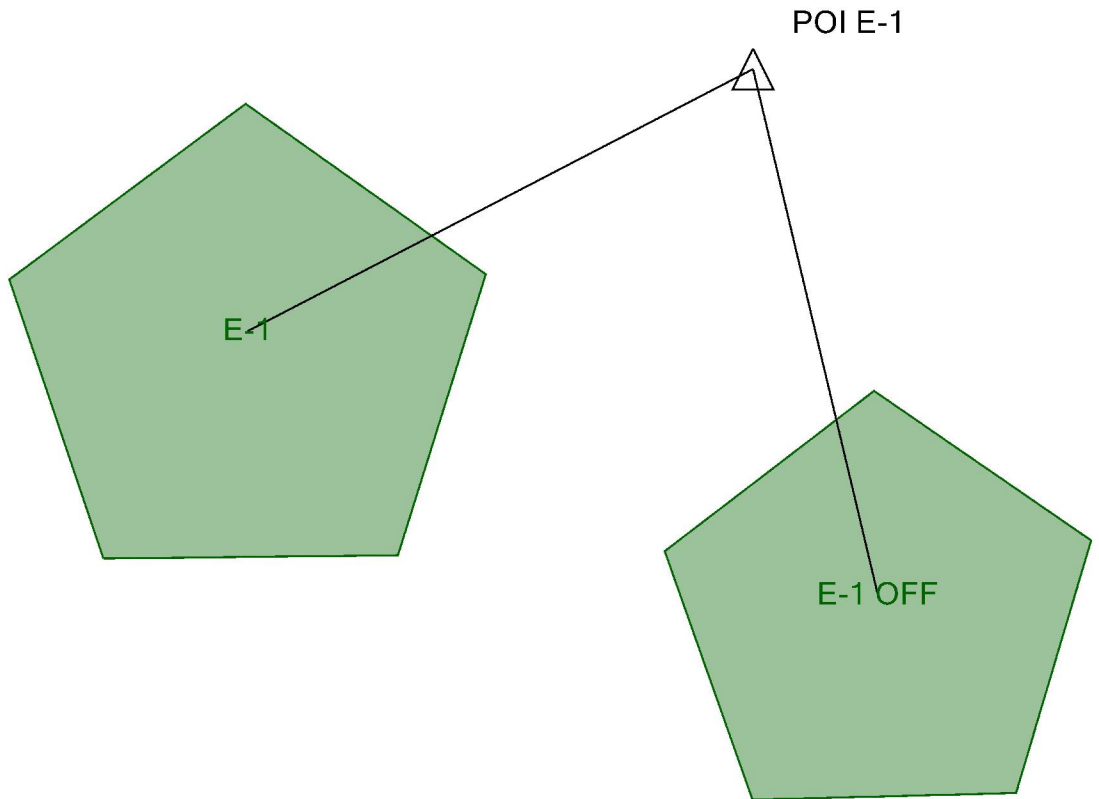


Figure G – Routing Curves for all Design Storms



**Figure H –
Pondpack Master Summary
(Pre-Developed and Post-Developed)**

Scenario: Pre-Development



Colton's Crossing 1st Plat Pre-Developed

Project Summary

| | |
|----------|-------------------------------------------------|
| Title | Colton's Crossing 1st Plat Pre- Developed |
| Engineer | Richard Michael |
| Company | Hg Consult, Inc |
| Date | 6/4/2025 |

Notes

Table of Contents

| |
|------------------------|
| Master Network Summary |
|------------------------|

2

Colton's Crossing 1st Plat Pre-Developed

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|---------|--------------------------|----------------------|---------------------------|----------------------|--------------------------------|
| E-1 | Pre-Development 2 year | 2 | 1.517 | 11.930 | 27.95 |
| E-1 | Pre-Development 10 year | 10 | 3.188 | 11.920 | 60.13 |
| E-1 | Pre-Development 100 year | 100 | 5.699 | 11.920 | 107.22 |
| E-1 OFF | Pre-Development 2 year | 2 | 0.389 | 11.930 | 7.16 |
| E-1 OFF | Pre-Development 10 year | 10 | 0.817 | 11.920 | 15.40 |
| E-1 OFF | Pre-Development 100 year | 100 | 1.460 | 11.920 | 27.46 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|---------|--------------------------|----------------------|---------------------------|----------------------|--------------------------------|
| POI E-1 | Pre-Development 2 year | 2 | 1.905 | 11.930 | 35.11 |
| POI E-1 | Pre-Development 10 year | 10 | 4.004 | 11.920 | 75.53 |
| POI E-1 | Pre-Development 100 year | 100 | 7.158 | 11.920 | 134.68 |

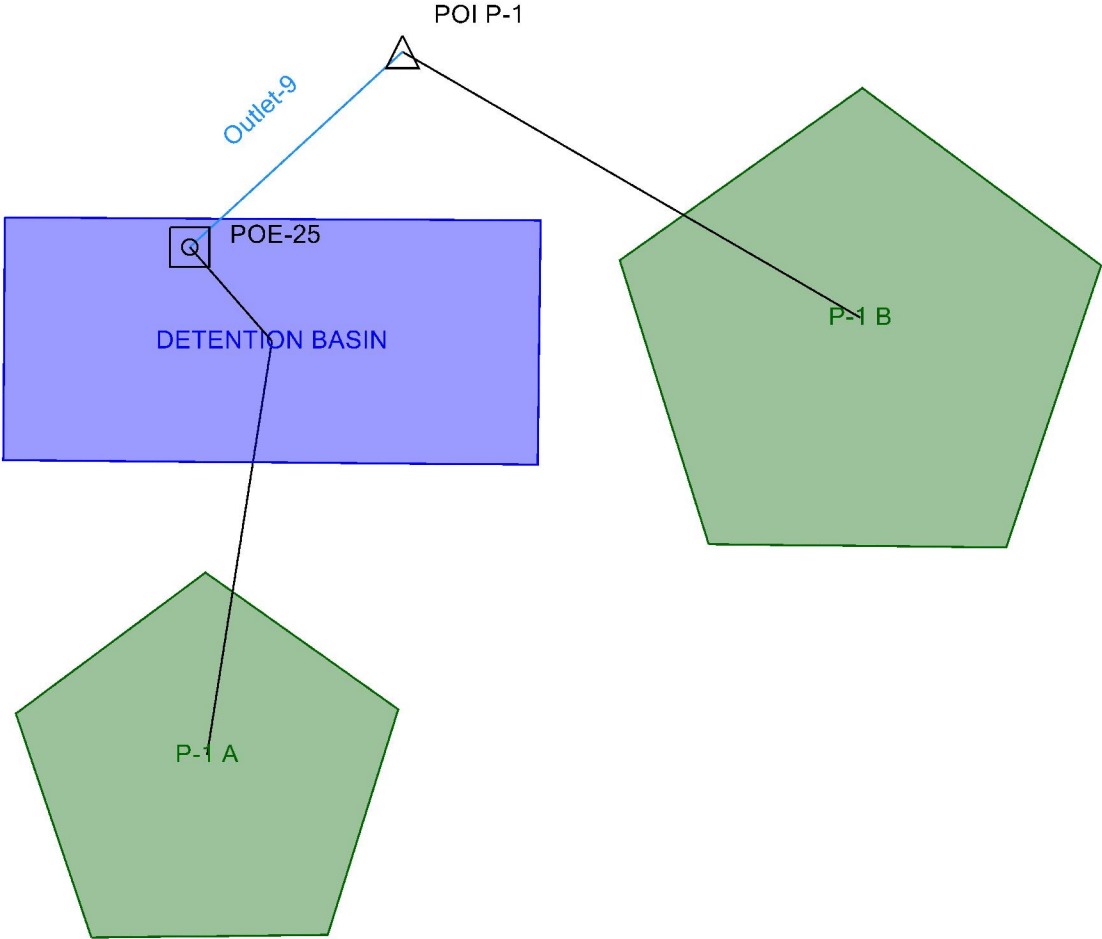
Colton's Crossing 1st Plat Pre-Developed

Index

M

Master Network Summary...2

Scenario: Post-Development



Colton's Crossing 1st Plat Post-Developed

Project Summary

| | |
|----------|--------------------------------------------------|
| Title | Colton's Crossing 1st Plat Post- Developed |
| Engineer | Richard Michael |
| Company | Hg Consult, Inc |
| Date | 6/4/2025 |

Notes

Table of Contents

| |
|------------------------|
| Master Network Summary |
|------------------------|

2

Colton's Crossing 1st Plat Post-Developed

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|-------|---------------------------|----------------------|---------------------------|----------------------|--------------------------------|
| P-1 B | Post-Development 2 year | 2 | 0.342 | 11.930 | 6.38 |
| P-1 B | Post-Development 10 year | 10 | 0.699 | 11.920 | 13.19 |
| P-1 B | Post-Development 100 year | 100 | 1.226 | 11.920 | 22.97 |
| P-1 A | Post-Development 2 year | 2 | 1.807 | 11.920 | 34.14 |
| P-1 A | Post-Development 10 year | 10 | 3.352 | 11.920 | 62.68 |
| P-1 A | Post-Development 100 year | 100 | 5.535 | 11.920 | 101.36 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|---------|---------------------------|----------------------|---------------------------|----------------------|--------------------------------|
| POI P-1 | Post-Development 2 year | 2 | 2.115 | 11.930 | 6.87 |
| POI P-1 | Post-Development 10 year | 10 | 3.997 | 12.010 | 20.73 |
| POI P-1 | Post-Development 100 year | 100 | 6.704 | 12.040 | 41.91 |

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ac-ft) |
|-----------------------|--------------------------|----------------------|---------------------------|----------------------|--------------------------------|--------------------------------------|------------------------------|
| DETENTION BASIN (IN) | Post-Development 2 year | 2 | 1.807 | 11.920 | 34.14 | (N/A) | (N/A) |
| DETENTION BASIN (OUT) | Post-Development 2 year | 2 | 1.773 | 13.180 | 1.85 | 949.88 | 1.049 |
| DETENTION BASIN (IN) | Post-Development 10 year | 10 | 3.352 | 11.920 | 62.68 | (N/A) | (N/A) |
| DETENTION BASIN (OUT) | Post-Development 10 year | 10 | 3.299 | 12.140 | 11.38 | 950.99 | 1.641 |

Colton's Crossing 1st Plat Post-Developed

Subsection: Master Network Summary

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ac-ft) |
|-----------------------|---------------------------|----------------------|---------------------------|----------------------|--------------------------------|--------------------------------------|------------------------------|
| DETENTION BASIN (IN) | Post-Development 100 year | 100 | 5.535 | 11.920 | 101.36 | (N/A) | (N/A) |
| DETENTION BASIN (OUT) | Post-Development 100 year | 100 | 5.478 | 12.090 | 30.78 | 952.86 | 2.653 |

Colton's Crossing 1st Plat Post-Developed

Index

M

Master Network Summary...2, 3

Colton's Crossing 1st Plat Post-Developed w/ Primary Outlet Clogged

Project Summary

| | |
|----------|----------------------------------------------------------------------------------|
| Title | Colton's Crossing 1st Plat Post- Developed w/ Primary Outlet Clogged |
| Engineer | Richard Michael |
| Company | Hg Consult, Inc |
| Date | 6/4/2025 |

Notes

Table of Contents

| |
|------------------------|
| Master Network Summary |
|------------------------|

2

Colton's Crossing 1st Plat Post-Developed w/ Primary Outlet Clogged

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|-------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| P-1 A | Post-Development 100 year | 100 | 241,102.000 | 11.920 | 101.36 |
| P-1 B | Post-Development 100 year | 100 | 53,383.000 | 11.920 | 22.97 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|---------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| POI P-1 | Post-Development 100 year | 100 | 279,316.000 | 11.960 | 105.73 |

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ft ³) |
|-----------------------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|--------------------------------------|-----------------------------------------|
| DETENTION BASIN (IN) | Post-Development 100 year | 100 | 241,102.000 | 11.920 | 101.36 | (N/A) | (N/A) |
| DETENTION BASIN (OUT) | Post-Development 100 year | 100 | 225,933.000 | 11.980 | 85.59 | 954.75 | 160,549.000 |

Colton's Crossing 1st Plat Post-Developed w/ Primary Outlet Clogged

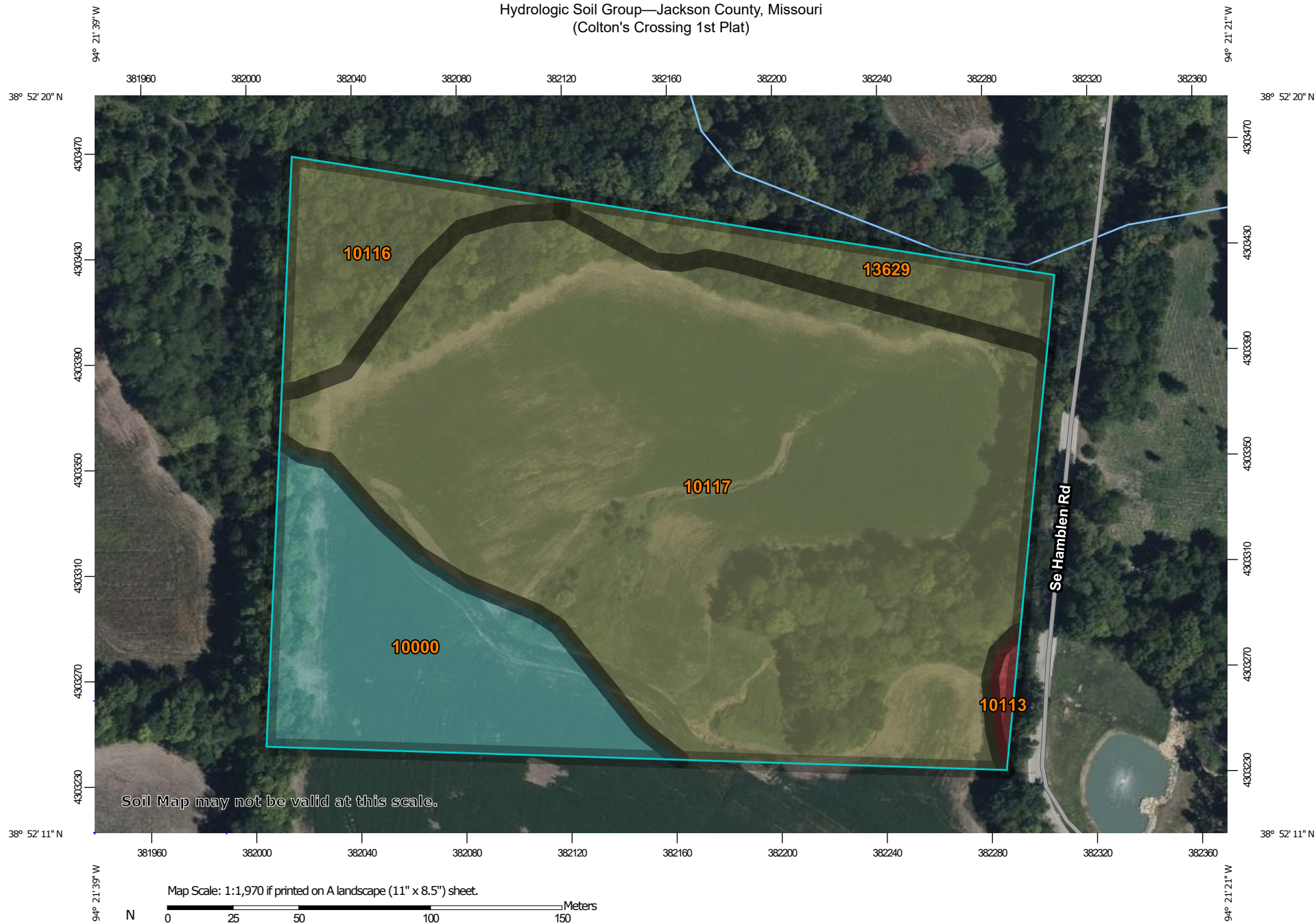
Index

M

Master Network Summary...2

Figure I - Web Soil Survey

Hydrologic Soil Group—Jackson County, Missouri
(Colton's Crossing 1st Plat)



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

6/5/2025
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Lines


 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Points






 A
 A/D
 B
 B/D

 C
 C/D
 D
 Not rated or not available


Water Features

 Streams and Canals

Transportation

 Rails
 Interstate Highways
 US Routes
 Major Roads
 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri
Survey Area Data: Version 27, Aug 27, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 30, 2022—Sep 8, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|-------------------------------------------------------------|--------|--------------|----------------|
| 10000 | Arisburg silt loam, 1 to 5 percent slopes | C | 2.4 | 16.5% |
| 10113 | Oska silty clay loam, 5 to 9 percent slopes, eroded | D | 0.1 | 0.6% |
| 10116 | Sampsel silty clay loam, 2 to 5 percent slopes | C/D | 1.1 | 7.2% |
| 10117 | Sampsel silty clay loam, 5 to 9 percent slopes | C/D | 10.3 | 69.8% |
| 13629 | Colo silt loam, 1 to 4 percent slopes, occasionally flooded | C/D | 0.9 | 5.9% |
| Totals for Area of Interest | | | 14.7 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Figure I – Stream Buffer Evaluation



MEMORANDUM

TO: HG Consult

FROM: Jonathan Polak, P.E. – Habitat Architects

DATE: September 29, 2022

RE: Colton's Crossing Development - Stream Buffer Setback Evaluation

Habitat Architects (*Habitat*) was contacted by HG Consult to complete an independent evaluation of applicable stream buffer setback requirements within the limits of the proposed Colton's Crossing Development. This evaluation was completed in accordance with the American Public Works Association (APWA) Section 5600 – Storm Drainage Systems and Facilities regulations and guidelines as adopted by the City of Lee's Summit, Jackson County, Missouri. The results of this evaluation are discussed in this memorandum and depicted on the attached graphics.

Field Evaluation

Habitat completed a field reconnaissance to identify and delineate water resources on the property (07/12/22). The field reconnaissance identified the project site as having one perennial tributary, known as Big Creek, traversing along the northern property boundary, and entering the property in two short segments. There were also four drainage features that exhibited ephemeral characteristics identified within the limits of the property. These characteristics include conveyance of hydrology, non-continuous flow, dependent upon direct precipitation event, and no groundwater influence.

These four drainages were similarly compared to the common features of stream geometry and characteristics as presented in APWA Section 5600, Subsection 5605, Figures 5605–1 through 5606-3. As mapped on the attached graphics, these drainages are each located within woodland corridors adjacent to farmed agricultural activities along the southern and western limits of the property. A brief description of each of the drainages are provided below:

Perennial Tributary

The perennial tributary found on the property, Big Creek, enters the property in two separate locations along the northern property boundary. The two locations are meanders in the tributary which only encroach on the property a few feet. There is a total of 151 linear feet (L.F.) of tributary that lie within the limits of the property. As noted during the field reconnaissance, Big Creek is approximately 25 feet wide at the ordinary high-water mark (OHM) with a bed composition made up of a mixture of silt and rock substrate. Big Creek maintains a base flow and exhibits a differentiation between a low flow channel and a bank full width. The tributary also has varying riffle/pool structures along its alignment.

Ephemeral Drainage 1 (E-1)

E-1 is an ephemeral drainage in the very northwest corner of the property where it traverses toward the northeast and eventually leaves the property and discharges into Big Creek north of the property boundary. The drainage only averages approximately 3 feet in width at the OHM and traverses approximately 511 L.F. of the northwest corner of the property. There is no base flow within the channel from a contributing groundwater or upland source. There are no channel characteristics such as riffles, pools, or sediment bars present within the narrow base width. The drainage exhibits erosive characteristics rather than traditional tributary or stream features.

Ephemeral Drainage 2 (E-2)

E-2 is an ephemeral drainage located in the southwest corner of the property where it originates in an existing wooded corridor. Similar to E-1, the drainage only averages approximately 3 feet in width at the OHM and traverses approximately 665 L.F. of the property before discharging off the property. The base of the drainage has an excessive amount of broken glass that appears to have been from previous dumping activities over several years. Below the glass the base is entirely comprised of soil with very little stone or rock present, indicative of erosive conditions likely attributable to the adjacent farming activities. There is no base flow within the channel from a contributing groundwater or upland source. There are no channel characteristics such as riffles, pools, or sediment bars present within the narrow base width.

Ephemeral Drainage 3 (E-3)

E-3 is a small ephemeral drainage, approximately 1 foot in width at the OHM. The drainage is located along the southern property boundary which originates from a visible erosive drainage within the adjacent agricultural field to the north. The drainage traverses approximately 223 L.F. of the property before existing the southern boundary.

There is no base flow within the channel from a contributing groundwater or upland source. There is no channel characteristics such as riffles, pools, or sediment bars present within the narrow 1-foot base width. As noted, the drainage appears to be a continuation of the erosive characteristic from the adjacent field rather than a traditional tributary or stream feature.

Ephemeral Drainage 4 (E-4)

E-4 is the last ephemeral drainage identified during the field reconnaissance and is located in a wooded corridor in the southern portion of the property. The drainage originates just north of the tree line from an erosive drainage coming off the adjacent agricultural field. The drainage exhibits similar erosive characteristics and averages approximately 4 feet in width at the OHM. The drainage traverses approximately 297 L.F. before exiting the property through the southern boundary. There is no base flow within the channel from a contributing groundwater or upland source. As the widest base width of the four drainages, there are signs of sediment deposition along the alignment; however, there are no typical stream or tributary characteristics such as riffles, pools, or a traditional meander sequence within the short section of drainage located on the property.

Design Guidelines and Desktop Review

A desktop review and stream buffer evaluation of the water resources identified on the property were performed consistent with APWA Section 5600, subsection 5605 Natural Streams. The guidance addressed by this evaluation includes the following criteria.

SECTION 5605 NATURAL STREAMS

5605.1 Scope

This section sets forth requirements for the protection of natural streams as a conveyance for stormwater. Unless otherwise provided for by City, State, or Federal ordinance, regulation, or standards, existing natural streams shall be preserved and protected in accordance with this section. Where natural streams are not preserved, the drainage will be handled through systems designed in accordance with Sections 5606 and 5607.

5605.3 Stream Preservation and Buffers Zones

B. Default Approach: *Where such comprehensive strategies have not been adopted, the following requirements shall be satisfied for all development/redevelopment proposed adjacent to or ultimately discharging to an existing natural channel:*

1. Streams having a tributary area in excess of 40 acres shall be preserved. Preservation of smaller streams is encouraged. Preservation may be waived by the City/County Engineer where it is impractical, provided that the project has also received appropriate state and federal permits.

2. Buffer zones shall be established around all preserved streams. The limit of buffer zones shall be formally designated on a plat, deed, easement, or restrictive covenant, as directed by the City. Buffer widths as measured from the ordinary high-water mark (OHM) outward in each direction shall exceed the dimensions shown in Table 5605-1.

Table 5605-1: Stream Buffer Widths

| Contributing Drainage Basin Size (acres) | Buffer Width* |
|-----------------------------------------------------|----------------------|
| Less than 40 acres | 40 Feet |
| 40 acres to 160 acres | 60 Feet |
| 160 acres to 5000 acres | 100 Feet |
| Greater than 5000 acres | 120 Feet |

*Measured from OHM outwards, measured separately in each direction

The perennial tributary (Big Creek) and the four ephemeral drainages on site were evaluated to determine drainage basin size. The results of the desktop evaluation are presented below.

Results

The evaluation for the contributing basin size of each tributary and drainage found on the property identified that Big Creek requires a buffer width of 100 feet due to it having a contributing water shed size of approximately 1,700 acres. The remaining drainages on the property (E-1, E-2, E-3, and E-4) all had contributing basin sizes between 8-11 acres. These basin sizes are well below the 40-acre threshold required for buffering. These drainages, although they do convey stormwater from the property, do not exhibit the general characteristics of a stream and tributary as defined in Section 5605 of the APWA guidance. Their respective size and continued erosive characteristics from adjacent agricultural practices contribute to minimal if not negative impacts to water quality due to soil loss within the drainage.

Recommendations

Habitat recommends the placement of a 100-foot buffer along Big Creek, especially those portions that encroach on the property. The remaining four ephemeral drainages do not require a stream setback or stream buffer preservation based on the APWA guidance; however, changes in the discharge of stormwater as it relates to future development and the removal of the existing drainages should be designed in accordance with APWA Section 5606 and 5607.

Furthermore, all potential impacts to either the ephemeral drainages or elements of Big Creek would require permitting with the U.S. Army Corps of Engineers due to the presence of water resources on the site.

Please contact me at (913) 526-5085 or by email at jpolak@habitatarchitects.net if you have any questions concerning the evaluation results.

Sincerely,

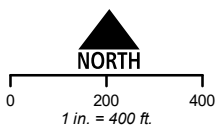
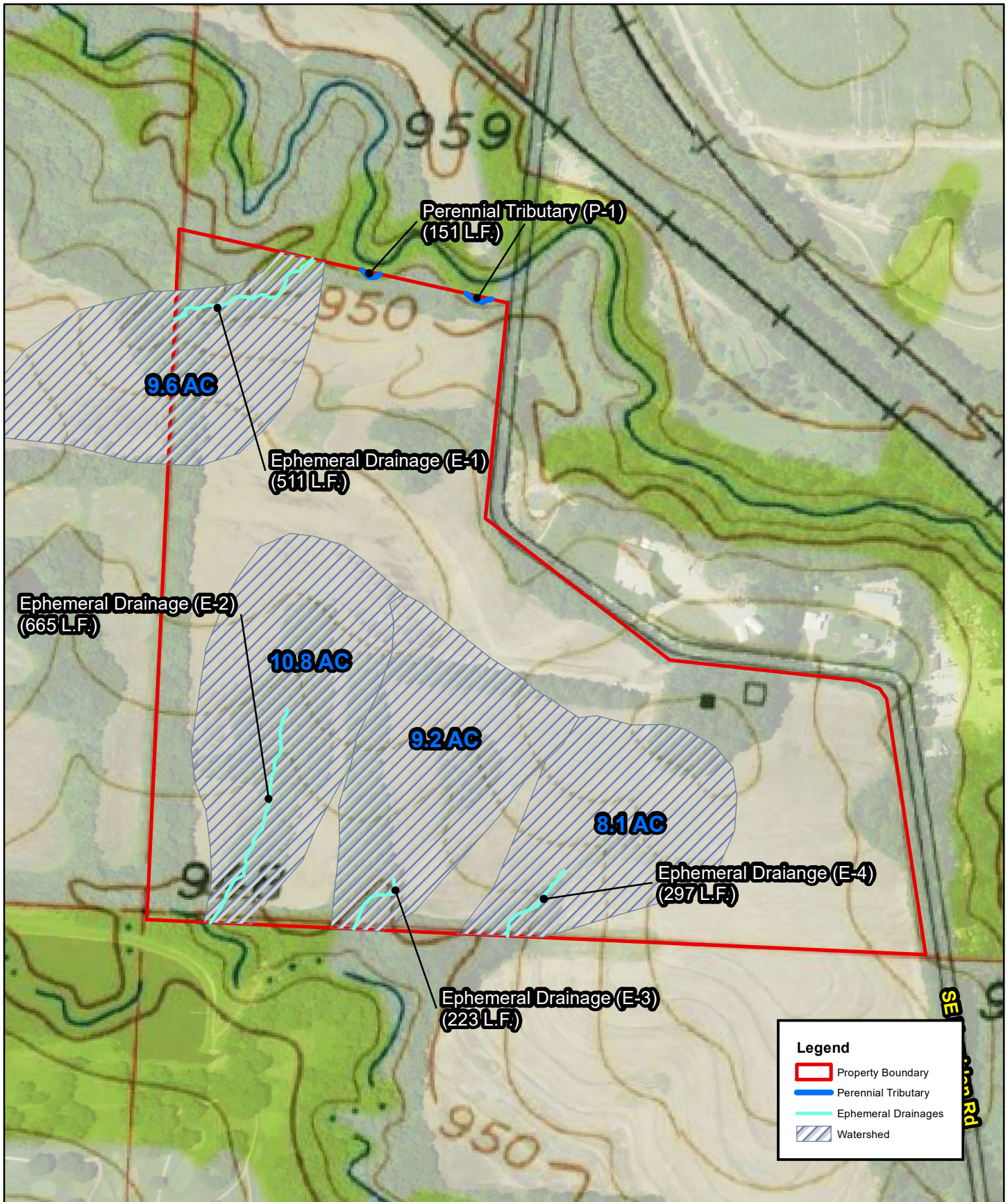
A handwritten signature in dark ink, appearing to read 'Jon Polak', written in a cursive style.

Jonathan L. Polak, P.E.
Environmental Engineer

Enclosures: Watershed Map
 Stream Buffer Setback Map

References:

Kansas City Metropolitan Chapter, American Public Works Association, Standard Specifications & Design Criteria, Section 5600 -Storm Drainage Systems & Facilities, February 16, 2011.



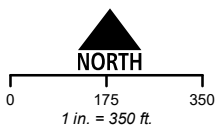
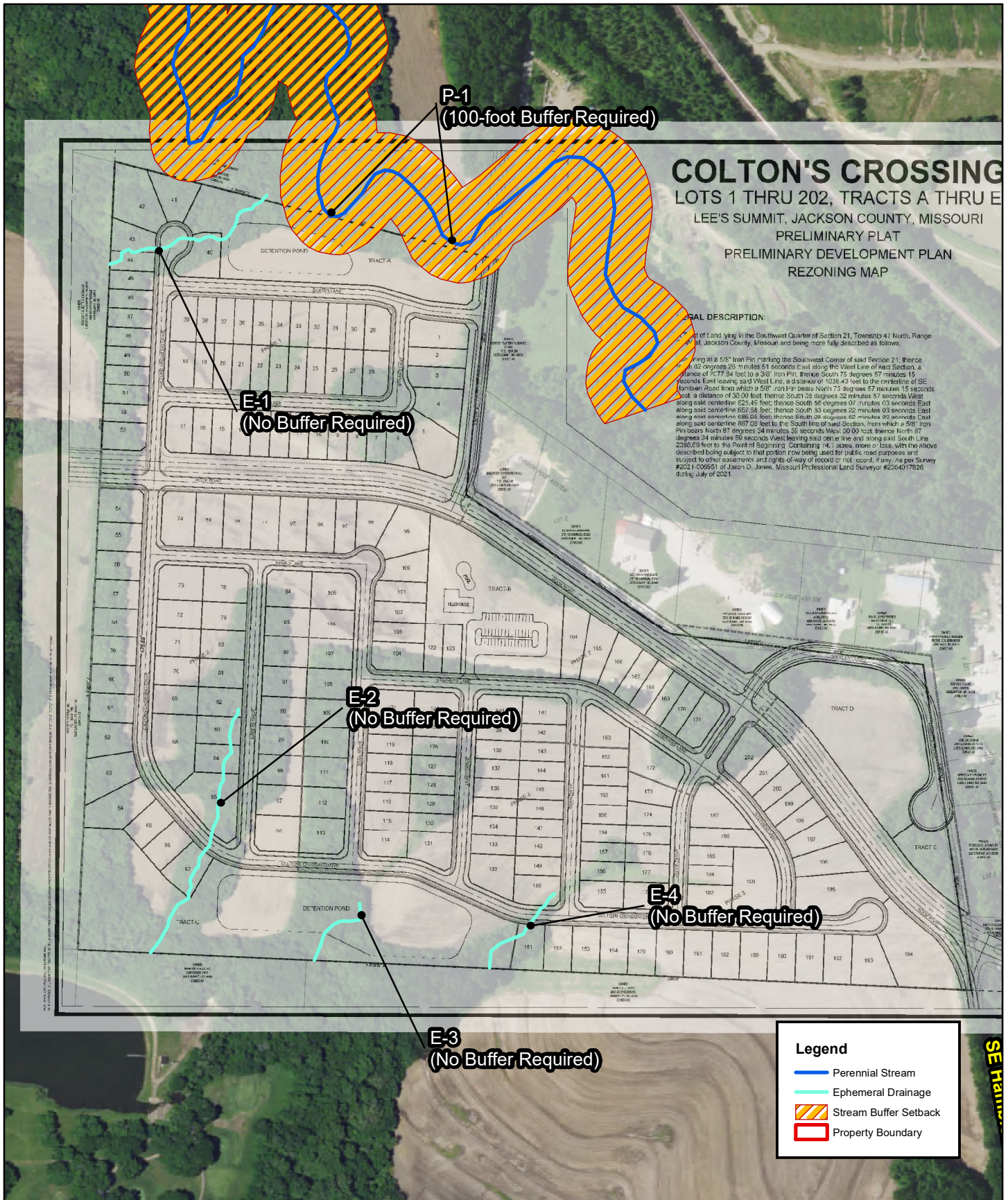
Source: NAIP 2020
 Location: SW 1/4 of Sec 21 - T47N - R31W
 Lee's Summit, Jackson County, MO
 Pleasant Hill, MO 1:24K Quadrangle

WATERSHED MAP

COLTON'S CROSSING DEVELOPMENT
 LEE'S SUMMIT, MISSOURI



Note: Watershed areas were based on the USGS topographic map contours. The watershed basin for Big Creek is not depicted due to scale and broader inclusion of the northern half of the project area.



Source: NAIP 2020
 Location: SW 1/4 of Sec 21 - T47N - R31W
 Lee's Summit, Jackson County, MO
 Pleasant Hill, MO 1:24K Quadrangle

STREAM BUFFER SETBACK
COLTON'S CROSSING DEVELOPMENT
LEE'S SUMMIT, MISSOURI

