

Design Calculations

For

***Summit Orchards
Lee's Summit, Missouri***

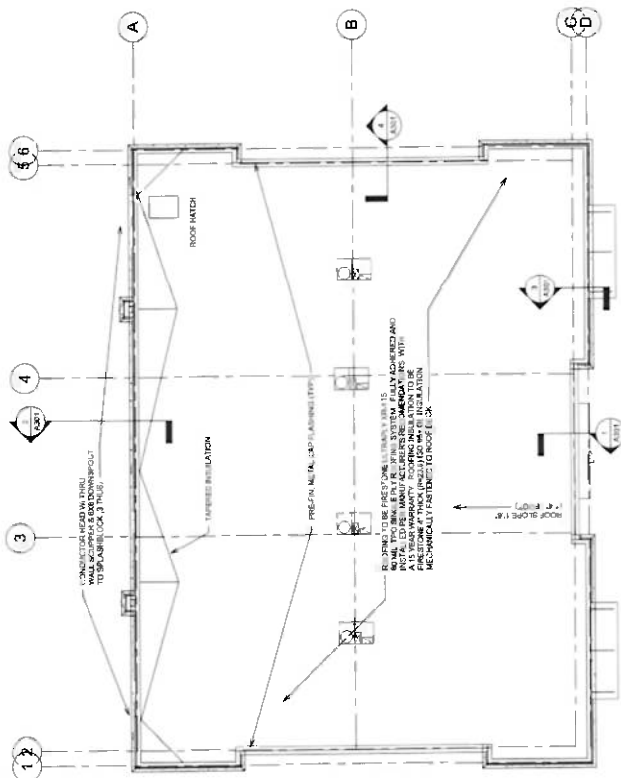
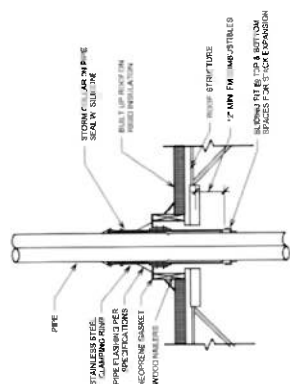
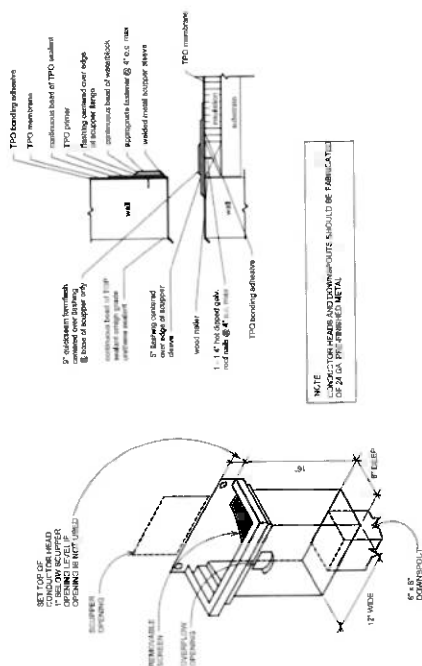
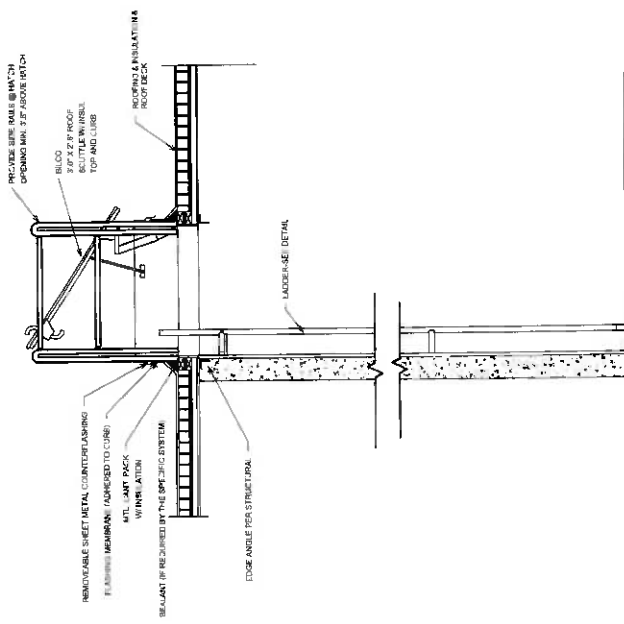
Architect,

Scharhag Architects
6247 Brookside Blvd., Suite #204
Kansas City, Missouri, 64113

Date: May 30, 2025



Joseph A. Towns, RA, PE, SE, AIA, NCARB, LEED AP, BD+C
Missouri Professional Engineer (Structural) #E-22017
Certification Applies to Pages Cover, through 63



6247 Brookside Blvd #204 Kansas City, Mo 64113
 Phone: 816-666-5055 Schraggarchitect@gmail.com

Scharhay
 KENNETH SCHRAH ARCHITECTS

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SUMMIT ORCHARDS

NEW BUILDING FOR
 LEES SUMMIT, MO

LEES SUMMIT, MO
 LEES SUMMIT, MO
 LEES SUMMIT, MO

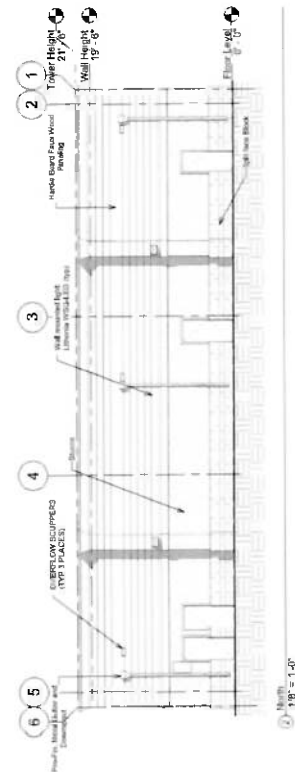
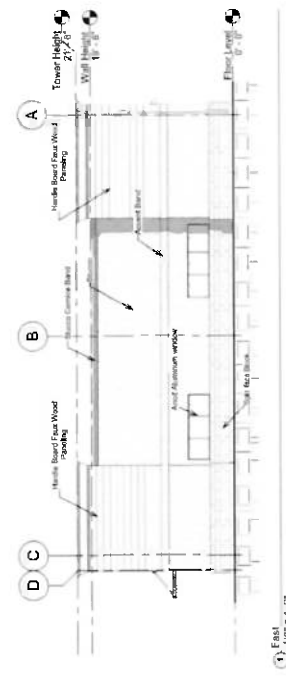
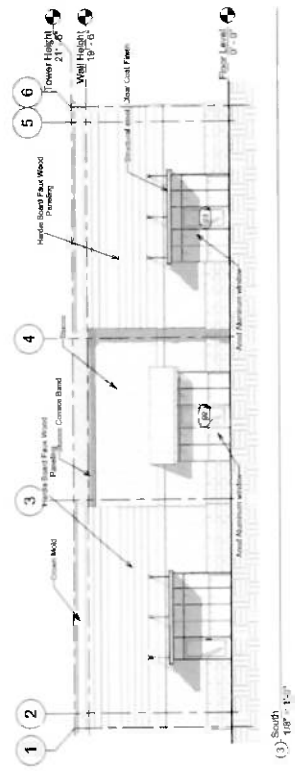
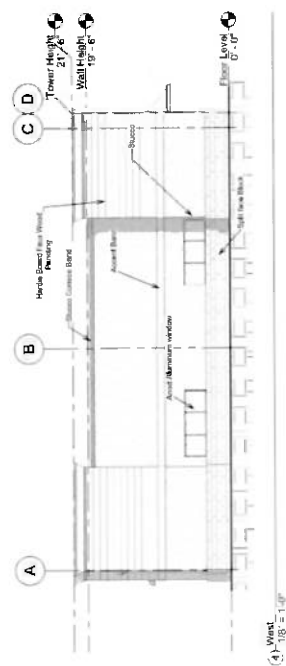
No.	Description	Date
1	Revision Schedule	

Elevations

Project Number: 2491
 Date: 02/15/2025

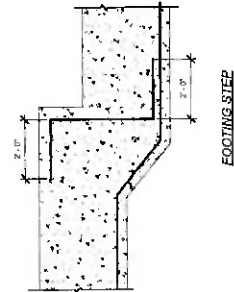
A201

Scale: 1/8" = 1'-0"

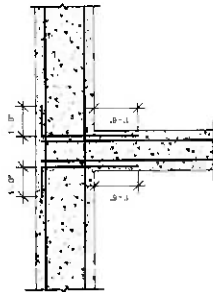


PROVIDE CLEAR SILICONE SEALER FOR BRICK

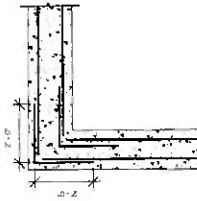
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FOOTING STEP



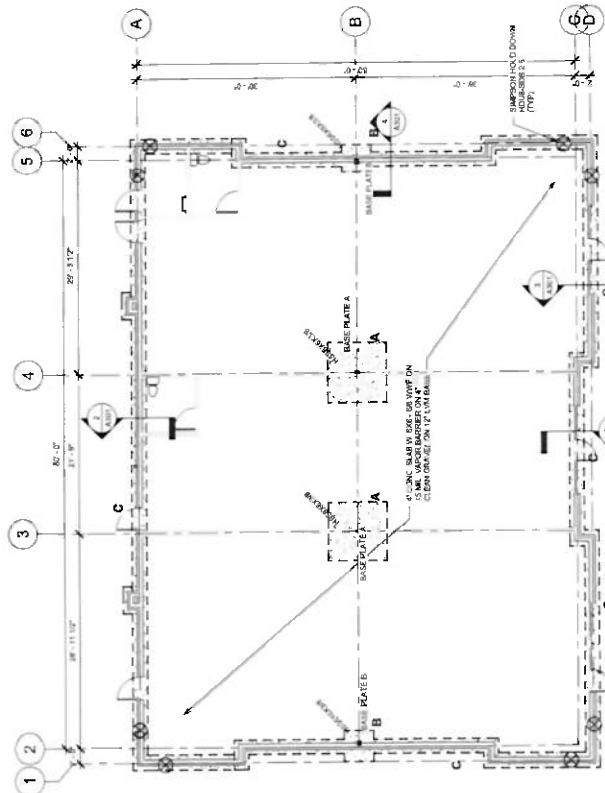
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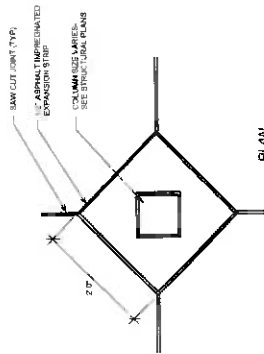
CORNER

⑤ Typical Footing Detail
1/2" = 1'-0"

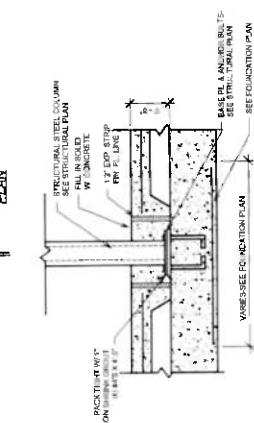
Type Mark	Type	Structural Foundation Schedule	Type Comments
A	8' x 8' x 2'-0" deep	(7) IR's each way	
B	4' x 4' x 2'-0" deep	(5) IR's each way at T.M. w/ (1) IR's each corner	
C	Bearing Footing	2'-0" w x 3'-0" deep w/2 (4) IR's each & 2 IR's @ 38" C	
		1 w/ IR's lower 3' x 3' IR's @ 38" C	



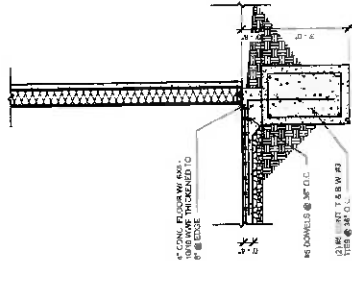
① Foundation Plan
1/8" = 1'-0"



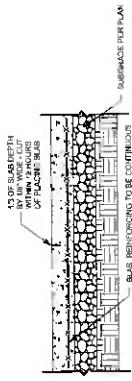
PLAN



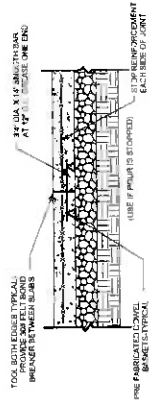
④ Column Detail
1/2" = 1'-0"



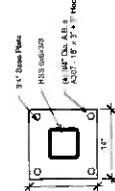
③ Footing Detail
1/2" = 1'-0"



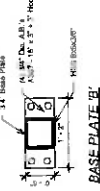
CONTROL JOINT DETAIL



③ Control Joint Detail
1/2" = 1'-0"



BASE PLATE 'A'



BASE PLATE 'B'

② Base Plate Details
1/2" = 1'-0"

Scharhag
 6247 Brookside Blvd., #204 Kansas City, Mo 64113
 Phone 816-655-5055 ScharhagArch@gmail.com

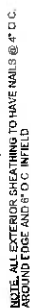
SUMMIT ORCHARDS
 NEW BUILDING FOR
 LEES SUMMIT, MO

Foundation

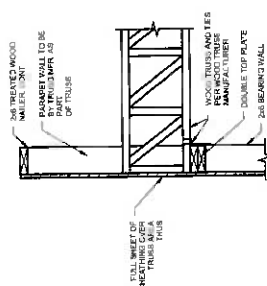
Project number 4891
 Date 02.19.2025

S101

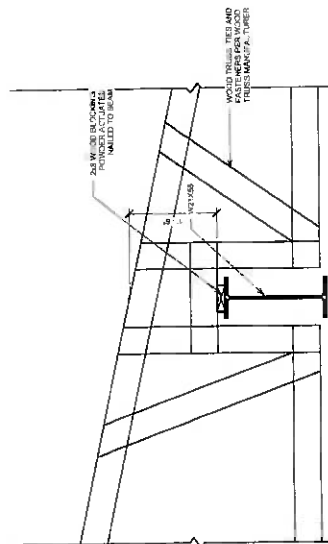
Scale As indicated



5) Typical Exterior sheathing and

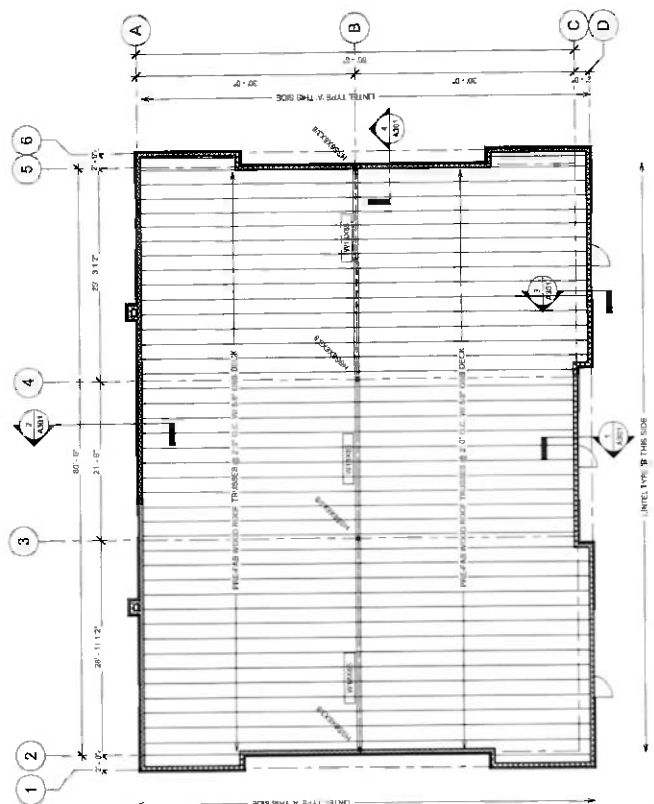


3) typical set in a 1 has beering wood
4" = 1" 1/2"



NOTE: TRUSS ATTACHMENT TO BE SIMPSON H1 CLIPS

4) type of section at inner bearing 2 wood

① Roof Framing Plan
1/8" = 1'-0"

1. THREE LATERAL NOTES TO FORM AN ALL-AROUND PROTECTIVE SHIELD.
2. EXPOSED SURFACES OF THE SHIELD SHALL BE PROTECTED BY A MINIMUM OF TWO LAYERS OF 1/2" THICK PANELS AT ALL LOCATIONS.
3. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
4. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
5. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
6. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
7. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
8. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
9. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.
10. THE SHIELD SHALL BE SECURED TO THE WALLS BY ANCHORS AND BOLTS, AND TO THE FLOOR BY ANCHORS AND BOLTS.

UNITEL SCHEDULE

UNITEL TYPE 'A'	THREE X 179
UNITEL TYPE 'B'	W14026

PROVIDE (4) 226'S BEARING AT EACH END OF UNITEL'S

TRUSSES TO BEAR AT 12'-0" AFF
TRUSSES TO BE 4'-0" DEEP AT NORTH WALL
TRUSSES TO BE 2'-0" DEEP AT SOUTH WALL

SUMMIT ORCHARDS - LOTS 4E-2A & 4E-2B

400 NW CHIPMAN ROAD
LEE'S SUMMIT, JACKSON COUNTY, MISSOURI
SEC. 31-48-31

SEE ADDITIONAL PLANS PREPARED BY OLSON ARCHITECTURAL GROUP ASSOCIATES AND SCHUMAKER ARCHITECTS

MCLAUGHLIN MUELLER INC. HAS SOLE RESPONSIBILITY FOR SHEET SA. HQ CONSULT INC. HAS SOLE RESPONSIBILITY FOR SHEET 35.
 14000 N. CENTRAL AVE. SUITE 500, BETHESDA, MD 20814



Engineering Primary
Ronald L. Cooper PE
781-4200

Engineering Alternates
Art Altm, PE
781-4230

CITY OF LOS ANGELES WATER UTILITIES PUBLIC UTILITIES	DOUG MUEGER	(310) 296-1126
	MARK SCHAUER	(310) 966-1930
	FLOR DIZENDENTE	(310) 347-4118
	BRIAN JONES	(310) 399-0633
	MARY LOPPE MARK MATHIAS	(310) 215-1550 (310) 325-6416
CHARLES CANNON ST	BARBARA BROWN	(310) 785-2545

NOTE: Contractor shall be responsible for determining the exact locations of all underground utilities or appurtenances prior to commencing construction. Existing underground utility shapes on the drawings are for reference only, and their accuracy and completeness are not guaranteed. Contractor shall be responsible for repair or replacement of all underground utilities damaged during construction.

I hereby certify that this project has been designed, and these plans prepared, to meet or exceed the design criteria of City of Lee's Summit, Missouri, in current usage, except as indicated below.

Exceptions:

DATE: _____

☒	FOR PERMIT
☐	FOR CONSTRUCTION

I have not been retained to coordinate as-built drawings for

[illegible]

Ronald L. Conner, PE
AGC Engineers, Inc.

AGC Engineers, Inc.

403 S. Leonard St., Suite D
Liberty, Missouri 64068
www.agcengineers.com
816.781.4200 ■
fax 792.3666



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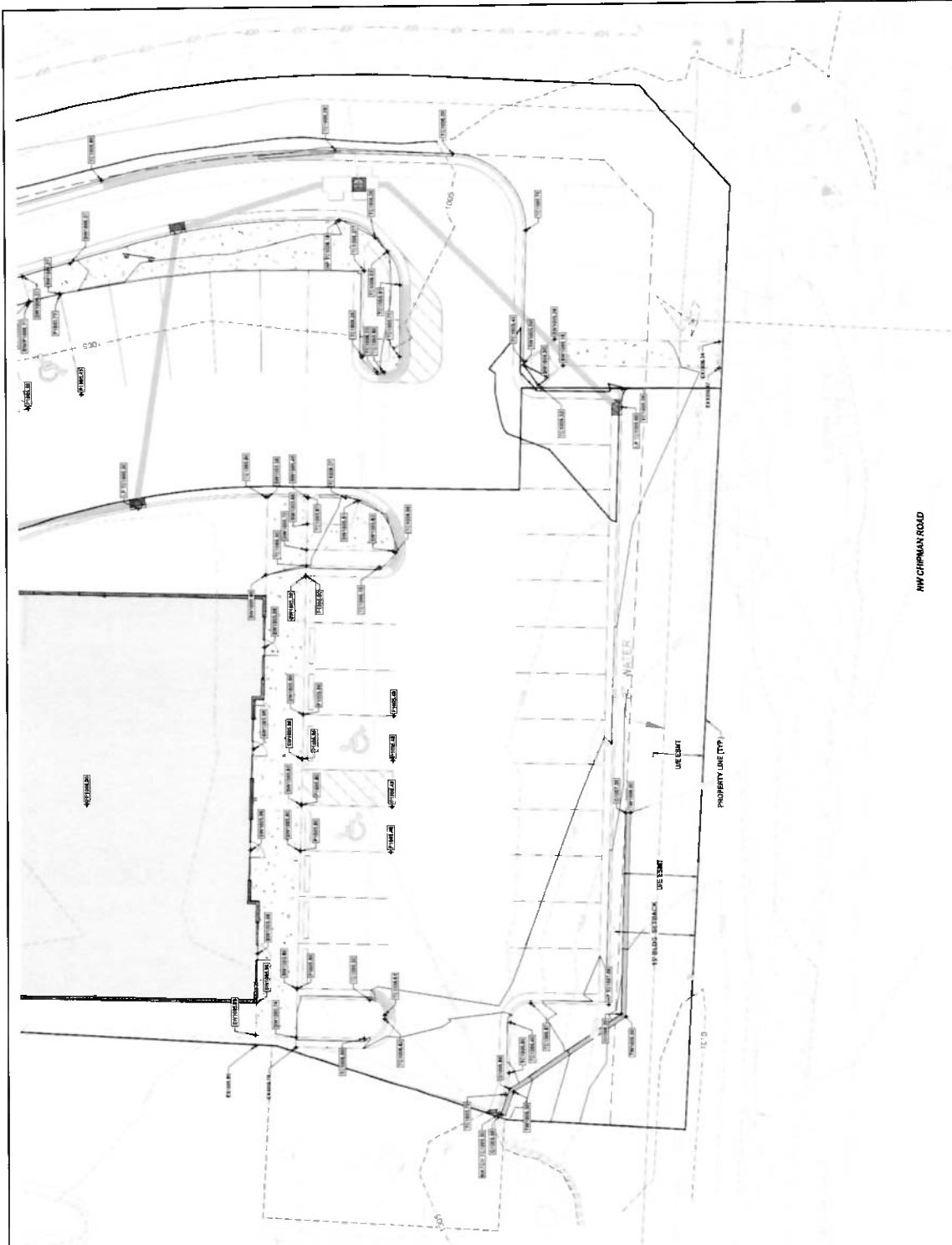




LEGEND

	EXISTING GROUND ELEVATION
	PROPOSED GROUND ELEVATION
	EXISTING PAVEMENT ELEVATION
	PROPOSED PAVEMENT ELEVATION
	TOP OF CURB ELEVATION
	TOP OF WALL ELEVATION
	LOW POINT
	HIGH POINT
	STORMWATER ELEVATION
	BASE OF WALL ELEVATION
	BASE OF CURB ELEVATION
	FINISHED FLOOR
	EXISTING CURB AND GUTTER
	PROPOSED CURB AND GUTTER
	RAMP
	LANDING
	TRANSITION
	GRADE BREAK

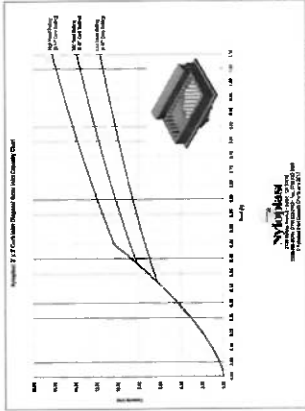
	SUMMIT ORCHARDS - SWIG LEE'S SUMMIT, JACKSON COUNTY, MISSOURI	
	SITE DEVELOPMENT PLANS SPOT ELEVATION PLAN	
401 S. Leonard St., Suite D Liberty, Missouri 64068 816.781.4200 Fax 792.3666 www.agcengineers.com		
		DATE: _____ 2-1-20
REVIEW: _____ DATE: _____		15



LEGEND	
	ZONE
	EXISTING GROUND ELEVATION
	PROPOSED
	SURFACE ELEVATION
	PAVEMENT ELEVATION
	TOP OF CURVE ELEVATION
	TOP OF WALL ELEVATION
	LOW POINT
	HIGH POINT
	VERTICAL ELEVATION
	HORIZONTAL ELEVATION
	VERTICALITY OF CURVE
	VERTICALITY OF PAVEMENT
	PROPOSED ELEVATION
	C&G CENTER AND OUTER
	C&G MODIFIED CURVE AND OUTER
	RAMP
	LANDING
	TRANSITION
	SHADE AREA

		SUMMIT ORCHARDS - SWIG LEE'S SUMMIT, JACKSON COUNTY, MISSOURI	
		SITE DEVELOPMENT PLANS SPOT ELEVATION PLAN	
AGC Engineers, Inc. 485 S. Leonard St., Suite D Liberty, Missouri 64068 816.781.4200 Fax: 792.3666 www.agcengineers.com		8	
DATE: _____ REVISION: _____ 2-17-23		FOR REVIEW	

16



CURB INLET DESIGN TABLE

Return Frequency: 10 yr

Area	Area A	Area B	Area C	Area D	Area E	Area F	Area G	Area H	Area I	Area J	Area K	Area L	Area M	Area N	Area O	Area P	Area Q	Area R	Area S	Area T	Area U	Area V	Area W	Area X	Area Y	Area Z
Area A	3396 SF																									
Area B		6342 SF																								
Area C			5300 SF																							
Area D				5074 SF																						
Area E					12350 SF																					
Area F						2275 SF																				

ROOF DRAIN DESIGN TABLE

Return Frequency: 10 yr

Area	Area A	Area B	Area C	Area D	Area E	Area F	Area G	Area H	Area I	Area J	Area K	Area L	Area M	Area N	Area O	Area P	Area Q	Area R	Area S	Area T	Area U	Area V	Area W	Area X	Area Y	Area Z
Area A	3396 SF																									
Area B		6342 SF																								
Area C			5300 SF																							
Area D				5074 SF																						
Area E					12350 SF																					
Area F						2275 SF																				

PIPE DESIGN TABLE

Return Frequency: 10 yr

Area	Area A	Area B	Area C	Area D	Area E	Area F	Area G	Area H	Area I	Area J	Area K	Area L	Area M	Area N	Area O	Area P	Area Q	Area R	Area S	Area T	Area U	Area V	Area W	Area X	Area Y	Area Z
Area A	3396 SF																									
Area B		6342 SF																								
Area C			5300 SF																							
Area D				5074 SF																						
Area E					12350 SF																					
Area F						2275 SF																				

PIPE DESIGN TABLE

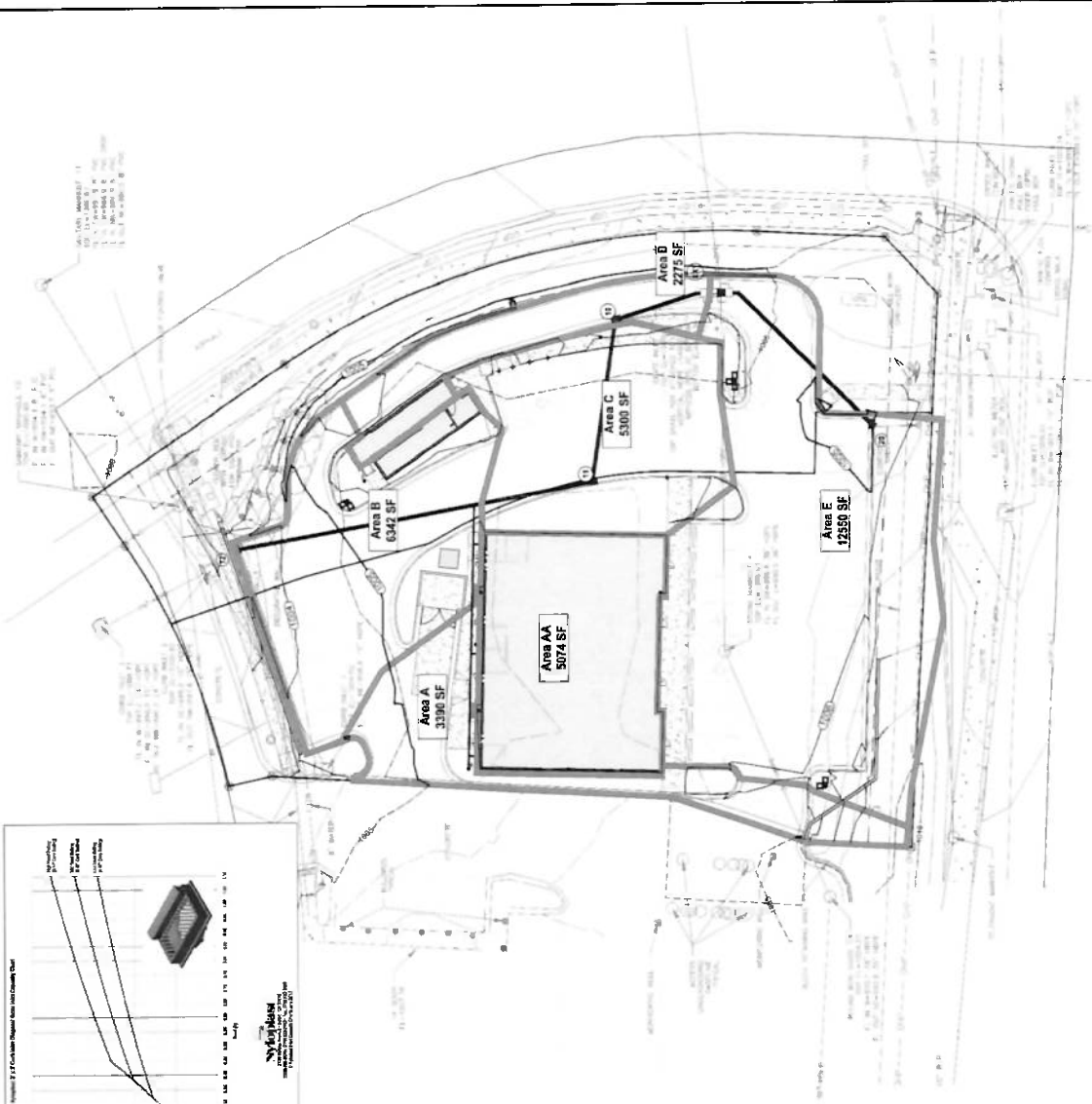
Return Frequency: 10 yr

Area	Area A	Area B	Area C	Area D	Area E	Area F	Area G	Area H	Area I	Area J	Area K	Area L	Area M	Area N	Area O	Area P	Area Q	Area R	Area S	Area T	Area U	Area V	Area W	Area X	Area Y	Area Z
Area A	3396 SF																									
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PIPE DESIGN TABLE

Return Frequency: 10 yr

Area	Area A	Area B	Area C	Area D	Area E	Area F	Area G	Area H	Area I	Area J	Area K	Area L	Area M	Area N	Area O	Area P	Area Q	Area R	Area S	Area T	Area U	Area V	Area W	Area X	Area Y	Area Z
Area A	3396 SF																									
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Area F						2275 SF																				



AGC Engineers, Inc.

405 S. Leonard St., Suite D
Liberty, Missouri 64068
816.781.4000
Fax 816.781.4066
www.agcengineers.com

Summit Orchards - SWIG

Lee's Summit, Jackson County, Missouri

Site Development Plans

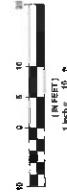
Drainage Area Map & Calcs

DATE: _____

REVISION: _____

2-10-22

17



- A DOMESTIC WATER INLET (RE MEP)
- B 1" DOMESTIC WATER LINE (CONFORM WITH MEP REQUIREMENTS AND WATER MAIN ALLOCATION)
- C 1" WATER METER AND METER PIT
- D GAS ENTRY (RE MEP)
- E GAS LINE (RE GAS OR MEP FOR SIZE AND MATERIAL)
- F SANITARY SEWER ENTRY (RE MEP)
- G 8" SANITARY SEWER LINE (3% MIN. SLOPE)
- H CLEANOUT
- I PHONE DATA SERVICE ENTRY (RE ARCH)
- J ELECTRICAL TRANSFORMER (RE MEP)
- K DOWNPOUT (RE ARCH) (SEE CONDUIT RAMP DETAIL)
- L 6" PVC DOWNPOUT/STORM LINE
- M ELECTRICAL ENTRY
- N INFORMATIONAL ENTRY (RE MEP)

2-17-33

SUMMIT ORCHARDS - SWIG LEE'S SUMMIT, JACKSON COUNTY, MISSOURI	10
SITE DEVELOPMENT PLANS UTILITY PLAN	



AGC Engineers, Inc.

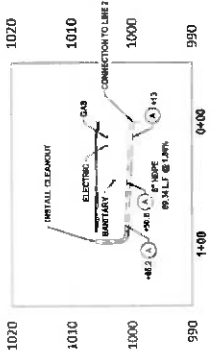
NOTE:

1. CONTRACTOR SHALL COORDINATE WITH ALL AFFECTED UTILITIES TO VERIFY DEPTHS, LOCATIONS, AND MATERIALS. ALL UTILITIES SHALL BE PROTECTED AND UNDERGROUND UTILITIES TO VERIFY DEPTHS. CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS.
2. SANITARY TRENCH CROSSING WATER MAINS SHALL BE INSTALLED WITH A MINIMUM 18" CLEARANCE FROM THE BOTTOM OF THE WATER MAIN. THE TRENCH SHALL BE FILL WITH CONCRETE AND SHALL BE PROTECTED BY A 12" THICK CONCRETE SLAB. THE TRENCH SHALL BE FILL WITH CONCRETE AND SHALL BE PROTECTED BY A 12" THICK CONCRETE SLAB.

KEY LEGEND

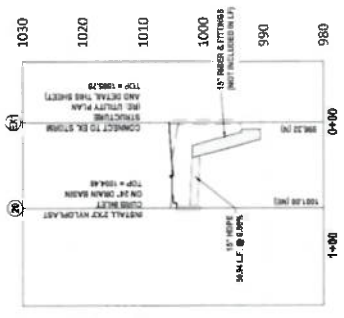
① DOWNHOLE CONNECTION

LINE 4

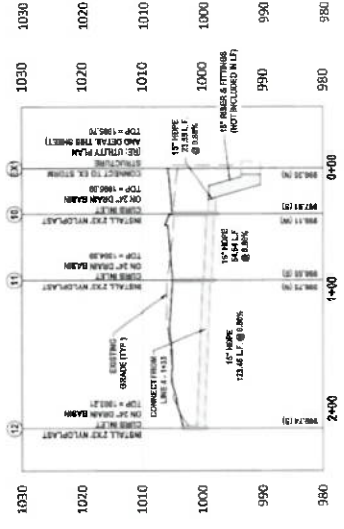


LINE 3 NOT USED

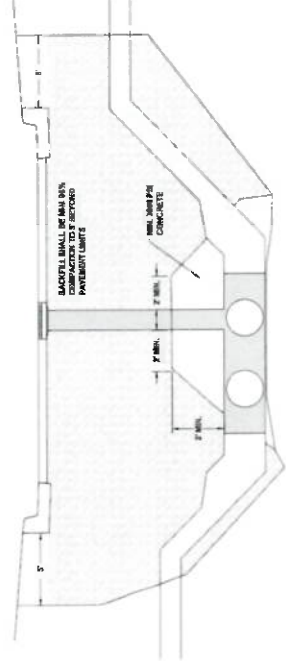
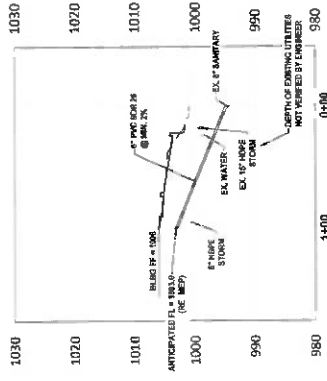
LINE 2



LINE 1



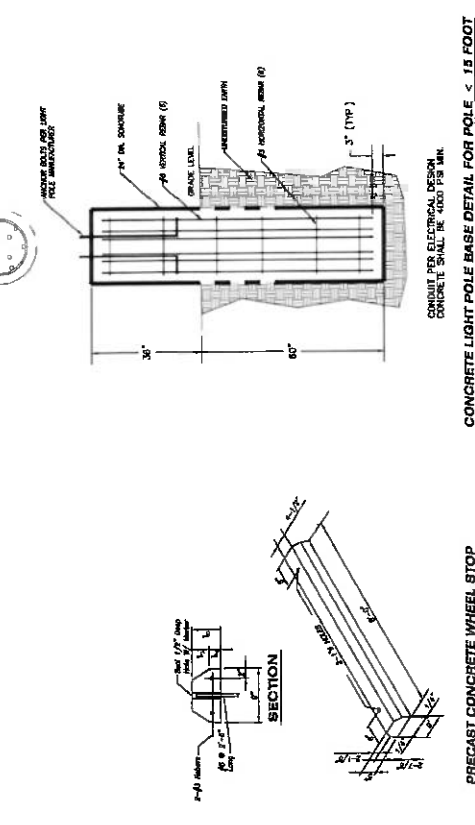
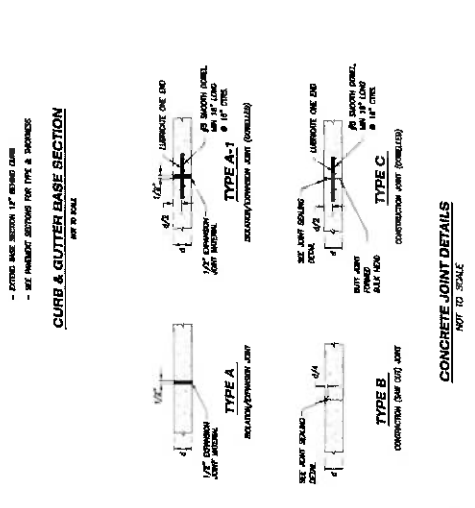
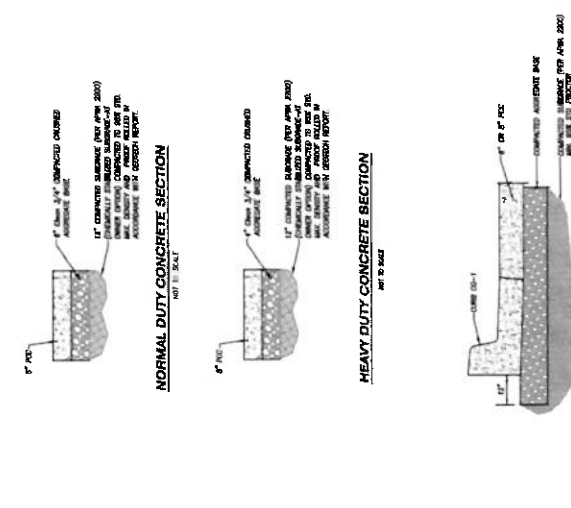
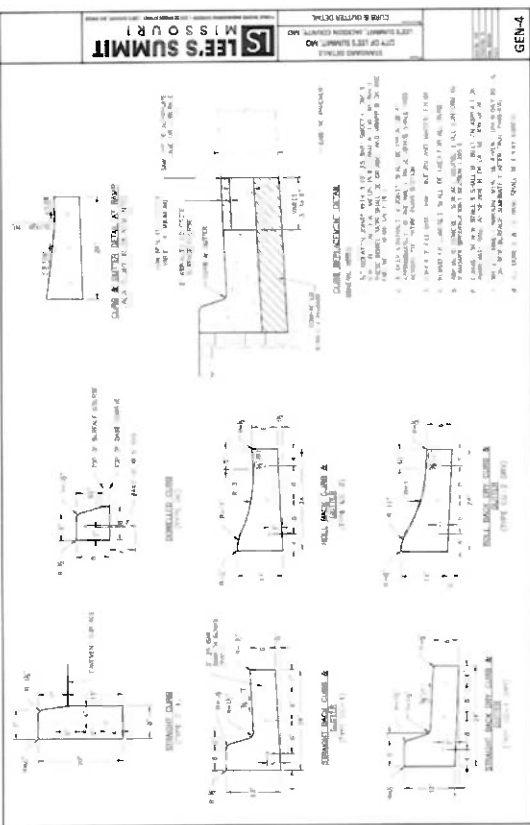
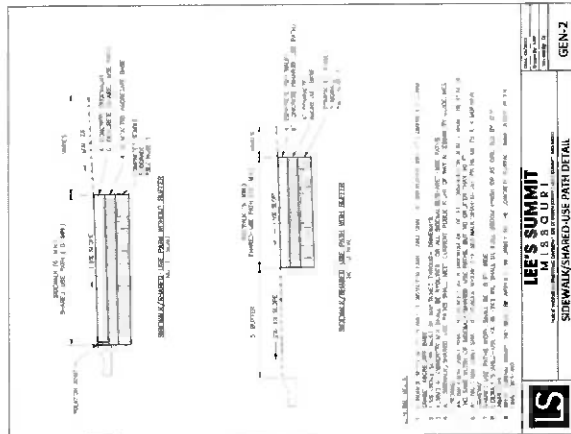
LINE A



CONNECTION TO EXISTING STORM STRUCTURE

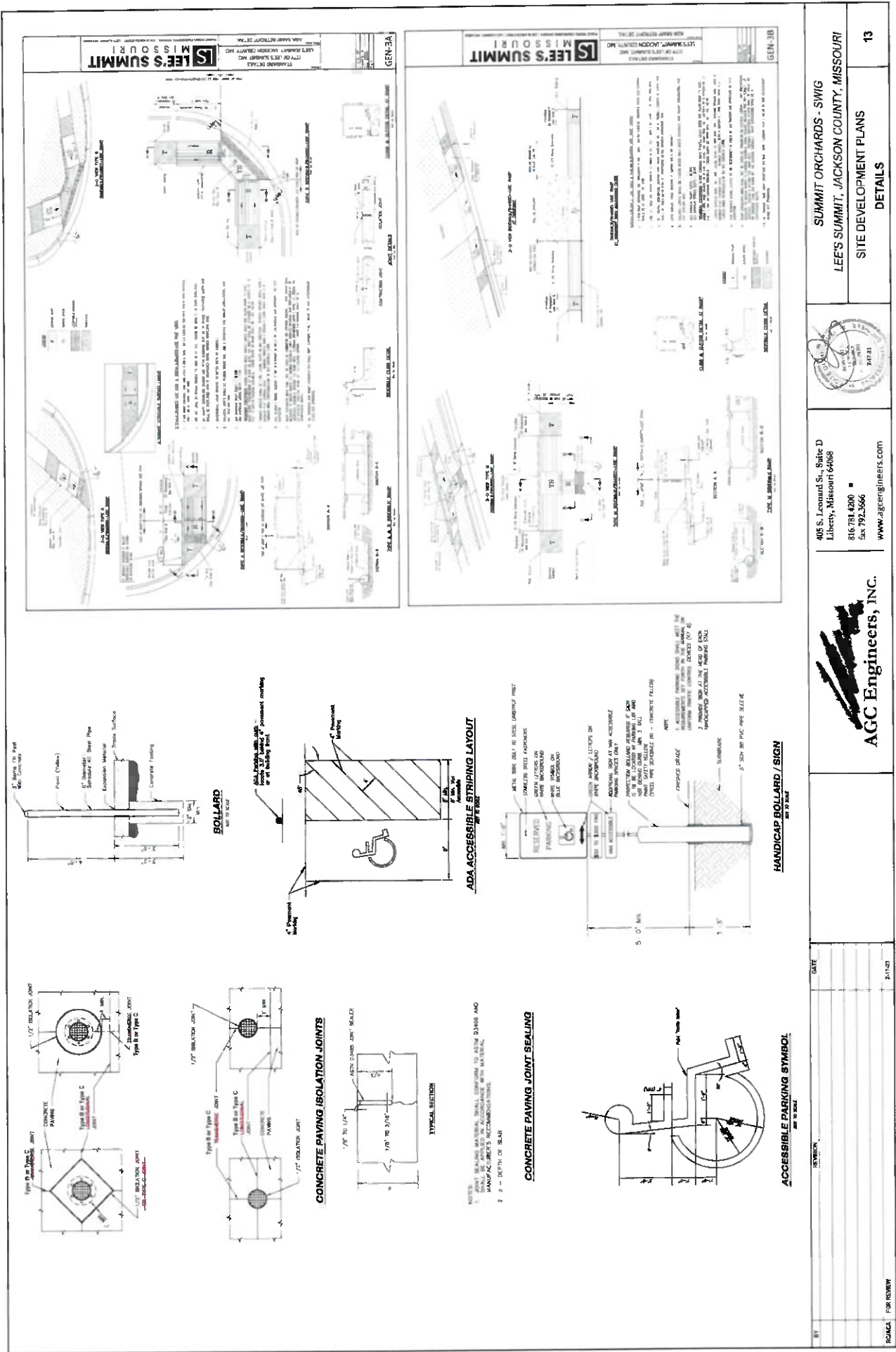
		485 S. Leonard St., Suite D Liberty, Missouri 64068 816.731.4000 Fax 792.3666 www.agcengineers.com		SUMMIT ORCHARDS - SWIG LEE'S SUMMIT, JACKSON COUNTY, MISSOURI SITE DEVELOPMENT PLANS UTILITY PROFILES	11
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19

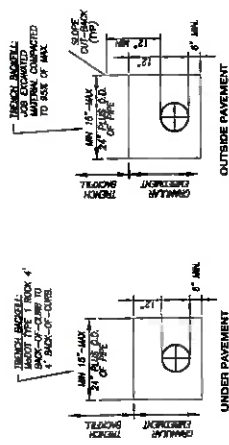


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20

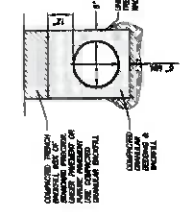


12

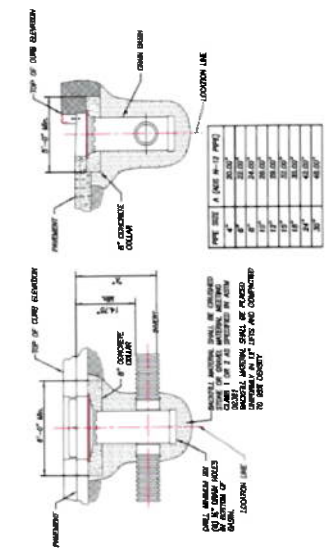


EMBEDMENT AND BACKFILL FOR SANITARY SEWERS

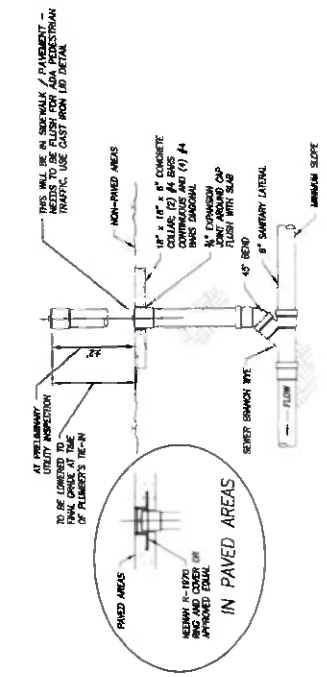
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4. EMBEDMENT SHALL BE 12" MIN. DEEP. THE EMBEDMENT SHALL BE 12" MIN. DEEP. THE EMBEDMENT SHALL BE 12" MIN. DEEP.



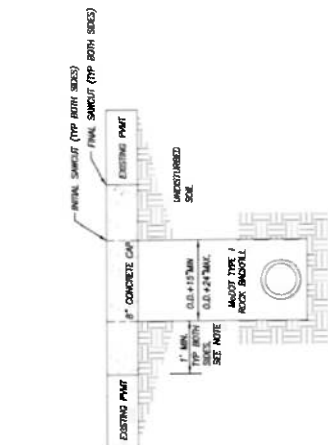
HDPE (HIGH DENSITY POLYETHYLENE) PIPE INSTALLATION DETAIL



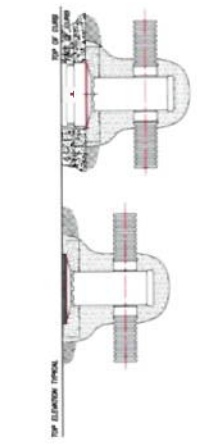
NYLOPLAST DRAIN BASIN - TYPICAL INSTALLATION



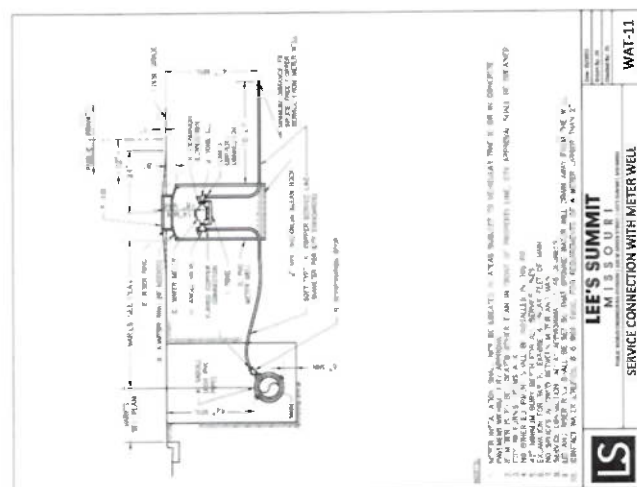
CLEAN-OUT DETAIL



STREET CROSSING RESTORATION DETAIL



CONSTRUCTION STAKING DETAIL - NYLOPLAST CURB INLET / DRAIN BASIN



LEE'S SUMMIT MISSOURI
SERVICE CONNECTION WITH METER WELL

WAT-11

405 S. Leonard St., Suite D Liberty, Missouri 64068 816.781.4200 Fax 792.5666 www.agcengineers.com	AGC Engineers, Inc.	SUMMIT ORCHARDS - SWIG LEE'S SUMMIT, JACKSON COUNTY, MISSOURI SITE DEVELOPMENT PLANS DETAILS
DATE	REVISION	14

Site plan showing building layout, parking areas, and surrounding terrain with annotations. Includes a north arrow and a scale bar. The plan shows a building with a parking lot and a road. The terrain is indicated by contour lines. The plan is titled 'Site Plan' and includes a legend for symbols used.

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DATE	
21743	

465 S. Leonard St., Suite D
Liberty, Missouri 64068
916.781.4200
fax 792.3666
www.agcengineers.com

SUMMIT ORCHARDS - SWIG
LEE'S SUMMIT, JACKSON COUNTY, MISSOURI

SITE DEVELOPMENT PLANS
DETAILS

15

Loads and Codes

TABLE 1607.1
MINIMUM UNIFORMLY DISTRIBUTED LIVE LOADS, L_u
AND MINIMUM CONCENTRATED LIVE LOADS^a

OCCUPANCY OR USE	UNIFORM (psf)	CONCENTRATED (pounds)
1. Apartments (see residential)	—	—
2. Access floor systems		
Office use	50	2,000
Computer use	100	2,000
3. Armories and drill rooms	150 ^a	—
4. Assembly areas		
Fixed seats (fastened to floor)	60 ^a	—
Follow spot, projections and control rooms	50	—
Lobbies	100 ^{ab}	—
Movable seats	100 ^a	—
Stage floors	150 ^a	—
Platforms (assembly)	100 ^{ab}	—
Other assembly areas	100 ^{ab}	—
5. Balconies and decks ^b	1.5 times the live load for the area served, not required to exceed 100	—
6. Catwalks	40	300
7. Corbices	60	—
8. Corridors		
First floor	100	—
Other floors	Same as occupancy served except as indicated	—
9. Dining rooms and restaurants	100 ^{ab}	—
10. Dwellings (see residential)	—	—
11. Elevator machine room and controlroom grating (on area of 2 inches by 2 inches)	—	300
12. Finish light floor plate construction (on area of 1 inch by 1 inch)	—	200
13. Fire escapes	100	—
On single-family dwellings only	40	—
14. Garages (passenger vehicles only)	40 ^c	Note a
Trucks and buses	See Section 1607.7	
15. Handrails, guards and grab bars	See Section 1607.8	
16. Helipads	See Section 1607.6	
17. Hospitals		
Corridors above first floor	80	1,000
Operating rooms, laboratories	60	1,000
Patient rooms	40	1,000
18. Hotels (see residential)	—	—
19. Libraries		
Corridors above first floor	80	1,000
Reading rooms	60	1,000
Stack rooms	150 ^{a, d}	1,000
20. Manufacturing		
Heavy	250 ^a	3,000
Light	125 ^a	2,000
21. Marquees, except one- and two-family dwellings	75	—
22. Office buildings		
Corridors above first floor	80	2,000
File and computer rooms shall be designed for heavier loads based on anticipated occupancy	—	—
Lobbies and first-floor corridors	100	2,000
Offices	50	2,000

(continued)

TABLE 1607.1—continued
MINIMUM UNIFORMLY DISTRIBUTED LIVE LOADS, L_u
AND MINIMUM CONCENTRATED LIVE LOADS^a

OCCUPANCY OR USE	UNIFORM (psf)	CONCENTRATED (pounds)
23. Penal institutions		
Cell blocks	40	—
Corridors	100	—
24. Recreational uses:		
Bowling alleys, poolrooms and similar uses	75 ⁽¹⁾	—
Dance halls and ballrooms	100 ^{ab}	—
Gymnasiums	100 ^{ab}	—
Ice skating rink	250 ^a	—
Reviewing stands, grandstands and bleachers	100 ^{a, c, d}	—
Roller skating rink	100 ^{ab}	—
Stadiums and arenas with fixed seats (fastened to floor)	60 ^{a, c, d}	—
25. Residential		
One- and two-family dwellings		
Uninhabitable attics without storage	10	—
Uninhabitable attics with storage ^{a, c, d}	20	—
Habitable attics and sleeping areas ^b	30	—
Canopies, including marquees	20	—
All other areas	40	—
Hotels and multifamily dwellings		
Private rooms and corridors serving them	40	—
Public rooms and corridors serving them	100	—
26. Roofs		
All roof surfaces subject to maintenance workers		300
Awnings and canopies:		
Fabric construction supported by a skeleton structure	5 ^{ab}	—
All other construction, except one- and two-family dwellings	20	—
Ordinary flat, pitched, and curved roofs (that are not occupiable)	20	—
Primary roof members exposed to a work floor		
Single panel point of lower chord of roof trusses or any point along primary structural members supporting roofs over manufacturing, storage warehouses, and repair garages		2,000
All other primary roof members		300
Occupiable roofs:		
Roof gardens	100	—
Assembly areas	100 ^{ab}	—
All other similar areas	Note 1	Note 1
27. Schools		
Classrooms	40	1,000
Corridors above first floor	80	1,000
First-floor corridors	100	1,000
28. Scuttles, skylight ribs and accessible ceilings	—	200
29. Sidewalks, vehicular driveways and yards, subject to trucking	250 ^{a, b}	8,000 ^a
30. Stairs and exits		
One- and two-family dwellings	40	300 ^f
All other	100	300 ^f

(continued)

TABLE 1607.1—continued
MINIMUM UNIFORMLY DISTRIBUTED LIVE LOADS, L_u
AND MINIMUM CONCENTRATED LIVE LOADS^a

OCCUPANCY OR USE	UNIFORM (psf)	CONCENTRATED (pounds)
31. Storage warehouses (shall be designed for heavier loads if required for anticipated storage)		—
Heavy	250 ^b	
Light	125 ^b	
32. Stores		
Retail		
First floor	100	1,000
Upper floors	75	1,000
Wholesale, all floors	125 ^b	1,000
33. Vehicle barriers	See Section 1607.9	
34. Walkways and elevated platforms (other than exitways)	60	—
35. Yards and terraces, pedestrians	100 ^a	—

For SI: 1 inch = 25.4 mm, 1 square inch = 645.16 mm².

1 square foot = 0.0929 m², 1 pound per square foot = 0.0479 kN/m².

1 pound = 0.004448 kN, 1 pound per cubic foot = 16 kg/m³.

- Floors in garages or portions of buildings used for the storage of motor vehicles shall be designed for the uniformly distributed live loads of this table or the following concentrated loads: (1) for garages restricted to passenger vehicles accommodating not more than nine passengers, 3,000 pounds acting on an area of 4 1/2 inches by 4 1/2 inches; (2) for mechanical parking structures without slab or deck that are used for storing passenger vehicles only, 2,250 pounds per wheel.
- The loading applies to stack room floors that support nonmobile, double-faced library book stacks, subject to the following limitations:
 - The nominal book stack unit height shall not exceed 90 inches.
 - The nominal shelf depth shall not exceed 12 inches for each face.
 - Parallel rows of double-faced book stacks shall be separated by aisles not less than 36 inches wide.
- Design in accordance with ICC 300.
- Other uniform loads in accordance with an approved method containing provisions for truck loadings shall be considered where appropriate.
- The concentrated wheel load shall be applied on an area of 4.5 inches by 4.5 inches.
- The minimum concentrated load on stair treads shall be applied on an area of 2 inches by 2 inches. This load need not be assumed to act concurrently with the uniform load.
- Where snow loads occur that are in excess of the design conditions, the structure shall be designed to support the loads due to the increased loads caused by drift buildup or a greater snow design determined by the building official (see Section 1608).
- See Section 1604.8.3 for decks attached to exterior walls.
- Uninhabitable attics without storage are those where the maximum clear height between the joists and rafters is less than 42 inches, or where there are not two or more adjacent trusses with web configurations capable of accommodating an assumed rectangle 42 inches in height by 24 inches in width, or greater, within the plane of the trusses. This live load need not be assumed to act concurrently with any other live load requirements.
- Uninhabitable attics with storage are those where the maximum clear height between the joists and rafters is 42 inches or greater, or where there are two or more adjacent trusses with web configurations capable of accommodating an assumed rectangle 42 inches in height by 24 inches in width, or greater, within the plane of the trusses.

The live load need only be applied to those portions of the joists or truss bottom chords where both of the following conditions are met:

- The attic area is accessible from an opening not less than 20 inches in width by 30 inches in length that is located where the clear height in the attic is not less than 30 inches.
- The slopes of the joists or truss bottom chords are not greater than two units vertical in 12 units horizontal.

The remaining portions of the joists or truss bottom chords shall be designed for a uniformly distributed concurrent live load of not less than 10 pounds per square foot.

(continued)

TABLE 1607.1—continued
MINIMUM UNIFORMLY DISTRIBUTED LIVE LOADS, L_u
AND MINIMUM CONCENTRATED LIVE LOADS^a

- Attic spaces served by stairways other than the pull-down type shall be designed to support the minimum live load specified for habitable attics and sleeping rooms.
- Areas of occupiable roofs, other than roof gardens and assembly areas, shall be designed for appropriate loads as approved by the building official. Unoccupied landscaped areas of roofs shall be designed in accordance with Section 1607.13.3.
- Live load reduction is not permitted.
- Live load reduction is only permitted in accordance with Section 1607.11.1.2 or Item 1 of Section 1607.11.2.
- Live load reduction is only permitted in accordance with Section 1607.11.1.3 or Item 2 of Section 1607.11.2.

1607.6 Helipads. Helipads shall be designed for the following live loads:

- A uniform live load, L , as specified in Items 1.1 and 1.2. This load shall not be reduced.
 - 40 psf (1.92 kN/m²) where the design basis helicopter has a maximum take-off weight of 3,000 pounds (13.35 kN) or less.
 - 60 psf (2.87 kN/m²) where the design basis helicopter has a maximum take-off weight greater than 3,000 pounds (13.35 kN).
- A single concentrated live load, L , of 3,000 pounds (13.35 kN) applied over an area of 4.5 inches by 4.5 inches (114 mm by 114 mm) and located so as to produce the maximum load effects on the structural elements under consideration. The concentrated load is not required to act concurrently with other uniform or concentrated live loads.
- Two single concentrated live loads, L , 8 feet (2438 mm) apart applied on the landing pad (representing the helicopter's two main landing gear, whether skid type or wheeled type), each having a magnitude of 0.75 times the maximum take-off weight of the helicopter, and located so as to produce the maximum load effects on the structural elements under consideration. The concentrated loads shall be applied over an area of 8 inches by 8 inches (203 mm by 203 mm) and are not required to act concurrently with other uniform or concentrated live loads.

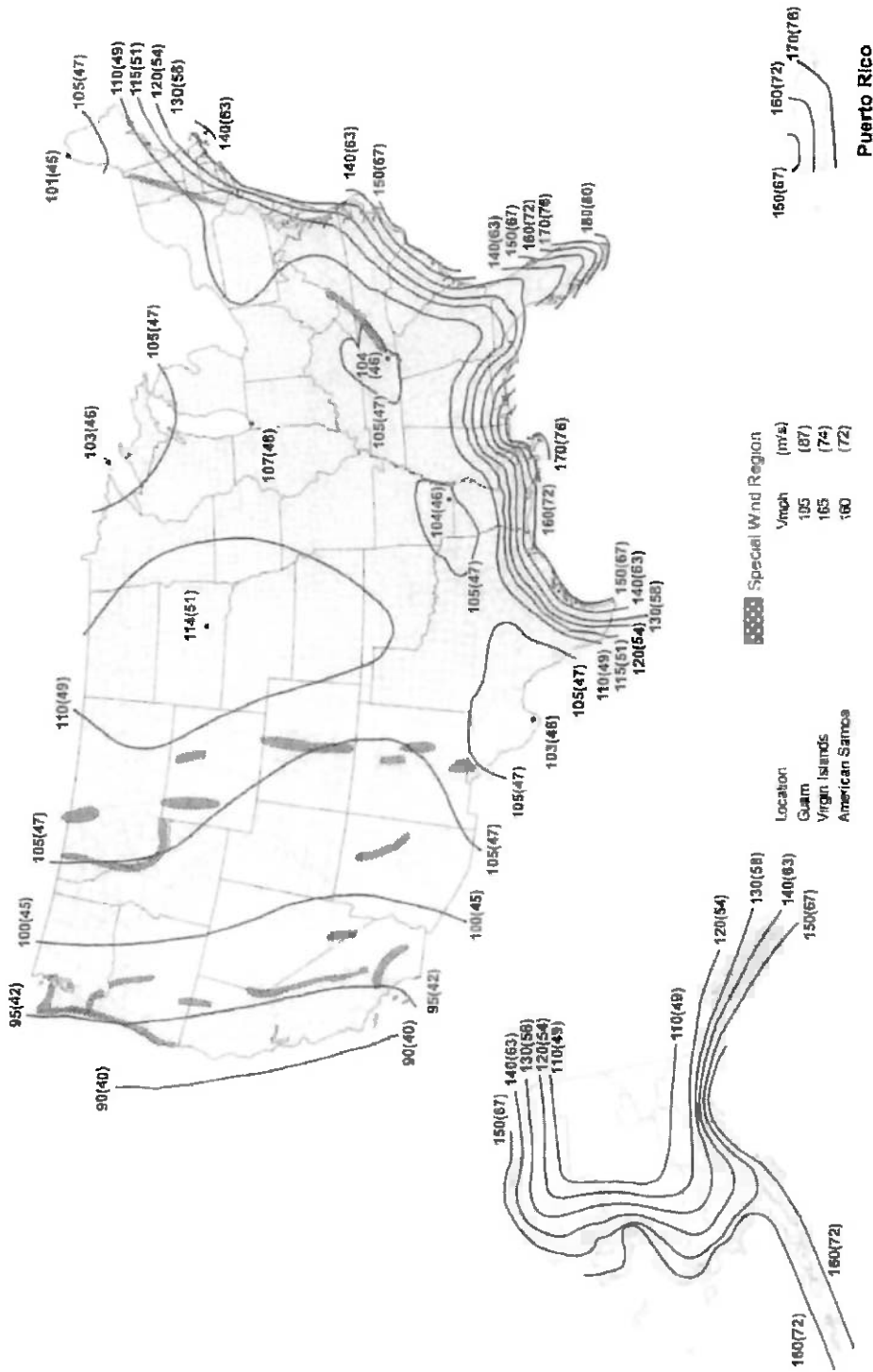
Landing areas designed for a design basis helicopter with maximum take-off weight of 3,000-pounds (13.35 kN) shall be identified with a 3,000 pound (13.34 kN) weight limitation. The landing area weight limitation shall be indicated by the numeral "3" (kips) located in the bottom right corner of the landing area as viewed from the primary approach path. The indication for the landing area weight limitation shall be a minimum 5 feet (1524 mm) in height.

1607.7 Heavy vehicle loads. Floors and other surfaces that are intended to support vehicle loads greater than a 10,000-pound (4536 kg) gross vehicle weight rating shall comply with Sections 1607.7.1 through 1607.7.5.

1607.7.1 Loads. Where any structure does not restrict access for vehicles that exceed a 10,000-pound (4536 kg) gross vehicle weight rating, those portions of the structure subject



FIGURE 1608.2—continued
GROUND SNOW LOADS, p_g , FOR THE UNITED STATES (psf)



Notes:

1. Values are nominal design 3-second gust wind speeds in miles per hour (mph) at 33 ft (10m) above ground for Exposure C category.
2. Linear interpolation is permitted between contours. Point values are provided to aid with interpolation.
3. Islands, coastal areas, and land boundaries outside the last contour shall use the last wind speed contour.
4. Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.
5. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (Annual Exceedance Probability = 0.00143, MRI = 700 Years).
6. Location-specific basic wind speeds shall be determined using www.atcouncil.org/windspeed

FIGURE 1609.3(1)
BASIC DESIGN WIND SPEEDS, V, FOR RISK CATEGORY II BUILDINGS AND OTHER STRUCTURES

Misc. Calculations

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Misc. Calcs - Continuous Grade Beam Check

Concrete Beam Calcs - 18"x36" Grade Beam

Typical Strip -

*	Section Trib Width (Selected)	3 ft	Per Drawings
*	Max Span	10 ft	Per Drawings
*	Loading Dead	1.5 kips/ft ²	Per Drawings
	Loading Live	0.5 kips/ft ²	Per Drawings
	Trib Area	1.5 feet	= 3feet/2000
	f' _c =	4000 psi	By Design
	f _y =	60000 psi	By Design
	Beam Ldg (Dead)	2.25 kips/lin. ft	
	Beam Ldg (Live)	0.75 kips/lin. ft	
	Moment (Dead)	28.13 kip-feet	M=wl ² /2
	Moment (Live)	9.38 kip-feet	M=wl ² /2
	Total Moment	37.50 kip-feet	summation
	Factored Moment (Dead)	39.38 kip-feet	M=wl ² /2 *1.4
	Factored Moment (Live)	15.94 kip-feet	M=wl ² /2 *1.6
	Total Factored Mom.	55.31 kip-feet	summation
	Reactions (Dead)	11.25 kips	
	Reactions (Live)	3.75 kips	
	Total Reaction		

31

b = 18.00 inch By Design
d = 30.00 inch By Design

Omega = 0.0114
Omega' = 0.0113

rho = 0.0008

As, Rqd As = 0.41 in²

As, min = 1.71 ACI 10.5.1
Select = 1-#6's 0.44 in²/ft

OK

Beam Check

T = Asfy = 26.40 kips

a = Asfy/.85f'cb = 0.43 inches

Moment Strength = 707.68 in-kips
or 58.97 kip-feet

OK

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Foundation Calcs - Continuous Footing

Typical

Wall Perimeter,

Roof Loads

1st Total Trib Width	12 feet	From Drawings
2nd Total Trib Width	0 feet	From Drawings
Dead Load	35 psf	Loads and Codes
Live Load	30 psf	Loads and Codes
Design Load	0.390 klf	Sum of Loads

Second Floor

1st Total Trib Width	0 feet	From Drawings
2nd Total Trib Width	0 feet	From Drawings
Dead Load	0 psf	Loads and Codes
Live Load	0 psf	Loads and Codes
Design Load	0 klf	Sum of Loads

First Floor

1st Total Trib Width	8.5 feet	From Drawings
2nd Total Trib Width	0 feet	From Drawings
Dead Load	60 psf	Loads and Codes
Live Load	100 psf	Loads and Codes
Total Wall Height (This section)	12 feet	From Drawings
Estimated Wall Weight	45 psf	Area * Load

Design Load	1.22 klf	Sum of Loads
Total Design Load	1.61 klf	Summation of Loads
Allowable Bearing Stress	2.00 k/ft ²	OK By IBC
Footing Width	0.81 ft	Load/Stress
Footing Depth	2.00 ft	By Design

Design Calculations

Summit Orchards

Lee's Summit, Missouri

LRFD, Short Hss Column Calculation

CITED TEXT: STRUCTURAL STEEL DESIGN, LRFD 3rd Edition, A. WILLIAMS PhD, SE

Member =	HSS6x6x3/8	AISC
Factored Load =	100 kips	Conservative
rx = ry =	2.28 inches	Ref: AISC
phi =	0.90	LRFD
Ag =	7.58 inches^2	AISC
Fy =	42.00 ksi	AISC
E =	29000.00 ksi	AISC
K =	1.00	
L =	12.00 feet	
	144.00	
rx = ry =	2.28 inches	
Fe =	71.75 ksi	E3-4
.44FY =	18.48 ksi	
Short Column, Eq. E3-2 Controls		
k = FY/Fe =	0.59	
Fcr =	32.87 ksi	E3-2
phi*Ag*Fc =	224.26 kips	
% Capacity =	45%	
	OK Say OK... full load not likely	

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Design Calculations

Summit Orchards

Lee's Summit, Missouri

Load Combinations: IBC 1605.2, IBC 2018

Dead Load	D	15 psf/total
Wind Load	W	20 psf/total
Flood Load	F	0 psf/total
Live Load (Floor)	L	40 psf/total
Height Load	H	1 unit factor
Snow Load	S	25 psf/total (Ice on Snow, IBC 1607)
Rain Load	R	15 psf/total
Earthquake Load	E	15 psf/total
LL adjustment	f1	0.5 other LL's
Snow adjustment	f2	0 Non-Saw Tooth Roofs

Load Cases:

1	$1.4(D + F) =$	21 Eq 16-1
2	$1.2(D + F) + 1.6(L + H) + .5(Lr \text{ or } S \text{ or } R)$	96.1 Eq 16-2
3	$1.2(D + F) + 1.6(Lr \text{ or } S \text{ or } R) + 1.6H + (f1L \text{ or } .5W)$	79.6 Eq 16-3
4	$1.2(D + F) + 1.0 W + f1L + 1.6H + .5(Lr \text{ or } S \text{ or } R)$	72.1 Eq 16-4
5	$1.2(D + F) + 1.0 E + f1L + 1.6H + f2S$	39.6 Eq 16-5
6	$.9D + 1.0 W + 1.6H$	35.1 Eq 16-6
7	$.9(D + F) + 1.0 E + 1.6H$	30.1 Eq 16-7
8	optional case	
9	optional case	
10	optional case	

Controlling Case: 2

96.1 psf/total

36

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Slab Calculation:

Slab thickness	4 inches
f' _c	4000 ksi in 28 days
k	200
desired safety factor	2.5
E _c	3604996.5 ksi
I	64.0 inches ⁴
L	0.0
Sec.Mod. per foot	32.0 Inches ³
allowable bending stress	227.7 Inches ²
Allowable load	1170.3 lbs per square foot

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Wood Frame Building

Misc. Calcs - Spread Footing Calculations

Footing Carrying; Corners

*	Dead Load (conservative estimate)	4	By Design
*	Live Load (conservative estimate)	5	By Design
	Total Column Load	9 kips	Per Drawings
*	Bending Moment	1 kip-feet	By Design, Seismic
	Bending Moment	12 in-kips	M*12
**	Allow. Soil Pressure	2000 psf	Conservative Estimated (IBC)
*	f'c =	4000 psi	By Design
	fy =	60000 psi	By Design

Select Footing Size

*	Footing Width (minor axis)	3 feet	By Design
**	Footing Length (major axis) L =	3 feet	By Design
*	Footing thickness	2.8 feet	By Design

Direct Soil Pressure 473 psf

Axial Bearing Stress = 1420 psf P/A
 $P/3Af*(4L/L-2e) =$ 1998 psf

78

Solve for "x" (length of bearing)= 4.27 feet $=((\text{Sum of Loads})*1000)/(0.5*Pa*Fw)$

Check Overturning = $M_o =$ 9 inch-kips $(M_{des}*.75)$

$M_r =$ 208 inch-kips $=((\text{Sum of Loads})*1000)/(0.5*Pa*F_r)$
S.F. = 23.06 M_r/M_o

Check Punching Shear

Column Size $V_c =$ 253 psi ACI
 $\text{Length} =$ 12 inches By Design
 $\text{Width} =$ 12 inches By Design

Punching Shear Failure Perimeter:

* Flexural Shear Critical Section = 23.76 inches Estimated @ $(.7071*t)$
Punching Shear Critical Section 11.88 inches $=\text{Flex Cr}/2$

$b_o =$ 143.03

Ultimate Load to Footing:
 $P_u =$ 14.10 kips $=1.4DL + 1.7LL$

Ultimate Punching Shear:

Soil Load due to Column Load Only

$P_c =$ 1000.00 psf $=P/A_{ftg}$
 $V_u =$ 26.56 kips $=P/L_{in \text{ at edge}}$

Calculate Depth Required:

$V_u/\phi*b_o*V_c =$ $d =$ 0.86 inches

Check Flexural Shear

$V_c =$ 126 ksi

Soil Pressure at Critical Section:

$P_{soil} =$ 2456.44

Total Shear Force 6680.96 lbs

$V_u =$ 12107.24 lbs

$d =$ 3.13 inch

Flexural Shear Does NOT Control Design

Check Bending

M= 35.71 kip-feet

Mu= 60.71 kip-feet

Select Reinforcement

Mu/ftg length = 20 kip-ft/ft

Minimum As = 0.73 inches²

** Try 5 - #6's 2.20 inches²/foot Each Way!!

Mu Capacity = 282 kip-ft/ft

OK

Check if Tensile Steel is Required at Top of Footing:

* Overburden = 2.50 feet

** Soil weight = 0.11 pcf

Mu = 0.59 kip-feet/foot

fc = Mc/I= 3.14 psi

fr = 205.55 psi

OK, No Top Steel Required

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Steel Girder at Mid Line of Building

Supporting Roof

Cap. Check - Max Span= 20 6096 mm Dim. Converted to mm

Trib Width	Per Beam (2 total)	60 ft	Per Drawings
Beam Span		20 ft	Per Drawings
Beam Loading Live =	LL = (1.6*.025)	0.04 kips/ft ²	Gravity Load Calcs
Beam Loading Dead=	DL = (1.4*.03)	0.04 kips/ft ²	Gravity Load Calcs
Trib Area	(half wall width, per bm)	30.00 feet	

Total Beam Loading 2.46 kips/lin. ft

Point Load 1		1 kips
(as applicable)	a =	10 ft
	b =	10 ft

Point Load 2		0 kips
(as applicable)	a =	0 ft
	b =	20 ft

Point Load 3		0 kips
(as applicable)	a =	0 ft
	b =	20 ft

Point Load 4		0 kips
(as applicable)	a =	0 ft
	b =	20 ft

Total Moment		$M_u = 0.9 * M_n =$	115.20 kip-feet 1382.40 kip-inches	$M_u = 0.9 * M_n =$	
Reactions		Right Reaction =	25.10 kips		
		Left Reaction =	25.10 kips		
		$Z_x \text{ req'd} =$	30.72 in ³	$= (M_u * 12) / (0.9 * F_y)$	
			OK		
Select	W21x44				
		Depth =	21.00 Inch		
		Area =	13.00 Inch ²		
		$Z_x =$	95.40 Inch ³		
		$I_{xx} =$	843.00 inch ⁴		
		$F_y =$	50.00 ksi		
Allowable Defl.	L/240		1.00 inches	Span/Allowable	
Deflection	Point & Uniform Ldg		0.37 inches	AISC Simple Bm	
		$Z_x \text{ act} =$	95.4 in ³		
		$Z_x \text{ req'd} =$	30.72 in ³		
			OK		
		$M(\text{plastic}) = F_y * Z =$	4770 kip-in	AISC LRFD	
		$M_y = F_y * S =$	4770 kip-in	AISC LRFD	
		$M_p \text{ Limit} = 1.5 * M_y =$	7155 kip-in	AISC LRFD	
			OK		
		$J =$	0.77		
		$L_p =$	10.10596	F10-5	
		$L_p \text{ (actual)} =$	5.0000		

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Wind Posts

Supporting Front Wall (Store Front)

Building Height	16	4877 mm	Dim. Converted to mm
-----------------	----	---------	----------------------

Trib Width	Building Length/4=	16.875 ft	Per Drawings
Wind Post Height		16 ft	Per Drawings
Beam Loading Live =	LL = (1.6*.025)	0.04 kips/ft^2	Gravity Load Calcs

Trib Area	(half wall width, per bm)	8.44 feet
-----------	---------------------------	-----------

Total Loading (Vertical)	0.34 kips/lin. ft
--------------------------	-------------------

Point Load 1 (as applicable)	a =	1 kips
	b =	8 ft

Point Load 2 (as applicable)	a =	0 kips
	b =	0 ft
		16 ft

Point Load 3 (as applicable)	a =	0 kips
	b =	0 ft
		16 ft

Point Load 4 (as applicable)	a =	0 kips
	b =	0 ft
		16 ft

Total Moment $M_u = .9 * M_n =$ 13.32 kip-feet $M_u = .9 * M_n =$
159.84 kip-inches

Reactions Right Reaction = 3.20 kips
Left Reaction = 3.20 kips

$Z_x \text{ req'd} =$ 3.55 in³ $= (M_u * 12) / (0.9 * F_y)$
OK

Select W12x26

Depth = 12.00 Inch
Area = 7.85 Inch²
Zx = 37.20 Inch³
Ixx = 204.00 inch⁴
Fy = 50.00 ksi

Allowable Defl. L/240 0.80 inches Span/Allowable

Deflection Point & Uniform Ldg 0.11 inches AISC Simple Bm

$Z_x \text{ act} =$ 37.2 in³

$Z_x \text{ req'd} =$ 3.55 in³
OK

$M(\text{plastic}) = F_y * Z =$ 1860 kip-in AISC LRFD
 $M_y = F_y * S =$ 1860 kip-in AISC LRFD
 $M_p \text{ Limit} = 1.5 * M_y =$ 2790 kip-in AISC LRFD
OK

J = 0.3

$L_p =$ 7.183287 F10-5
 $L_p \text{ (actual)} =$ 5.0000

Attachment to Footing

$M_u =$ 13.32 kip-ft

Bolt Centers 16 inches

Couple Force = Mu/Ctrs	9.99 Kips
Number of Bolts Anchors	2 bolts
Force Per Bolt Force/no.	4.995 kips
Select Bolt	3/4" A307
Capacity	14 kips
	OK

Design Calculations

Summit Orchards

Lee's Summit, Missouri

The following calculations are based on "out-to-out" dimensions as determined by the designing engineer.

All values are IBC, "simplified method" for structures under 30 feet in height.

Unit Description:	80'x60'x19'	Monoslope
Length:	80 feet	Re: Plan Drawings OUT TO OUT
Width:	60 feet	Re: Plan Drawings OUT TO OUT
Eave Height:	19 feet	Re: Plan Drawings
Roof Mean Height above eave:	1 feet	Re: Plan Drawings
Height Adjustment Factor:	1	Height Adjustmt Lamda, Fig 28.6-1
Design Wind Speed:	115 mph	IBC Table 1609.6.2.1 (1), pg 294
Roof Slope:	14.5 degrees	By Calculation
Exposure:	B	ASCE, pg195
Floors Considered in Calcs:	1 Floor	Re: Plan Drawings
For Simplicity and 120 Loading, Wall Forces Rounded to 20 psf Roof Forces take as Exp C Rounded to -30		
From IBC: Longitudinal		(Wind Force at End of Building)
Wind Pressure to Eave:	20 psf	ASCE Table 27.6-1
Wind Pressure to Roof:	-30 psf	ASCE Table 27.6-2
Vertical Pressures:		
Windward:	20 psf	ASCE Table 27.6-1
Leeward:	0 psf	
From IBC: Transverse		(Wind Force at Length of Building)
Wind Pressure to Eave:	20 psf	ASCE Table 27.6-1
Wind Pressure to Roof:	-30 psf	ASCE Table 27.6-2
Vertical Pressures:		
Windward:	20 psf	ASCE Table 27.6-1
Leeward:	0 psf	

Presumed Dead Loads

Roof:	16 psf	Re: Plan Drawings
Floor:	0 psf	Re: Plan Drawings, Slab on Grade
Ext. Walls:	16 psf	Re: Plan Drawings

MWFRS - Longitudinal -

80'x60'x19'

Horizontal Wind Loads

Building Width	60 feet	Re: Plan Drawings
Building Eave Height	19 feet	Re: Elevation Drawings
Roof Mean Height above eave	1 feet	Re: Elevation Drawings
Wind Pressure to Eave	20 psf	IBC Table 1609.6.2.1(1)
Wind Pressure to Roof	-30 psf	IBC Table 1609.6.2.1(1)
Height Adjustment Factor	1	IBC Table 1609.6.2.1 (4)
Total Wind Load at Walls	22.8 kips	By Calculation
Total Wind Load at Roof	-1.8 kips	By Calculation

Total Wind Shear (Longitudinal) 21 kips By Calculation

Unit Shear Stress at Base 0.13 kips/ft By Calculation

Theoretical Chord Stress at T.O.W.

Bending Moment:	157.5 k-ft	$M = (wl^2)/8$
Bending Stress:	2.0 k/in ²	Stress = M/d
Area for 2 Plate top chord:	10.5 in ²	By Calculation
Stress per Square Inch:	187.5 psi	By Calculation

OK

Shear to Top of Wall: 10.5 kips By Calculation

Theor. OT Reactions: 2.49 kips By Calculation

Theor. Panel Shear Stress: 0.26 klf By IBC

Lineal Feet Required: 9.78 feet By Calculation

OK

MWFRS - Transverse -

80'x60'x19'

Horizontal Wind Loads

Building Length	80 feet	Re: Plan Drawings
Building Eave Height	19 feet	Re: Elevation Drawings
Roof Mean Height above eave	1 feet	Re: Elevation Drawings
Wind Pressure to Eave	20 psf	IBC Table 1609.6.2.1(1)
Wind Pressure to Roof	-30 psf	IBC Table 1609.6.2.1(1)

Height Adjustment Factor	1	IBC Table 1609.6.2.1 (4)
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Total Wind Load at Walls	30.4 kips	By Calculation
Total Wind Load at Roof	-0.6 kips	By Calculation

Total Wind Shear (Transverse)	29.8 kips	By Calculation
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Unit Stress at Base (Transverse)	0.248333 kips/ft	By Calculation
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Theoretical Chord Stress at T.O.W.

Bending Moment:	298.0 k-ft	$M=(wl^2)/8$
Bending Stress:	5.0 k/in ²	Stress=M/d
Area for 2 Plate top chord:	10.5 in ²	By Calculation
Stress per Square Inch:	473.0 psi	By Calculation

Check Design

Shear to Top of Wall:	14.9 kips	By Calculation
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Theor. OT Reactions:	3.5 kips	By Calculation
Theor. Panel Shear Stress:	0.3 klf	By IBC
Lineal Feet Required:	13.9 feet	By Calculation

OK

MWFRS - Longitudinal - 80'x60'x19'

Vertical Wind Loads (Uplift)

Building Width	60 feet	Re: Plan Drawings
Building Eave Height	19 feet	Re: Elevation Drawings
Roof Mean Height above eave	1 feet	Re: Elevation Drawings
Wind Pressure to Leeward	-10.7 psf	IBC Table 1609.6.2.1(1)

4/6

Height Adjustment Factor	1	IBC Table 1609.6.2.1 (4)
Total Wind Load at Roof	-25.7 kips	By Calculation
Total Wind Force Vertical (Longitudinal)	-0.3 kips/ft	By Calculation
Dead Load Forces		
Roof:	0.480 klf	By Calculation
Floors:	0.000 klf	By Calculation
Walls:	0.304 klf	By Calculation
Total:	0.784 klf	By Calculation
NET, Unit Stress at Foundation (Longitudinal)	0.463 kips/ft	By Calculation Dead Load Controls, Uplift < DL

MWFRS - Transverse - 80'x60'x19'

Vertical Wind Loads (Uplift)

Building Length	80 feet	Re: Plan Drawings
Building Eave Height	19 feet	Re: Elevation Drawings
Roof Mean Height above eave	1 feet	Re: Elevation Drawings
Wind Pressure to Windward	20 psf	IBC Table 1609.6.2.1(1)
Height Adjustment Factor	1	IBC Table 1609.6.2.1 (4)
Total Wind Windward Pressure	48 kips	By Calculation
Total Wind Force Vertical (Transverse)	0.6 kips/ft	By Calculation
Dead Load Forces		
Roof:	0.48 klf	By Calculation
Floors:	0 klf	By Calculation
Walls:	0.304 klf	By Calculation
Total:	0.784 klf	By Calculation
NET, Unit Stress at Foundation (Transverse)	1.384 kips/ft	By Calculation Dead Load Controls, Uplift < DL

MWFRS - Longitudinal - 80'x60'x19'

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OTM - Horizontal Wind Forces

Total Wind Shear (Longitudinal)	21.00 kips	By Calculation
Total Wind Force Vertical (Longitudinal)	-25.68 kips	By Calculation Controlling Value ONLY
Summing Moments at End	46.68 kips	By Calculation
Unit Stress at Extrema (longitudinal)	0.78 kips/ft Dead Load Controls	By Calculation

MWFRS - Transverse - 80'x60'x19'

OTM - Horizontal Wind Forces

Total Wind Shear (Transverse)	29.80 kips	By Calculation
Total Wind Force Vertical (Transverse)	48.00 kips	By Calculation Controlling Value ONLY
Summing Moments at End	77.80 kips	By Calculation
Unit Stress at Extrema (Transverse)	0.97 kips/ft Hold Downs Required	By Calculation

Foundation Loads Due to Wind

Longitudinal Wind Loads

Shear Stress/foot	0.13 kips/ft	By Calculation
Vertical Force/foot	0.46 kips/ft	By Calculation
OT Force (Vertical)	0.78 kips/ft	By Calculation
Total Shear	21.00 kips	By Calculation
Shear @ Brace = $T_{\text{shear}}/2 =$	10.50 kips	By Calculation

Transverse Wind Loads

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Shear Stress/foot	0.25 kips/ft	By Calculation
Vertical Force/foot	1.38 kips/ft	By Calculation
OT Force (Vertical)	0.97 kips/ft	By Calculation
Total Shear	29.80 kips	By Calculation

Simpson Hold Down Confirmation

By Standard, Check Simpson HD8A, w/ 5/8" A307, Bolt Embed 12" min.	3.66 kips/conn.	Simpson, pg 29
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Controlling Vertical Load: Hold Down Spacing:	0.97 kips/ft	By Calculation
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OK, Hold Downs per Code and Calculation

Nail Pattern Confirmation, for Structural Sheathing

By Standard, Check	0.27 kips/ft	6" o.c. at Edges
Edge Condition for 15/32" Plywood with 2x4 studs, and 8d, 1 3/8" nails.	0.36 kips/ft	4" o.c. at Edges

Controlling Shear Stress	0.25 kips/ft	By Calculation
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Design Edge Pattern 6 in. o.c Edge Spacing Required

Shear Wall Quantity Confirmation

Transverse Loading

SW2	1/2" Gyp blkcd	134 plf	Table 2306.3.1
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Lineal feet available for SW1	135 lf	By Calculation
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Shear Capacity	18.09 kips	By Calculation
Factored Capacity	18.09 kips	By Calculation

Total Shear	29.80 kips	By Calculation
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% Shear Resisted	61%
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% Shear Remaining	39% Additional Capacity Required
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SW1	15/32" Shtg blkcd	255 plf	Table 2306.3.1
Lineal feet available for SW1	135 lf		By Calculation
Shear Capacity	34.43 kips		By Calculation
Opening Reduction Factor	0.77		Table 2305.3.7.2
Wind Increase Factor	1.40		IBC 2306.4.1
Factored Capacity	37.11 kips		By Calculation
Combined Capacity	55.20 kips		By Calculation
Total Shear	29.80 kips		By Calculation
% Shear Resisted	185%		
% Shear Remaining	-85%	Shear Demand Met	

Longitudinal Loading

SW2	1/2" Gyp blkcd	175 plf	Table 2306.3.1
Lineal feet available for SW1	115 lf		By Calculation
Shear Capacity	20.125 kips		By Calculation
Reduction Factor	1		
Factored Capacity	20.125 kips		By Calculation
Total Shear	21 kips		By Calculation
% Shear Resisted	96%		
% Shear Remaining	4%	Additional Capacity Required	

SW1	15/32" Shtg blkcd	255 plf	Table 2306.3.1
Lineal feet available for SW1	115 lf		By Calculation
Shear Capacity	29.33 kips		By Calculation
Opening Reduction Factor	1		
Wind Increase Factor	1.40		IBC 2306.4.1
Factored Capacity	41.06 kips		By Calculation
Combined Capacity	61.18 kips		By Calculation

Total Shear	21.00 kips	By Calculation
% Shear Resisted	291%	
% Shear Remaining	-191%	Shear Demand Met

Shear Wall Design, Wind

Longitudinal Loading

SW3	1/2" Gyp blkcd	175 plf	Table 2306.3.1
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Lineal feet available for SW1	115 lf	By Calculation
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Shear Capacity	20.13 kips	By Calculation
Reduction Factor	1	
Factored Capacity	20.13 kips	By Calculation

Total Shear	21.00 kips	By Calculation
% Shear Resisted	96%	
% Shear Remaining	4%	

SW2	15/32" Shtg blkcd	255 plf	Table 2306.3.1
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Lineal feet available for SW1	115 lf	By Calculation
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Shear Capacity	21.00 kips	By Calculation
Opening Reduction Factor	1	
Wind Increase Factor	1.40	IBC 2306.4.1
Factored Capacity	29.40 kips	By Calculation

Combined Capacity	49.53 kips	By Calculation
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Total Shear	21.00 kips	By Calculation
% Shear Resisted	236%	
% Shear Remaining	-136%	Capacity Demand Met

Design Calculations

Summit Orchards

Lee's Summit, Missouri

Misc. Calcs - Window Headers 9'-0"

Supporting - Roof - Wall - Parapet

Beam Designation None

Beam Span	Max. Typical	12 feet	Re: Plan Drawings
Uniform Load Width		16.88 feet	Re: Plan Drawings
Uniform Load (total load LL+DL)	$1.6 \times .025 + 1.4 \times .035$	0.075 ksf	Load & Codes
Beam Loading		1.27 klf	ULW * UL
Point Load 1		0.0 kips	
Point Load 1 Location		6.0 feet	
Point Load 2		0.0 kips	By Design
Point Load 2 Location		6.0 feet	
Point Load 3		0.0 kips	
Point Load 3 Location		6.0 feet	

For Conservatism All Moments Consider at Midspan !!
All beams considered continually braced at top flange !!

Moments	Uniform Load	22.781 k-ft	$M = (w l^2) / 8$
	Point Load 1	0.00 k-ft	$M = (w l^2) / 8$
	Point Load 2	0.00 k-ft	$M = (w l^2) / 8$
	Point Load 2	0.00 k-ft	$M = (w l^2) / 8$
	Total	22.78 k-ft	Summation
Allow Deflection	L 360	0.400 inches	Span/allowable
Reaction		7.59375 kips	$= (w * l) * \text{span} / 2$

Size Beam

By Design

b =	4.5 inches
d =	14.0 inches
lxx =	1029.0 inches ⁴
E =	1800 ksi
Deflection, Uniform	0.3188 inches
Deflection, PL 1	0.0000 inches
Deflection, PL 2	0.0000 inches
Deflection, PL 3	0.0000 inches
Deflection Total	0.3188 inches
	OK
Shear Stress	0.121 ksi

Check Bending Stresses

Sxx=	147.0 inches ³
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Adjustment Factors

Cd	0.95	Section 2.3.2 Duration
Cm	1.00	ASD Wood Design Manual
Ct	1.00	ASD Wood Design Manual
Cl	Braced	Section 4.4.1 Stability
Cf	1.00	ASD Wood Design Manual
Cv	1.03	Table 5A Wood Supplement page 57
Adjusted Cv	1.00	Max Value from Suppl. page 57
Cfu	1.00	ASD Wood Design Manual
Cr	1.15	ASD Rep Factor, NDS Section 4.3.9 Ref: Page 30
Fb=	1800	#2 GRD, DF

F'b=	2019.87 psi
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Actual fb=	1859.69 psi
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OK

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Design Calculations

Summit Orchards

Lee's Summit, Missouri

Misc. Calcs - Studs @ Windows - Max Load

Column Capacity - 2x6 Studs

Column Designation	None		
		BLOCKING REQ'D	
* Column Length	unbraced length	8.0 feet	Re: Plan Drawings
* Trib Width		14.4 feet	Re: Plan Drawings
Trib Length		33.8 feet	Re: Plan Drawings
* Uniform Load	Loads (LL + DL)	0.1 ksf	Load & Codes
	Additional Load (xxx)	0.0 kips	
Column Loading		29.1 kips	Sum(Loads above)
* Column "d"	12-2x6's	13.0 inches	Re: Plan Drawings
* Column "b"		5.5 inches	Re: Plan Drawings
Wind Loading	Considered in Other Calcs	0 kips	By Design & Drawings
		0 kips	By Design & Drawings
		0 kips	By Design & Drawings
		0 kips	By Design & Drawings
		0 kips	By Design & Drawings

For Conservatism Column Consider Unbraced !!

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Total Design Load **29.10938 kips** **Sum (Loads above)**

Adjustment Factors

Cd **0.9** Table 2.3.2, pg. 9
 Cm **1** Table 4B, NDS Sup, pg 36, **
 Ct **1** Table 2.3.3, pg. 9
 Cf **1** ASD Wood Design Manual
 * Bearing Stress = **825** Bearing Stress Unfactored
 Fc= 742.5 H.2, pg 157, See definition

$l = l_e$
 l/d Ratio = 7.384615 H.2, pg 157, NDS
OK

* Kce = 0.3 Equation H3, pg 157, NDS
 E=E' 1500000 psi
 Fce= 8251.953 Equation H2, pg 157, NDS
 F'c= 728.396 Equation H1, pg 157, NDS

* Logic Statement Design Stress 728.396 psi Lesser Value of F'c or Fce

* c= 0.80 Equation H2, pg 157, NDS
 Cp = 0.68 Equation 3.7-1, pg 19, NDS

Capacity **P'= 36.33 kips** **$=((F_c * C_p) * (d * b))/1000$**

Capacity Check **OK**

Seismic



SEISMIC LOADS - ASCE 7-2010

Site Class Soil Definition	D	Per Geotechnical recommendation
	.2 Second Response $S_s =$	0.12 Map Figure 22-1 p.211
	$F_a =$	1.6 Table 11.4-1
SMS =	$F_a \times S_s =$	0.192 Eq. 11.4-1
SDS =	$2/3 \text{ SMS} =$	0.128 Eq. 11.4-3
	1 Second Response $S_1 =$	0.06 Map Figure 22-2 p.213
	$F_v =$	2.4 Table 11.4-2
SM1 =	$F_v \times S_1 =$	0.144 Eq. 11.4-2
SD1 =	$2/3 \text{ SM1} =$	0.096 Eq. 11.4-4
Occupancy	II	Table 1-1 (p3)
Seismic Design Category	A	Table 11.4-1 (p115)
	B	Table 11.4-2 (p115)
Importance Factor $I =$	1	Table 11.5-1, Category I (p116)
Redundancy $r =$	1	12.3.4.1 (Design Category B or C) (p1)
Ordinary Steel Concentrically Braced Frame		
Overstrength factor $W_o =$	6.5	Table 12.2-1 Ordinary Wood Framing
Response Modification Coeff $R =$	3	Table 12.2-1 Ordinary Wood Framing
Base Shear for Building $V = C_s W$		Eq. 12.8-1 (p129)
$C_s =$	$SDS =$ R / I	0.042667 Use Eq. 12.8-2
Max. $C_s =$	$SD1 =$ $(R / I) T$	0.336359 Eq. 12.8-3
	$T_a =$	CT $h_{nx} =$ 0.1 Eq. 12.8-7
		CT = 0 Table 12.8-2 -All other systems
		$h_n =$ 8 Taken at Median height
		$x =$ 0.8 Table 12.8-2-All other systems
	$T \leq$	$C_u T_a =$ 0.2 OK
		$C_u =$ 1.6 Table 12.8-1 (p129) for $SD1 < .1$
		(See Eq. 12.8-4 for period $T > T_L$ of 12 sec for Max C_s)
Min. $C_s =$	$.5 S_1 =$ R / I	0.01 $\leq$.0 Eq. 12.8-5 and 12.8-6
Dead Load =	80x60x.035	168.00
Dead Load =		

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168.00

Total Dead Load W for Bldg=

168 k

Total Base Shear V = Cs W =

7.17 k

To building Frame

60



FIGURE 1613.2.1(1)—continued
RISK-TARGETED MAXIMUM CONSIDERED EARTHQUAKE (MCE_R) GROUND MOTION RESPONSE ACCELERATIONS FOR THE
CONTERMINOUS UNITED STATES OF 0.2-SECOND SPECTRAL RESPONSE ACCELERATION (5% OF CRITICAL DAMPING)



FIGURE 1613.2.1(2)—continued
 RISK-TARGETED MAXIMUM CONSIDERED EARTHQUAKE (MCE_B) GROUND MOTION RESPONSE ACCELERATIONS FOR THE
 CONTERMINOUS UNITED STATES OF 1-SECOND SPECTRAL RESPONSE ACCELERATION (5% OF CRITICAL DAMPING)

LORAC DESIGN GROUP, LLC

Structural Engineers

End of Review

