



LANE SUPPLY, INC.

120 Fairview
Arlington, TX 76010
817-261-9116

DESIGN CALCULATIONS FOR :

Chick-fil-A #05248 Outside Meal Delivery Canopy
SWC Highway 50 & State Route 291
Lee's Summit, MO

Twelve-Column Canopy :	31'-3" X 76'-5" Canopy
Lane Reference Number :	LSC-78798
Date :	12-Nov-24

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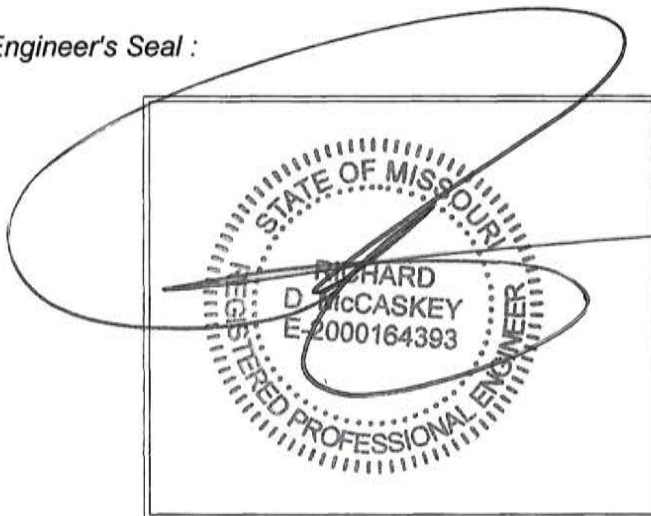
Canopy Calculations :

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Attachments :

Lane SL-316 Deck Panel Properties
Lane Standard Base Plate Design
Design Sketch

Engineer's Seal :



C.O.A. 2001015838

NOV 12 2024

Calculations By:

Lane Supply, Inc.

LSC - 78798

Customer:

Chick-fil-A #05248 Outside Meal Delivery Canopy

By: CP

Project:

31'-3" X 76'-5" Canopy

Check:

Code:

2018 International Building Code

Roof Loads:

Dead Load =	3.00	psf	(SL-316 Deck)
Live/Snow Load =	20.00	psf	
TOTAL =	23.00	psf	

Fascia Load:

Height =	10.00	in.
Dead Load =	5.83	plf

Wind Loads:

Risk Category =	II		
V, ULT Speed =	116	m.p.h. Exp	C
V, ASD Speed =	90	m.p.h. Exp	C
Height =	20	ft	
Kd =	0.85		
Kh =	0.90		
G =	0.85		
qz =	15.81	psf	

Lateral Load =	1.0 (H)•qz =	16.00	psf
Deck Uplift =	-1.7 (V)•G•qz =	-22.85	psf
Frame Uplift =	-1.1 (V)•G•qz =	-14.78	psf

Seismic:

Base Shear : V =	CS • W =	0.085	• W
Site Class =	D	(Default)	
Risk Category =	II		
Ss(0.2) =	0.100		
S1(1.0) =	0.068		
Fa =	1.60		
Fv =	2.40		
SMS = Fa•Ss =	0.160	(11.4-1)	
SM1 = Fv•S1 =	0.163	(11.4-2)	
SDS = 2/3•SMS =	0.107	(11.4-3)	
SD1 = 2/3•SM1 =	0.109	(11.4-4)	
R =	1.25		
CS = (SDS/R) =	0.085	(12.8-2)	

Seismic Design Category Based on SDS : A

Seismic Design Category Based on SD1 : B

Design Category : B

Section 7.1.2--Symbols & Notation

C_e =	1.2	Exposure Factor as determined from Table 7.3-1
C_t =	1.2	Thermal factor as determined from Table 7.3-2
D =	Snow Density in pcf as determined from Eq. 7.7-1	
h_b =	Height of balanced snow load determined by dividing P_f by D , in feet.	
h_d =	Height of snow drift, in feet	
h_c =	Clear height from top of balanced snow to top of parapet, ft	
h_r =	6.00	= Fascia height, ft
I_s =	1.0	= Importance factor (see Table 1.5-2).
P_f =	Snow load on flat roofs, psf.	
P_g =	20	=ground snow, psf.
P_d =	Maximum intensity of drift surcharge load, psf.	
l_u =	31.708333	= Length of roof upwind of the drift, feet
w =	Width of snow drift, in feet	

Section 7.3--Flat-Roof Snow Loads, P_f

The snow load, P_f , on a roof with a slope equal to or less than 5° shall be calculated in psf using equation 7.3-1, but not less than the following minimum values for low slope roofs: where P_g is 20 psf or less $P_f = I(P_g)$, where P_g exceeds 20 psf, $P_f = 20(I)$.

Section 7.7 & Section 7.8

The geometry of the surcharge load due to snow drifting shall be approximated by a triangle as shown in figure 7.7-2. Drift loads shall be superimposed on the balanced snow load. If h_c/h_b is less than 0.2, drift loads are not required to be applied.

The height of such drifts shall be taken as $0.75 \times h_d$ as determined from Fig 7.6-1, with l_u equal to the length of the roof upwind of the projection or parapet wall. If the side of a roof projection is less than 15 ft long, a drift load is not required to be applied to that side. If the height, h_d , is equal to or less than h_c , the drift width shall equal $4h_d$ and the drift height shall equal h_d . If this height exceeds h_c , the drift width, w , shall equal $4h_d^2/h_c$ and the drift height shall equal h_c . However, the drift width w shall not exceed $8h_c$. The maximum intensity of the drift surcharge load, p_d , equals $h_d \times D$ where the snow density, D , is defined by Eq 7.7-

Section 7.10--Rain-On-Snow Surcharge Load

For locations where P_g is 20 psf or less but not zero, all roofs with a slope less than $W/50$, shall have a 5 psf rain-on-snow surcharge load applied to establish the design snow loads. This additional load applies only to the sloped roof (balanced) load case and need not be used in combination with drift, sliding, unbalanced, or partial loads.

$$P_f = 0.7 \times C_e \times C_t \times I_s \times P_g \quad \text{Eq 7.3-1}$$

$$P_f = 20.0 \text{ psf}$$

$$h_d = 0.75 \times (0.43(l_u)^{1/3} \times (P_g + 10)^{1/4 - 1.5}) \quad \text{Ref. Fig. 7.6-1}$$

$$h_d = 1.26 \text{ ft}$$

$$D = 0.13P_g + 14 < 30 \text{ psf} \quad \text{Eq 7.7-1}$$

$$D = 16.60 \text{ psf}$$

$$h_b = 1.20 \text{ ft}$$

$$h_c = h_r - h_b = 4.80 \text{ ft}$$

$$h_c/h_b = 3.98$$

Consider Drift

$$w = 5.06 \text{ ft}$$

$$P_d = D \times h_d < D \times h_c$$

$$P_d = 20.98 \text{ psf}$$

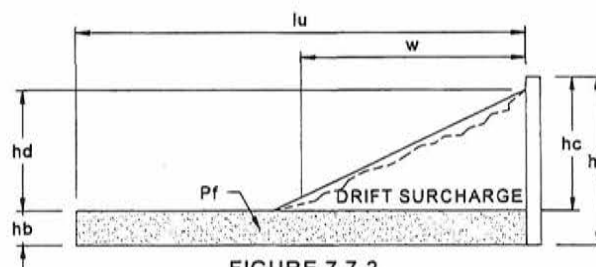
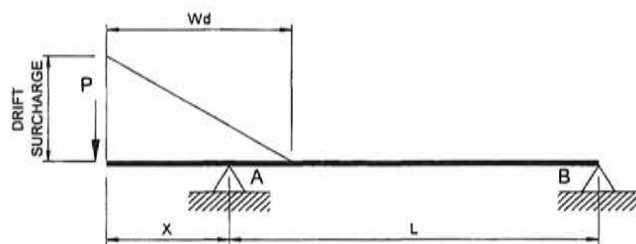


FIGURE 7.7-2
Configuration of Snow Drifts on Lower Roofs

USE 20 GAUGE GRADE C DECK

+S=.3961 in³ -S=.3036 in³ FY=40 ksi

$w_d = 3.00$ psf
 $w_s = 20.00$ psf
 Deck : $w_w = -22.85$ psf
 Frame : $w_w = -14.78$ psf
 $P = 5.83$ plf
 (Drift Surcharge) $P_m = 20.98$ psf
 $L = 6.50$ ft
 $X = 1.75$ ft
 (Drift Length) $W_d = 5.06$ ft



$R_{Ad} = 23.11$ plf	$R_{Bd} = 7.47$ plf
$R_{As} = 158.28$ plf	$R_{Bs} = 59.76$ plf
Frame : $R_{Aw} = -77.40$ plf	Frame : $R_{Bw} = -44.56$ plf
Deck : $R_{Aw} = -119.62$ plf	Deck : $R_{Bw} = -68.87$ plf
$R_{A(d+s)} = 181.39$ plf	$R_{B(d+s)} = 67.23$ plf
Frame : $R_{A(d+w)} = -54.29$ plf	Frame : $R_{B(d+w)} = -37.09$ plf
Deck : $R_{A(d+w)} = -96.51$ plf	Deck : $R_{B(d+w)} = -61.40$ plf
$M_{Ad} = -14.80$ ft-lbs/ft	
$M_{As} = -59.05$ ft-lbs/ft	
Deck : $M_{Aw} = 34.99$ ft-lbs/ft	
$M_{A(d+s)} = -73.85$ ft-lbs/ft	$M_{AB(d+s)} = 98.24$ ft-lbs/ft
Deck : $M_{A(d+w)} = 20.18$ ft-lbs/ft	Deck : $M_{AB(d+w)} = -94.94$ ft-lbs/ft

USE 20 GAUGE GRADE C DECK

$+S = .3961 \text{ in}^3$ $-S = .3036 \text{ in}^3$ $FY = 40 \text{ ksi}$

DECK DESIGN:

Deck 1

$W_d = 3.00$ psf	23.00 psf
$W_i = 20.00$ psf	^A B^
Deck : $W_w = -22.85$ psf	$ \text{-----} L \text{-----} $
Frame : $W_w = -14.78$ psf	
$L = 6.50$ ft	$R_d = 9.75$ plf
	$R_i = 65.00$ plf
	Frame : $R_w = -48.05$ plf
	Deck : $R_w = -74.25$ plf
$M(d+l) = 121.47$ ft-lbs/ft	$R(d+l) = 74.75$ plf
Deck : $M(d+w) = -104.82$ ft-lbs/ft	Frame : $R(d+w) = -38.30$ plf
	Deck : $R(d+w) = -64.50$ plf

USE 20 GAUGE GRADE C DECK

$+S = .3961 \text{ in}^3$ $-S = .3036 \text{ in}^3$ $FY = 40 \text{ ksi}$

P1						P2
v	23.00 PSF	o	o	o		v
	^A	^B	^C	^D	^E	
<--- X1 --->	<-----L1----->	<---L2--->	<---L3--->	<-----L4----->	<---X2--->	

Wd=	3.00	psf
WI=	20.00	psf
Deck : Ww=	-22.85	psf
Frame : Ww=	-14.78	psf
P1=	5.83	plf
P2=	5.83	plf
MAd=	5.22	ft-lbs/ft
MAI=	5.63	ft-lbs/ft
Deck : MAw=	-6.43	ft-lbs/ft
MA(d+l)=	10.84	ft-lbs/ft
Deck : MA(d+w)=	-1.21	ft-lbs/ft
MAB(d+l)=	47.34	ft-lbs/ft
Deck : MAB(d+w)=	-42.47	ft-lbs/ft
MBC(d+l)=	121.47	ft-lbs/ft
Deck : MBC(d+w)=	-104.82	ft-lbs/ft
MCD(d+l)=	121.47	ft-lbs/ft
Deck : MCD(d+w)=	-104.82	ft-lbs/ft
MDE(d+l)=	125.51	ft-lbs/ft
Deck : MDE(d+w)=	-87.35	ft-lbs/ft
MEd=	31.62	ft-lbs/ft
MEI=	92.52	ft-lbs/ft
Deck : MEw=	-105.69	ft-lbs/ft
ME(d+l)=	124.14	ft-lbs/ft
Deck : ME(d+w)=	-74.07	ft-lbs/ft

X1=	0.75	ft
L1=	4.17	ft
L2=	6.50	ft
L3=	6.50	ft
L4=	7.00	ft
X2=	3.04	ft

RAAd=	15.59	plf
RAI=	58.02	plf
Frame : RAw=	-42.88	plf
RA(d+l)=	73.60	plf
Frame : RA(d+w)=	-27.30	plf
RBd=	14.75	plf
RBI=	106.67	plf
Frame : RBw=	-77.85	plf
RB(d+l)=	121.41	plf
Frame : RB(d+w)=	-63.10	plf
RCd=	19.50	plf
RCI=	130.00	plf
Frame : RCw=	-96.09	plf
RC(d+l)=	149.50	plf
Frame : RC(d+w)=	-76.59	plf
RDd=	15.73	plf
RDI=	135.00	plf
Frame : RDw=	-90.02	plf
RD(d+l)=	150.73	plf
Frame : RD(d+w)=	-74.29	plf
REd=	29.98	plf
REI=	144.05	plf
Frame : REw=	-106.48	plf
RE(d+l)=	174.03	plf
Frame : RE(d+w)=	-76.50	plf

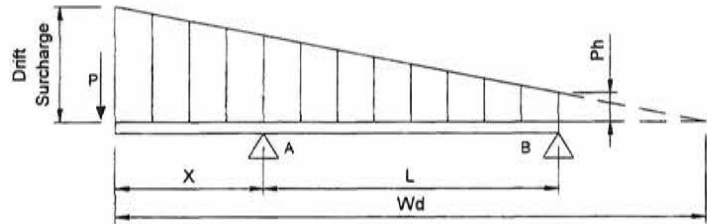
USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksi

Deck Design

Deck 2

wd= 3.00 psf
 ws= 20.00 psf
 Deck : Ww= -22.85 psf
 Frame : Ww= -14.78 psf
 P= 5.83 plf
 (Drift Surcharge)Pm= 20.98 psf
 L= 4.17 ft
 X= 0.75 ft
 Wd= 5.06 ft
 Ph= 0.58 psf



RAd= 15.59 plf
 RAs= 99.15 plf
 Frame : RAw= -42.88 plf
 Deck : RAw= -66.28 plf

RBd= 5.00 plf
 RBs= 52.18 plf
 Frame : RBw= -29.80 plf
 Deck : RBw= -46.06 plf

RA(d+s)= 114.74 plf
 Frame : RA(d+w)= -27.30 plf
 Deck : RA(d+w)= -50.69 plf

RB(d+s)= 57.18 plf
 Frame : RB(d+w)= -24.80 plf
 Deck : RB(d+w)= -41.06 plf

Md(@ OH)= -5.22 fl-lbs/ft
 Ms(@ OH)= -11.23 fl-lbs/ft
 Deck : Mw(@ OH)= 6.43 fl-lbs/ft
 MOH(d+s)= -16.45 fl-lbs/ft
 Deck : MOH(d+w)= 1.21 fl-lbs/ft

MSP(d+s)= 61.70 fl-lbs/ft
 Deck : MSP(d+w)= -42.47 fl-lbs/ft

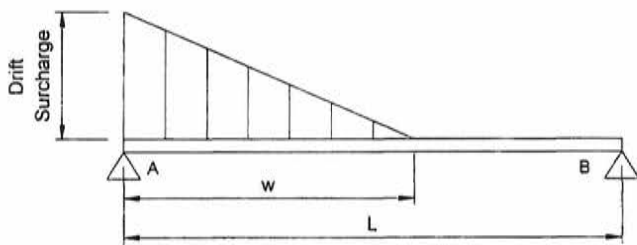
USE 20 GAUGE GRADE C DECK

+S=.3958 in^3 -S=.3195 in^3 FY=40 ksi

Deck Design

Deck 2

wd=	3.00	psf
ws=	20.00	psf
Deck : Ww=	-22.85	psf
Frame : Ww=	-14.78	psf
(Drift Surcharge)Pm=	0.58	psf
L=	6.50	ft
W=	0.14	ft



RA _d =	9.75	plf	RB _d =	9.75	plf
RA _s =	65.04	plf	RB _s =	65.00	plf
Frame : RA _w =	-48.05	plf	Frame : RB _w =	-48.05	plf
Deck : RA _w =	-74.25	plf	Deck : RB _w =	-74.25	plf
RA(d+s)=	74.79	plf	RB(d+s)=	74.75	plf
Frame : RA(d+w)=	-38.30	plf	Frame : RB(d+w)=	-38.30	plf
Deck : RA(d+w)=	-64.50	plf	Deck : RB(d+w)=	-64.50	plf

MSP(d+s)=	121.41	ft-lbs/ft
Deck : MSP(d+w)=	-104.77	ft-lbs/ft

USE 20 GAUGE GRADE C DECK

+S=.3958 in³ -S=.3195 in³ FY=40 ksi

DECK DESIGN:

Deck 2

Wd=	3.00	psf
Wl=	20.00	psf
Deck : Ww=	-22.85	psf
Frame : Ww=	-14.78	psf
L=	6.50	ft

23.00	psf
^A	^B
<-----	----->
L	

M(d+l)=	121.47	ft-lbs/ft
Deck : M(d+w)=	-104.82	ft-lbs/ft

R _d =	9.75	plf
R _l =	65.00	plf
Frame : R _w =	-48.05	plf
Deck : R _w =	-74.25	plf
R(d+l)=	74.75	plf
Frame : R(d+w)=	-38.30	plf
Deck : R(d+w)=	-64.50	plf

USE 20 GAUGE GRADE C DECK

+S=.3961 in³ -S=.3036 in³ FY=40 ksi

P1					P2
v	23.00 PSF	o	o	o	v
	^A	^B	^C	^D	^E
<--- X1 --->	<-----L1----->	<---L2--->	<---L3--->	<-----L4----->	<---X2--->

Wd=	3.00 psf	X1=	1.79 ft
WI=	20.00 psf	L1=	6.50 ft
Deck : Ww=	-22.85 psf	L2=	6.50 ft
Frame : Ww=	-14.78 psf	L3=	6.50 ft
P1=	5.83 plf	L4=	7.00 ft
P2=	5.83 plf	X2=	3.04 ft

MAd=	15.27 ft-lbs/ft
MAI=	32.10 ft-lbs/ft
Deck : MAw=	-36.67 ft-lbs/ft
MA(d+l)=	47.37 ft-lbs/ft
Deck : MA(d+w)=	-21.40 ft-lbs/ft

MAB(d+l)=	113.96 ft-lbs/ft
Deck : MAB(d+w)=	-94.39 ft-lbs/ft

MBC(d+l)=	121.47 ft-lbs/ft
Deck : MBC(d+w)=	-104.82 ft-lbs/ft

MCD(d+l)=	121.47 ft-lbs/ft
Deck : MCD(d+w)=	-104.82 ft-lbs/ft

MDE(d+l)=	125.51 ft-lbs/ft
Deck : MDE(d+w)=	-87.35 ft-lbs/ft

MEd=	31.62 ft-lbs/ft
MEI=	92.52 ft-lbs/ft
Deck : MEw=	-105.69 ft-lbs/ft
ME(d+l)=	124.14 ft-lbs/ft
Deck : ME(d+w)=	-74.07 ft-lbs/ft

RAAd=	23.31 plf
RAI=	105.77 plf
Frame : RAw=	-78.18 plf
RA(d+l)=	129.08 plf
Frame : RA(d+w)=	-54.88 plf

RBd=	17.15 plf
RBI=	130.00 plf
Frame : RBw=	-92.44 plf
RB(d+l)=	147.15 plf
Frame : RB(d+w)=	-75.29 plf

RCd=	19.50 plf
RCI=	130.00 plf
Frame : RCw=	-96.09 plf
RC(d+l)=	149.50 plf
Frame : RC(d+w)=	-76.59 plf

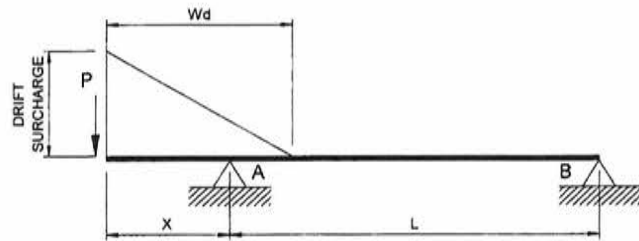
RDd=	15.73 plf
RDI=	135.00 plf
Frame : RDw=	-90.02 plf
RD(d+l)=	150.73 plf
Frame : RD(d+w)=	-74.29 plf

REd=	29.98 plf
REI=	144.05 plf
Frame : REw=	-106.48 plf
RE(d+l)=	174.03 plf
Frame : RE(d+w)=	-76.50 plf

USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksi

$w_d = 3.00$ psf
 $w_s = 20.00$ psf
 Deck : $w_w = -22.85$ psf
 Frame : $w_w = -14.78$ psf
 $P = 5.83$ plf
 (Drift Surcharge) $P_m = 20.98$ psf
 $L = 6.50$ ft
 $X = 1.79$ ft
 (Drift Length) $W_d = 5.06$ ft



$RA_d = 23.31$ plf	$RB_d = 7.40$ plf
$RA_s = 159.68$ plf	$RB_s = 59.19$ plf
Frame : $RA_w = -78.18$ plf	Frame : $RB_w = -44.40$ plf
Deck : $RA_w = -120.83$ plf	Deck : $RB_w = -68.61$ plf
$RA(d+s) = 182.98$ plf	$RB(d+s) = 66.59$ plf
Frame : $RA(d+w) = -54.88$ plf	Frame : $RB(d+w) = -36.99$ plf
Deck : $RA(d+w) = -97.52$ plf	Deck : $RB(d+w) = -61.21$ plf
$MA_d = -15.27$ ft-lbs/ft	
$MA_s = -61.80$ ft-lbs/ft	
Deck : $MA_w = 36.67$ ft-lbs/ft	
$MA(d+s) = -77.06$ ft-lbs/ft	$MAB(d+s) = 96.41$ ft-lbs/ft
Deck : $MA(d+w) = 21.40$ ft-lbs/ft	Deck : $MAB(d+w) = -94.39$ ft-lbs/ft

USE 20 GAUGE GRADE C DECK

$+S=.3961$ in³ $-S=.3036$ in³ $FY=40$ ksi

DECK DESIGN:

Deck 1

$W_d = 3.00$ psf	23.00 psf
$W_l = 20.00$ psf	$\hat{A}$ $\hat{B}$
Deck : $W_w = -22.85$ psf	$ <----- L -----> $
Frame : $W_w = -14.78$ psf	
$L = 6.50$ ft	$R_d = 9.75$ plf
	$R_l = 65.00$ plf
	Frame : $R_w = -48.05$ plf
	Deck : $R_w = -74.25$ plf
$M(d+l) = 121.47$ ft-lbs/ft	$R(d+l) = 74.75$ plf
Deck : $M(d+w) = -104.82$ ft-lbs/ft	Frame : $R(d+w) = -38.30$ plf
	Deck : $R(d+w) = -64.50$ plf

USE 20 GAUGE GRADE C DECK

$+S=.3961$ in³ $-S=.3036$ in³ $FY=40$ ksi

BEAM DESIGN:		P-a	
Wd=	36.11	plf	P
Wl=	158.28	plf	v
Ww=	-77.40	plf	194.39 plf
Pd=	30.54	lbs	^A B^
Pl=	0.00	lbs	<----X----> <----- L ----->
Pw=	0.00	lbs	
L=	12.00	ft	
X=	2.00	ft	
		Deflections: (inches)	Overhang Midspan
		DL=	-0.006 0.013
		DL+LL=	-0.036 0.073
		(+downward, -upward)	
MA(d) =	133	ft-lbs	RA d= 331 lbs
MA(l) =	317	ft-lbs	RA l= 1293 lbs
MA(w) =	-155	ft-lbs	RA w= -632 lbs
MA(d+l) =	450	ft-lbs lu=	RA(d+l)= 1623 lbs
MA(d+w) =	-21	ft-lbs lu=	RA(d+w)= -302 lbs
			RB d= 206 lbs
			RBI(Max)= 950 lbs
			RB w= -452 lbs
MAB(d+l)=	3433	ft-lbs lu=	RB(d+l)= 1155 lbs
MAB(d+w)=	-733	ft-lbs lu=	RB(d+w)= -246 lbs
USE: W8X13		Fy =	50 ksi

BEAM DESIGN:		P-b	
Wd=	27.22	plf	P
Wl=	130.00	plf	v
Ww=	-92.61	plf	157.22 plf
Pd=	36.54	lbs	^A B^
Pl=	0.00	lbs	<----X----> <----- L ----->
Pw=	0.00	lbs	
L=	12.00	ft	
X=	2.00	ft	
		Deflections: (inches)	Overhang Midspan
		DL=	-0.005 0.012
		DL+LL=	-0.037 0.075
		(+downward, -upward)	
MA(d) =	128	ft-lbs	RA d= 265 lbs
MA(l) =	260	ft-lbs	RA l= 1062 lbs
MA(w) =	-185	ft-lbs	RA w= -756 lbs
MA(d+l) =	388	ft-lbs lu=	RA(d+l)= 1327 lbs
MA(d+w) =	-58	ft-lbs lu=	RA(d+w)= -491 lbs
			RB d= 153 lbs
			RBI(Max)= 780 lbs
			RB w= -540 lbs
MAB(d+l)=	2767	ft-lbs lu=	RB(d+l)= 933 lbs
MAB(d+w)=	-1148	ft-lbs lu=	RB(d+w)= -388 lbs
USE: W8X10		Fy =	50 ksi

BEAM DESIGN:		P-c	
Wd=	29.50 plf	P	
Wl=	130.00 plf	v	159.50 plf
Ww=	-96.09 plf		^A B^
Pd=	37.92 lbs	<----X---->	<----- L ----->
Pl=	0.00 lbs		
Pw=	0.00 lbs		
L=	12.00 ft		
X=	2.00 ft		
		Deflections: (inches)	Overhang Midspan
		DL=	-0.006 0.013
		DL+LL=	-0.038 0.076
		(+downward, -upward)	
MA(d) =	135 ft-lbs		RA d= 285 lbs
MA(l) =	260 ft-lbs		RA l= 1062 lbs
MA(w) =	-192 ft-lbs		RA w= -785 lbs
MA(d+l) =	395 ft-lbs lu=	1.33 ft	RA(d+l)= 1347 lbs
MA(d+w) =	-57 ft-lbs lu=	2.00 ft	RA(d+w)= -500 lbs
			RB d= 166 lbs
			RB l(Max)= 780 lbs
			RB w= -561 lbs
MAB(d+l)=	2804 ft-lbs lu=	6.00 ft	RB(d+l)= 946 lbs
MAB(d+w)=	-1170 ft-lbs lu=	1.33 ft	RB(d+w)= -395 lbs
USE: W8X10		Fy =	50 ksi

BEAM DESIGN:		P-d	
Wd=	25.73 plf	P	
Wl=	135.00 plf	v	160.73 plf
Ww=	-90.02 plf		^A B^
Pd=	35.52 lbs	<----X---->	<----- L ----->
Pl=	0.00 lbs		
Pw=	0.00 lbs		
L=	12.00 ft		
X=	2.00 ft		
		Deflections: (inches)	Overhang Midspan
		DL=	-0.005 0.011
		DL+LL=	-0.038 0.077
		(+downward, -upward)	
MA(d) =	123 ft-lbs		RA d= 252 lbs
MA(l) =	270 ft-lbs		RA l= 1103 lbs
MA(w) =	-180 ft-lbs		RA w= -735 lbs
MA(d+l) =	393 ft-lbs lu=	1.33 ft	RA(d+l)= 1354 lbs
MA(d+w) =	-58 ft-lbs lu=	2.00 ft	RA(d+w)= -484 lbs
			RB d= 144 lbs
			RB l(Max)= 810 lbs
			RB w= -525 lbs
MAB(d+l)=	2832 ft-lbs lu=	6.00 ft	RB(d+l)= 954 lbs
MAB(d+w)=	-1129 ft-lbs lu=	1.33 ft	RB(d+w)= -381 lbs
USE: W8X10		Fy =	50 ksi

BEAM DESIGN:

P-g

Wd= 27.22 plf
 Wl= 130.00 plf
 Ww= -92.61 plf
 L= 11.42 ft

157.22 plf

^ ^
 |<----- L ----->|

Md= 443.5 ft-lbs
 Ml= 2118.0 ft-lbs
 Mw= -1508.9 ft-lbs

Rd= 155 lbs
 Rl= 742 lbs
 Rw= -529 lbs
 R(d+l)= 897 lbs
 R(d+w)= -373 lbs

M(d+l)= 2561.6 ft-lbs
 M(d+w)= -1065.3 ft-lbs

Lu= 11.42 ft OK
 Lu= 1.33 ft OK

USE: W8X10

Fy =

50 ksi

Deflections: (inches)

Midspan

DL=

0.012

DL+LL=

0.067

(+downward, -upward)

BEAM DESIGN:

P-h

Wd= 29.50 plf
 Wl= 130.00 plf
 Ww= -96.09 plf
 L= 11.42 ft

159.50 plf

^ ^
 |<----- L ----->|

Md= 480.6 ft-lbs
 Ml= 2118.0 ft-lbs
 Mw= -1565.6 ft-lbs

Rd= 168 lbs
 Rl= 742 lbs
 Rw= -549 lbs
 R(d+l)= 910 lbs
 R(d+w)= -380 lbs

M(d+l)= 2598.7 ft-lbs
 M(d+w)= -1085.0 ft-lbs

Lu= 11.42 ft OK
 Lu= 1.33 ft OK

USE: W8X10

Fy =

50 ksi

Deflections: (inches)

Midspan

DL=

0.013

DL+LL=

0.068

(+downward, -upward)

BEAM DESIGN: P-i

Wd= 25.73 plf
 WI= 135.00 plf
 Ww= -90.02 plf
 L= 11.42 ft

160.73 plf
 ^ ^
 |<----- L ----->|

Md= 419.3 ft-lbs
 MI= 2199.5 ft-lbs
 Mw= -1466.6 ft-lbs

Rd= 147 lbs
 RI= 771 lbs
 Rw= -514 lbs
 R(d+I)= 918 lbs
 R(d+w)= -367 lbs

M(d+I)= 2618.7 ft-lbs
 M(d+w)= -1047.4 ft-lbs

Lu= 11.42 ft OK
 Lu= 1.33 ft OK

USE: W8X10 Fy = 50 ksi

Deflections: (inches) Midspan
 DL= 0.011
 DL+LL= 0.069
 (+downward, -upward)

BEAM DESIGN: P-j

Wd= 39.98 plf
 WI= 144.05 plf
 Ww= -106.48 plf
 L= 11.42 ft

184.03 plf
 ^ ^
 |<----- L ----->|

Md= 651.3 ft-lbs
 MI= 2346.9 ft-lbs
 Mw= -1734.8 ft-lbs

Rd= 228 lbs
 RI= 822 lbs
 Rw= -608 lbs
 R(d+I)= 1050 lbs
 R(d+w)= -380 lbs

M(d+I)= 2998.2 ft-lbs
 M(d+w)= -1083.5 ft-lbs

Lu= 11.42 ft OK
 Lu= 1.33 ft OK

USE: W8X10 Fy = 50 ksi

Deflections: (inches) Midspan
 DL= 0.017
 DL+LL= 0.079
 (+downward, -upward)

BEAM DESIGN: P-k

Wd=	33.59	plf			
WI=	99.15	plf			
Ww=	-42.88	plf			
L=	23.35	ft			
	132.74	plf			
	$\overline{\Lambda}$				
	<----- L ----->				
			Rd=	392	lbs
			RI=	1158	lbs
			Rw=	-501	lbs
Md=	2289.8	ft-lbs			
MI=	6759.7	ft-lbs	R(d+l)=	1550	lbs
Mw=	-2923.8	ft-lbs	R(d+w)=	-109	lbs
M(d+l)=	9049.5	ft-lbs	Lu=	7.78	ft
M(d+w)=	-634.0	ft-lbs	Lu=	1.33	ft
					OK
					OK

USE: W8X18 Fy = 50 ksi

Deflections: (inches)	Midspan
DL=	0.125
DL+LL=	0.495
(+downward, -upward)	

BEAM DESIGN: P-l

Wd=	32.75	plf			
WI=	117.22	plf			
Ww=	-77.85	plf			
L=	23.35	ft			
	149.97	plf			
	$\overline{\Lambda}$				
	<----- L ----->				
			Rd=	382	lbs
			RI=	1369	lbs
			Rw=	-909	lbs
Md=	2232.6	ft-lbs			
MI=	7991.7	ft-lbs	R(d+l)=	1751	lbs
Mw=	-5307.5	ft-lbs	R(d+w)=	-527	lbs
M(d+l)=	10224.4	ft-lbs	Lu=	7.78	ft
M(d+w)=	-3074.8	ft-lbs	Lu=	1.33	ft
					OK
					OK

USE: W8X18 Fy = 50 ksi

Deflections: (inches)	Midspan
DL=	0.122
DL+LL=	0.559
(+downward, -upward)	

BEAM DESIGN: P-m

Wd= 37.50 plf
Wl= 130.00 plf
Ww= -96.09 plf
L= 23.35 ft

167.50 plf
^ ^
|<----- L ----->|

Md= 2556.6 ft-lbs
Ml= 8863.0 ft-lbs
Mw= -6551.4 ft-lbs

Rd= 438 lbs
Rl= 1518 lbs
Rw= -1122 lbs
R(d+l)= 1956 lbs
R(d+w)= -684 lbs

M(d+l)= 11419.7 ft-lbs
M(d+w)= -3994.7 ft-lbs

Lu= 7.78 ft OK
Lu= 1.33 ft OK

USE: W8X18 Fy = 50 ksi

Deflections: (inches) Midspan
DL= 0.140
DL+LL= 0.625
(+downward, -upward)

BEAM DESIGN: P-n

Wd= 33.73 plf
Wl= 135.00 plf
Ww= -90.02 plf
L= 23.35 ft

168.73 plf
^ ^
|<----- L ----->|

Md= 2299.8 ft-lbs
Ml= 9203.9 ft-lbs
Mw= -6137.3 ft-lbs

Rd= 394 lbs
Rl= 1576 lbs
Rw= -1051 lbs
R(d+l)= 1970 lbs
R(d+w)= -657 lbs

M(d+l)= 11503.7 ft-lbs
M(d+w)= -3837.5 ft-lbs

Lu= 7.78 ft OK
Lu= 1.33 ft OK

USE: W8X18 Fy = 50 ksi

Deflections: (inches) Midspan
DL= 0.126
DL+LL= 0.629
(+downward, -upward)

BEAM DESIGN:

P-o

Wd= 47.98 plf
 Wl= 144.05 plf
 Ww= -106.48 plf
 L= 23.35 ft

192.03 plf

^ ^

|<----- L ----->|

Md= 3270.8 ft-lbs
 Ml= 9820.9 ft-lbs
 Mw= -7259.4 ft-lbs

Rd= 560 lbs
 Rl= 1682 lbs
 Rw= -1243 lbs
 R(d+l)= 2242 lbs
 R(d+w)= -683 lbs

M(d+l)= 13091.8 ft-lbs
 M(d+w)= -3988.6 ft-lbs

Lu= 7.78 ft OK
 Lu= 1.33 ft OK

USE: W8X18

Fy = 50 ksi

Deflections: (inches)

Midspan

DL= 0.179

DL+LL= 0.716

(+downward, -upward)

BEAM DESIGN:

P-p

Wd= 36.31 plf
 Wl= 159.68 plf
 Ww= -78.18 plf
 Pd= 19.69 lbs
 Pl= 0.00 lbs
 Pw= 0.00 lbs
 L= 12.75 ft
 X= 1.13 ft

| P

v 195.98 plf

^A B^

|<----X---->|<----- L ----->|

Deflections: (inches)

Overhang

Midspan

DL= -0.005 0.018

DL+LL= -0.028 0.099

(+downward, -upward)

MA(d) = 45 ft-lbs
 MA(l) = 101 ft-lbs
 MA(w) = -49 ft-lbs

RAd= 296 lbs
 RAl= 1206 lbs
 RAw= -590 lbs

MA(d+l) = 146 ft-lbs lu= 1.33 ft
 MA(d+w) = -4 ft-lbs lu= 1.13 ft

RA(d+l)= 1501 lbs
 RA(d+w)= -295 lbs

RBd= 228 lbs
 RB(Max)= 1018 lbs
 RBw= -495 lbs

MAB(d+l)= 3960 ft-lbs lu= 6.38 ft
 MAB(d+w)= -849 ft-lbs lu= 1.33 ft

RB(d+l)= 1246 lbs
 RB(d+w)= -267 lbs

USE: W8X13

Fy = 50 ksi

BEAM DESIGN:

P-q

Wd= 27.15 plf
 Wl= 130.00 plf
 Ww= -92.44 plf
 L= 12.75 ft

157.15 plf

^ ^
 |<----- L ----->|

		Rd=	173 lbs	
		RI=	829 lbs	
		Rw=	-589 lbs	
Md=	551.7 ft-lbs	R(d+l)=	1002 lbs	
MI=	2641.6 ft-lbs	R(d+w)=	-416 lbs	
Mw=	-1878.5 ft-lbs			
M(d+l)=	3193.4 ft-lbs	Lu=	6.38 ft	OK
M(d+w)=	-1326.7 ft-lbs	Lu=	1.33 ft	OK

USE: W8X10

Fy =

50 ksi

Deflections: (inches)

Midspan

DL=

0.018

DL+LL=

0.105

(+downward, -upward)

BEAM DESIGN:

P-r

Wd= 29.50 plf
 Wl= 130.00 plf
 Ww= -96.09 plf
 L= 12.75 ft

159.50 plf

^ ^
 |<----- L ----->|

		Rd=	188 lbs	
		RI=	829 lbs	
		Rw=	-613 lbs	
Md=	599.4 ft-lbs	R(d+l)=	1017 lbs	
MI=	2641.6 ft-lbs	R(d+w)=	-425 lbs	
Mw=	-1952.6 ft-lbs			
M(d+l)=	3241.1 ft-lbs	Lu=	6.38 ft	OK
M(d+w)=	-1353.2 ft-lbs	Lu=	1.33 ft	OK

USE: W8X10

Fy =

50 ksi

Deflections: (inches)

Midspan

DL=

0.020

DL+LL=

0.106

(+downward, -upward)

BEAM DESIGN: P-s

Wd= 25.73 plf
 Wl= 135.00 plf
 Ww= -90.02 plf
 L= 12.75 ft

160.73 plf
 ^ ^
 |<----- L ----->|

Md= 522.9 ft-lbs	Rd= 164 lbs	
MI= 2743.2 ft-lbs	RI= 861 lbs	
Mw= -1829.2 ft-lbs	Rw= -574 lbs	
	R(d+l)= 1025 lbs	
	R(d+w)= -410 lbs	
M(d+l)= 3266.1 ft-lbs	Lu= 6.38 ft	OK
M(d+w)= -1306.3 ft-lbs	Lu= 1.33 ft	OK

USE: W8X10 Fy = 50 ksi

Deflections: (inches)	Midspan
DL=	0.017
DL+LL=	0.107
(+downward, -upward)	

BEAM DESIGN: P-t

Wd= 39.98 plf
 Wl= 144.05 plf
 Ww= -106.48 plf
 L= 12.75 ft

184.03 plf
 ^ ^
 |<----- L ----->|

Md= 812.3 ft-lbs	Rd= 255 lbs	
MI= 2927.1 ft-lbs	RI= 918 lbs	
Mw= -2163.7 ft-lbs	Rw= -679 lbs	
	R(d+l)= 1173 lbs	
	R(d+w)= -424 lbs	
M(d+l)= 3739.5 ft-lbs	Lu= 6.38 ft	OK
M(d+w)= -1351.4 ft-lbs	Lu= 1.33 ft	OK

USE: W8X10 Fy = 50 ksi

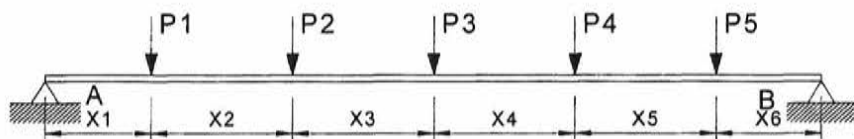
Deflections: (inches)	Midspan
DL=	0.027
DL+LL=	0.123
(+downward, -upward)	

BEAM DESIGN:		P-u	
Wd=	36.31	plf	P
Wl=	159.68	plf	v 195.98 plf
Ww=	-78.18	plf	^A B^
Pd=	30.85	lbs	<-----X-----> <----- L ----->
Pl=	0.00	lbs	
Pw=	0.00	lbs	
L=	13.50	ft	
X=	1.35	ft	
		Deflections: (inches)	Overhang Midspan
		DL=	-0.007 0.022
		DL+LL=	-0.039 0.124
		(+downward, -upward)	
MA(d) =	75	ft-lbs	RA _d = 331 lbs
MA(l) =	146	ft-lbs	RA _l = 1305 lbs
MA(w) =	-72	ft-lbs	RA _w = -639 lbs
MA(d+l) =	221	ft-lbs lu=	RA(d+l)= 1636 lbs
MA(d+w) =	3	ft-lbs lu=	RA(d+w)= -308 lbs
			RB _d = 240 lbs
			RBI(Max)= 1078 lbs
			RB _w = -522 lbs
MAB(d+l)=	4427	ft-lbs lu=	RB(d+l)= 1317 lbs
MAB(d+w)=	-956	ft-lbs lu=	RB(d+w)= -283 lbs
USE: W8X13		Fy =	50 ksi

BEAM DESIGN:		P-v	
Wd=	27.15	plf	P
Wl=	130.00	plf	v 157.15 plf
Ww=	-92.44	plf	^A B^
Pd=	36.48	lbs	<-----X-----> <----- L ----->
Pl=	0.00	lbs	
Pw=	0.00	lbs	
L=	13.50	ft	
X=	1.35	ft	
		Deflections: (inches)	Overhang Midspan
		DL=	-0.006 0.021
		DL+LL=	-0.040 0.127
		(+downward, -upward)	
MA(d) =	74	ft-lbs	RA _d = 262 lbs
MA(l) =	119	ft-lbs	RA _l = 1062 lbs
MA(w) =	-85	ft-lbs	RA _w = -755 lbs
MA(d+l) =	193	ft-lbs lu=	RA(d+l)= 1324 lbs
MA(d+w) =	-10	ft-lbs lu=	RA(d+w)= -493 lbs
			RB _d = 178 lbs
			RBI(Max)= 878 lbs
			RB _w = -618 lbs
MAB(d+l)=	3543	ft-lbs lu=	RB(d+l)= 1055 lbs
MAB(d+w)=	-1482	ft-lbs lu=	RB(d+w)= -440 lbs
USE: W8X10		Fy =	50 ksi

BEAM DESIGN:		P-y			
Wd=	39.98	plf	P		
Wl=	144.05	plf	v	184.03	plf
Ww=	-106.48	plf	^A B^		
Pd=	174.86	lbs	<-----X----->	<-----	L ----->
Pl=	0.00	lbs			
Pw=	0.00	lbs	Deflections: (inches)	Overhang	Midspan
L=	13.50	ft	DL=	-0.007	0.027
X=	1.35	ft	DL+LL=	-0.044	0.145
			(+downward, -upward)		
MA(d) =	273	ft-lbs	RA d= 519 lbs		
MA(l) =	132	ft-lbs	RA l= 1177 lbs		
MA(w) =	-98	ft-lbs	RA w= -870 lbs		
MA(d+l) =	406	ft-lbs lu=	1.33	ft	RA(d+l)= 1696 lbs
MA(d+w) =	176	ft-lbs lu=	1.35	ft	RA(d+w)= -351 lbs
			RB d= 250 lbs		
			RB l(Max)= 972 lbs		
			RB w= -712 lbs		
MAB(d+l)=	4057	ft-lbs lu=	6.75	ft	RB(d+l)= 1222 lbs
MAB(d+w)=	-1604	ft-lbs lu=	1.33	ft	RB(d+w)= -462 lbs
USE: W8X10			Fy =	50	ksi

P1d= 331 lbs
P1l= 1293 lbs
P1w= -632 lbs
P2d= 265 lbs
P2l= 1062 lbs
P2w= -756 lbs
P3d= 285 lbs
P3l= 1062 lbs
P3w= -785 lbs
P4d= 252 lbs
P4l= 1103 lbs
P4w= -735 lbs
P5d= 375 lbs
P5l= 1176 lbs
P5w= -870 lbs



X1 = 1.08 ft
X2 = 6.50 ft
X3 = 6.50 ft
X4 = 6.50 ft
X5 = 7.00 ft
X6 = 1.25 ft
L = 28.83 ft

Wd= 40.00 plf
Wl= 0.00 plf
Ww= 0.00 plf

RA(d)= 1324 lbs
RA(l)= 2936 lbs
RA(w)= -1815 lbs
RA(d+l)= 4260 lbs
RA(d+w)= -491 lbs

RB(d)= 1337 lbs
RB(l)= 2759 lbs
RB(w)= -1963 lbs
RB(d+l)= 4096 lbs
RB(d+w)= -626 lbs

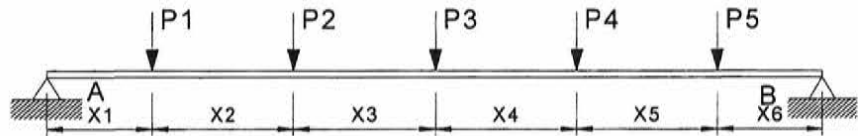
Deflection

dl= 0.30 in
dl+l= 0.90 in

Mspan(d+l) = 26307.6 ft-lbs lu= 7.00 ft
Mspan(d+w) = -3768.4 ft-lbs lu= 7.00 ft

USE: W8X40 Fy = 50 ksi

P1d= 409 lbs
P1l= 1853 lbs
P1w= -890 lbs
P2d= 308 lbs
P2l= 1522 lbs
P2w= -1069 lbs
P3d= 334 lbs
P3l= 1522 lbs
P3w= -1109 lbs
P4d= 291 lbs
P4l= 1581 lbs
P4w= -1039 lbs
P5d= 454 lbs
P5l= 1687 lbs
P5w= -1229 lbs



X1 = 1.08 ft
X2 = 6.50 ft
X3 = 6.50 ft
X4 = 6.50 ft
X5 = 7.00 ft
X6 = 1.25 ft
L = 28.83 ft

Wd= 58.00 plf
Wl= 0.00 plf
Ww= 0.00 plf

RA(d)= 1730 lbs
RA(l)= 4209 lbs
RA(w)= -2562 lbs
RA(d+l)= 5940 lbs
RA(d+w)= -832 lbs

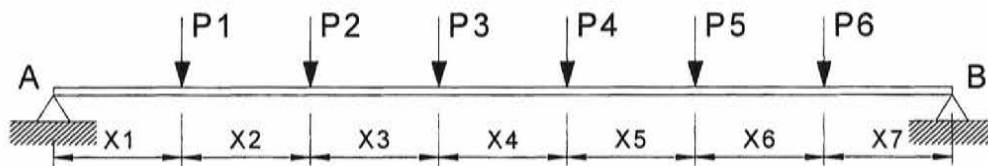
RB(d)= 1738 lbs
RB(l)= 3955 lbs
RB(w)= -2774 lbs
RB(d+l)= 5693 lbs
RB(d+w)= -1035 lbs

Deflection

dl= 0.25 in
dl+ll= 0.80 in

Mspan(d+l) = 36600.2 ft-lbs lu= 7.00 ft
Mspan(d+w) = -6263.6 ft-lbs lu= 7.00 ft

USE: W8X58 Fy = 50 ksi



P1d= 263 lbs
 P1l= 1062 lbs
 P1w= -519 lbs
 P2d= 392 lbs
 P2l= 1158 lbs
 P2w= -501 lbs
 P3d= 538 lbs
 P3l= 2111 lbs
 P3w= -1438 lbs
 P4d= 606 lbs
 P4l= 2260 lbs
 P4w= -1671 lbs
 P5d= 541 lbs
 P5l= 2347 lbs
 P5w= -1565 lbs
 P6d= 788 lbs
 P6l= 2504 lbs
 P6w= -1851 lbs

Wd = 54.00 plf
 Wl = 0.00 plf
 Ww = 0.00 plf

X1= 1.08 ft
 X2= 2.33 ft
 X3= 4.17 ft
 X4= 6.50 ft
 X5= 6.50 ft
 X6= 7.00 ft
 X7= 1.25 ft
 L = 28.83 ft

RA(d)= 2273 lbs
 RA(l)= 5534 lbs
 RA(w)= -3383 lbs

 RA(d+l)= 7807 lbs
 RA(d+w)= -1110 lbs

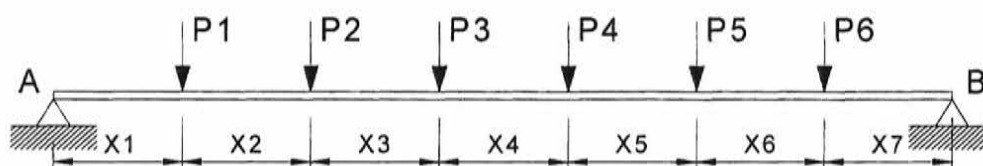
RB(d)= 2413 lbs
 RB(l)= 5907 lbs
 RB(w)= -4161 lbs

 RB(d+l)= 8320 lbs
 RB(d+w)= -1748 lbs

Mspan(d+l) = 53625.1 ft-lbs Lu= 7.00 ft
 Mspan(d+w) = -10658.1 ft-lbs Lu= 7.00 ft

DL Defl. = 0.26 in.
 DL+LL Defl. = 0.89 in.

USE: W10X54 Fy = 50 ksi



P1d= 296 lbs
 P1l= 1206 lbs
 P1w= -590 lbs
 P2d= 392 lbs
 P2l= 1158 lbs
 P2w= -501 lbs
 P3d= 555 lbs
 P3l= 2198 lbs
 P3w= -1498 lbs
 P4d= 626 lbs
 P4l= 2347 lbs
 P4w= -1735 lbs
 P5d= 558 lbs
 P5l= 2437 lbs
 P5w= -1625 lbs
 P6d= 815 lbs
 P6l= 2600 lbs
 P6w= -1922 lbs

Wd = 54.00 plf
 Wl = 0.00 plf
 Ww = 0.00 plf
 X1= 1.08 ft
 X2= 2.33 ft
 X3= 4.17 ft
 X4= 6.50 ft
 X5= 6.50 ft
 X6= 7.00 ft
 X7= 1.25 ft
 L = 28.83 ft

RA(d)= 2333 lbs
 RA(l)= 5811 lbs
 RA(w)= -3549 lbs
 RA(d+l)= 8144 lbs
 RA(d+w)= -1216 lbs

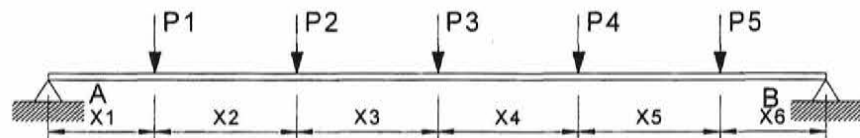
RB(d)= 2466 lbs
 RB(l)= 6134 lbs
 RB(w)= -4322 lbs
 RB(d+l)= 8600 lbs
 RB(d+w)= -1856 lbs

Mspan(d+l) = 55400.4 ft-lbs Lu= 7.00 ft
 Mspan(d+w) = -11366.0 ft-lbs Lu= 7.00 ft

DL Defl. = 0.26 in.
 DL+LL Defl. = 0.92 in.

USE: W10X54 Fy = 50 ksi

P1d= 467 lbs
P1l= 2096 lbs
P1w= -1017 lbs
P2d= 351 lbs
P2l= 1706 lbs
P2w= -1207 lbs
P3d= 381 lbs
P3l= 1706 lbs
P3w= -1255 lbs
P4d= 332 lbs
P4l= 1772 lbs
P4w= -1175 lbs
P5d= 504 lbs
P5l= 1891 lbs
P5w= -1390 lbs



X1 = 1.08 ft
X2 = 6.50 ft
X3 = 6.50 ft
X4 = 6.50 ft
X5 = 7.00 ft
X6 = 1.25 ft
L = 28.83 ft

Wd= 58.00 plf
Wl= 0.00 plf
Ww= 0.00 plf

RA(d)= 1857 lbs
RA(l)= 4736 lbs
RA(w)= -2907 lbs
RA(d+l)= 6593 lbs
RA(d+w)= -1050 lbs

Deflection

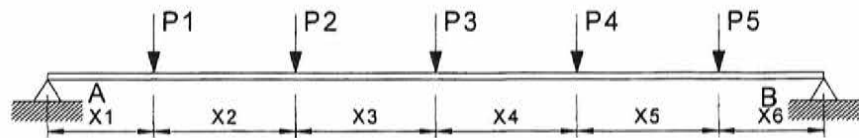
dl= 0.27 in
dl+ll= 0.89 in

RB(d)= 1852 lbs
RB(l)= 4434 lbs
RB(w)= -3138 lbs
RB(d+l)= 6287 lbs
RB(d+w)= -1285 lbs

Mspan(d+l) = 40407.0 ft-lbs lu= 7.00 ft
Mspan(d+w) = -7831.3 ft-lbs lu= 7.00 ft

USE: W8X58 Fy = 50 ksi

P1d= 331 lbs
P1l= 1305 lbs
P1w= -639 lbs
P2d= 262 lbs
P2l= 1062 lbs
P2w= -755 lbs
P3d= 283 lbs
P3l= 1062 lbs
P3w= -785 lbs
P4d= 249 lbs
P4l= 1103 lbs
P4w= -736 lbs
P5d= 519 lbs
P5l= 1177 lbs
P5w= -870 lbs



X1 = 1.08 ft
X2 = 6.50 ft
X3 = 6.50 ft
X4 = 6.50 ft
X5 = 7.00 ft
X6 = 1.25 ft
L = 28.83 ft

Wd= 40.00 plf
Wl= 0.00 plf
Ww= 0.00 plf

RA(d)= 1327 lbs
RA(l)= 2949 lbs
RA(w)= -1822 lbs
RA(d+l)= 4276 lbs
RA(d+w)= -495 lbs

RB(d)= 1471 lbs
RB(l)= 2761 lbs
RB(w)= -1964 lbs
RB(d+l)= 4232 lbs
RB(d+w)= -493 lbs

Deflection

dl= 0.30 in
dl+l= 0.91 in

Mspan(d+l) = 26376.1 ft-lbs lu= 7.00 ft
Mspan(d+w) = -3724.5 ft-lbs lu= 7.00 ft

USE: W8X40 Fy = 50 ksi

Column Design

AISC 15th ed, Use First Order Analysis Criteria

P DL =	2.47 kips	Clr. Ht.=	10.17 ft
P LL =	6.13 kips	Fascia Ht.=	1.00 ft
P WL =	-4.32 kips	Col. Trib=	18.05 ft
Base Shear =	0.20 kips	Wind Load=	16.00 psf
Total Base Shear =	1.89 kips	# of COL.=	2
M WL =	$w(\text{Fascia Ht} \cdot 2.5 \cdot \text{Col Trib} / \# \text{ of col} \cdot L) + w(\text{Wrap} \cdot 1/2 \text{ Clr. Ht}^2)$		Max All. Defl = 1.28 in
M Seis =	Base Shear x L		Max Defl Ratio = L / 100
M Unbal =	Live Load x Col. Trib.x (Canopy Width/2)^2/2		Max Defl. = 0.15 in, OK
L =	Clr. Ht. + Fascia Ht/2		
Pr =	8.60 kips	1.6Pr < 0.5Py First-Order Analysis Allowed (A-7-1)	
Py =	326.60 kips		
N =	0.00	•Yi (A-7-2)	
B2 =	1.05	OK, A-8-6	
M WL =	4.68	kip-ft	
M Seis =	2.18	kip-ft	
M DL(Nod) =	0.11	kip-ft	
M LL(Nod) =	0.27	kip-ft	
M Unbal DL=	0.00	kip-ft	
M Unbal LL=	0.00	kip-ft	
M Unbal WL=	0.00	kip-ft	

Use: TS8X8X1/4	
Fy =	46.00 ksi
K =	1.00
L, Col =	10.67 ft
A =	7.10 in^2
I =	70.70 in^4
Cm =	1.00
Pe1 =	393.14 kips
B1 =	1.04 (A-8-3)
P, All =	175.01 kips
M, All =	44.10 kip-ft

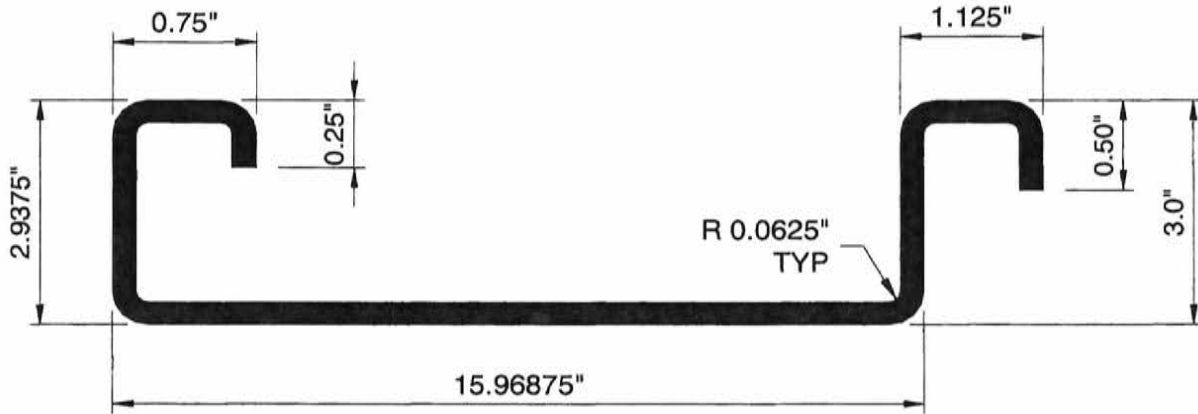
Load Combination	Pr, Kips	Mr, Kip-ft	Equation	Result
D+L	8.60	0.40	0.03	OK
D+W	2.47	4.96	0.12	OK
D+0.7E	2.47	1.70	0.05	OK
D+0.75W+0.75L	7.07	3.96	0.11	OK
D+0.525E+0.75L	7.07	1.52	0.05	OK

Top Connection : Standard Cap Plate	Base Plate : LBP 8 - 20
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FOOTING DESIGNED BY OTHERS



120 Fairview
Arlington, Texas 76010
817-261-9116



SL-316 DECK PANEL

Section Properties

Gage	Wt, psf	Thickness, in	ASTM 653	+I, in ⁴	-I, in ⁴	+S, in ³	-S, in ³	+M, ft-lbs/ft	-M, ft-lbs/ft
20	2.20	0.0359	Grade 40	0.9346	0.4680	0.3961	0.3036	592.70	454.44
			Grade 50	0.9208	0.4522	0.3879	0.2880	725.86	538.92
18	2.93	0.0478	Grade 40	1.2486	0.6827	0.5329	0.4377	797.77	655.28
			Grade 50	1.2129	0.6518	0.5141	0.4296	962.09	803.92

Notes:

- 1 Designed per AISI Cold Formed Steel Manual, 2016 ed.
- 2 Complete calculations are available upon request.
- 3 $\pm M$ is allowable bending moment.

Issued 12-5-17



LANE SUPPLY, INC.

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817-261-9116
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STANDARD BASE PLATE DESIGN

LBP # (D - M)	M (ft-k)	P _{BOLT} (k)	Bolt Dia. (in)	t _{REQ'D} (in)	t _{ACTUAL} (in)	Weld Req'd (1/16 in)	Weld Actual (in)	Base Plate Mark
8 - 10	10	5.58	1 1/2	0.72	3/4	1.52	1/4	LBP 1
8 - 20	20	10.91	1 1/2	0.99	1	3.03	5/16	LBP 2
8 - 30	30	16.00	1 1/2	1.17	1 1/4	4.55	5/16	LBP 3
8 - 40	40	20.87	1 1/2	1.32	1 1/2	6.06	F.P.	LBP 4
8 - 50	50	26.09	1 1/2	1.46	1 1/2	7.58	F.P.	LBP 5

TS 8 X 8 COLUMN:

D= 8 in.

e= 2 in.

b,d= 8 in.

CONSTANTS:

A36 Steel Plate

E70xx Electrode

A307 Anchor Bolts

Fy = 36 ksi

Fw = 0.928 k/in/16th

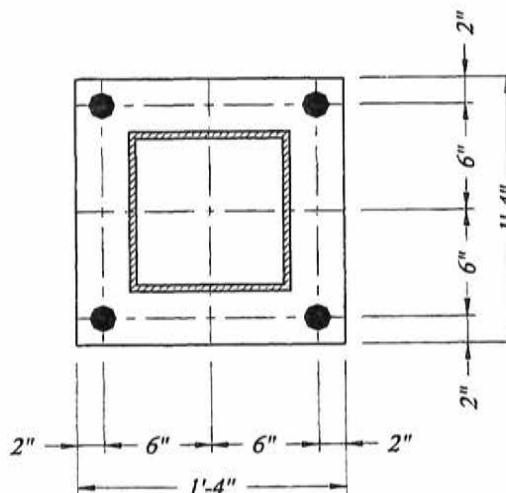
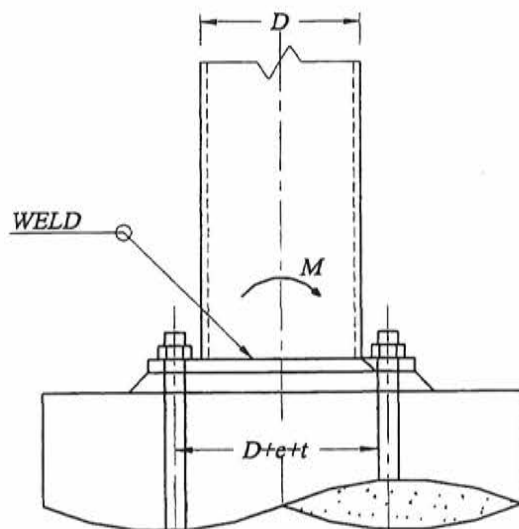
Ft = 20 ksi

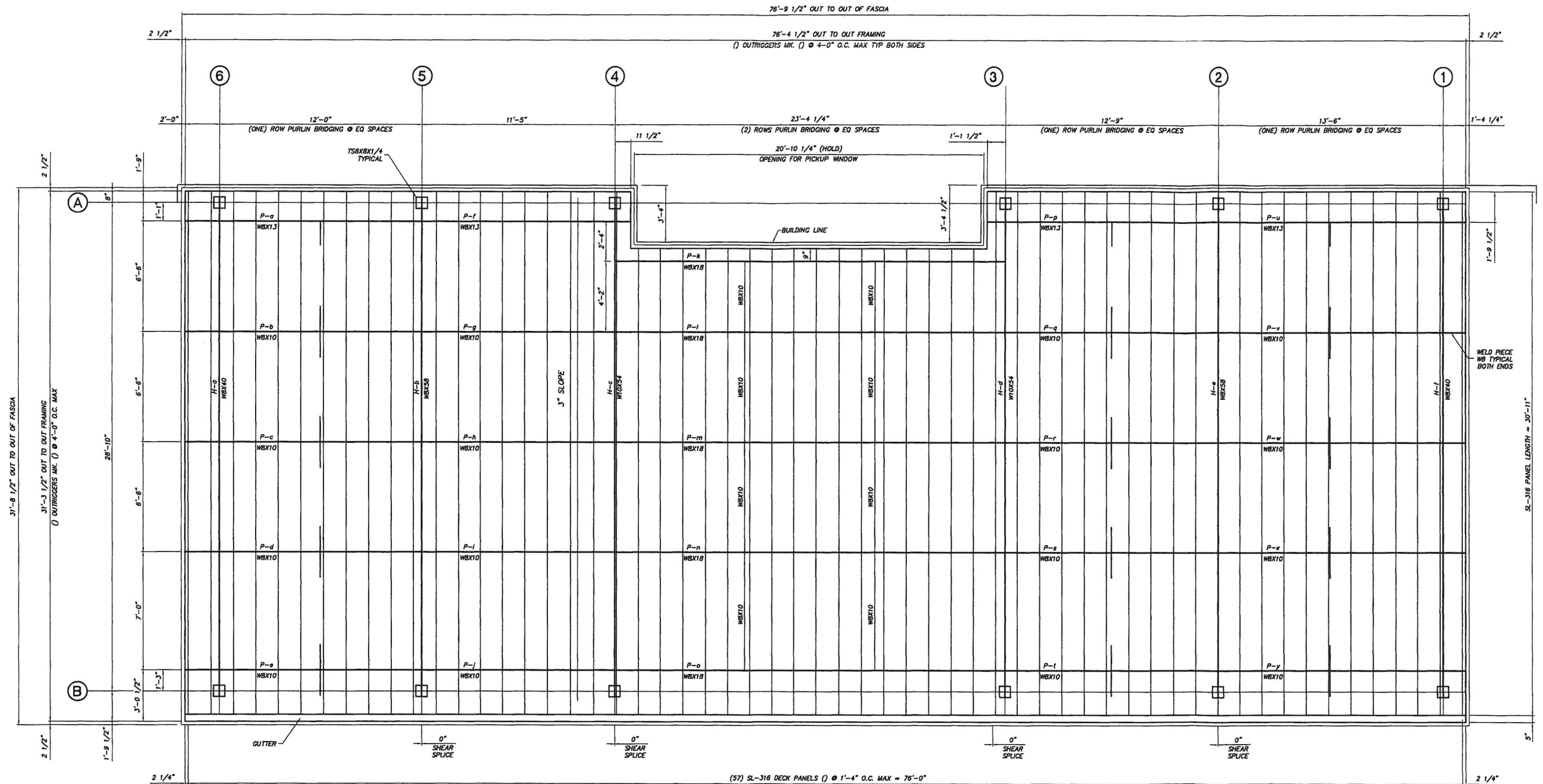
EQUATIONS:

$$P_{BOLT} = \frac{M \times 12 \text{ in/ft}}{2 \text{ bolts } (D+e+t)}$$

$$Weld = \frac{M \times 12 \text{ in/ft}}{S_{Weld} \times Fw} = \frac{M \times 12 \text{ in/ft}}{Fw (bd+d^2/3)}$$

$$t_{REQ'D} = \sqrt{\frac{6 \times P \times e \times 2 \text{ bolts}}{0.75 \times Fy \times (D+2t)}}$$





CANOPY LONGITUDINAL DIRECTION
 LOADS PRESENTED ARE ASD LOADS WITH FACTOR OF 1.0 EXCEPT WIND FACTORED WITH 0.6
 VERTICAL SIGN CONVENTION
 COLUMNS DESIGN LOADS:
 DEAD LOAD = 2.75 kips
 LIVE/SNOW LOAD = 6.25 kips
 WIND LOAD = -4.50 kips
 TRANSVERSE BASE MOMENT WIND $M_w = \pm 4.75$ ft-kips
 BASE MOMENT SEISMIC BOTH DIRECTIONS $M_s = \pm 2.25$ ft-kips
 $M_{dl}(nod) = 0.11$ ft-kips
 $M_{ll}(nod) = 0.27$ ft-kips
 TRANSVERSE BASE SHEAR WIND = ± 0.45 kips
 BASE SHEAR SEISMIC BOTH DIRECTIONS = ± 0.21 kips

DESIGN LOADS:

DEAD LOAD = 3 p.s.f.(DECK + LIGHTS) + WEIGHT OF STRUCTURAL COMPONENTS
 LIVE LOAD = 20 p.s.f.
 SNOW LOAD = 20 p.s.f.
 WIND LOAD $V_{ULT} = 116$ m.p.h. EXP. C
 WIND LOAD $V_{ASD} = 90$ m.p.h. EXP. C
 BLDG CODE = 2018 INTERNATIONAL BUILDING CODE
 EQUIVALENT LATERAL FORCE PROCEDURE
 LATERAL FORCE RESISTING SYSTEM = CANTILEVERED COLUMN SYSTEM-ORDINARY STEEL MOMENT FRAME
 $P_f = 20$ p.s.f.
 $C_e = 1.2$
 $C_t = 1.2$
 $I_s = 1.0$
 $W = 5.06$ ft
 $P_d = 20.98$ p.s.f.
 SITE CLASS = D (DEFAULT)
 $S_s(0.2) = 0.100$
 $S_1(1.0) = 0.068$
 $SDS = 0.107$
 $SD_1 = 0.109$
 $F_a = 1.60$
 $F_v = 2.40$
 $R = 1.25$
 IMPORTANCE FACTOR = 1.0
 RISK CATEGORY = II
 SEISMIC DESIGN CATEGORY = B
 $CS = 0.085$
 CONSTRUCTION TYPE = VB
 OCCUPANCY CATEGORY = M
 TOTAL SEISMIC BASE SHEAR BOTH DIRECTIONS = 1.89 KIPS