MACRO STORM WATER DRAINAGE STUDY

Oldham Village

SW Quadrant SW Oldham Parkway & MO 291 South

Site Acreage: 49.68 Acres (Future Buildout)

Lee's Summit, MO

PREPARED BY:



Prepared On: May 22, 2024

Revision

Matthew J. Schlicht, PE

Date	Comment	Ву
6-25-24	Revised Per city Comment	AEP
11-1-24	Revised Design & per City Comment	AEP



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3. GENERAL INFORMATION

The macro storm study has been prepared to evaluate potential negative downstream hydraulic impacts and propose potential mitigation measures associated with the redevelopment of the proposed Planned Mixed Use Development, Oldham Village. The proposed redevelopment will consist of three multi-family communities in addition to multiple commercial establishments. The site is located at the southwest corner of SW Oldham Parkway and MO 291 Highway. The proposed master development contains 45.41 acres with future potential up to 49.68 acres. The existing site is developed and contains primarily hard surface. An existing earthen detention basin is located on the southwest corner of the site. The detention basin drains into the upper most reach of Cedar Creek. The site consists of land located in Section 7, Township 47 North, and Range 31 West. See Exhibit A for an aerial view of the site along with a historical aerial of the site and surrounding area. A proposed site plan is also included in Exhibit A.

3.1 FEMA FLOODPLAIN DETERMINATION

The property is located in an Area of Minimal Flood Hazard, Zone X, according to Flood Emergency Management Agency (FEMA) Firm Map Number 29095C0419G, effective January 20, 2017.

See Exhibit B for a FEMA FIRMette which includes the proposed project area.

3.2 NRCS SOIL CLASSIFICATION

Soil classifications published by the United States Department of Agriculture/National Resources Conservation Service (USDA/NRCS) website for Jackson County, Missouri, Version 24, August 31, 2022. The existing site contains three major soil types:

10082 Arisburg-Urban Land Complex, 1 to 5 Percent Slopes

Hydrologic Soils Group (HSG): Type C

10181 Udarents-Urban Land-Sampsel Complex, 5 to 9 Percent Slopes

(HSG): Type C

99033 Udarents-Urban Land Complex, 2 to 9 Percent Slopes

(HSG): Type C

See Exhibit C for a detailed soils report of the proposed project site.

4. METHODOLOGY

This Macro Storm Drainage Study has been prepared to evaluate potential hydrologic impacts from the proposed redevelopment and recommend improvements to eliminate any potential negative impacts. The study utilized existing contours to create the Existing Drainage Area Map. The study conforms to the requirements of the City of Lee's Summit, Missouri "Design and Construction Manual" and all applicable codes and criteria referred to therein. If attenuation is to be employed it shall meet the Comprehensive Control Strategy with extended detention as outlined in APWA Section 5600.

Using the above criteria, the proposed site was evaluated using SCS Methods to calculate storm runoff volumes, peak rates of discharge, existing and proposed hydrographs and required storage volumes for attenuation facilities. The analysis contains results for the 2, 10 and 100-year design storms.

5. EXISTING CONDITIONS ANALYSIS

The site consists of one (1) drainage basin. The basin includes a substantial amount of offsite area to the north, south and east. The basin drains to Point of Interest A located approximately 260 feet west of the sites western

property boundary. POI A is the termination point for the FEMA FIS on Cedar Creek. The tributary area to the POI is 147.45+/- acres. The basin consists of 49.68 acres of proposed master development which includes potential future parcels and 97.77 acres of right-of-way and offsite area. The drainage basin has been essentially built out in the past and therefore currently has both open and enclosed storm sewer systems active throughout the basin. The basin generally drains to Cedar Creek located along the west central portion of the property. The basin is fairly symmetric with nearly equal portions draining from the north, east and south. The existing onsite detention basin area (Tract B) adjacent to Cedar Creek will continue to serve as detention for the proposed redevelopment.

An Existing Drainage Map may be found in Exhibit D. Hydraflow Hydrograph software was utilized to calculate SCS Method peak discharge rates. A complete breakdown of Existing and Proposed hydrographs may be found in Exhibit E. The following tables summarize the results of the Existing Conditions analysis.

Table 5.1 Existing Conditions Subarea

Subarea	Area (ac.)	Curve Number	Tc (min)
A	147.45	88	28.8

Table 5.2 Existing Conditions Runoff Data: Peak Discharge Rates

Subarea	Q2 (cfs)	Q10 (cfs)	Q100 (cfs)
A	303.47	508.68	809.50

Per APWA Section 5608.4 and City of Lee's Summit criteria, the performance criteria for detention is to provide detention to limit peak flow rates at downstream points of interest to maximum release rates:

- 50% storm peak rate less than or equal to 0.5 cfs per site acre
- 10% storm peak rate less than or equal to 2.0 cfs per site acre
- 1% storm peak rate less than or equal to 3.0 cfs per site acre

The allowable offsite contribution was determined by the area ratio method. The allowable offsite peak discharge is the product of the ratio of offsite area to onsite area multiplied by a given storms existing peak discharge rate. The allowable peak discharge rate is the sum of the offsite allowable plus the onsite allowable per APWA Section 5608.4. See allowable 100-year peak discharge rate calculation below.

Example (100-YR): $[(97.77 / 147.45 \times 809.50) + (49.68 \times 3.0)] = 685.80 \text{ cfs}$

Table 5.3 Existing Conditions APWA Allowable Peak Discharge Release Rates

POI	Onsite Area (ac.)	Offsite Area (ac.)	Q2 (cfs)	Q10 (cfs)	Q100 (cfs)
A	49.68	97.77	226.06	436.65	685.80

There are a few very minor subareas that are peripheral (free release) areas on the site consisting primarily of turf with no hard infrastructure improvements. These areas are not being negatively impacted by the proposed improvements. Subarea A will be the focus of this report.

6. PROPOSED CONDITIONS ANALYSIS

The proposed conditions analysis will include potential future Oldham Village lots located along MO 291 Highway south of SW Oldham Parkway. The proposed onsite area including potential future lots is 49.68 acres. Tributary runoff will be conveyed via both open and enclosed storm sewer systems to POI "A". A new retention system

shall be constructed to attenuate post development runoff from Subarea A1 which includes a large percentage of right-of-way and offsite area. Detained peak discharge rates from Subarea A1 will be combined with peak discharge rates from Subarea A to determine the overall peak discharge rates at POI "A". The proposed peak discharge rates will be compared to allowable discharge rates to determine if they meet or exceed the City's Comprehensive Control Storm Water Management criteria. The Proposed Drainage Map may be found in Exhibit F.

Proposed Flow Rates

Existing Subarea A has been divided into two subareas to account for proposed attenuation. Subarea A1 is located generally in the north and accounts for all proposed and potential future improvements for Oldham Marketplace. Subarea 1 will drain via open and enclosed storm sewer systems to a new earthen detention basin located adjacent to Cedar Creek on a parcel of property labeled Tract B. The remainder of the property which will not be detained is generally located in the southern portion of the basin and will be referred to as Subarea B. The composite curve numbers utilized for Subareas A and B consist of the following classifications and land usage specific curve numbers; right-of-way and single family residential 82, multi-family residential 88 and commercial 94.

Table 6.1 Proposed Conditions Subarea Data

Subarea	Area (ac.)	Composite CN	Tc (min)
A1	128.42	88	28.8
A	19.02	82	15.7

Table 6.2 Proposed Conditions Runoff Data: Subarea Peak Discharge Rates

Subarea	Q2 (cfs)	Q10 (cfs)	Q100 (cfs)
A1	264.31	443.03	705.02
A	43.70	79.44	133.37
Combined (A1 + A)	294.69	498.80	799.42

As shown in Table 6.2 above Subarea A1 will require detention to attenuate storm runoff peak discharge rates at or below regulatory levels at POI A.

6.1. DETENTION

A new single stage earthen Retention basin A1 is being proposed in Subarea A1 to attenuate proposed peak discharge rates. The majority of runoff draining along the west property line and the retention basin will drain directly into the basin. A swale will be constructed beginning at elevation 1004 to convey the remainder of the tributary area to the existing stream. The proposed swale will mitigate any potential drainage impacts to the northern most three residential properties. Following are a list of design parameters for the attenuation system.

Designation: Retention Basin A1

Type: Earthen Basin Side Slopes: 3:1 Max.

Bottom Slope: 0% (Retention) Basin Bottom Elevation: 987.00 Permanent Pool Elevation: 995.95

Basin Top Berm Elevation: 1004.50 (Top contour crowned for drainage)

Basin Top Berm Width: 6' at 1004.00 Basin Volume: 1,072,486 cf @ 1004.00 Control Structure: (3) 8'x6' Precast Concrete Box with Interior 6" Baffle/Weir Wall Baffle Wall Orifice: (1) 6.70" Sq. Rectangular Orifice (WQv Orifice) Screened

Weir Wall Crest Elevation: 997.30, L = 24' Control Structure Top Elevation: 1002.50

Control Structure Emergency Overflow: 24'L x 2.75'W, Crest Elev.=1002.50, Crest Length Total = 53.5 LF

Control Structure Influent Pipe: 60" HDPE, FL (In) = 995.95, FL (Out) = 995.80, L=20.5', S= 0.73% Control Structure Effluent Pipe: 60" HDPE, FL (In) = 995.60, FL (Out) = 994.00, L=50.0', S=3.20% Emergency Spillway: Earthen Broad Crested Weir, Crest Elevation=1002.50, Crest Length=204'

Consecutive 100-YR Q=705.02 cfs, Emergency Spillway HGL=1003.50, Freeboard=1.00'

Sediment Storage Required: 5-Year Accumulated per APWA Figure 5608-1 = 80 x 49.68 x 5 = 19,872 cf

Sediment Storage Provided: Bottom = 989.65, Depth = 0.30', V = 22,212 cf @ El = 989.95

The earthen broad crested weir emergency spillway location shall be located north of the residential subdivision to release solely onto City parkland adjacent to Cedar Creek in case of an emergency. The permanent pool shall be 6' deep with an additional 0.35' of sedimentation allowance. The pond will not support fish which requires a minimum 10' of depth plus sedimentation allowance. The Retention Basin Plan for the Development may be found in Exhibit G. Retention Basin A1 emergency spillway calculations may be found in Exhibit H. See Table 6.3 for a summary of detention basin data.

Table 6.3 Proposed Conditions Detention Basin A1 Data

	Peak Q In (cfs)	Tp In (min.)	Peak Q Out (cfs)	Tp Out (min)	Peak W.S.E.	Max. Storage Vol. (cf)
	Basin A1					
2-Year	264.31	731	161.78	746	999.05	369,916
10-Year	443.03	731	301.26	743	1000.29	530,207
100-Year	705.02	731	472.42	743	1002.00	768,651

As shown in the table above all proposed peak discharge rates from Subarea A1 have been attenuated. See Table 6.4 below for a summary of proposed peak discharge rates at POI "A" which consists of combined subareas post detained A1 and A.

Table 6.4 Proposed Conditions Post Detention Point of Interest Peak Discharge Rates

Point of Interest	Q2 (cfs)	Q10 (cfs)	Q100 (cfs)
A	169.09	315.94	495.24

As shown in the above table all peak discharge rates attributable to Proposed POI "A" have been attenuated below both Existing and Allowable Peak Discharge rates as outlined in Tables 5.2 and 5.3, respectively.

Table 6.5 below provides a comparison of runoff data between Proposed, Existing and Allowable Conditions for the Proposed Development.

Table 6.5 Point of Interest Discharge Comparison

POI	Condition	Q2 (cfs)	Q10 (cfs)	Q100 (cfs)
	Proposed	169.09	315.94	495.24
	Existing	303.47	508.68	809.50
A	Difference	-134.38	-192.74	-314.26
	Allowable	226.06	436.65	685.80
	Difference	-56.97	-120.71	-190.56

All proposed peak discharge rates as shown in Table 6.5 will be significantly below allowable.

7. 40 HOUR EXTENDED DETENTION

In addition to mitigation of peak flow rates, APWA Section 5608.4 also requires 40 hour extended detention of runoff from the local 90% mean annual event (1.37"/24-hour rainfall). The proposed detention facility will release the water quality event over a period of 40-72 hours. See Exhibit I for 40 hour extended detention calculations for the basin.

8. DOWNSTREAM PEAK DISCHARGE EVALUATION

City personnel have requested the evaluation of peak discharge rates, downstream at the next major point of interest, to determine if attenuation on the subject project is efficacious for the watershed. FEMA completed a revised Flood Insurance Study (FIS) for Cedar Creek on January 20, 2017. As stated earlier in the report our drainage boundary for the project stormwater management analysis started at the termination of the recently revised FEMA FIS. To accommodate the City's request and to provide weight to our downstream analysis we consulted the FEMA FIS to select a downstream POI that could be corroborated. The first downstream POI in which peak discharge rates had been quantified in the FIS occurred approximately 580 feet downstream of Southwest Lakeview Boulevard. We selected said point, referred to as POI B for the purposes of this report, to determine and evaluate downstream peak discharge rates. See Exhibit J for FEMA FIS data and a Downstream Drainage Area Map.

The additional area (Subarea B) tributary to POI B downstream of POI A is 87.50 acres. Subarea B consists of park land, single family residential and a portion of Pleasant Lee Middle School Campus. The composite runoff coefficient for Subarea B equates to 0.51 or a curve number of 82. Composite curve number calculations may be found in Exhibit J along with time of concentration calculations. Hydraflow was used to generate existing and proposed peak discharge rates at POI B using SCS Methodology. Hydrographs pertaining to the downstream peak discharge evaluation may be found in Exhibit E.

In order to confirm the SCS model was calibrated to the FEMA FIS data for Subarea B was combined with data from Existing Subarea A. The combined data was used to generate hydrograph "EX POI B – FIS CALIBRATION" to determine if our data was generating results commensurate with the FEMA FIS. FEMA does not provide peak discharge rates for the 2-year storm event. The 10 and 100-year FEMA FIS peak discharge rates at POI B are 536 cfs and 869 cfs, respectively. The "POI B – NO DETENTION" hydrograph generated peak discharge rates for the 10 and 100-year storm events of 548 cfs and 892 cfs, respectively. The 10 and 100-year peak discharge rates are within 2.24% and 2.65%, respectively. Based on the aforementioned results obtained from the independently derived data both the data and the methodology utilized were determined to be accurate for planning and design.

In order to provide an accurate downstream peak discharge comparison at POI B we utilized the systematic combining of hydrographs for both existing and proposed conditions. Hydrograph EX POI B – NO DETENTION combines existing POI A hydrograph with existing Subarea B hydrograph to yield the existing 10 and 100 year peak discharge rates at POI B. Hydrograph PROP POI B – WITH DETENTION combines proposed POI A which accounts for detention as detailed in Section 6 with existing Subarea B hydrograph to yield the proposed 10 and 100 year peak discharge rates at POI B. This is the method used when breaking a watershed and detaining a portion.

Table 8.1 below provides a Point of Interest peak discharge rate comparison between Existing and Proposed conditions at POI B.

Table 8.1 Point of Interest Discharge Comparison

POI	Condition	Q10 (cfs)	Q100 (cfs)
	Proposed	575.82	963.41
В	Existing	804.35	1309.46
	Difference	-228.53	-346.05

The proposed condition in Table 8.1 above represents 49.68 acres of Subarea A1 being attenuated based on a comprehensive control strategy as outlined in Section 6.1. The data compiled in Table 8.1 confirms that attenuation as outlined earlier in the report reduces peak discharge rates at both Points of Interest therefore reducing the likelihood of any potential flooding in the watershed.

9. STREAM BUFFER DETERMINATION

The south east portion of Subarea A is conveyed to POI A by a natural stream which constitutes part of the headwater complex tributary to Cedar Creek. A retention basin is being proposed in the stream bed and surrounding area therefore a stream buffer evaluation is required. Stream buffers are provided for natural streams which contain wide swaths of riparian area consisting of mature trees and steep slopes. The buffer is formed to protect the natural stream and surrounding property from encroachment of permanent hard surface development and other construction activities. One factor used to determine if a natural stream requires a buffer is tributary area. The regulatory requirement according to APWA is 40 acres. See Exhibit F Proposed Drainage Map for tributary area (hatched) contributing to the natural stream at the west property line. The stream tributary at the centerline of the stream along the west property line is 34.21 acres. The tributary area is below the 40 acre threshold therefore a stream buffer is not required and in stream retention may be utilized for attenuation purposes.

10. WETLAND DETERMINATION

The property in question makes up the headwaters for Cedar Creek. The channel located on the property is ephemeral therefore not under United States Army Corp of Engineers (USACE) jurisdiction. The property is not identified as wetlands in the National Wetlands Inventory. See Exhibit K for an aerial photo from the National Wetlands Inventory of the subject property and surrounding area. The main branch of Cedar Creek is identified as Riverine in the National Wetlands Inventory. It is our opinion that the subject property does not contain wetlands as defined by the USACE.

11. CONCLUSIONS & RECOMMENDATIONS

Runoff from the Development will be reduced below both existing and allowable for the Subarea. A retention basin is being proposed in Subarea A1 to attenuate peak discharge rates. Retention Basin A1 will attenuate all proposed peak discharge rates below both Existing and Allowable. Proposed peak discharge rates meet or exceed APWA Section 5600 Comprehensive Control Strategy targets. Onsite Attenuation utilizing comprehensive control strategy with extended detention as outlined will reduce peak discharge rates downstream. It is the opinion of the Professional Engineer that the proposed storm water management improvements outlined in the report will help mitigate any potential negative hydraulic impacts onsite and downstream and therefore recommends approval of said improvements and the storm study.

12. EXHIBITS

- o Exhibit A
 - Aerial View of Site
 - Historical Aerial View of Site & Surrounding Area
 - Overall Site Plan
- Exhibit B
 - FEMA FIRMette
- o Exhibit C
 - NRCS Soils Report
- o Exhibit D
 - Existing Drainage Area Map
- **Exhibit E**
 - Hydraflow Hydrograph Report
- o Exhibit F
 - Proposed Drainage Area Map
- o Exhibit G
 - Detention Plan
- o Exhibit H
 - Emergency Spillway Calculations
- o Exhibit I
 - 40 Hour Extended Detention Calculations
- Exhibit J (Downstream Peak Discharge Evaluation)
 - FEMA FIS Data
 - Downstream Drainage Area Maps
 - With Parcels
 - Without Parcels
 - Composite Curve Number Calculations
 - Time of Concentration Calculations
- o Exhibit K
 - Aerial Photo National Wetlands Inventory

Exhibit A

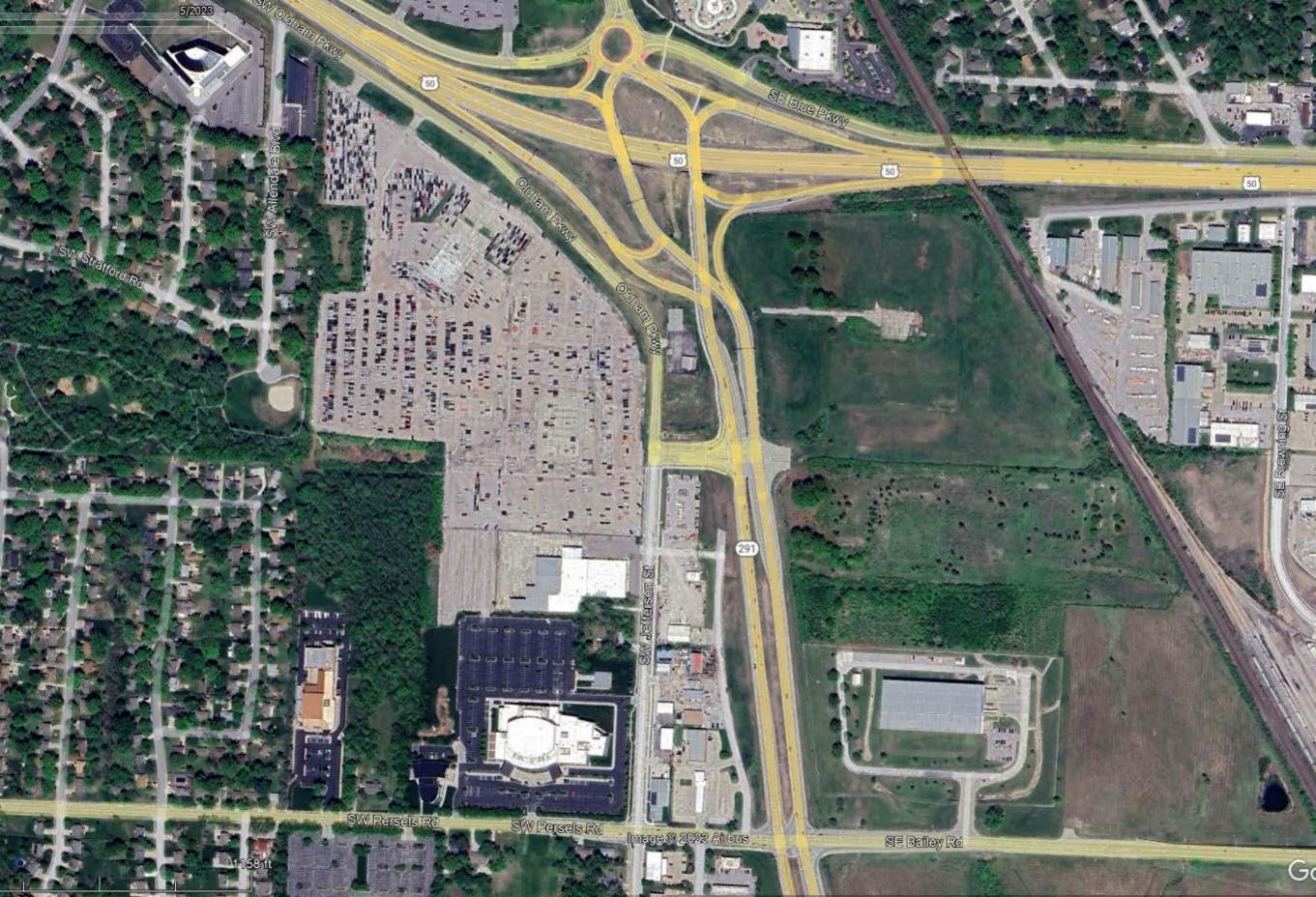
Aerial View of Site

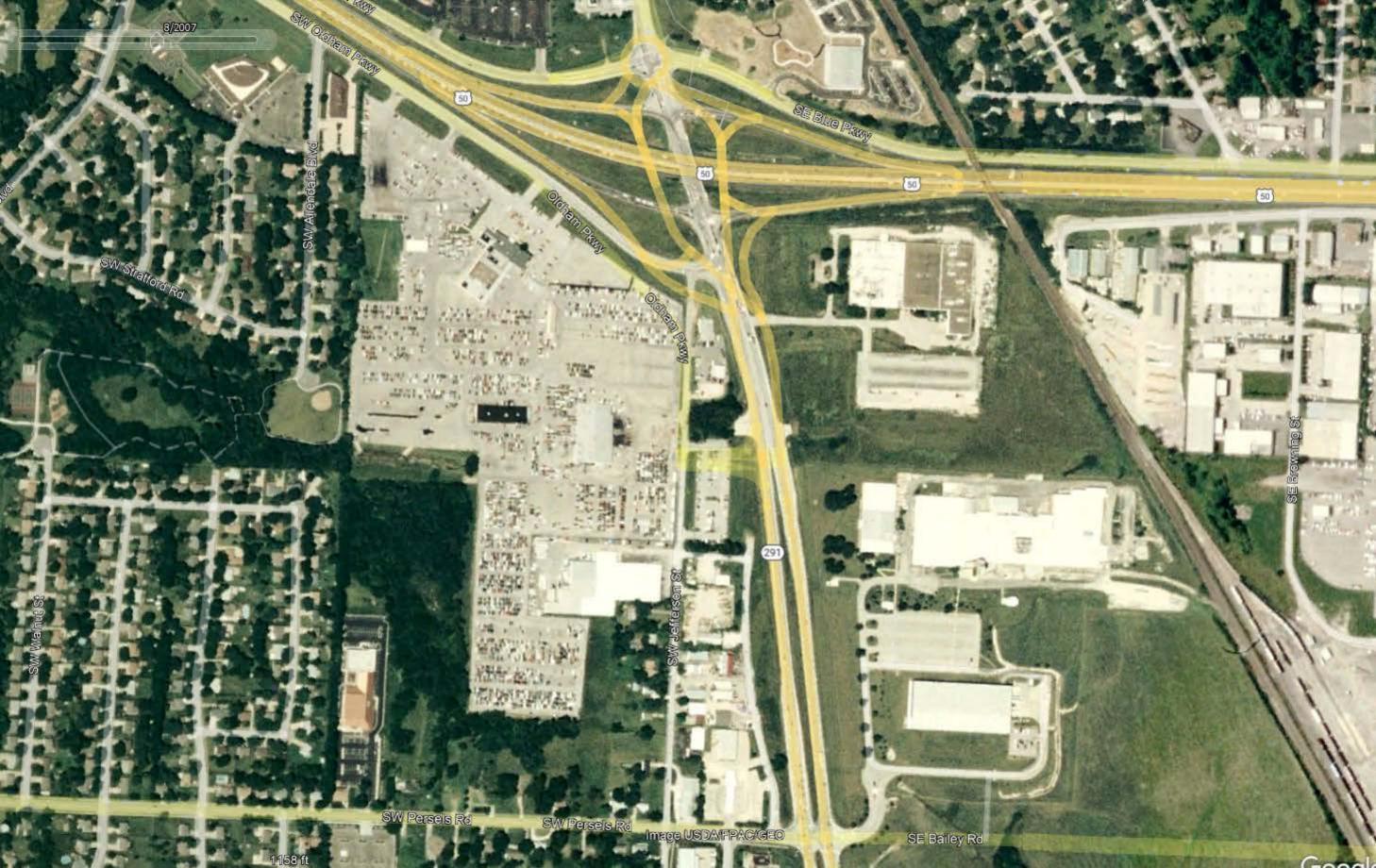
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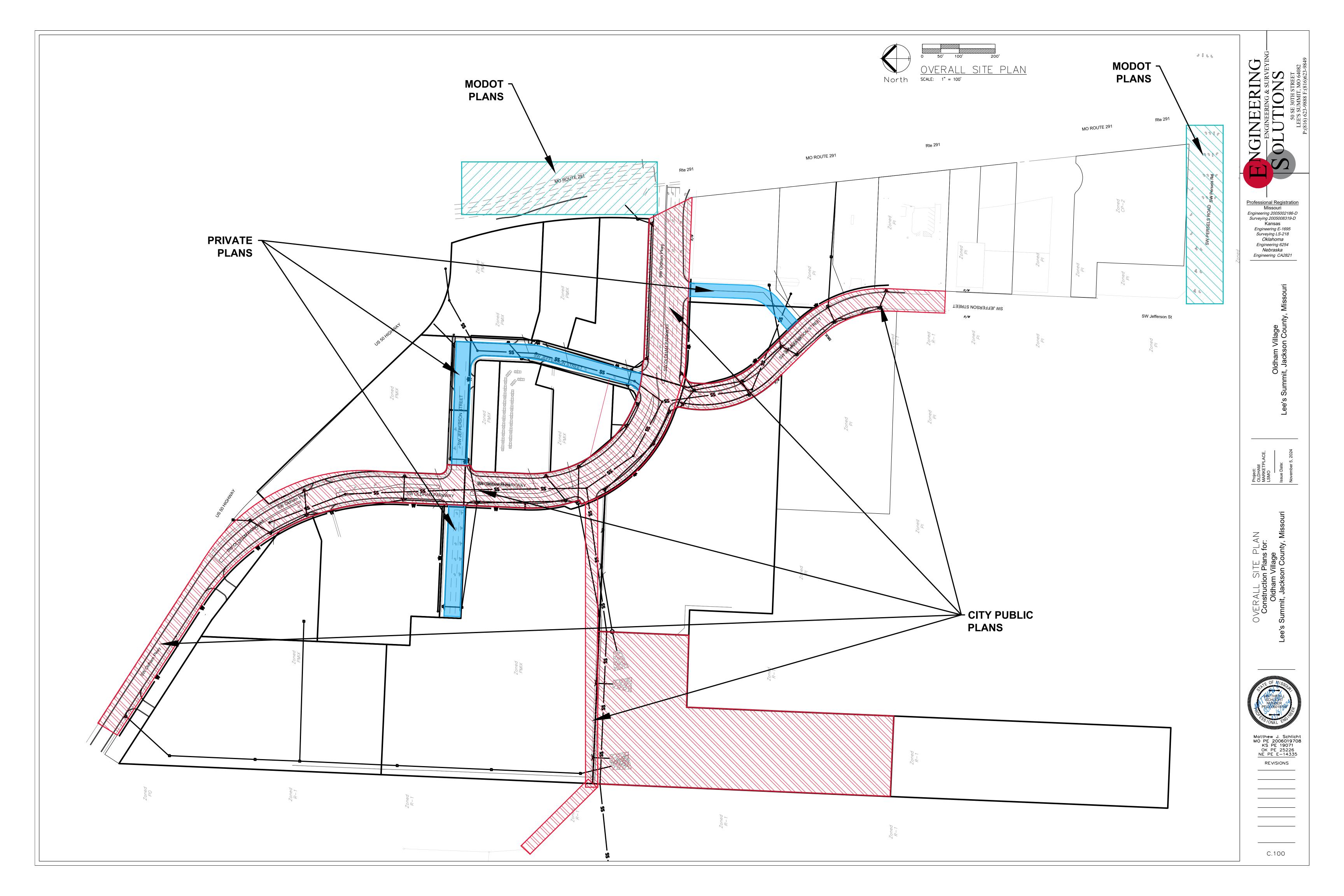
Aerial View of Surrounding Area

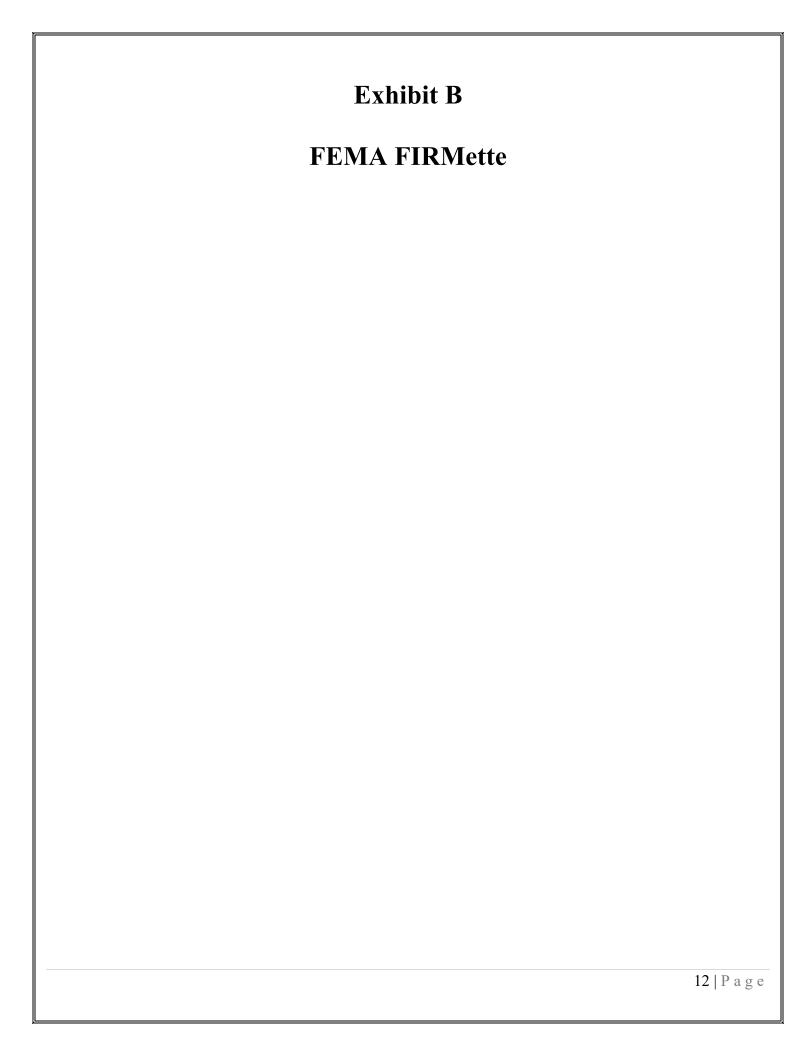
&

Overall Site Plan



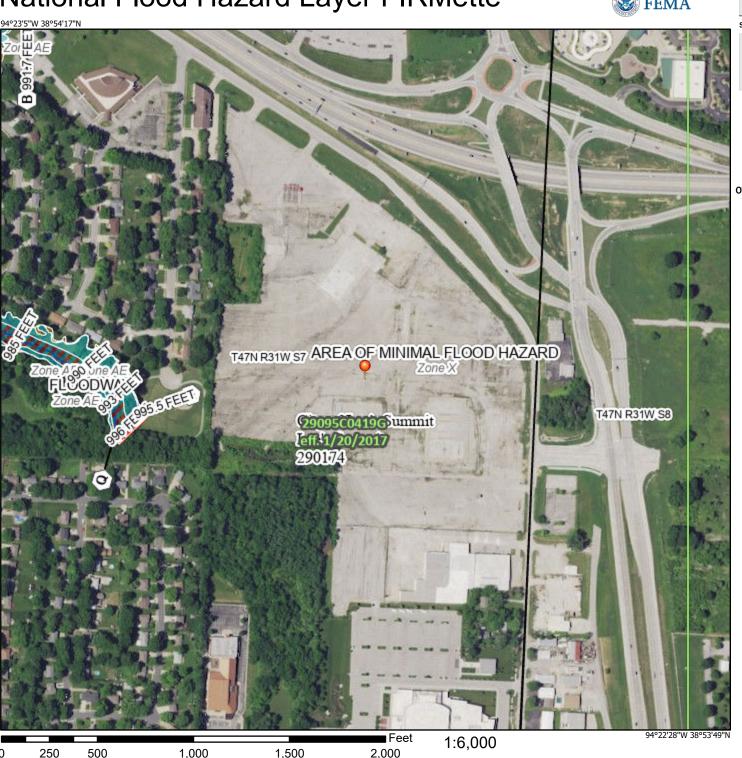






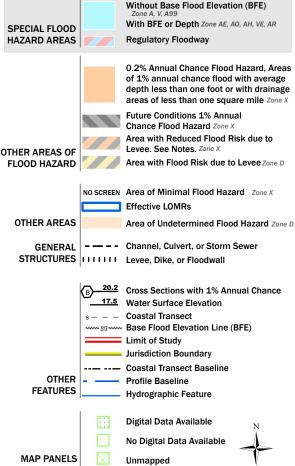
National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



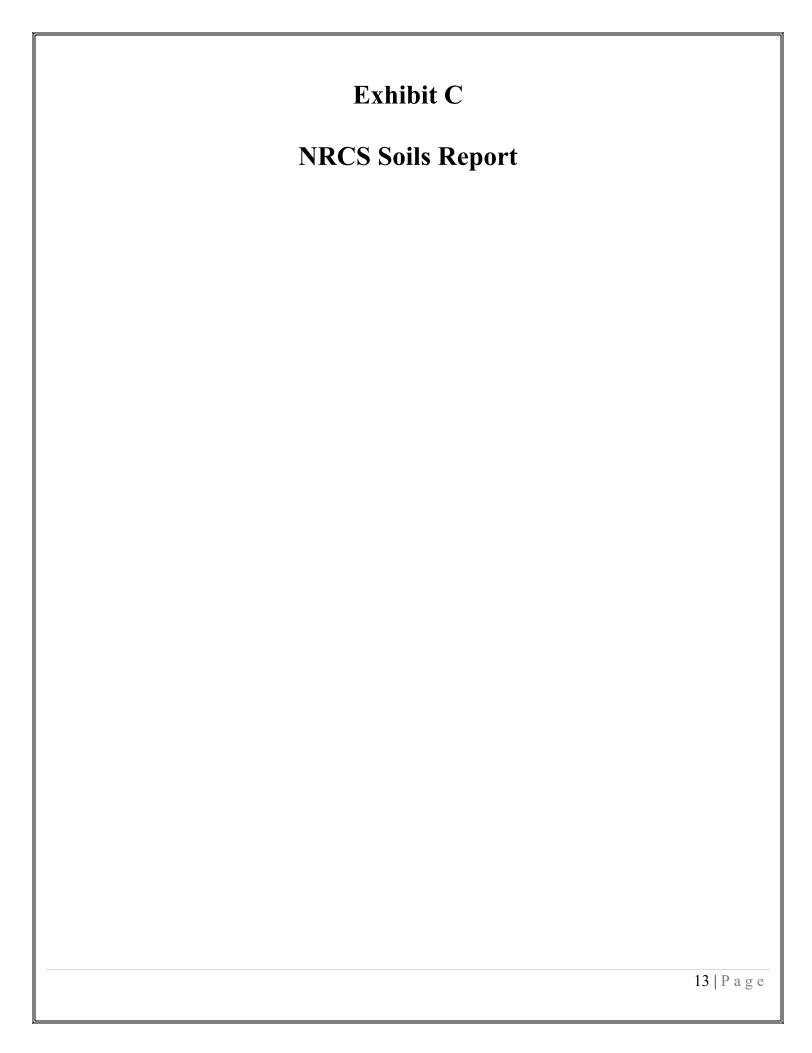
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/9/2023 at 12:56 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.





VRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Jackson County, Missouri

Oldham Marketplace



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(0)

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

Š

Gravel Pit

.

Gravelly Spot

0

Landfill Lava Flow

٨

Marsh or swamp

2

Mine or Quarry

0

Miscellaneous Water

0

Perennial Water
Rock Outcrop

4

Saline Spot

. .

Sandy Spot

0

Severely Eroded Spot

Λ

Sinkhole

Ø.

Sodic Spot

Slide or Slip

8

Spoil Area



Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

Water Features

_

Streams and Canals

Transportation

ransp

Rails

~

Interstate Highways

US Routes

 \sim

Major Roads

~

Local Roads

Background

1

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Jackson County, Missouri Survey Area Data: Version 24, Aug 31, 2022

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Aug 30, 2022—Sep 8. 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
10082	Arisburg-Urban land complex, 1 to 5 percent slopes	2.1	5.8%
10181	Udarents-Urban land-Sampsel complex, 5 to 9 percent slopes	10.2	28.2%
99033	Udarents-Urban land complex, 2 to 9 percent slopes	23.8	65.9%
Totals for Area of Interest		36.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Jackson County, Missouri

10082—Arisburg-Urban land complex, 1 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w7ld Elevation: 750 to 1,130 feet

Mean annual precipitation: 39 to 45 inches Mean annual air temperature: 50 to 55 degrees F

Frost-free period: 177 to 220 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Arisburg and similar soils: 61 percent

Urban land: 30 percent Minor components: 9 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Arisburg

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex Parent material: Loess

Typical profile

Ap - 0 to 6 inches: silt loam A - 6 to 13 inches: silt loam

Bt - 13 to 19 inches: silty clay loam Btg - 19 to 56 inches: silty clay loam BCg - 56 to 79 inches: silty clay loam

Properties and qualities

Slope: 1 to 5 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: High (about 11.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: R107XB007MO - Loess Upland Prairie

Hydric soil rating: No

Description of Urban Land

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Minor Components

Sampsel

Percent of map unit: 3 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Concave

Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna

Hydric soil rating: Yes

Greenton

Percent of map unit: 3 percent

Landform: Hillslopes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: R109XY002MO - Loess Upland Prairie

Hydric soil rating: No

Sharpsburg

Percent of map unit: 3 percent

Landform: Ridges

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: R109XY002MO - Loess Upland Prairie

Hydric soil rating: No

10181—Udarents-Urban land-Sampsel complex, 5 to 9 percent slopes

Map Unit Setting

National map unit symbol: 1n85g

Elevation: 600 to 900 feet

Mean annual precipitation: 33 to 43 inches Mean annual air temperature: 50 to 57 degrees F

Frost-free period: 175 to 220 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Udarents and similar soils: 46 percent

Urban land: 39 percent

Sampsel and similar soils: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udarents

Setting

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Mine spoil or earthy fill

Typical profile

C1 - 0 to 5 inches: silt loam C2 - 5 to 80 inches: silty clay loam

Properties and qualities

Slope: 5 to 9 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.14 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: R107XB002MO - Deep Loess Upland Prairie

Other vegetative classification: Mixed/Transitional (Mixed Native Vegetation)

Hydric soil rating: No

Description of Urban Land

Setting

Landform: Hillslopes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Across-slope shape: Convex

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Description of Sampsel

Settina

Landform: Hillslopes

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Convex

Parent material: Residuum weathered from shale

Typical profile

Ap - 0 to 13 inches: silty clay loam Bt - 13 to 80 inches: silty clay

Properties and qualities

Slope: 5 to 9 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 0 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C/D

Ecological site: R109XY010MO - Interbedded Sedimentary Upland Savanna

Other vegetative classification: Grass/Prairie (Herbaceous Vegetation)

Hydric soil rating: No

99033—Udarents-Urban land complex, 2 to 9 percent slopes

Map Unit Setting

National map unit symbol: 1n85n Elevation: 710 to 1,470 feet

Mean annual precipitation: 31 to 47 inches Mean annual air temperature: 46 to 57 degrees F

Frost-free period: 170 to 220 days

Farmland classification: Not prime farmland

Map Unit Composition

Udarents and similar soils: 50 percent

Urban land: 45 percent *Minor components:* 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udarents

Setting

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Mine spoil or earthy fill

Typical profile

C1 - 0 to 5 inches: silt loam C2 - 5 to 80 inches: silty clay loam

Properties and qualities

Slope: 2 to 9 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.14 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 9.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Other vegetative classification: Mixed/Transitional (Mixed Native Vegetation)

Hydric soil rating: No

Description of Urban Land

Setting

Landform position (two-dimensional): Backslope

Across-slope shape: Convex

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

Minor Components

Knox

Percent of map unit: 3 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: R107XB003MO - Deep Loess Exposed Backslope Savanna,

F107XB004MO - Deep Loess Protected Backslope Woodland

Hydric soil rating: No

Sibley

Percent of map unit: 2 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: R109XY002MO - Loess Upland Prairie

Hydric soil rating: No

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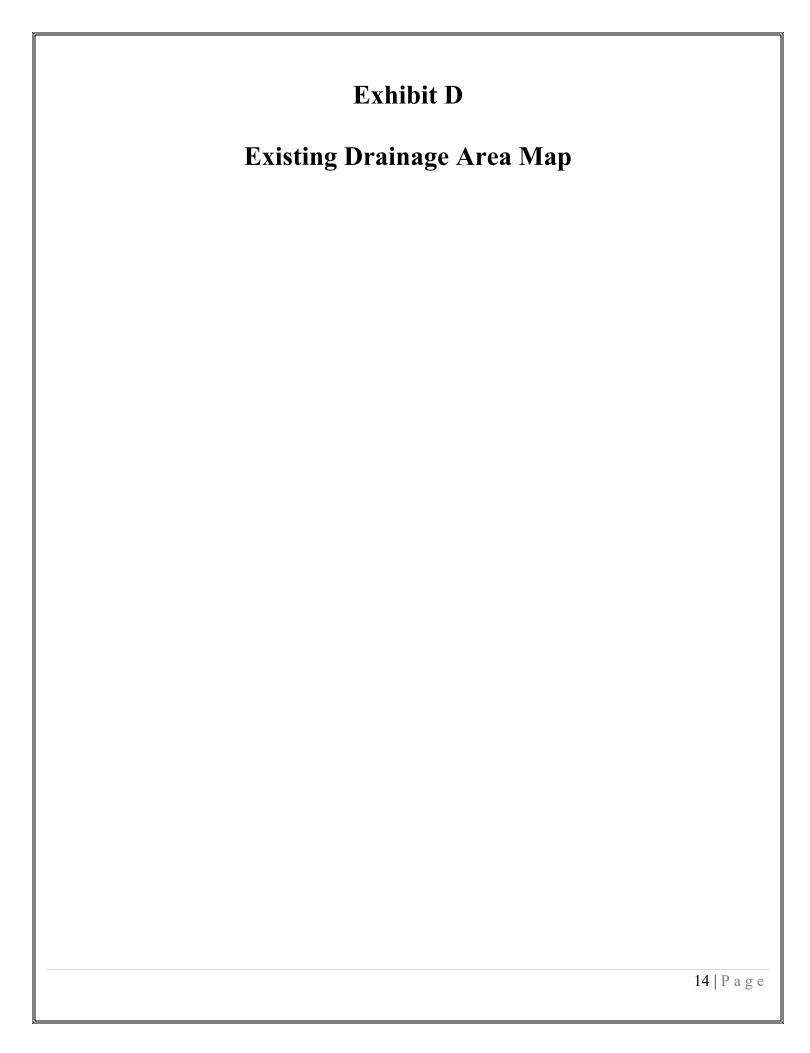
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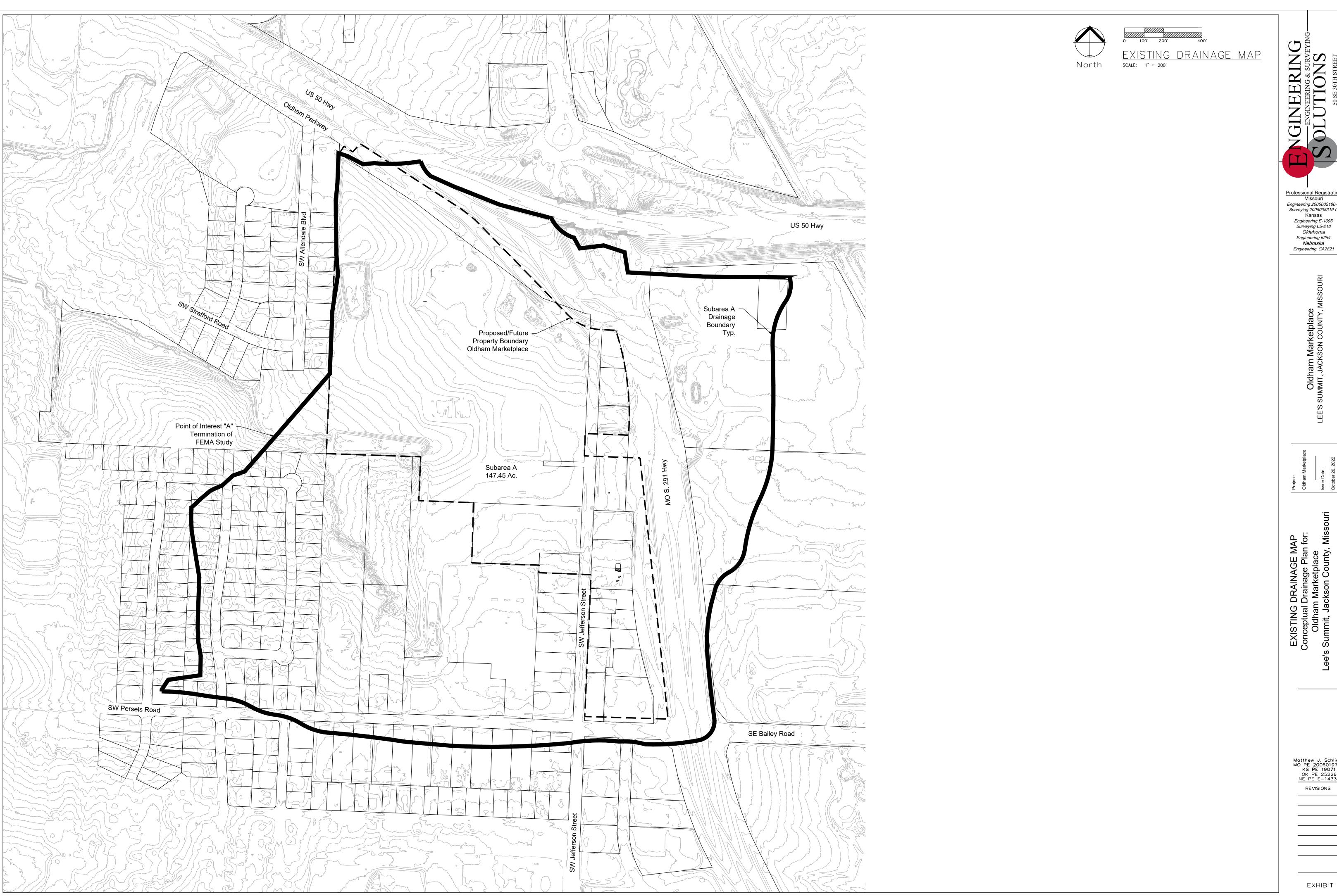
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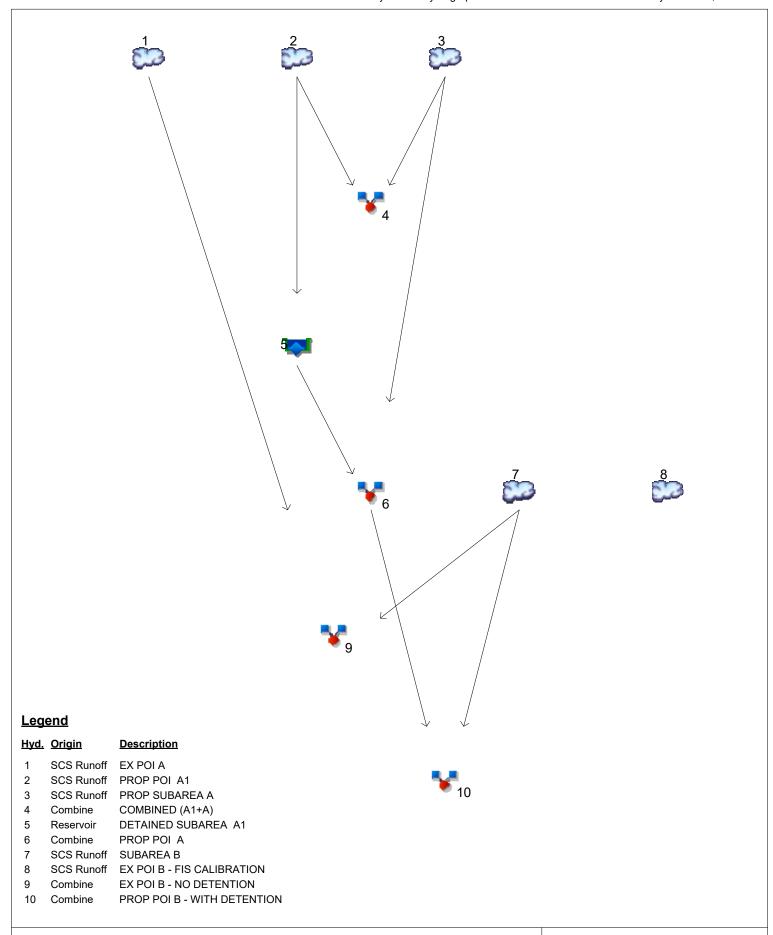
Motthew J. Schlicht MO PE 2006019708 KS PE 19071 OK PE 25226 NE PE E-14335 REVISIONS

Exhibit E Hydraflow Hydrograph Report 15 | P a g e

Wednesday, 11 / 6 / 2024

Watershed Model Schematic

Project: OLDHAM VILLAGE 241105.gpw



Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

SCS Runoff 1-yr 2-yr 3-yr 5-yr 10-yr 25-yr 50-yr 100-yr 25-yr 50-yr 100-yr 25-yr 25-yr	-	Hydrograph	Inflow				Hydrograph					
2 SCS Runoff 264.31 443.03 705.02 PROP POI A1 3 SCS Runoff 43.70 79.44 133.37 PROP SUBAREA A 4 Combine 2, 3 294.69 498.80 799.42 COMBINED (A1+A) 5 Reservoir 2 161.78 301.26 472.42 DETAINED SUBAREA A1 6 Combine 3, 5 169.09 315.94 495.24 PROP POI A 7 SCS Runoff 173.67 317.20 534.31 SUBAREA B 8 SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION 9 Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	0.		nya(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
3 SCS Runoff 43.70 79.44 133.37 PROP SUBAREA A 4 Combine 2, 3 294.69 498.80 799.42 COMBINED (A1+A) 5 Reservoir 2 161.78 301.26 472.42 DETAINED SUBAREA A1 6 Combine 3, 5 169.09 315.94 495.24 PROP POI A 7 SCS Runoff 173.67 317.20 534.31 SUBAREA B 8 SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION 9 Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	1	SCS Runoff			303.47			508.68			809.50	EX POI A
Combine 2, 3 294.69 498.80 799.42 COMBINED (A1+A) Reservoir 2 161.78 301.26 472.42 DETAINED SUBAREA A1 Combine 3, 5 169.09 315.94 495.24 PROP POI A SCS Runoff 173.67 317.20 534.31 SUBAREA B SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	2	SCS Runoff			264.31			443.03			705.02	PROP POI A1
5 Reservoir 2	3	SCS Runoff			43.70			79.44			133.37	PROP SUBAREA A
6 Combine 3, 5 169.09 315.94 495.24 PROP POI A 7 SCS Runoff 173.67 317.20 534.31 SUBAREA B 8 SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION 9 Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	1	Combine	2, 3		294.69			498.80			799.42	COMBINED (A1+A)
7 SCS Runoff 173.67 317.20 534.31 SUBAREA B 8 SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION 9 Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	5	Reservoir	2		161.78			301.26			472.42	DETAINED SUBAREA A1
3 SCS Runoff 316.51 548.30 892.27 EX POI B - FIS CALIBRATION Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	6	Combine	3, 5		169.09			315.94			495.24	PROP POLA
O Combine 1, 7, 464.88 804.35 1309.46 EX POI B - NO DETENTION	7	SCS Runoff			173.67			317.20			534.31	SUBAREA B
	3	SCS Runoff			316.51			548.30			892.27	EX POI B - FIS CALIBRATION
10 Combine 6, 7, 286.31 575.82 963.41 PROP POI B - WITH DETENTION)	Combine	1, 7,		464.88			804.35			1309.46	EX POI B - NO DETENTION
	10	Combine	6, 7,		286.31			575.82			963.41	PROP POI B - WITH DETENTION

Proj. file: OLDHAM VILLAGE 241105.gpw

Wednesday, 11 / 6 / 2024

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hydrailow Hydrographs Extension for Au							·		
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	303.47	1	731	1,214,296				EX POI A
2	SCS Runoff	264.31	1	731	1,057,578				PROP POI A1
3	SCS Runoff	43.70	1	723	124,615				PROP SUBAREA A
4	Combine	294.69	1	730	1,182,192	2, 3			COMBINED (A1+A)
5	Reservoir	161.78	1	746	1,012,054	2	999.05	369,916	DETAINED SUBAREA A1
6	Combine	169.09	1	745	1,136,668	3, 5			PROP POLA
7	SCS Runoff	173.67	1	726	571,646				SUBAREA B
8	SCS Runoff	316.51	1	744	1,789,688				EX POI B - FIS CALIBRATION
9	Combine	464.88	1	729	1,785,939	1, 7,			EX POI B - NO DETENTION
10	Combine	286.31	1	730	1,708,315	6, 7,			PROP POI B - WITH DETENTION
OLI	DHAM VILLA	GE 24110)5.gpw		Return P	eriod: 2 Ye	ear	Wednesday	v, 11 / 6 / 2024

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

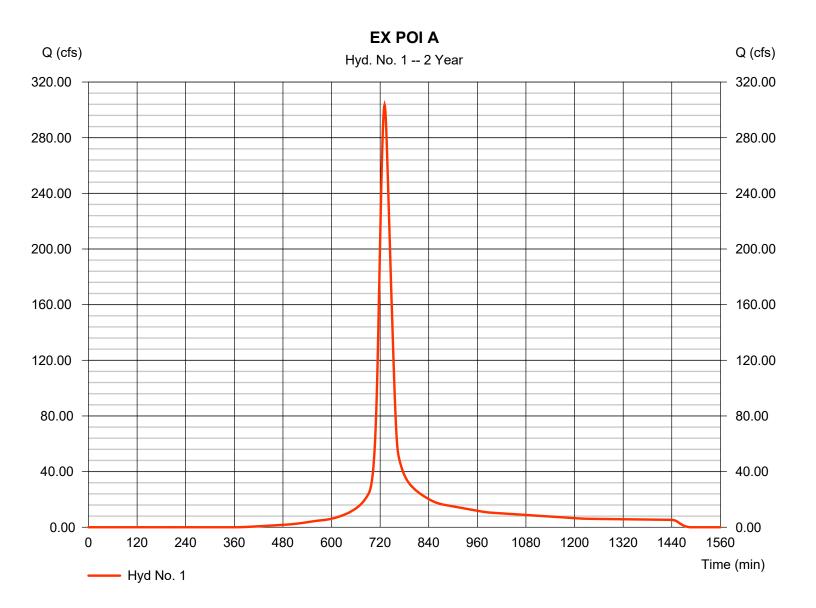
Wednesday, 11 / 6 / 2024

Hyd. No. 1

EX POI A

Hydrograph type = SCS Runoff Peak discharge = 303.47 cfsStorm frequency = 2 yrsTime to peak = 731 min Time interval = 1 min Hyd. volume = 1,214,296 cuft Drainage area Curve number = 147.450 ac = 88 Hydraulic length Basin Slope = 0.0 %= 0 ft

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 3.50 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

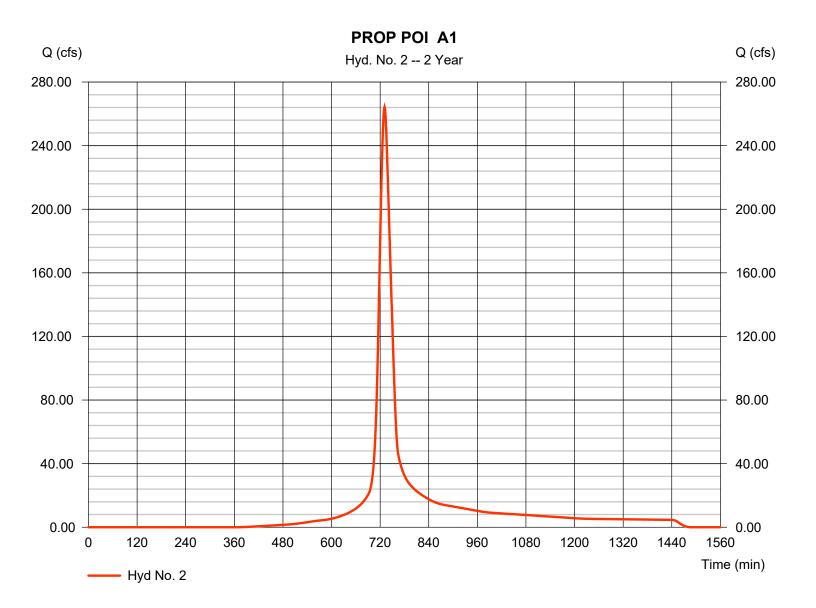
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Hyd. No. 2

PROP POL A1

Hydrograph type = SCS Runoff Peak discharge = 264.31 cfsStorm frequency = 2 yrsTime to peak = 731 min Time interval = 1 min Hyd. volume = 1,057,578 cuft Drainage area Curve number = 128.420 ac = 88 Hydraulic length Basin Slope = 0.0 %= 0 ft

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 3.50 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



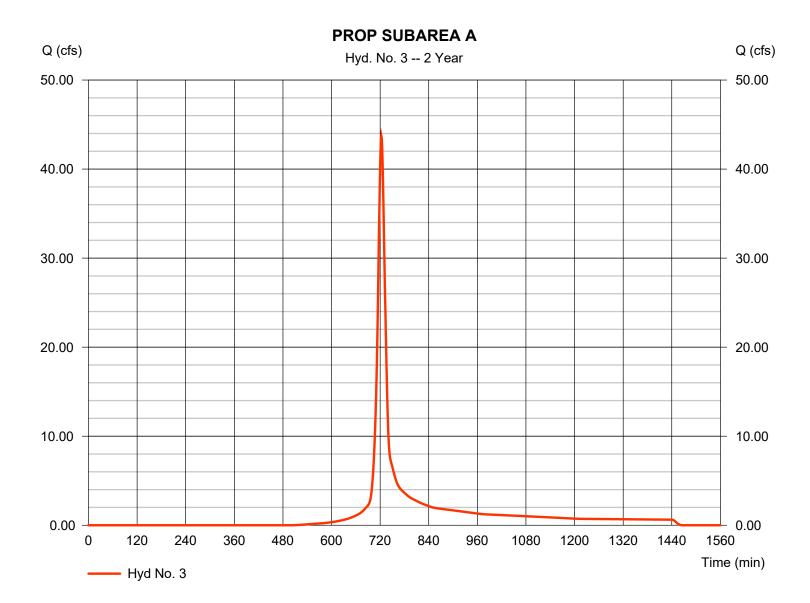
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 3

PROP SUBAREA A

Hydrograph type = SCS Runoff Peak discharge = 43.70 cfsStorm frequency = 2 yrsTime to peak = 723 min Time interval = 1 min Hyd. volume = 124,615 cuft Curve number Drainage area = 19.020 ac= 82 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 15.70 min = User Total precip. = 3.50 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

= 294.69 cfs

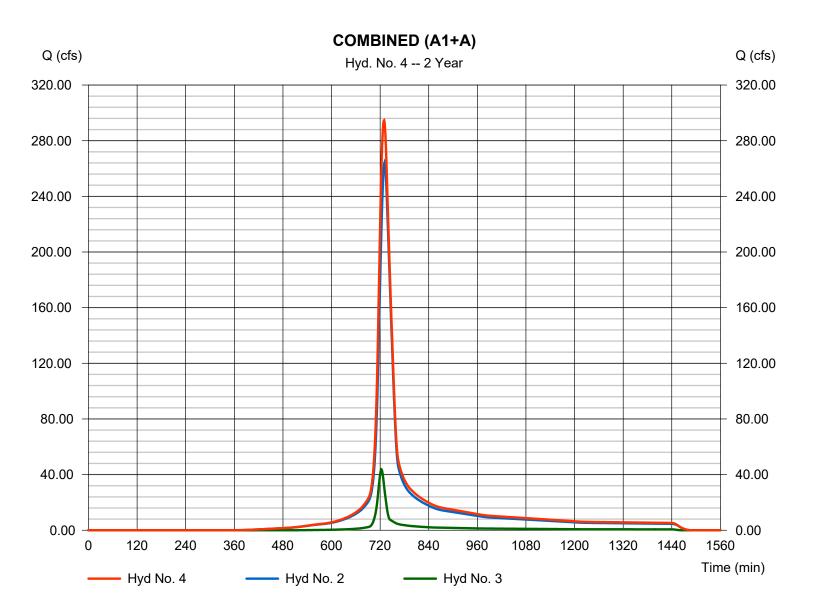
= 730 min

Hyd. No. 4

COMBINED (A1+A)

Hydrograph type = Combine Peak discharge
Storm frequency = 2 yrs Time to peak
Time interval = 1 min Hyd yolume

Time interval = 1 min Hyd. volume = 1,182,192 cuft Contrib. drain. area = 147.440 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

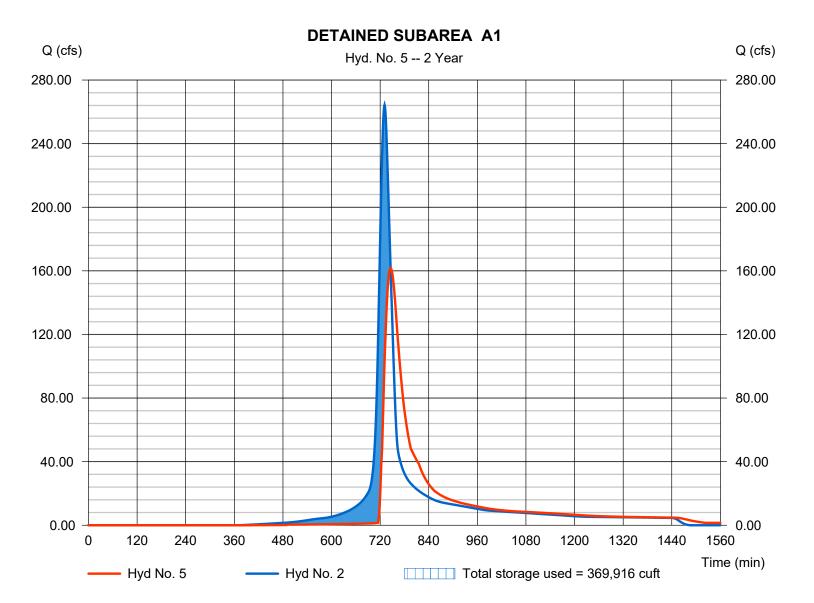
Hyd. No. 5

DETAINED SUBAREA A1

Hydrograph type = Reservoir Peak discharge = 161.78 cfsStorm frequency Time to peak = 746 min = 2 yrsTime interval = 1 min Hyd. volume = 1,012,054 cuft Inflow hyd. No. = 2 - PROP POI A1 Max. Elevation $= 999.05 \, \text{ft}$

Reservoir name = Retention Basin A1 Max. Storage = 369,916 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Pond No. 1 - Retention Basin A1

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 995.95 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	995.95	108,955	0	0
0.05	996.10	109,246	5,455	5,455
2.05	998.00	121,115	230,361	235,816
4.05	1000.00	133,209	254,324	490,140
6.05	1002.00	145,530	278,739	768,879
8.05	1004.00	158,077	303,607	1,072,486

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 60.00 6.70 = 24.00 0.00 0.00 Rise (in) 0.00 0.00 Crest Len (ft) 0.00 Span (in) = 60.00 6.70 0.00 0.00 Crest El. (ft) = 997.30 0.00 0.00 0.00 No. Barrels = 3 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 995.60 995.70 0.00 0.00 Weir Type = Rect Length (ft) = 50.000.00 0.00 0.00 Multi-Stage No = Yes No No Slope (%) = 2.000.00 0.00 n/a N-Value = .010 .013 .013 n/a = 0.000 (by Wet area) Orifice Coeff. = 0.600.67 0.60 0.60 Exfil.(in/hr) Multi-Stage = n/a Yes No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIV A cfs	CIV B cfs	CIV C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	995.95	0.00	0.00			0.00						0.000
0.05	5,455	996.10	3.94 ic	0.39 ic			0.00						0.393
2.05	235,816	998.00	48.71 ic	1.38 ic			46.81						48.19
4.05	490,140	1000.00	273.56 ic	1.30 ic			269.71 s						271.02
6.05	768,879	1002.00	472.67 oc	1.17 ic			471.47 s						472.64
8.05	1,072,486	1004.00	650.47 ic	1.05 ic			649.41 s						650.46

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

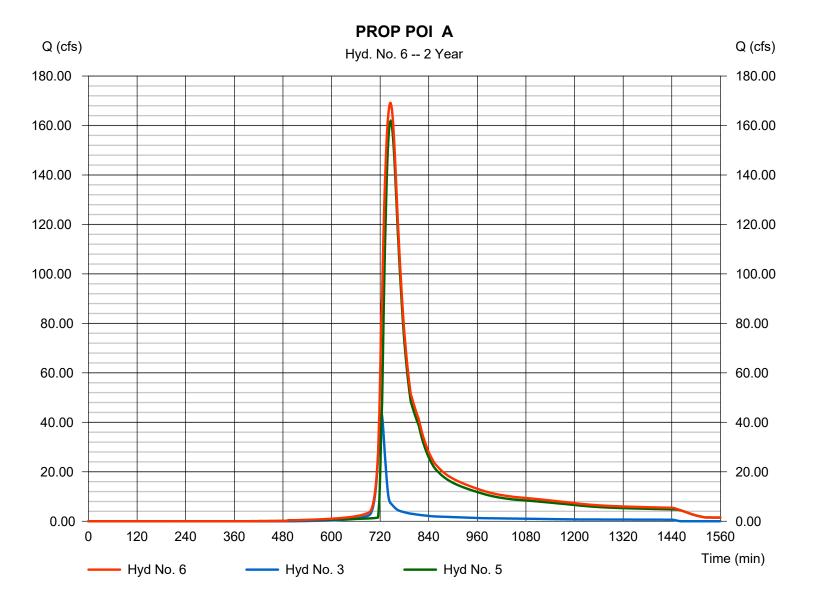
Wednesday, 11 / 6 / 2024

Hyd. No. 6

PROP POI A

Hydrograph type= CombinePeak discharge= 169.09 cfsStorm frequency= 2 yrsTime to peak= 745 minTime interval= 1 minHvd. volume= 1.136.668 cm

Time interval = 1 min Hyd. volume = 1,136,668 cuft Contrib. drain. area = 19.020 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

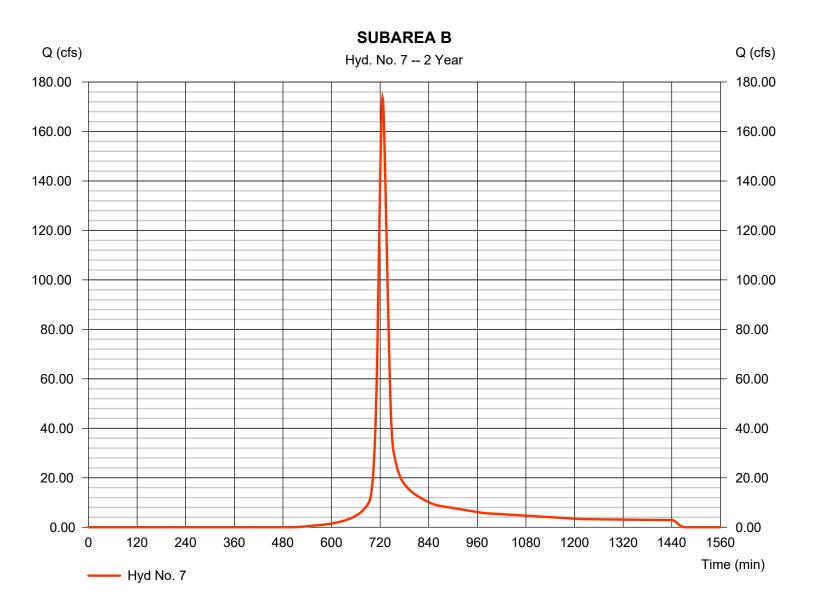
Wednesday, 11 / 6 / 2024

Hyd. No. 7

SUBAREA B

Hydrograph type = SCS Runoff Peak discharge = 173.67 cfsStorm frequency = 2 yrsTime to peak = 726 min Time interval = 1 min Hyd. volume = 571,646 cuft Drainage area Curve number = 87.500 ac = 82 = 0 ftBasin Slope = 0.0 %Hydraulic length

Tc method= UserTime of conc. (Tc)= 21.90 minTotal precip.= 3.50 inDistribution= Type IIStorm duration= 24 hrsShape factor= 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Wednesday, 11 / 6 / 2024

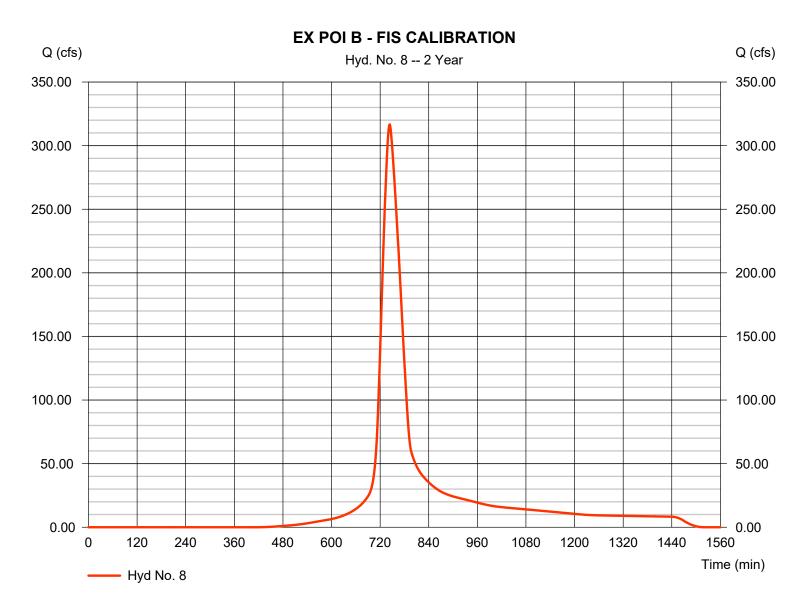
= 484

Hyd. No. 8

Storm duration

EX POI B - FIS CALIBRATION

Hydrograph type = SCS Runoff Peak discharge = 316.51 cfsStorm frequency = 2 yrsTime to peak = 744 min Time interval = 1 min Hyd. volume = 1,789,688 cuft Drainage area Curve number = 234.960 ac = 86 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 49.40 min = User Total precip. = 3.50 inDistribution = Type II



Shape factor

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

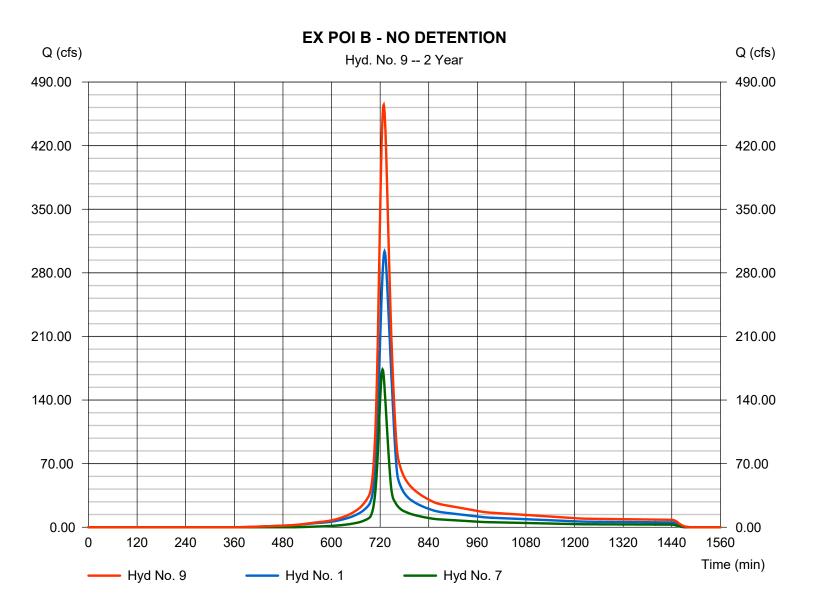
Wednesday, 11 / 6 / 2024

Hyd. No. 9

EX POI B - NO DETENTION

Hydrograph type = Combine
Storm frequency = 2 yrs
Time interval = 1 min
Inflow hyds. = 1, 7

Peak discharge = 464.88 cfs Time to peak = 729 min Hyd. volume = 1,785,939 cuft Contrib. drain. area = 234.950 ac



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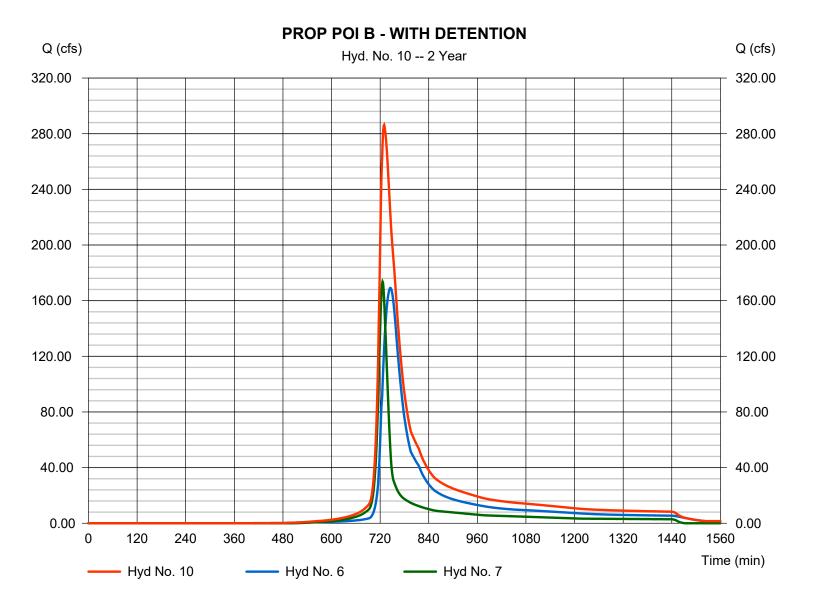
Wednesday, 11 / 6 / 2024

Hyd. No. 10

PROP POI B - WITH DETENTION

Hydrograph type= CombinePeak discharge= 286.31 cfsStorm frequency= 2 yrsTime to peak= 730 minTime interval= 1 minHyd. volume= 1,708,315

Time interval = 1 min Hyd. volume = 1,708,315 cuft Contrib. drain. area = 87.500 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

	- Hydrallow Hydr						, 3	Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. V2023			
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description		
1	SCS Runoff	508.68	1	731	2,065,624				EX POI A		
2	SCS Runoff	443.03	1	731	1,799,034				PROP POI A1		
3	SCS Runoff	79.44	1	723	227,792				PROP SUBAREA A		
4	Combine	498.80	1	729	2,026,826	2, 3			COMBINED (A1+A)		
5	Reservoir	301.26	1	743	1,752,238	2	1000.29	530,207	DETAINED SUBAREA A1		
6	Combine	315.94	1	740	1,980,029	3, 5			PROP POLA		
7	SCS Runoff	317.20	1	726	1,044,953				SUBAREA B		
8	SCS Runoff	548.30	1	743	3,116,573				EX POI B - FIS CALIBRATION		
9	Combine	804.35	1	728	3,110,575	1, 7,			EX POI B - NO DETENTION		
10	Combine	575.82	1	728	3,024,981	6, 7,			PROP POI B - WITH DETENTION		
OLI	DHAM VILLA	GE 24110)5.gpw	1	Return P	eriod: 10 Y	′ear	Wednesda	y, 11 / 6 / 2024		

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

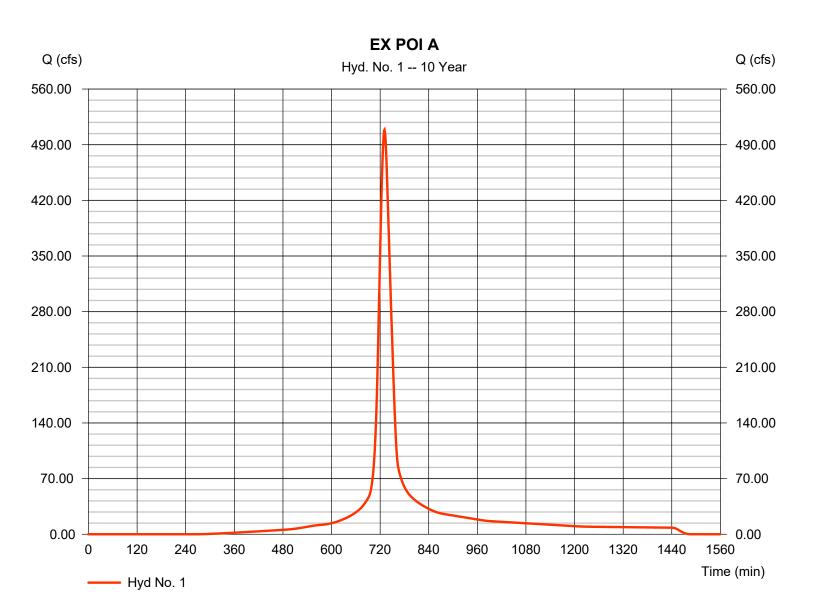
Wednesday, 11 / 6 / 2024

Hyd. No. 1

EX POI A

Hydrograph type = SCS Runoff Peak discharge = 508.68 cfsStorm frequency = 10 yrsTime to peak = 731 min Time interval = 1 min Hyd. volume = 2,065,624 cuft Drainage area Curve number = 147.450 ac = 88

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 5.20 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



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Wednesday, 11 / 6 / 2024

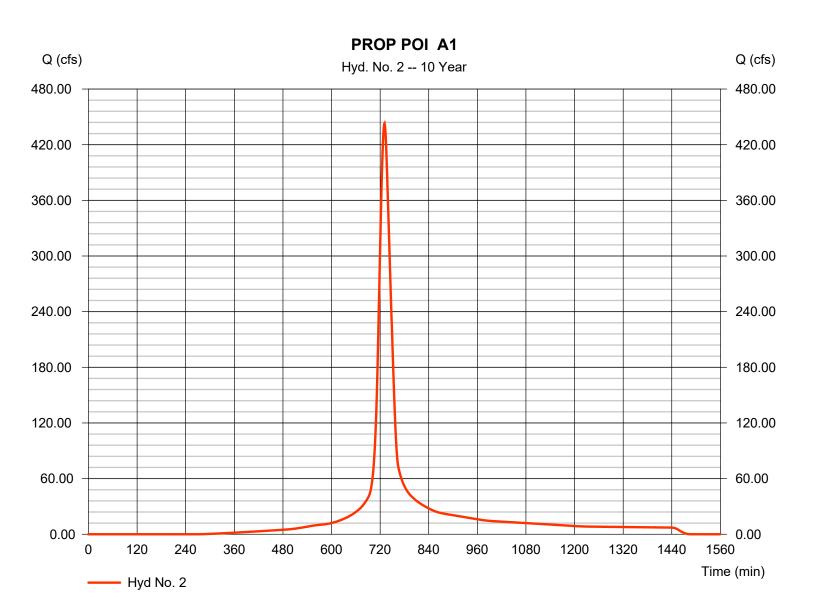
Hyd. No. 2

PROP POL A1

Hydrograph type= SCS RunoffPeak discharge= 443.03 cfsStorm frequency= 10 yrsTime to peak= 731 minTime interval= 1 minHyd. volume= 1,799,034 cuftDrainage area= 128 420 acCurve number= 88

Drainage area = 128.420 ac Curve number = 88 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 5.20 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



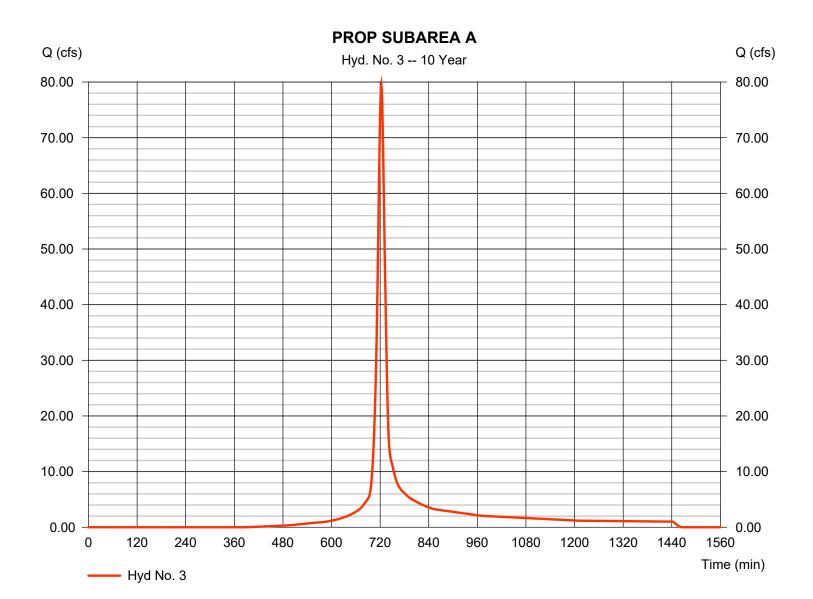
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 3

PROP SUBAREA A

= 79.44 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 10 yrsTime to peak = 723 min Time interval = 1 min Hyd. volume = 227,792 cuft Drainage area Curve number = 19.020 ac= 82 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 15.70 min = User Total precip. = 5.20 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

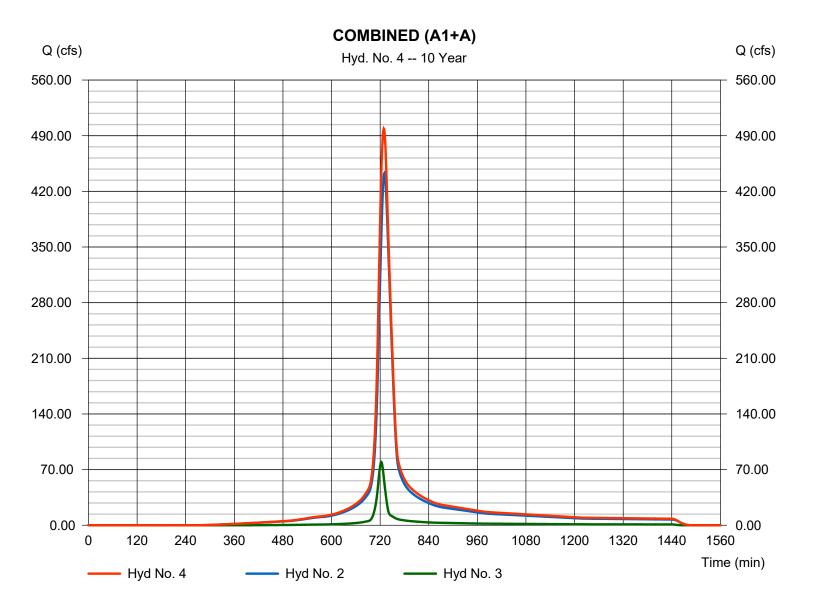
Wednesday, 11 / 6 / 2024

Hyd. No. 4

COMBINED (A1+A)

Hydrograph type= CombinePeak discharge= 498.80 cfsStorm frequency= 10 yrsTime to peak= 729 minTime interval= 1 minHyd. volume= 2,026,826

Time interval = 1 min Hyd. volume = 2,026,826 cuft Contrib. drain. area = 147.440 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 5

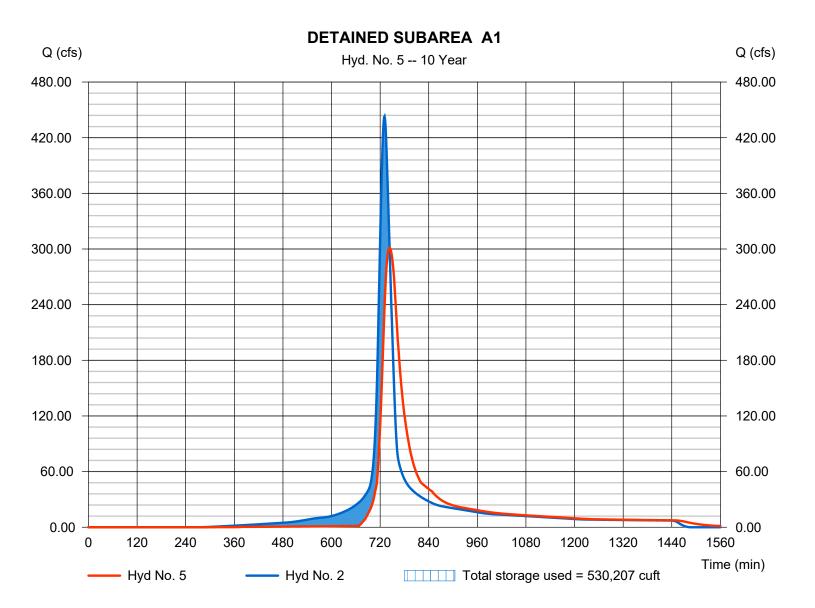
DETAINED SUBAREA A1

Hydrograph type= ReservoirPeak discharge= 301.26 cfsStorm frequency= 10 yrsTime to peak= 743 minTime interval= 1 minHyd. volume= 1,752,238 cuft

Inflow hyd. No. = 2 - PROP POI A1 Max. Elevation = 1000.29 ft

Reservoir name = Retention Basin A1 Max. Storage = 530,207 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

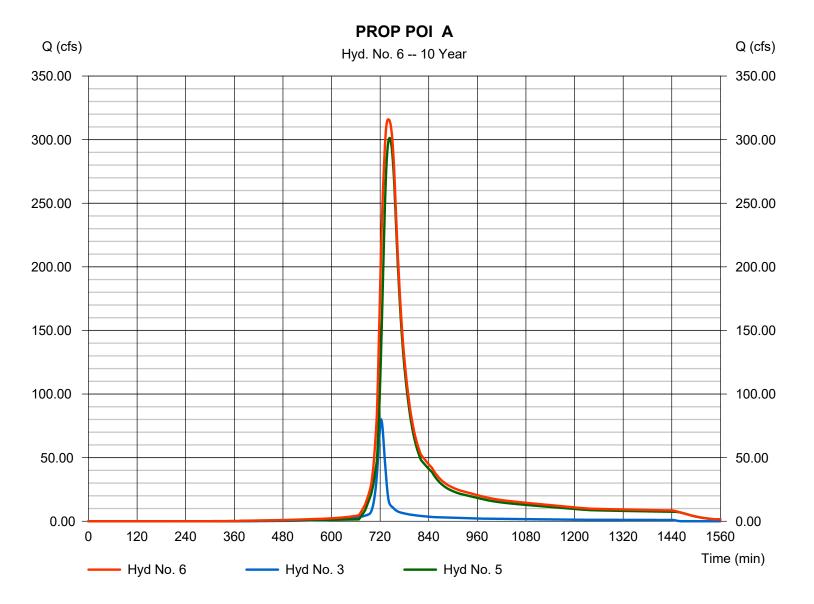
Wednesday, 11 / 6 / 2024

Hyd. No. 6

PROP POI A

Hydrograph type = Combine Peak discharge = 315.94 cfs
Storm frequency = 10 yrs Time to peak = 740 min

Time interval = 1 min Hyd. volume = 1,980,029 cuft Contrib. drain. area = 19.020 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

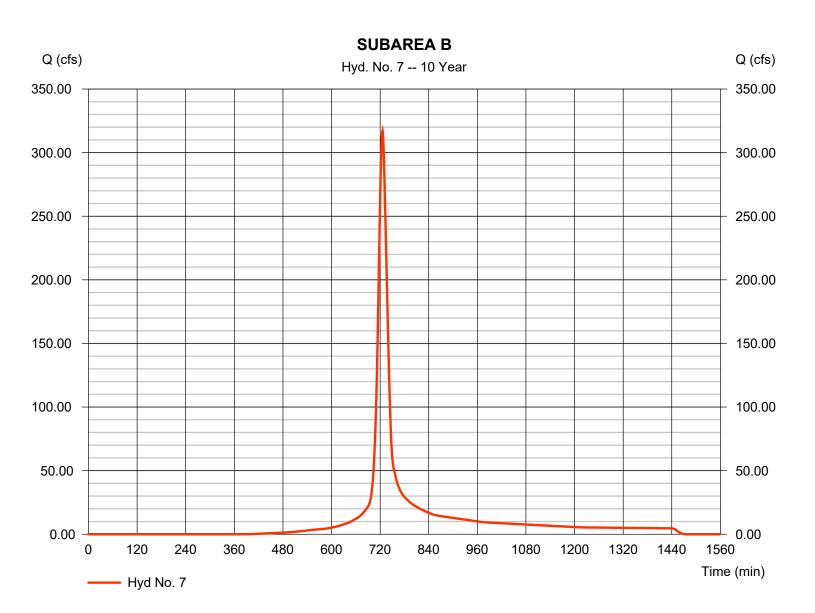
Wednesday, 11 / 6 / 2024

Hyd. No. 7

SUBAREA B

Hydrograph type= SCS RunoffPeak discharge= 317.20 cfsStorm frequency= 10 yrsTime to peak= 726 minTime interval= 1 minHyd. volume= 1,044,953 cuft

Tc method = User Time of conc. (Tc) = 21.90 min
Total precip. = 5.20 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Wednesday, 11 / 6 / 2024

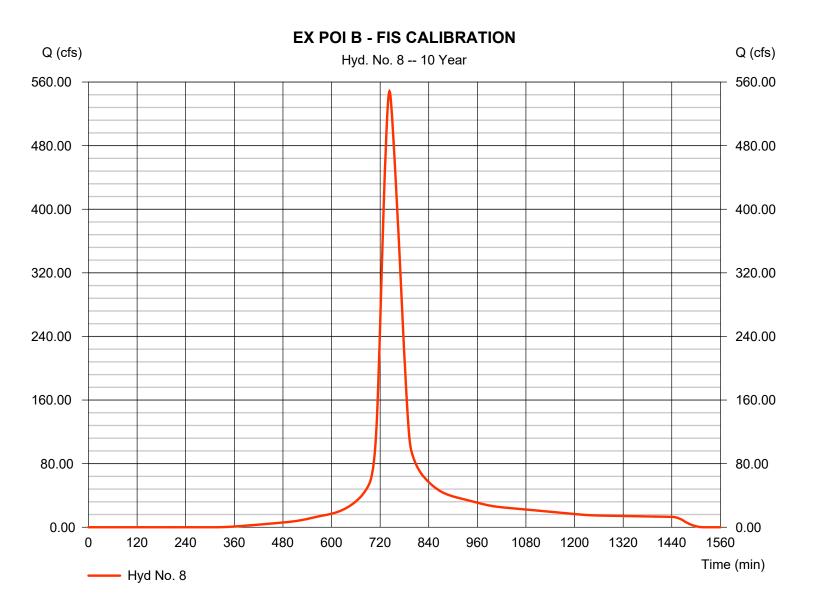
= 484

Hyd. No. 8

Storm duration

EX POI B - FIS CALIBRATION

Hydrograph type = SCS Runoff Peak discharge = 548.30 cfsStorm frequency = 10 yrsTime to peak = 743 min Time interval = 1 min Hyd. volume = 3,116,573 cuft Drainage area Curve number = 234.960 ac = 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 49.40 min = User Total precip. = 5.20 inDistribution = Type II



Shape factor

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

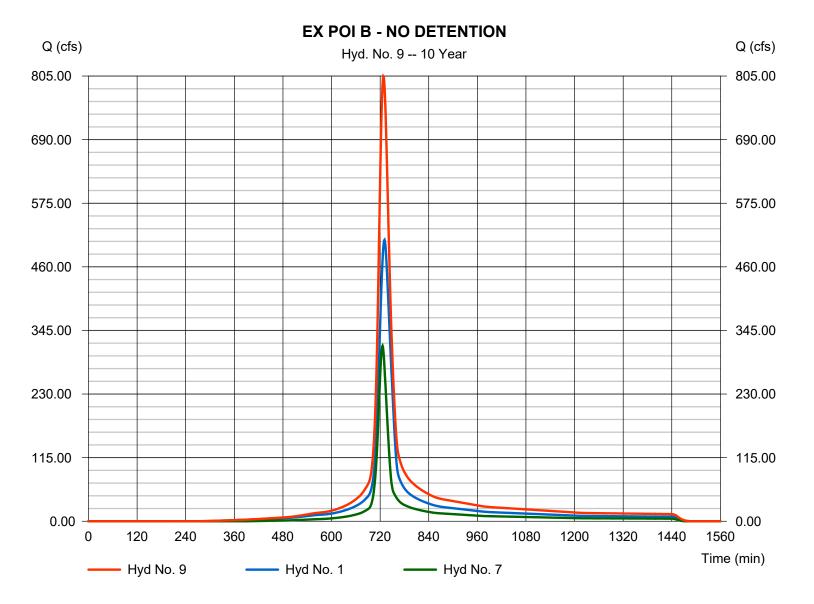
Wednesday, 11 / 6 / 2024

Hyd. No. 9

EX POI B - NO DETENTION

Hydrograph type= CombinePeak discharge= 804.35 cfsStorm frequency= 10 yrsTime to peak= 728 minTime interval= 1 minHyd. volume= 3,110,575

Time interval = 1 min Hyd. volume = 3,110,575 cuft Contrib. drain. area = 234.950 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

= 575.82 cfs

Hyd. No. 10

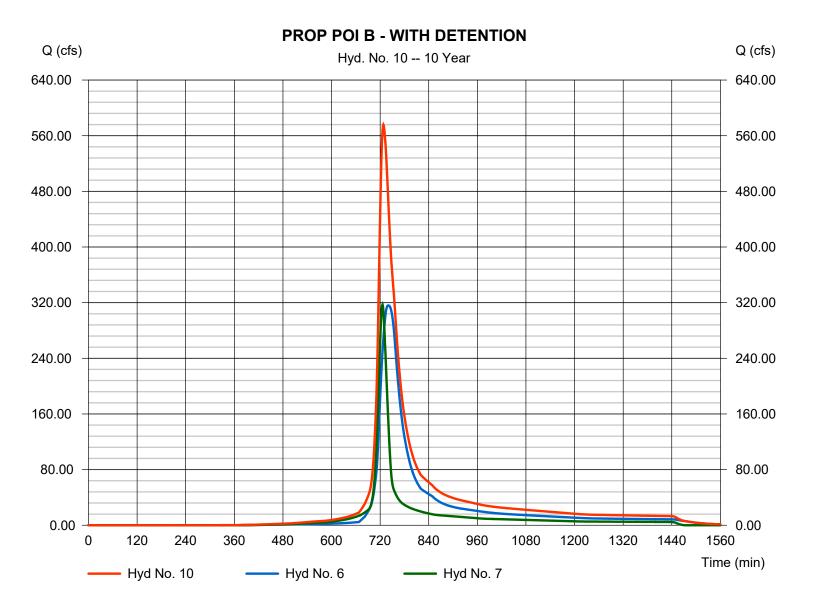
PROP POI B - WITH DETENTION

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min

Time to peak = 728 min Hyd. volume = 3,024,981 cuft

Peak discharge

Inflow hyds. = 6, 7 Contrib. drain. area = 87.500 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hydrailow Hydrographs Extension for Autodeske Civil 3De by Autodesk,							, , , ,	
Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
SCS Runoff	809.50	1	731	3,358,744				EX POI A
SCS Runoff	705.02	1	731	2,925,259				PROP POI A1
SCS Runoff	133.37	1	723	389,754				PROP SUBAREA A
Combine	799.42	1	729	3,315,014	2, 3			COMBINED (A1+A)
Reservoir	472.42	1	743	2,877,564	2	1002.00	768,651	DETAINED SUBAREA A1
Combine	495.24	1	742	3,267,319	3, 5			PROP POLA
SCS Runoff	534.31	1	726	1,787,923				SUBAREA B
SCS Runoff	892.27	1	743	5,152,304				EX POI B - FIS CALIBRATION
Combine	1309.46	1	728	5,146,663	1, 7,			EX POI B - NO DETENTION
Combine	963.41	1	727	5,055,237	6, 7,			PROP POI B - WITH DETENTION
L DHAM VILLA	⊥ GE 24110	⊥)5.gpw		Return P	eriod: 100	∖ Year	Wednesday	⊥ y, 11 / 6 / 2024
	type (origin) SCS Runoff SCS Runoff SCS Runoff Combine Reservoir Combine SCS Runoff SCS Runoff Combine Combine	type (origin) flow (cfs) SCS Runoff 809.50 SCS Runoff 705.02 SCS Runoff 133.37 Combine 799.42 Reservoir 472.42 Combine 495.24 SCS Runoff 534.31 SCS Runoff 892.27 Combine 1309.46 Combine 963.41	type (origin) flow (cfs) interval (min) SCS Runoff 809.50 1 SCS Runoff 705.02 1 SCS Runoff 133.37 1 Combine 799.42 1 Reservoir 472.42 1 Combine 495.24 1 SCS Runoff 534.31 1 SCS Runoff 892.27 1 Combine 1309.46 1	type (origin) flow (cfs) interval (min) Peak (min) SCS Runoff 809.50 1 731 SCS Runoff 705.02 1 731 SCS Runoff 133.37 1 723 Combine 799.42 1 729 Reservoir 472.42 1 743 Combine 495.24 1 726 SCS Runoff 892.27 1 743 Combine 1309.46 1 728 Combine 963.41 1 727	type (origin) flow (cfs) interval (min) Peak (min) volume (cuft) SCS Runoff 809.50 1 731 3,358,744 SCS Runoff 705.02 1 731 2,925,259 SCS Runoff 133.37 1 723 389,754 Combine 799.42 1 729 3,315,014 Reservoir 472.42 1 743 2,877,564 Combine 495.24 1 742 3,267,319 SCS Runoff 534.31 1 726 1,787,923 SCS Runoff 892.27 1 743 5,152,304 Combine 1309.46 1 728 5,146,663 Combine 963.41 1 727 5,055,237	type (origin)	type (origin) flow (cfs) (min) (min) (cuft) volume (cuft) hyd(s) elevation (ft) (min) (cuft) (cuft) elevation (ft) (cuft) (cuft) elevation (ft) elevati	type (origin) flow (orig) interval (min) volume (cuft) hyd(s) elevation (ft) strge used (cuft) SCS Runoff 809.50 1 731 3,359,744 SCS Runoff 133.37 1 723 389,754 Combine 799.42 1 729 3,315.014 2,3 Reservoir 472.42 1 743 2,877.564 2 1002.00 768,651 Combine 496.24 1 742 3,267.319 3,5 SCS Runoff 534.31 1 726 1,787.923 SCS Runoff 892.27 1 743 5,152,304

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

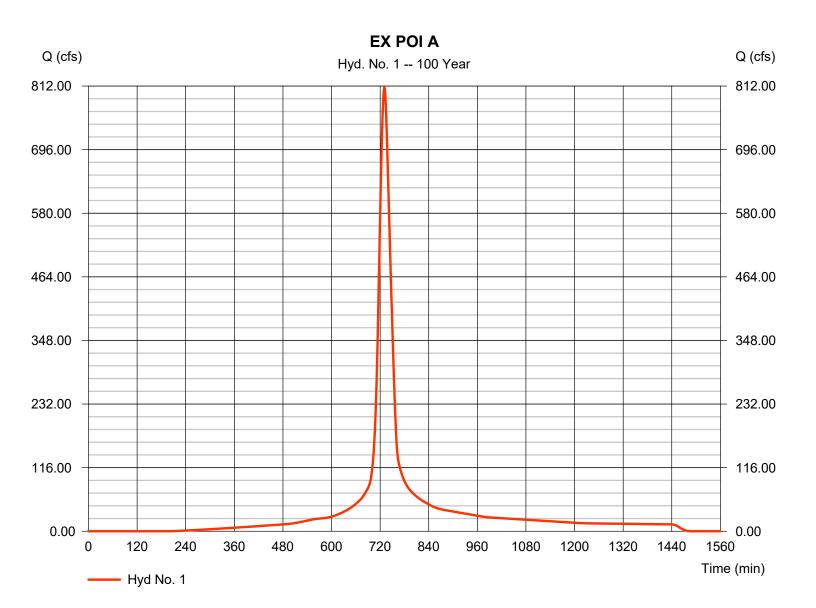
Hyd. No. 1

EX POI A

Hydrograph type= SCS RunoffPeak discharge= 809.50 cfsStorm frequency= 100 yrsTime to peak= 731 minTime interval= 1 minHyd. volume= 3,358,744 cuft

Drainage area = 147.450 ac Curve number = 88 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 7.70 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

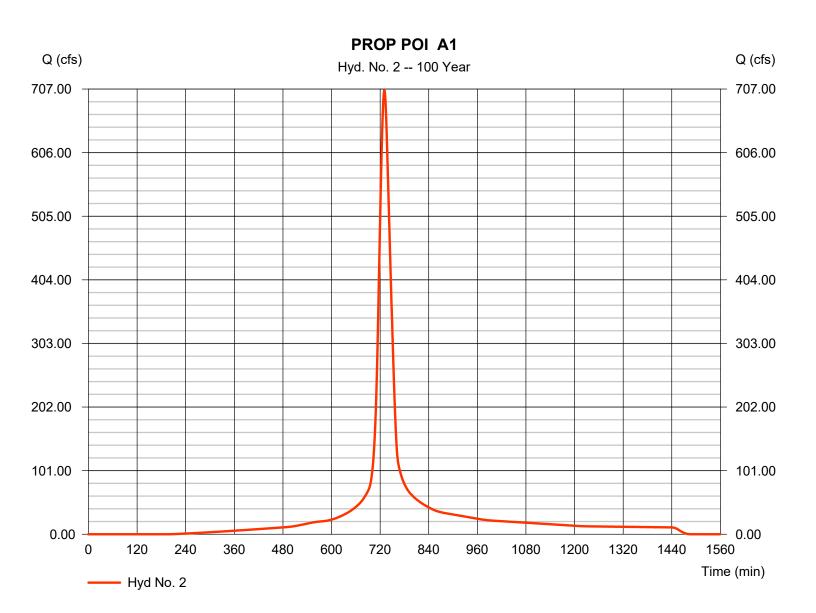
Hyd. No. 2

PROP POL A1

Hydrograph type= SCS RunoffPeak discharge= 705.02 cfsStorm frequency= 100 yrsTime to peak= 731 minTime interval= 1 minHyd. volume= 2,925,259 cuft

Drainage area = 128.420 ac Curve number = 88 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 28.80 min
Total precip. = 7.70 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



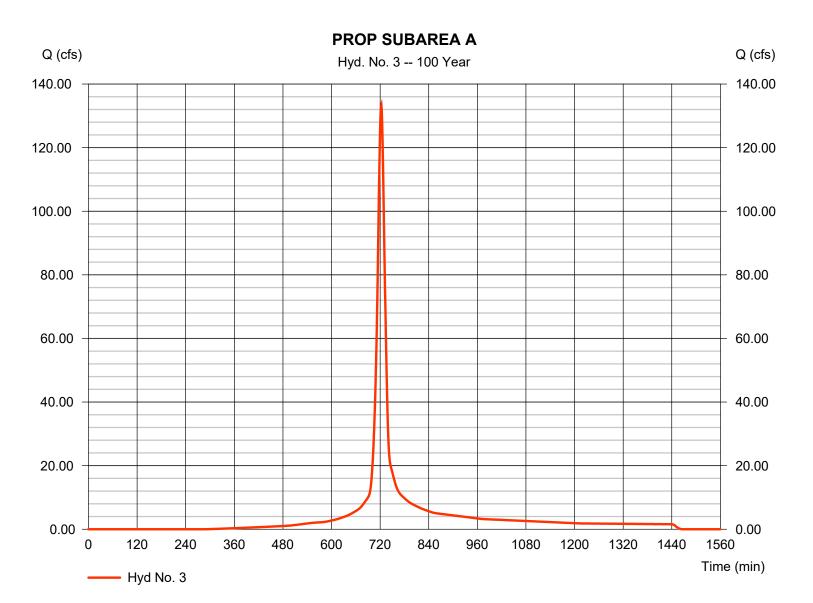
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 3

PROP SUBAREA A

Hydrograph type = SCS Runoff Peak discharge = 133.37 cfsStorm frequency = 100 yrsTime to peak = 723 min Time interval = 1 min Hyd. volume = 389,754 cuft Drainage area Curve number = 19.020 ac= 82 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 15.70 min = User Total precip. = 7.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

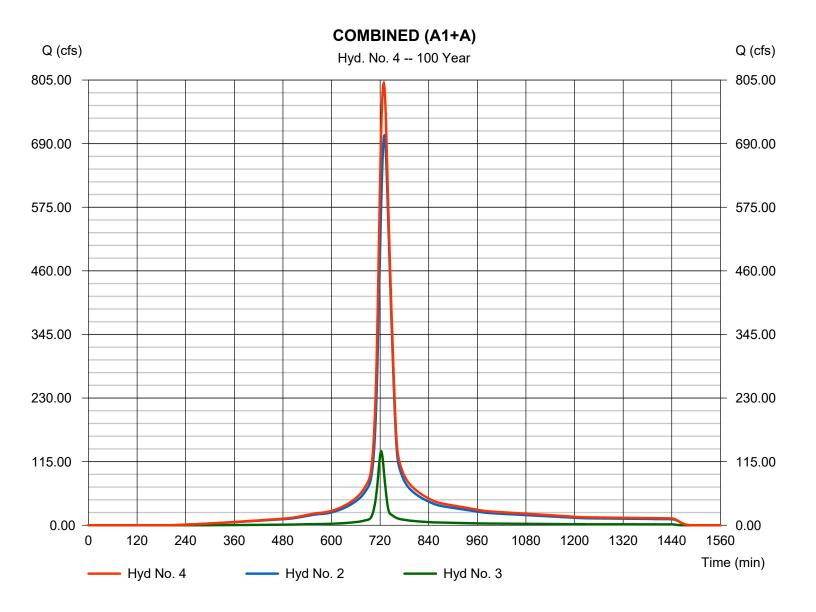
Wednesday, 11 / 6 / 2024

Hyd. No. 4

COMBINED (A1+A)

Hydrograph type = Combine Peak discharge = 799.42 cfs Storm frequency = 100 yrs Time to peak = 729 min

Time interval = 1 min Hyd. volume = 3,315,014 cuft Contrib. drain. area = 147.440 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 5

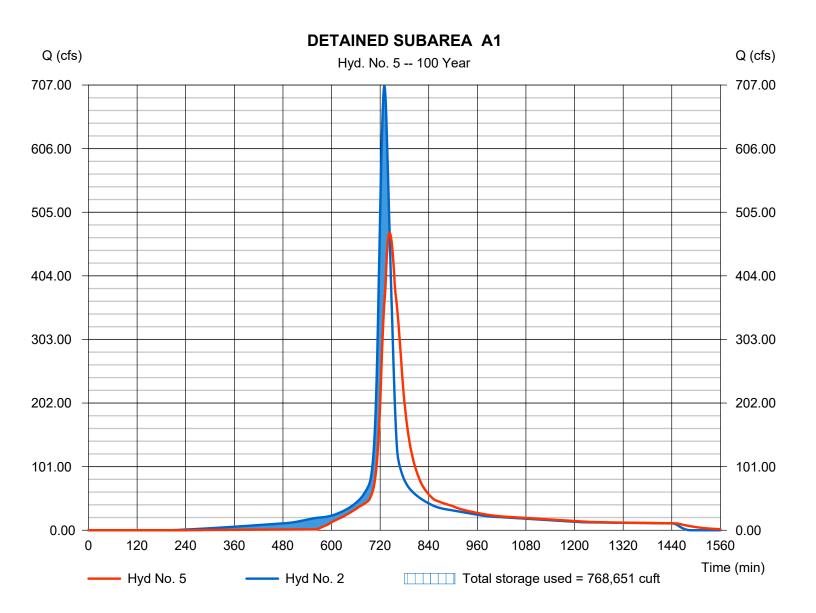
DETAINED SUBAREA A1

Hydrograph type= ReservoirPeak discharge= 472.42 cfsStorm frequency= 100 yrsTime to peak= 743 minTime interval= 1 minHyd. volume= 2,877,564 cuft

Inflow hyd. No. = 2 - PROP POL A1 Max. Elevation = 1002.00 ft

Reservoir name = Retention Basin A1 Max. Storage = 768,651 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

= 495.24 cfs

= 742 min

Hyd. No. 6

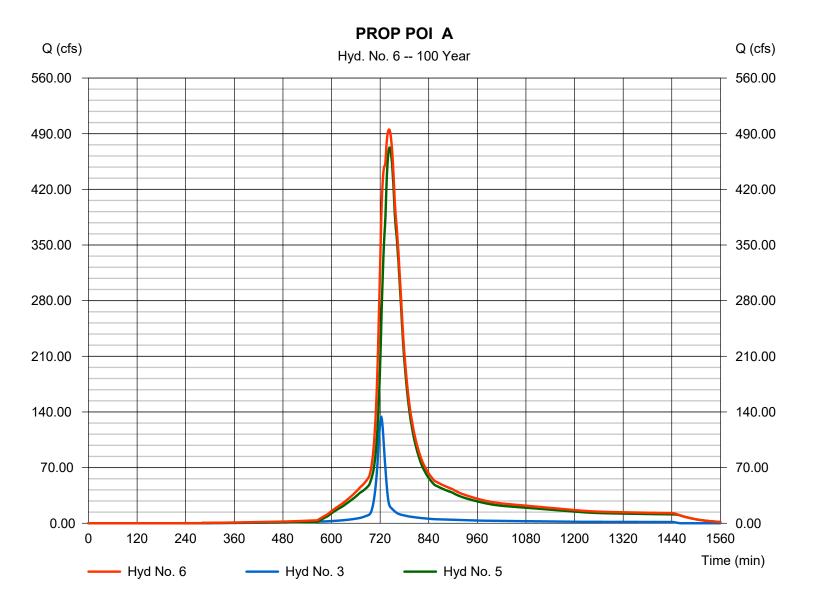
PROP POI A

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 1 min

Time interval = 1 min Hyd. volume = 3,267,319 cuft Contrib. drain. area = 19.020 ac

Peak discharge

Time to peak



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

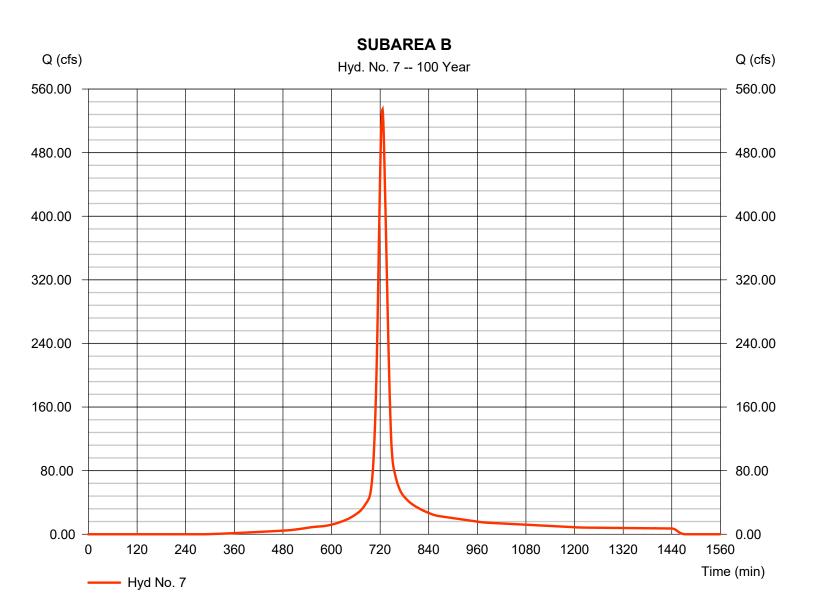
Hyd. No. 7

SUBAREA B

Hydrograph type= SCS RunoffPeak discharge= 534.31 cfsStorm frequency= 100 yrsTime to peak= 726 minTime interval= 1 minHyd. volume= 1,787,923 cuft

Drainage area = 87.500 ac Curve number = 82 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 21.90 min
Total precip. = 7.70 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Wednesday, 11 / 6 / 2024

= 484

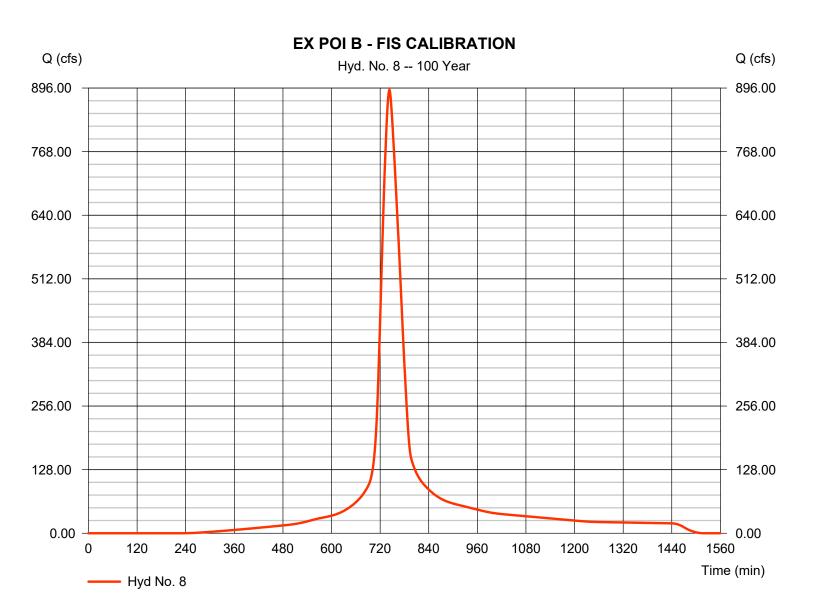
Hyd. No. 8

Storm duration

EX POI B - FIS CALIBRATION

Hydrograph type = SCS Runoff Peak discharge = 892.27 cfsStorm frequency = 100 yrsTime to peak = 743 min Time interval = 1 min Hyd. volume = 5,152,304 cuft Curve number Drainage area = 234.960 ac = 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 49.40 min = User Total precip. = 7.70 inDistribution = Type II

Shape factor



Hydrograph Report

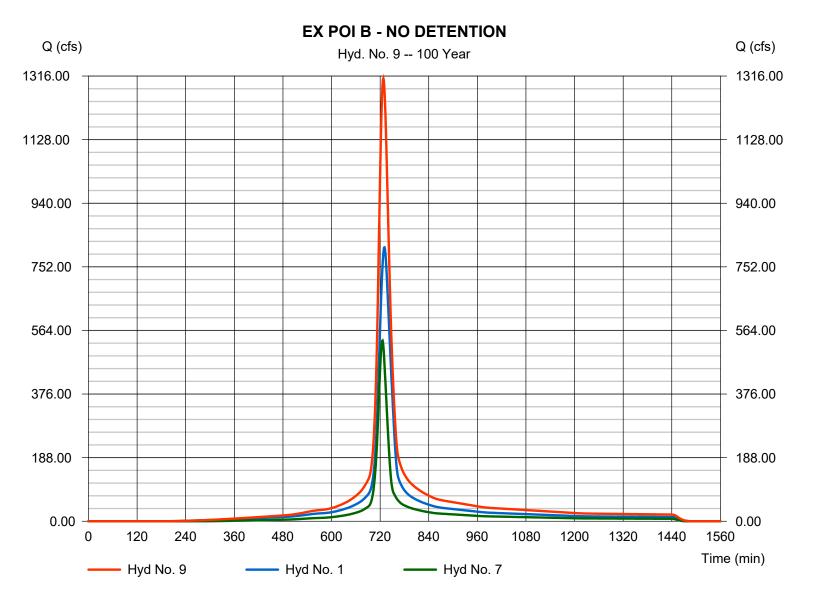
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Hyd. No. 9

EX POI B - NO DETENTION

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 1, 7 Peak discharge = 1309.46 cfs
Time to peak = 728 min
Hyd. volume = 5,146,663 cuft
Contrib. drain. area = 234.950 ac



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 6, 7

Wednesday, 11 / 6 / 2024

= 963.41 cfs

Hyd. No. 10

Inflow hyds.

PROP POI B - WITH DETENTION

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min

Time to peak = 727 min Hyd. volume = 5,055,237 cuft Contrib. drain. area = 87.500 ac

Peak discharge

PROP POI B - WITH DETENTION Q (cfs) Q (cfs) Hyd. No. 10 -- 100 Year 966.00 966.00 828.00 828.00 690.00 690.00 552.00 552.00 414.00 414.00 276.00 276.00 138.00 138.00 0.00 0.00 120 240 360 480 600 720 840 960 1080 1200 1320 1440 1560 Time (min) Hyd No. 10 - Hyd No. 6 Hyd No. 7

Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 11 / 6 / 2024

Return Period	Intensity-Duration-Frequency Equation Coefficients (FHA)										
(Yrs)	В	D	E	(N/A)							
1	64.1474	17.7000	0.8922								
2	95.7859	19.2000	0.9317								
3	0.0000	0.0000	0.0000								
5	118.7799	19.1000	0.9266								
10	125.1300	18.2000	0.9051								
25	158.9867	18.7000	0.9180								
50	171.2459	18.3000	0.9078								
100	187.3624	18.1000	0.9031								

File name: KCMO.IDF

Intensity = B / (Tc + D)^E

Return	Intensity Values (in/hr)											
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	3.96	3.31	2.86	2.52	2.25	2.04	1.87	1.72	1.60	1.49	1.40	1.32
2	4.92	4.13	3.56	3.14	2.81	2.54	2.32	2.14	1.98	1.85	1.73	1.63
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.23	5.23	4.51	3.98	3.56	3.22	2.94	2.71	2.52	2.35	2.20	2.07
10	7.27	6.09	5.26	4.63	4.14	3.75	3.43	3.16	2.93	2.74	2.57	2.42
25	8.70	7.30	6.30	5.54	4.96	4.49	4.10	3.78	3.51	3.27	3.07	2.89
50	9.83	8.24	7.11	6.26	5.60	5.07	4.64	4.27	3.97	3.70	3.47	3.27
100	11.00	9.21	7.95	7.00	6.26	5.67	5.19	4.78	4.44	4.14	3.89	3.66

Tc = time in minutes. Values may exceed 60.

Precip. file name: Z:\acad\KCMO.pcp

	Rainfall Precipitation Table (in)											
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr				
SCS 24-hour	1.37	3.50	0.00	3.30	5.20	6.00	6.80	7.70				
SCS 6-Hr	0.00	1.80	0.00	0.00	2.60	0.00	0.00	4.00				
Huff-1st	0.00	1.55	0.00	2.75	4.00	5.38	6.50	8.00				
Huff-2nd	2.49	3.10	0.00	4.01	4.64	5.52	6.21	6.90				
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				
Huff-Indy	0.00	1.55	0.00	2.75	4.00	5.38	6.50	8.00				
Custom	0.00	1.75	0.00	2.80	3.90	5.25	6.00	7.10				

Hydraflow Table of Contents

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

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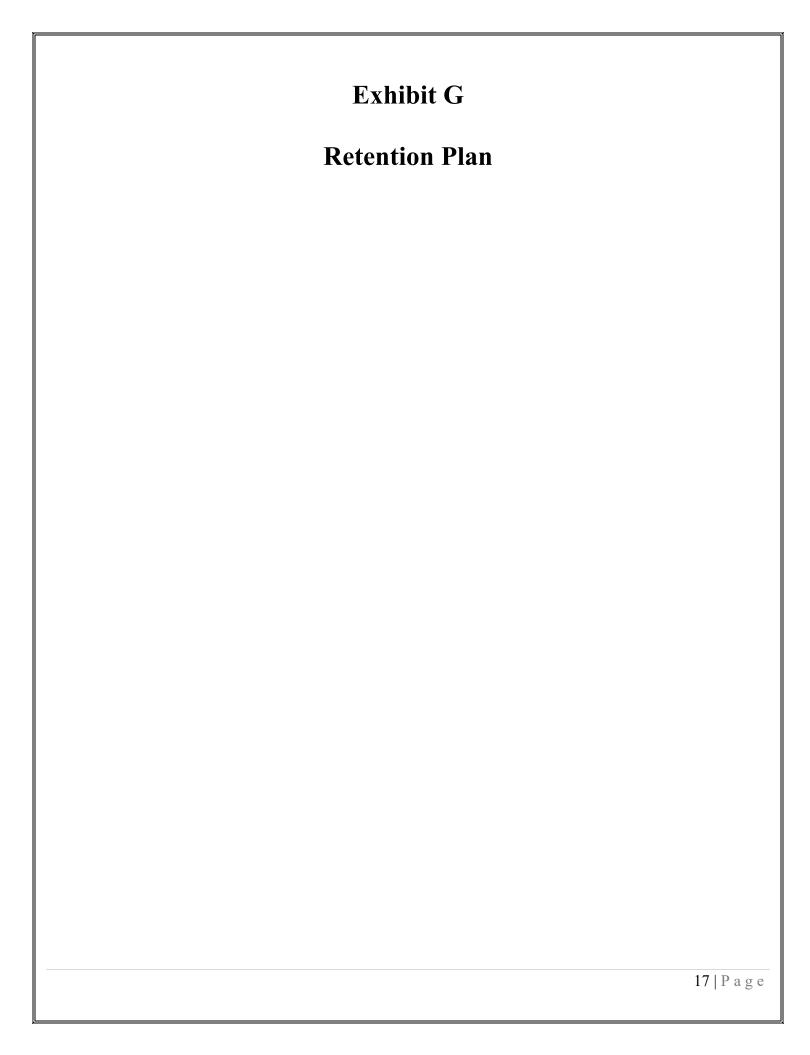
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Hydrograph No. 2, SCS Runoff, PROP POI A1						
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Exhibit F Proposed Drainage Area Map 16 | P a g e



Professional Registration
Missouri
Engineering 2005002186-D
Surveying 2005008319-D
Kansas
Engineering E-1695
Surveying LS-218
Oklahoma Engineering 6254 Nebraska Engineering CA2821

Matthew J. Schlicht MO PE 2006019708 KS PE 19071 OK PE 25226 NE PE E-14335



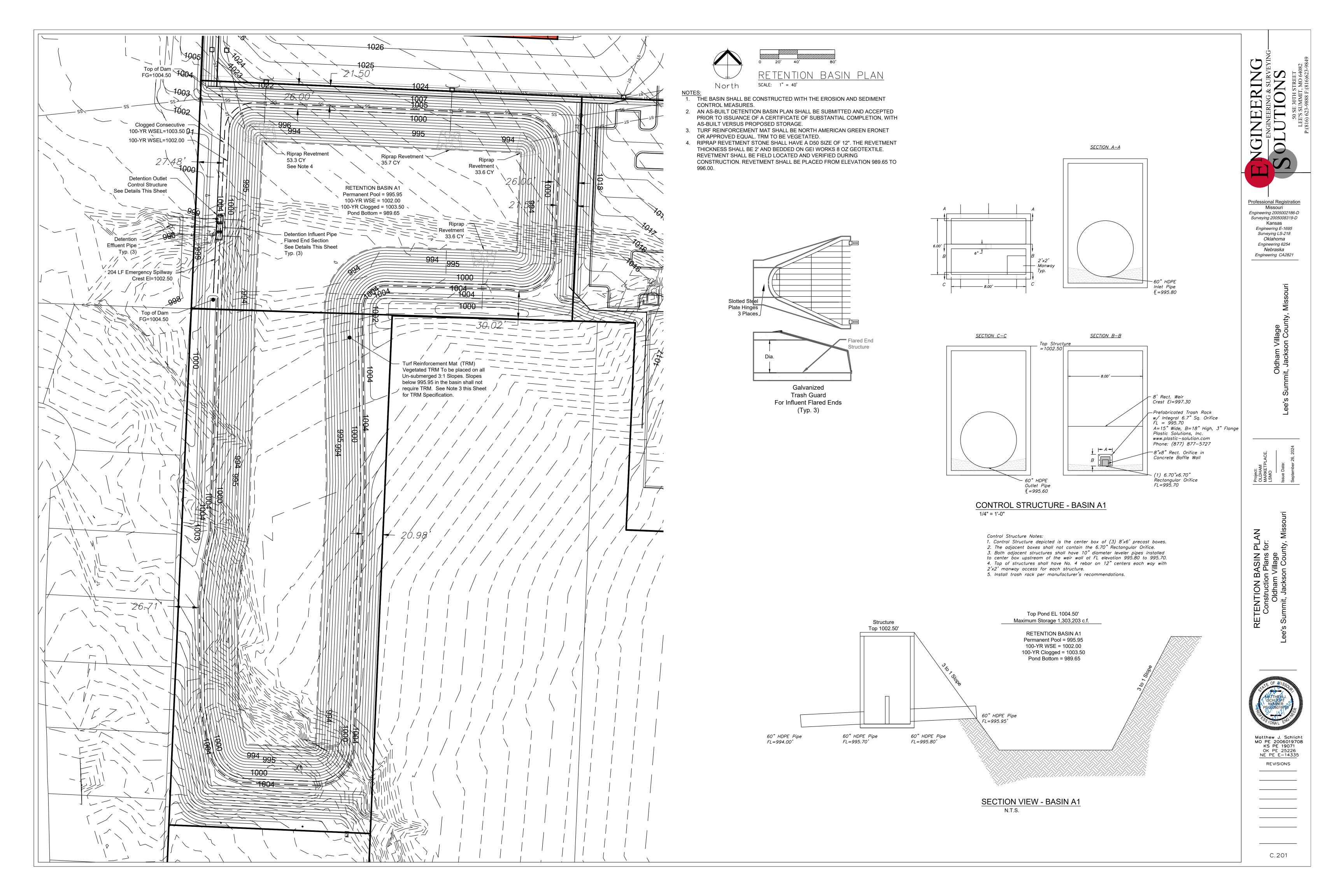


Exhibit H **Emergency Spillway Calculations** 18 | P a g e

Combination Broad + Sharp Crest Weir Capacity - Emergency Spillway

Oldham Village

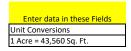
Peak Discharge (cfs)	705.02
Broad Crested Weir	
Capacity (cfs)	528
Crest Length (ft)	204
Weir Coefficient, C	2.6
Required Head, H (ft)	0.997
Sharp Crested Weir	
Capacity (cfs)	177.02
Crest Length (ft)	53.5
Weir Coefficient, C	3.33
Required Head, H (Ft)	0.996
100-YR WSE	1002.00 (Hydraflow)
Required 100-YR Freeboard (ft)	0.5
Emergency Spillway Crest Elevation	1002.50
Required Head Emergency Spillway, H (ft)	1.00
Clogged 100-YR WSE	1003.50
Clogged Consecutive 100-YR freeboard (ft)	1.00
Top of Dam	1004.50

Exhibit I 40 Hour Extended Detention Calculations 19 | P a g e

Calculate Water Quality for Storm Study

Project: Oldham Village (Retention Basin A1) To Calculate: WQv = P * Rv * A

_	
P (in) =	1.37
P (ft) =	0.11
Impervious Area (sq. ft.) =	1,341,652.77
Total Area (sq. ft.) =	2,164,060.80
Impervious Area (ac) =	30.80
Total Area (acre) =	49.68



Date: 11-1-2024

Rv = (0.05 * 0.009(I)) = Percent Impervious (I) 63.33 WQ, (cu. ft.) = 153,172 WQ, (ac. ft.) = 3.516

Pond Volume

Elevation	Area (Sq. Ft.)	Volume (Cu. Ft.)
995.95	108,955	0
996	109,246	5,455
998	121,115	235,816
1,000	133,209	490,140
1,002	145,530	768,879
1,004	158,077	1,072,486

40 HOUR DETENTION CALC.

To Calculate:

40 Hour Detention (EDDB)

 A_T (ac) =

I. Basin Water Quality Storage Volume

Step 1) Tributary area To EDDB, At (ac) = Step 2) Calculate WQ_v using Sec. 6 (ac-ft) = Step 3) Add 20 Percent to Step 2.

3.516 WQ_v (ac. ft.)= V_{design} (ac-ft) = 4.220

II.a. Water Quality Outlet Type

Step 1) Set water quality outlet type

Type 1 = single orifice

Type 2 = perforated riser or plate

Type 3 = v-notch weir

Outlet Type =

49.68

0.67

1.064

0.66

997.28

Step 2) Proceed to Step lib, lic, or lid based on selection

> Ilb. Water Quality Outlet, Single Orifice Z_{WQ} (ft) : 1.33 See Below to Calc. Z_{WO}

> > H_{WQ} (ft) =

Q_{WQ} (cfs) =

CO (unitless) =

Step 1) Depth of water quality volume at outlet Step 2) Average Head of water volume over invert of

Orifice Step 3) Average Water quality outflow rate

Step 4) Set value of orifice discharge coefficient a) 0.66 when thickness of riser/weir plate \leq orifice

b) 0.80 when thickness of riser/weir plate > orifice

Step 5) Water quality outlet orifice dia.

 D_0 (in) = 6.72 6.718209605

(if orifice dia. < 4 inches, use outlet type 2 or 3)

To Calculate Z_{WQ} (ft) interpolate from Storm Study (Sheet 13)

Elevation 1 =	996.00	Storage 1 =	5,455.00
Elevation X =		Storage X =	153,172.03
Elevation 2 =	998.00	Storage 2 =	235,816.00
			•

Elevation X =

Lowest Elevation of Pond = Elevation X 997.28 Z_{WQ} (ft) = 1.33

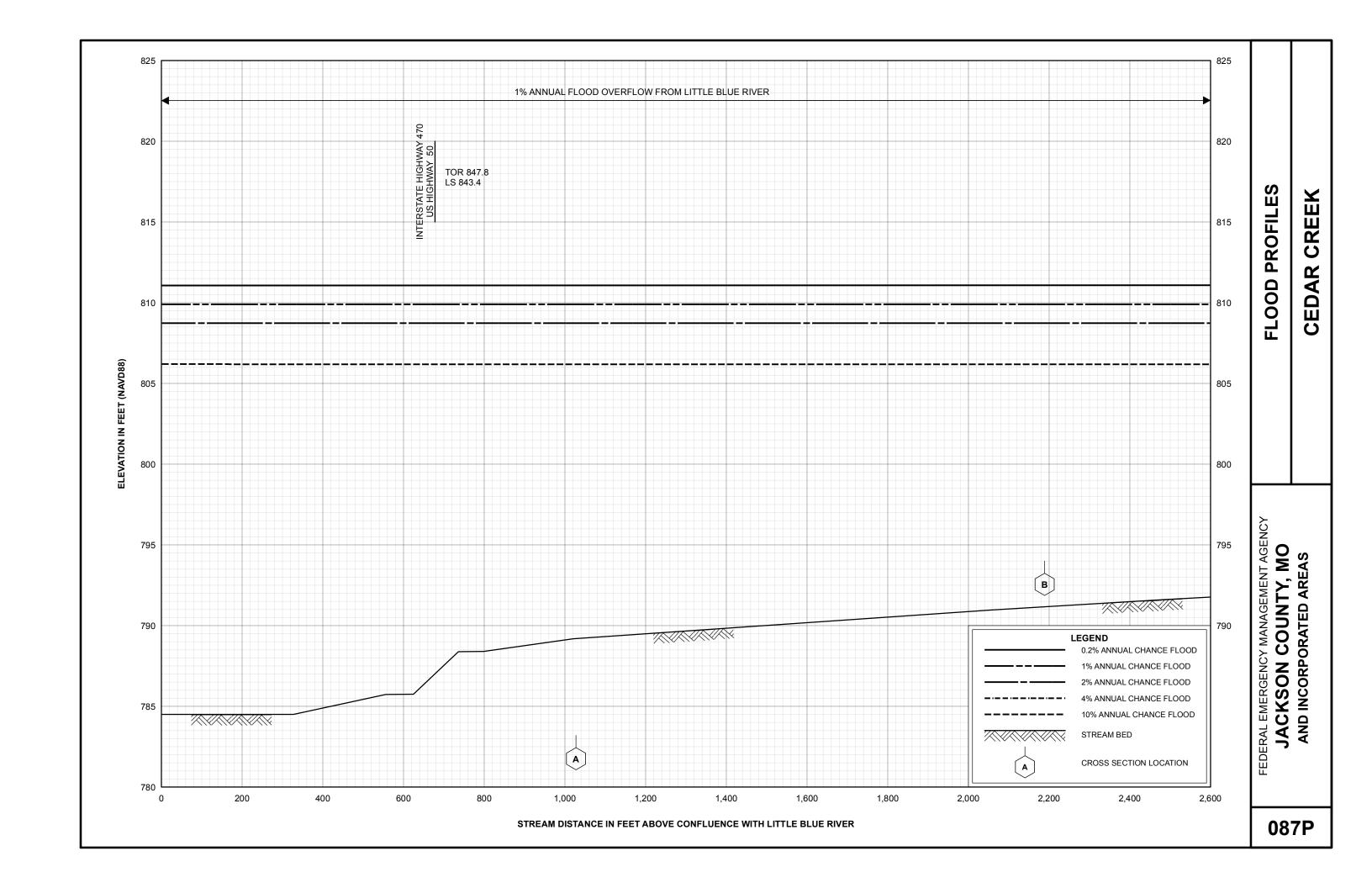
Exhibit J

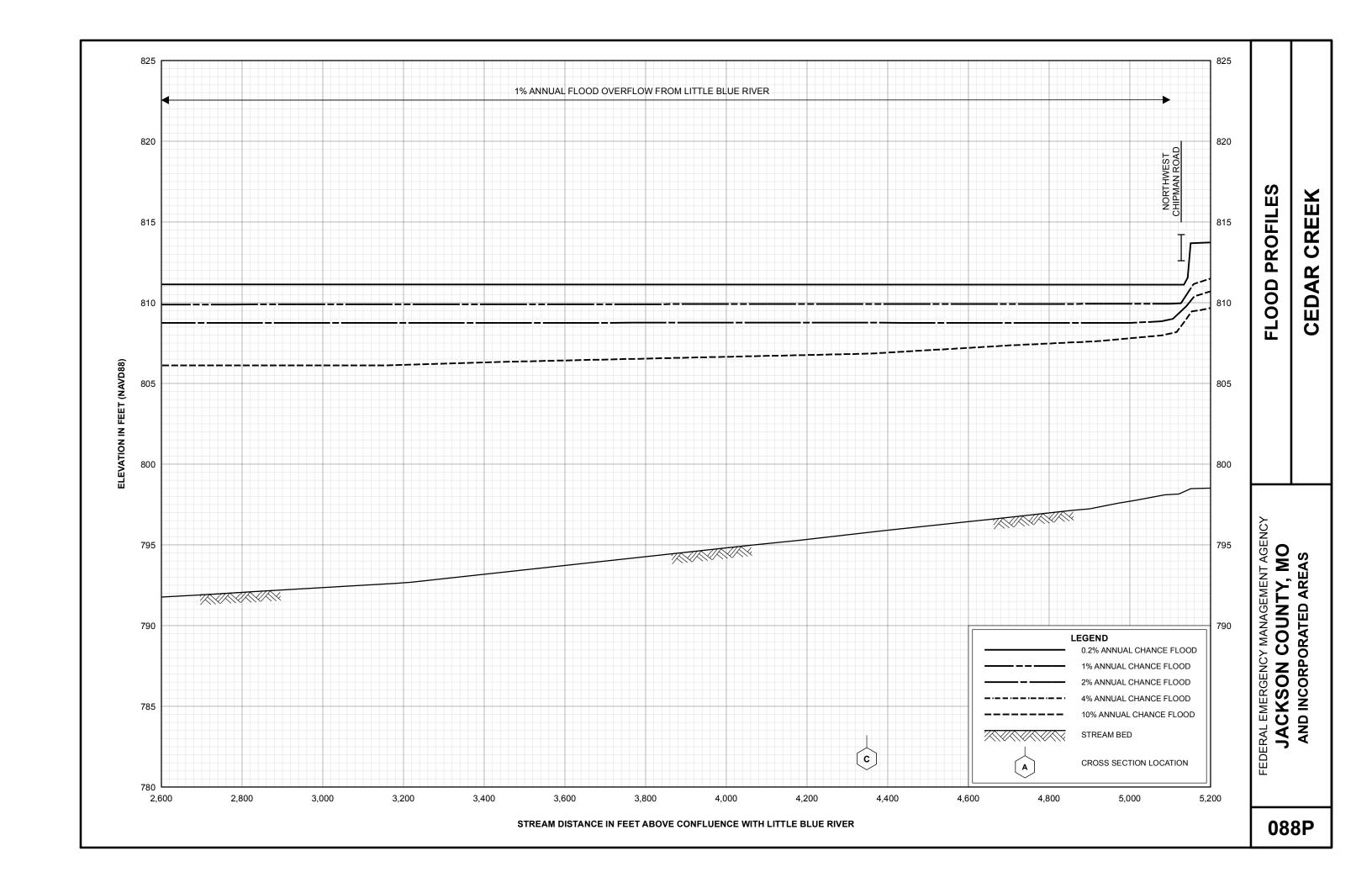
FEMA FIS Data

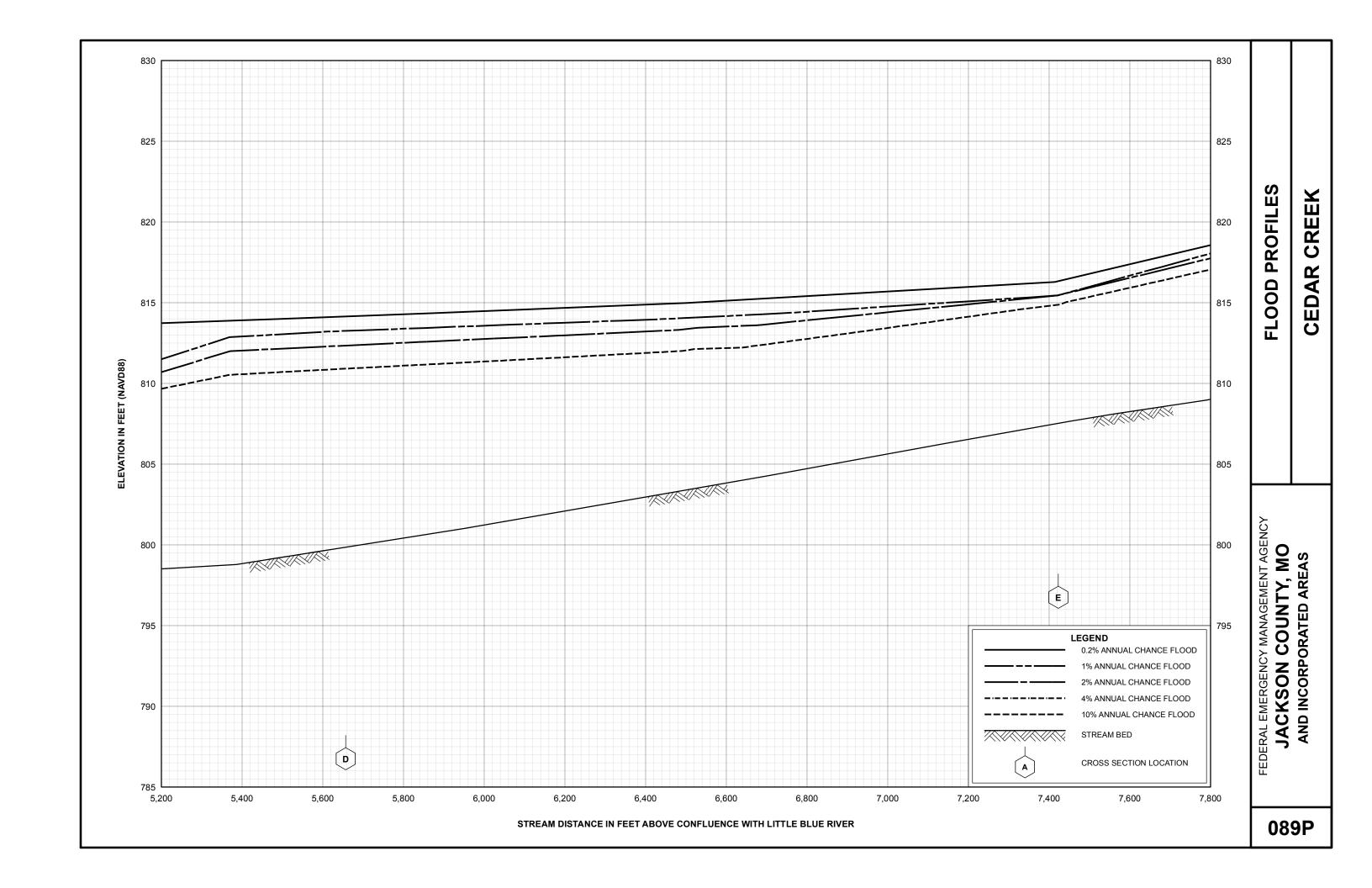
Downstream Drainage Area Maps With Parcels Without Parcels

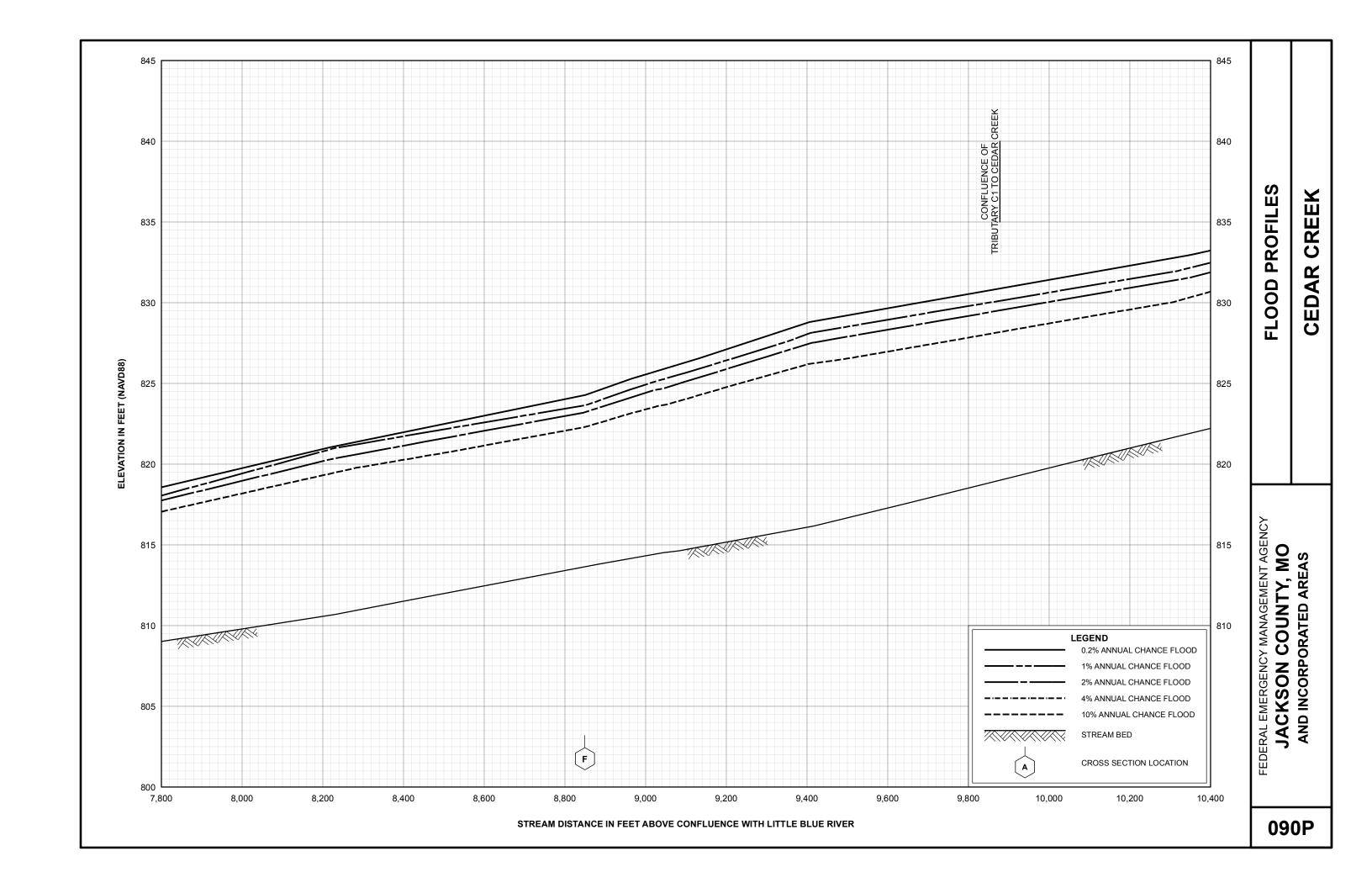
Composite Curve Number Calculations

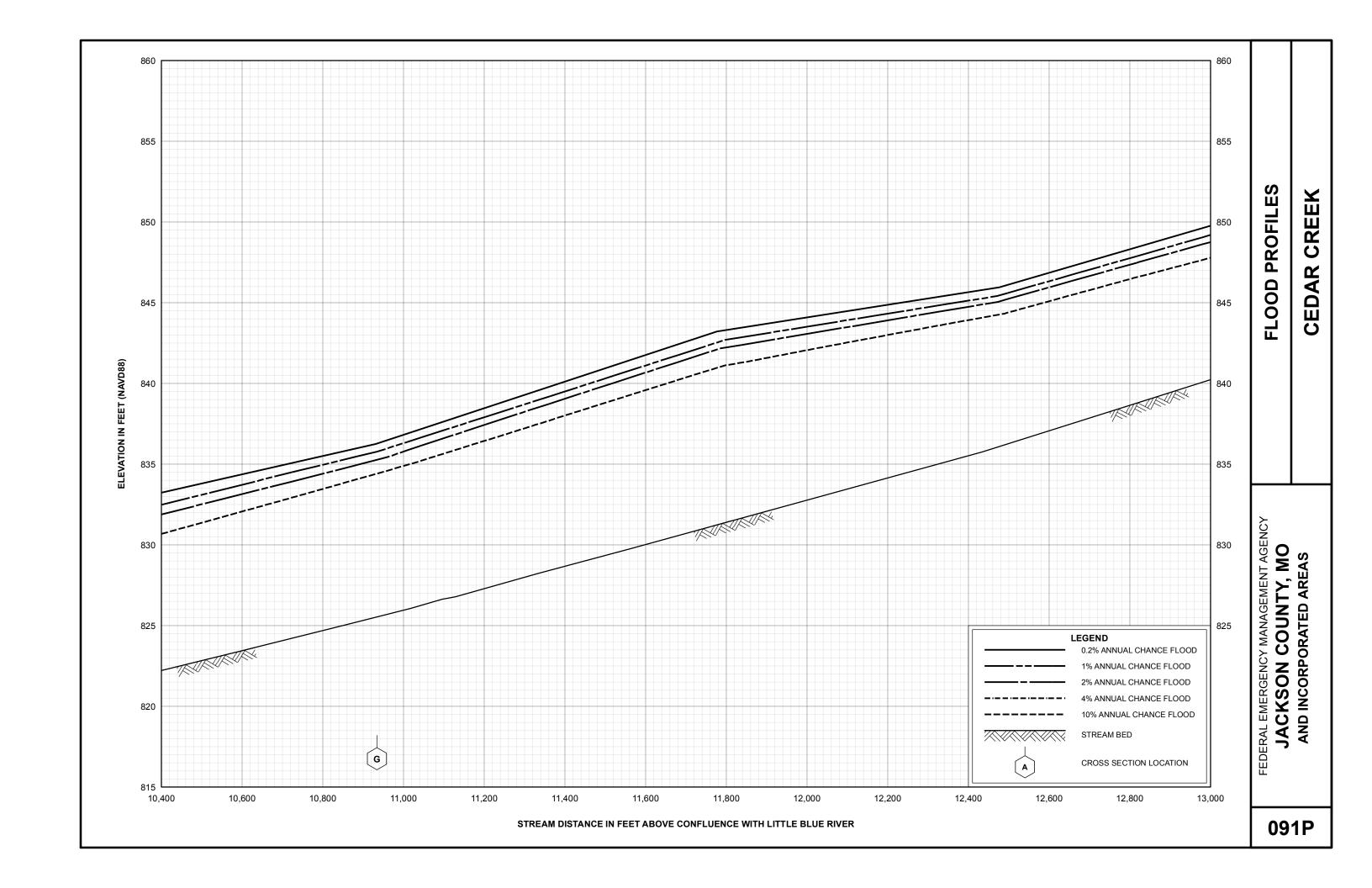
Time of Concentration Calculations

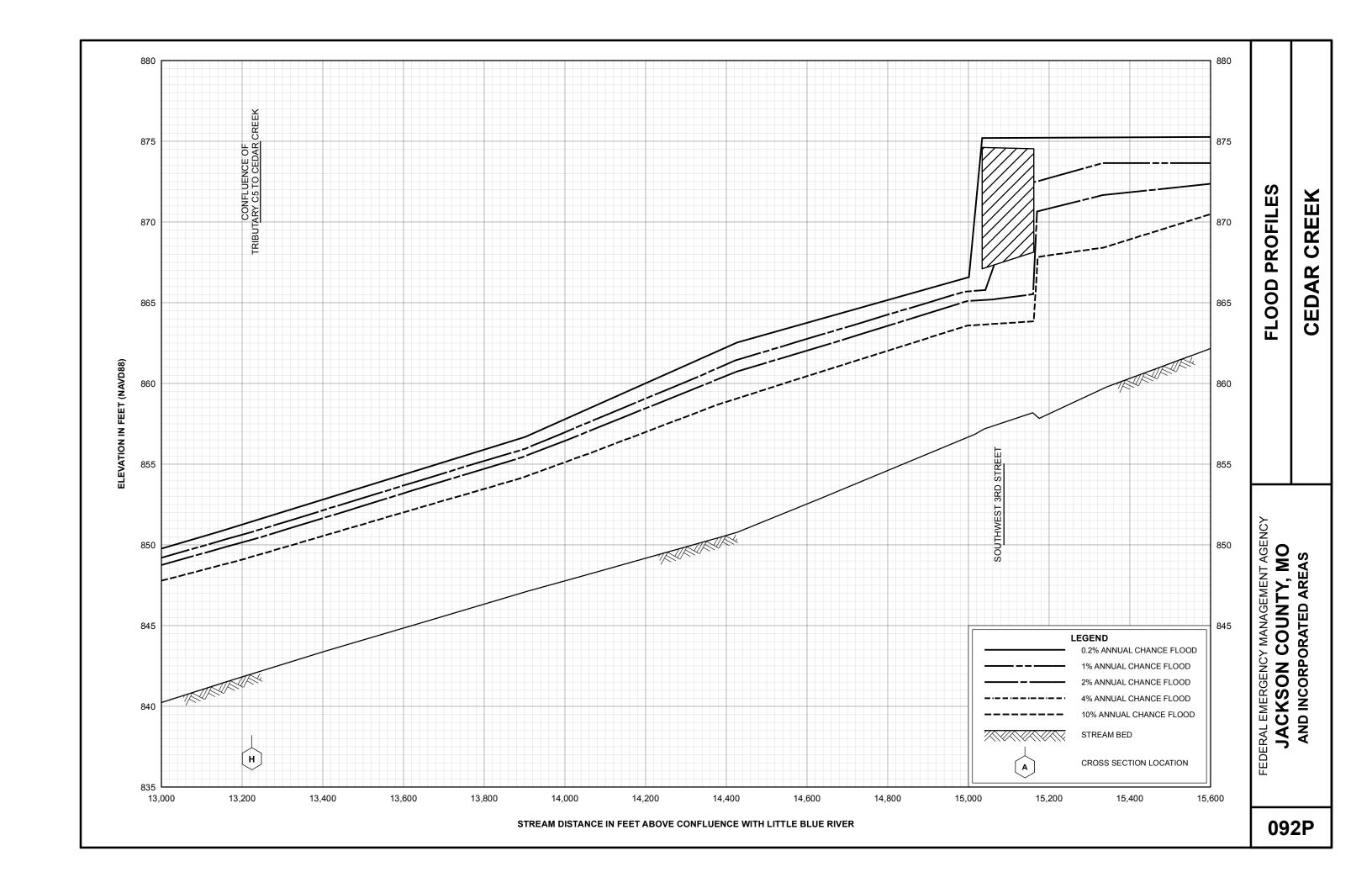


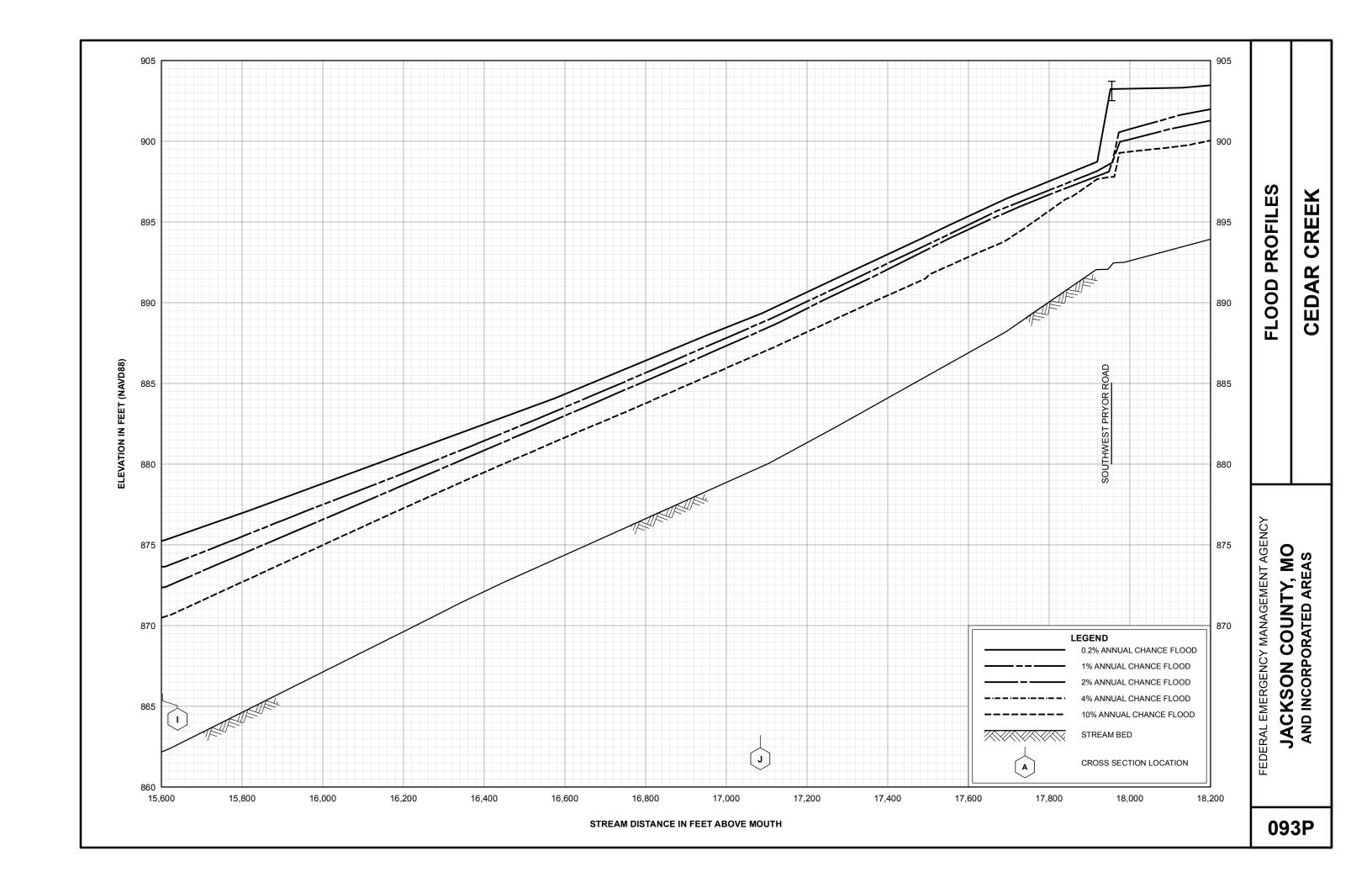


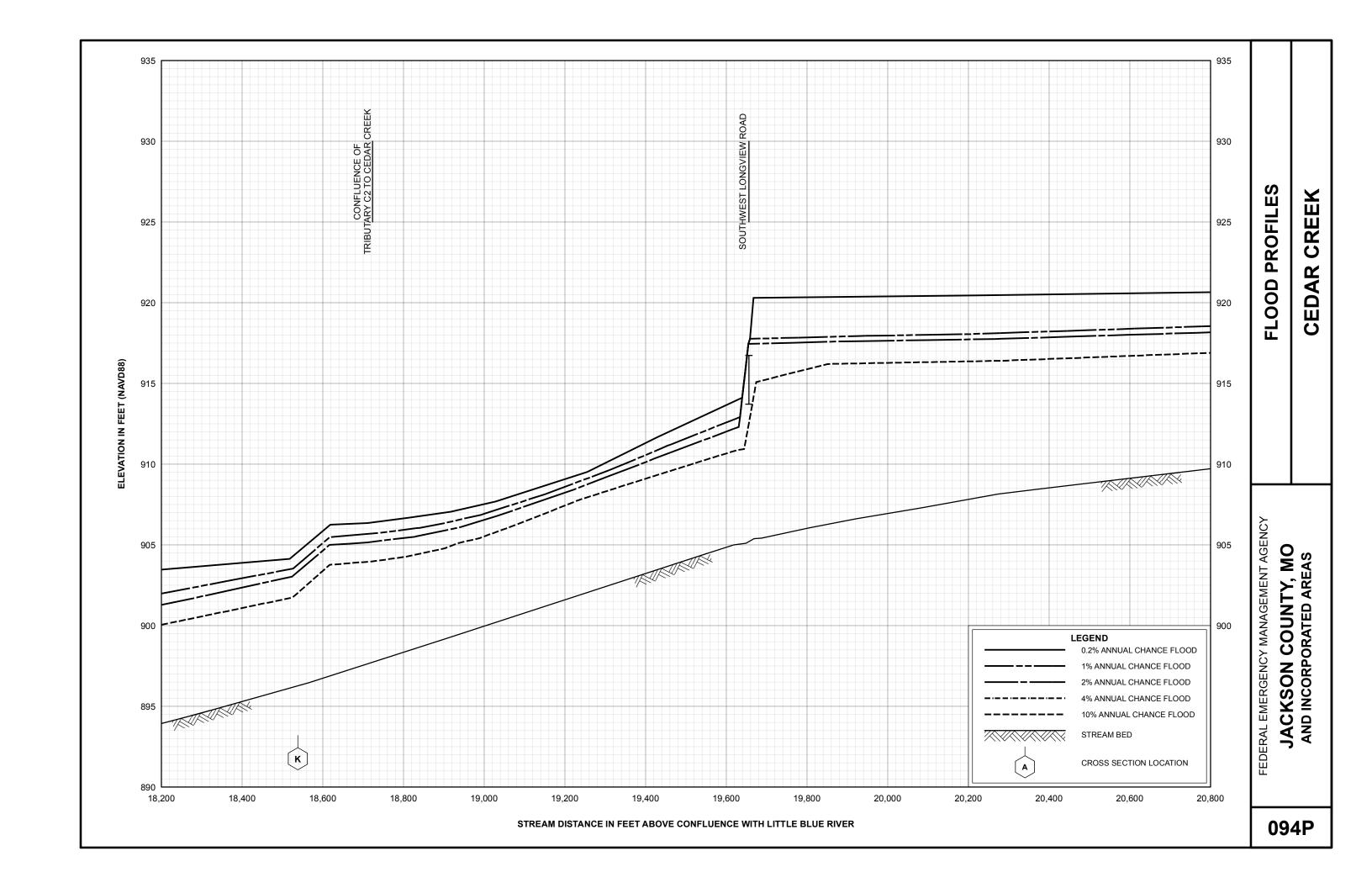


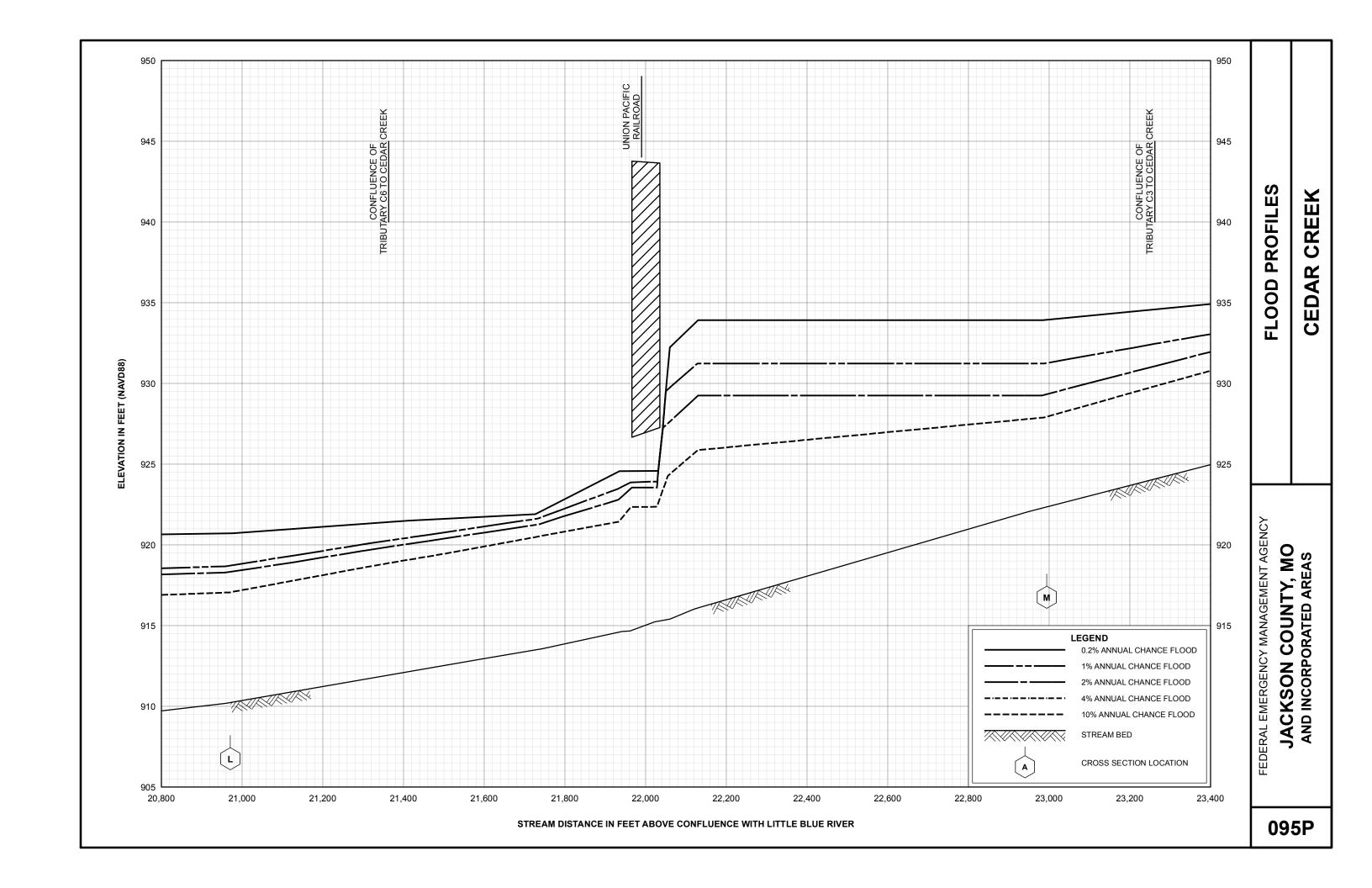


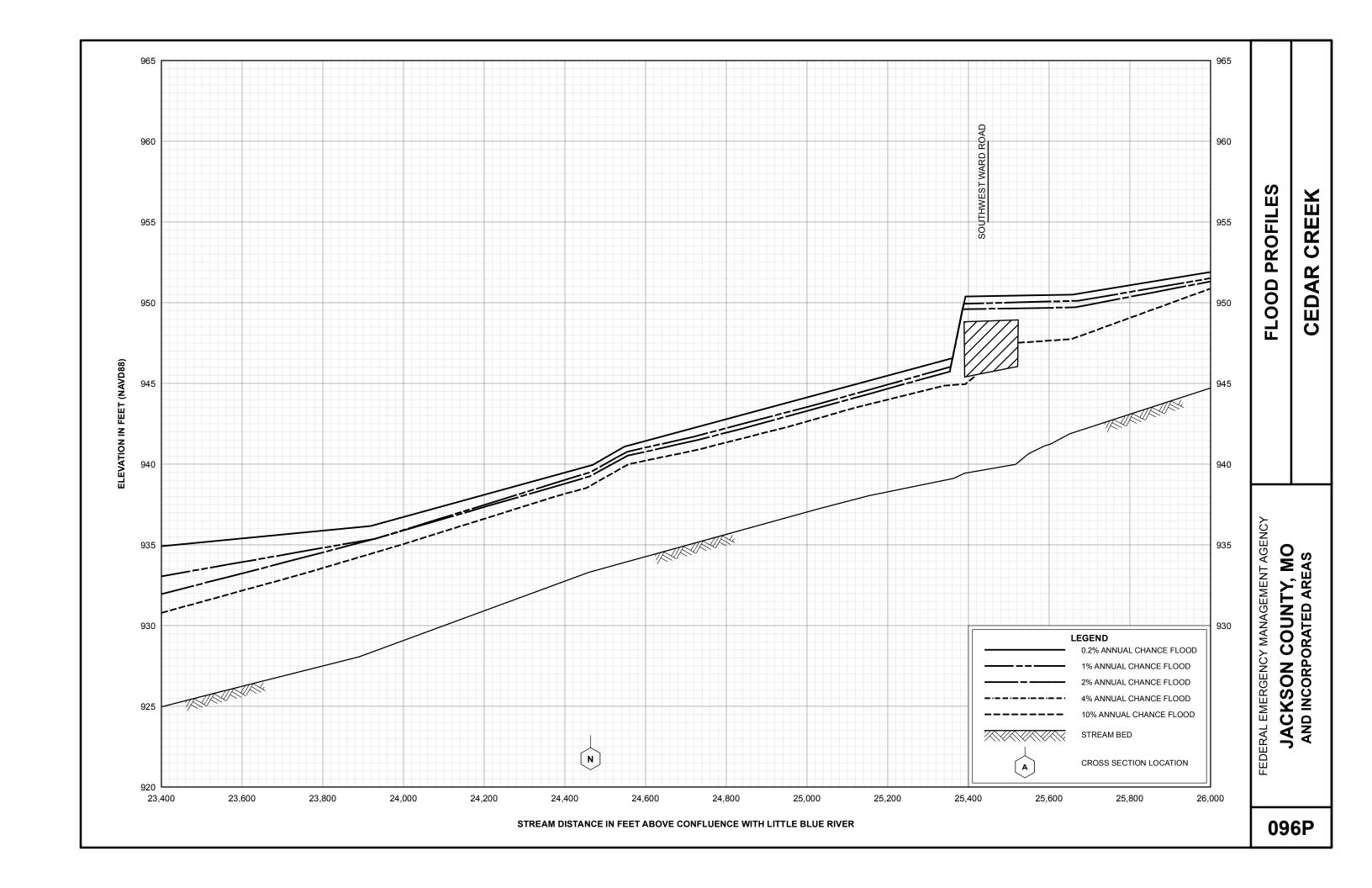


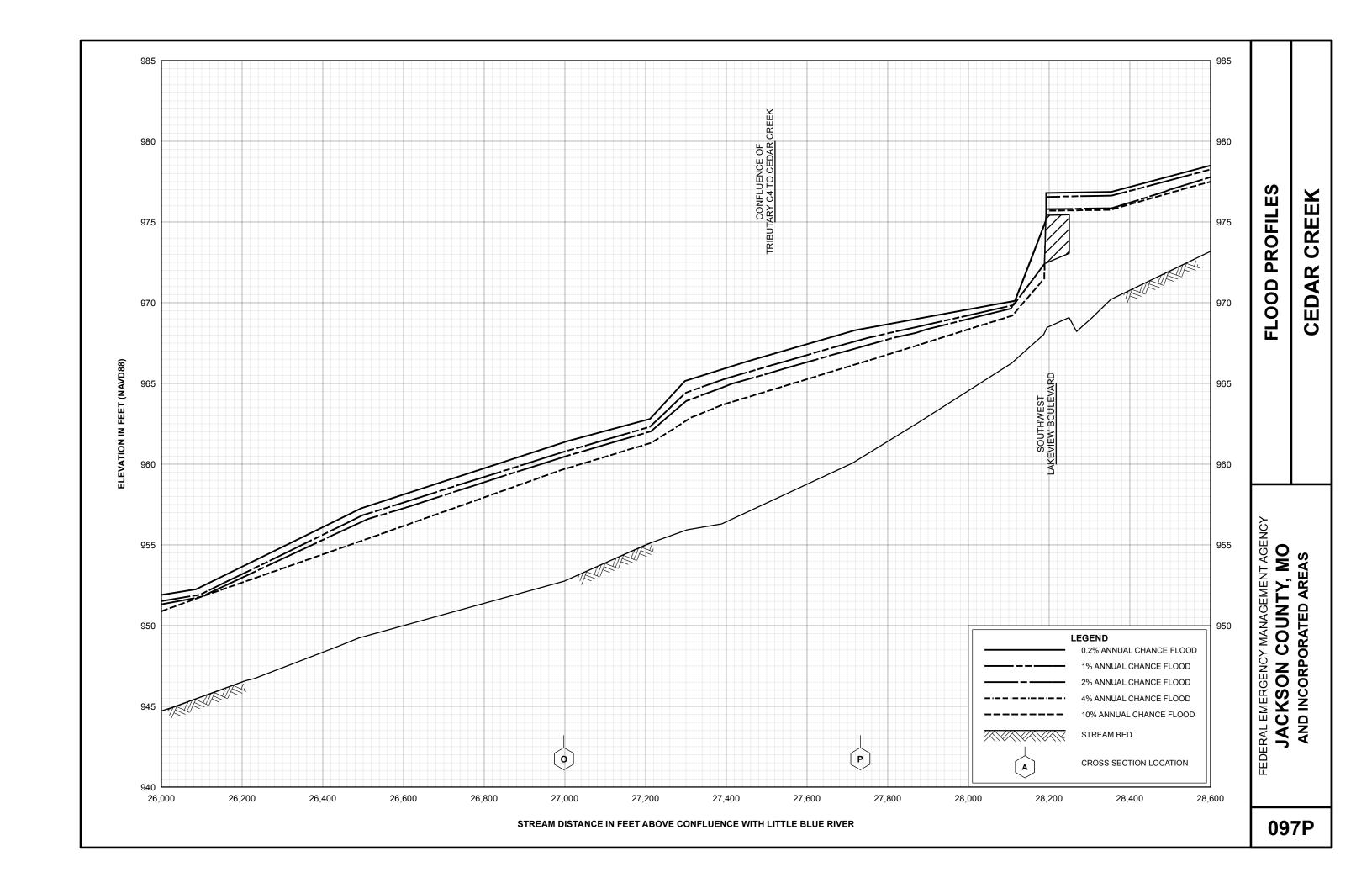












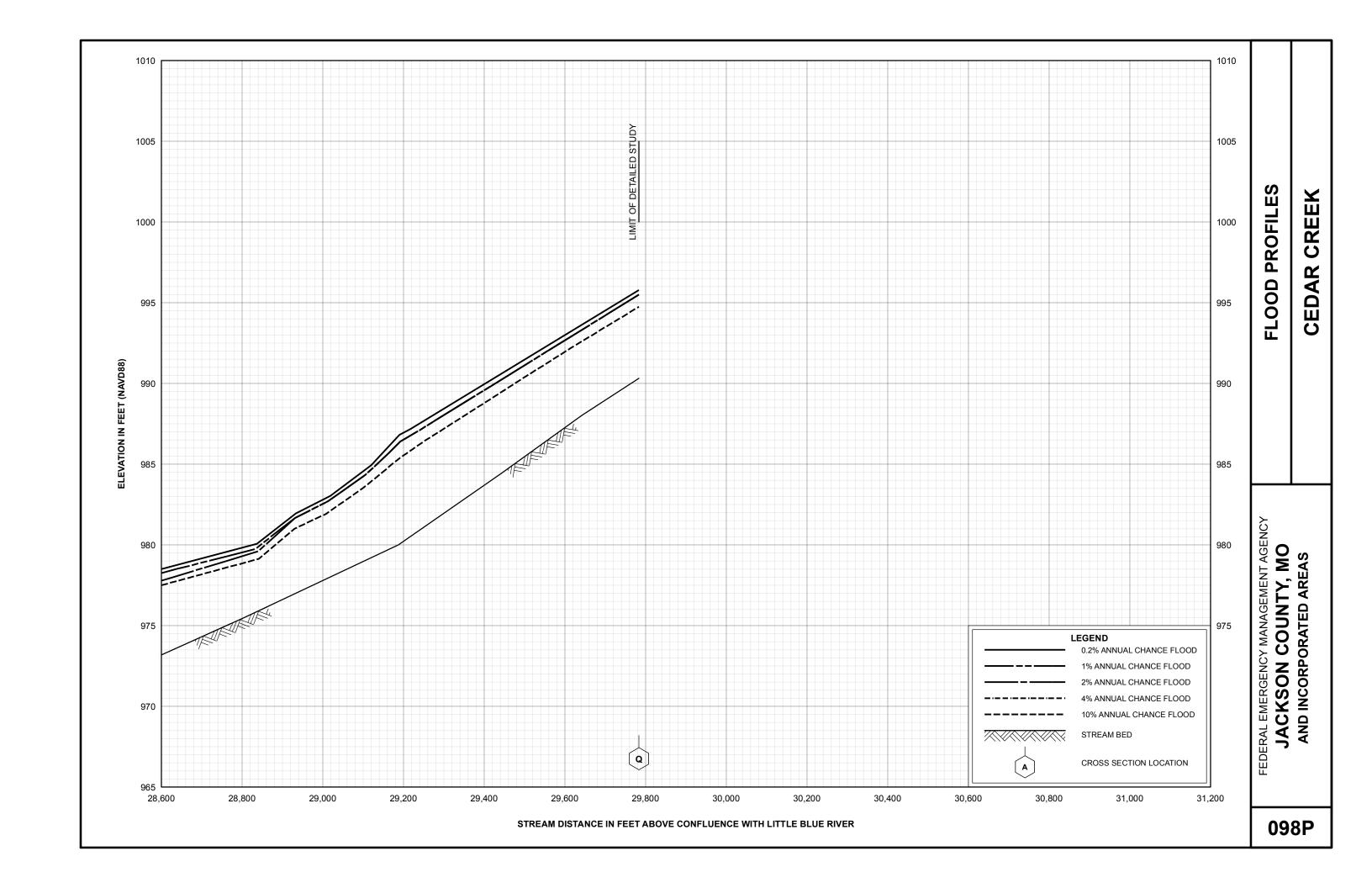


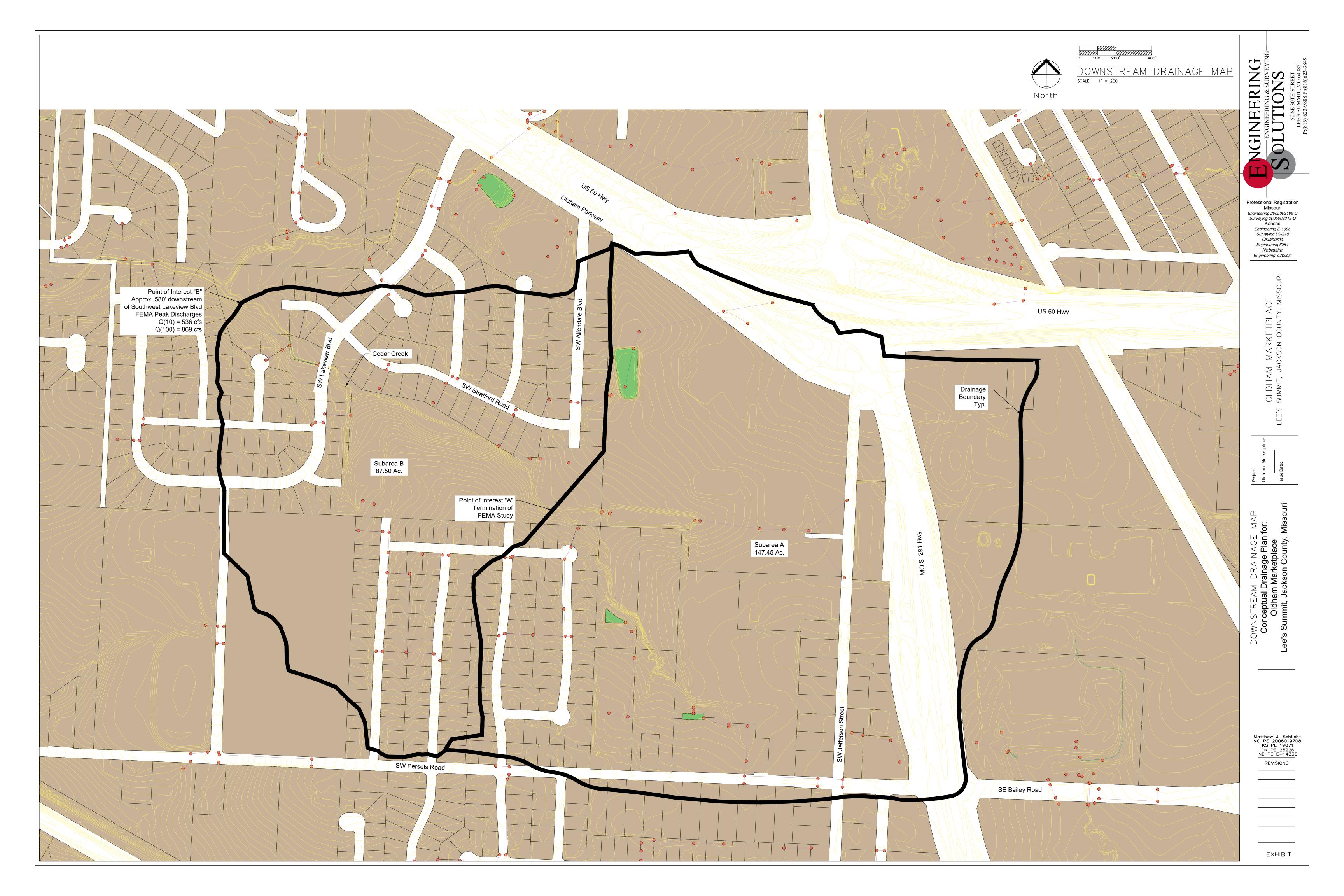
TABLE 3 – SUMMARY OF DISCHARGES (CONT'D)

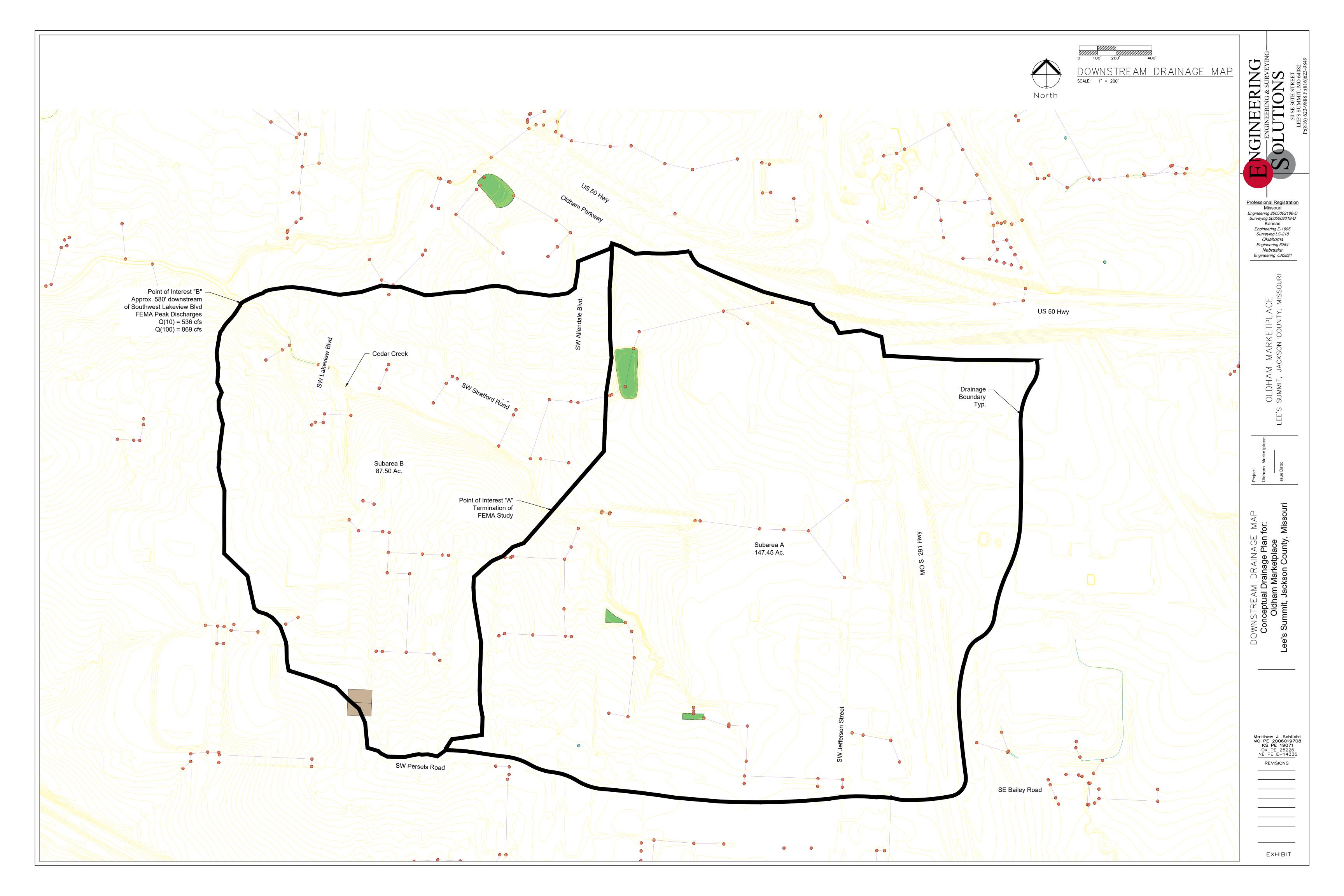
DEAK ANNITAL CHANCE DISCHARGES (CES)

	PEAK ANNUAL CHANCE DISCHARGES (CFS)								
FLOODING SOURCE	DRAINAGE AREA	10-Percent	4-Percent-	2-Percent-	1-Percent-	0.2-Percent			
AND LOCATION	(sq. miles)	Annual Chance	Annual-Chance	Annual-Chance	Annual-Chance	Annual-Chance			
BURLINGTON CREEK (CONT'D)									
Just downstream of Tom Watson	0.4	955	N/A	1,288	1,535	1,943			
Parkway	0.4	933	IV/A	1,200	1,333	1,943			
BURLINGTON CREEK									
TRIBUTARY 1									
Just downstream of Northwest 62 nd	0.4	955	N/A	1,289	1,535	1,943			
Terrace	0.4	933	IV/A	1,209	1,333	1,943			
BURLINGTON CREEK									
TRIBUTARY 2									
Approximately 1,000 feet upstream									
of the confluence with Burlington	0.5	650	N/A	1,014	1,302	1,806			
Creek									
Approximately 1,500 feet upstream									
of the confluence with Burlington	0.5	524	N/A	817	1,050	1,462			
Creek									
BURR OAK CREEK									
Approximately 1,500 feet									
downstream of Northwest Pink Hill	4.3	1,400	N/A	2,900	3,600	5,200			
Road									
At Northwest Pink Hill road	1.7	800	N/A	1,700	2,100	3,000			
BURR OAK CREEK TRIBUTARY									
Approximately 500 feet upstream of	1.6	610	N/A	1,200	1,500	2,200			
confluence with Burr Oak Creek	1.0	010	1 1/11	1,200	1,500	2,200			
CEDAR CREEK									
At confluence with Little Blue	*	3,900	N/A	5,780	6,750	8,240			
River		,		,	•	,			
At Northwest Chipman Road	*	3,840	N/A	5,710	6,680	8,180			
Approximately 0.8 miles upstream	*	3,470	N/A	5,130	5,990	7,310			
of Northwest Chipman Road		2,	1 1/1 1	2,120	2,220	7,510			
*Data not available.									

TABLE 3 – SUMMARY OF DISCHARGES (CONT'D)

			CHANCE DISC	CHARGES (CFS)			
FLOODING SOURCE	DRAINAGE AREA	10-Percent	4-Percent-	2-Percent-	1-Percent-	0.2-Percent	
AND LOCATION	(sq. miles)	Annual Chance	Annual-Chance	Annual-Chance	Annual-Chance	Annual-Chance	
CEDAR CREEK (CONT'D)							
Approximately 1,870 feet	*	2,760	N/A	4,070	4,740	5,780	
downstream of Southwest 3 rd Street	·	2,700	IN/A	4,070	4,740	3,700	
Approximately 580 feet upstream of	*	1,710	N/A	2,520	2,900	2.540	
Southwest Pryor Drive	4	1,710	N/A	2,320	2,900	3,540	
Approximately 1,040 feet							
downstream of Union Pacific	*	1,480	N/A	2,140	2,470	2,990	
Railroad							
Approximately 990 feet upstream of	*	1.040	NT/A	1.500	1.720	2,000	
Union Pacific Railroad	*	1,040	N/A	1,500	1,720	2,090	
Approximately 580 feet							
downstream of Southwest Lakeview	*	536	N/A	766	869	1,050	
Boulevard							
CRACKERNECK CREEK							
At confluence with Little Blue	6.7	4.610	NT/A	7.500	0.100	15 270	
River	0.7	4,610	N/A	7,580	9,180	15,370	
DYKE BRANCH							
At confluence with Indian Creek	6.9	4,250	5,030	5,850	7,330	9,520	
At Holmes Road	6.9	4,240	5,010	5,810	7,320	9,510	
At Bannister Road	6.8	4,220	4,990	5,740	7,290	9,470	
Approximately 800 ft upstream of	67	4.210	4.000	5.700	7.270	0.450	
Bannister Road	6.7	4,210	4,980	5,720	7,270	9,450	
Approximately 2200 feet	6.5	4.160	4.020	7.660	7 100	0.240	
downstream of Wornall Road	6.5	4,160	4,920	5,660	7,190	9,340	
Approximately 775 feet	C 1	4 1 40	4.000	5 (50	7.200	0.250	
downstream of Wornall Road	6.4	4,140	4,900	5,650	7,200	9,350	
Approximately 580 feet	7.0	4.010	4.77.0	5 470	6.070	0.000	
downstream of Wornall Road	5.9	4,010	4,750	5,470	6,950	9,000	
*Data not available.							





APWA	STOR	M DR	AINAGE	"TC" (COMF	UTATIO	ONS F	OR: OL	DHAN	1 MAR	KETPLA	ACE															
						Surface	e types:	Asph/Conc	Bus/Com	Dirt	Grass/Park	Lake	MultFam	SnglFam	Undev	Other											·
		yello	ow areas are	self comp	uting	SURFACI	E CODES	Α	В	D	G	L	M	S	U	Z											
			overwrite if	necessary		"C" V	'alues	0.90	0.87	0.60	0.30	0.90	0.66	0.51	0.3				TC	COMPUTATI	ION						
								Overwri	te Lengt	h - DnElev	or Slope	SURFACE	P=Paved		Overwrite	Slope or Elev	vations									k	
			TOTAL WA	TERSHED					if ned	essary		CODE	U=Unpave	ed	if	necessary	_	Cal	Used	Cal	Cal					1.25	
							OVE	RLAND FLO	W - 100'	MAX		Р	CH	ANNEL FLOV	V - FIRST REA	ACH		Overland	Min 5	Channel	Channel	Total					
AREA	TOTAL	TOTAL	WTRSHD	UP	DN	SURFACE	"C"	OVRLND	UP	DN	SLOPE	or	CHANNEL	UP	DN	SLOPE	VELOCITY	Flow	Max 15	One	Two		Intensity	Intensity	CFS	CFS	AREA
ID	SQ.FT.	ACRES	LENGTH	ELEV	ELEV	CODE	VALUE	LENGTH	ELEV	ELEV	%	U	LENGTH	ELEV	ELEV	%	F/S	T(I)	T(I)	T(T)	T(T)	T© 10	10 I	100 I	10 Q	100 Q	ID
A1 EX	6422990	147.45	2875.0	1038.0	992.0	Z	0.68	100.0	1038.0	1036.0	2.0	U	2775.0	1036.0	992.0	1.59	2.0	6.0	6.0	22.8	0.0	28.8	3.9	5.6	386.86	705.96	A1 EX
A1 PROP	5594420	128.43	2875.0	1038.0	992.0	Z	0.68	100.0	1038.0	1036.0	2.0	U	2775.0	1036.0	992.0	1.59	2.0	6.0	6.0	22.8	0.0	28.8	3.9	5.6	336.95	614.89	A1 PROP
Α	828570	19.02	1772.0	1054.0	992.0	Z	0.51	100.0	1054.0	1052.0	2.0	Р	1672.0	1052.0	992.0	3.59	3.9	8.4	8.4	7.2	0.0	15.7	5.1	7.2	49.00	87.89	Α
В	3811703	87.50	3243.0	1056.0	962.0	Z	0.51	100.0	1056.0	1052.0	4.0	Р	3143.0	1052.0	962.0	2.86	3.4	6.7	6.7	15.2	0.0	21.9	4.4	6.4	196.43	355.65	В
A1 + B	10234693	234.96	5085.0	1038.0	962.0	Z	0.60	100.0	1038.0	1036.0	2.0	Ū	4985.0	1036.0	962.0	1.48	2.0	7.1	7.1	42.3	0.0	49.4	2.8	4.2	396.39	734.54	A1 + B
											REACH	Ū	2210.0	992.0	962.0	1.36	1.9	19.6									

Composite Curve Numbers Oldham Marketplace Subbasin

Ex Land Usage POI A	Area (ac.)	CN	Area x CN
Right-of-Way	29.32	82	2404.24
Residential Multi-Family	18.47	88	1625.75
Residential Single-Family	19.30	82	1582.60
Undeveloped	9.87	74	730.38
Commercial	70.48	94	6625.12
Total Area	147.44		12968.09
Composite CN	88		
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Prop Land Usage POI A1	Area (ac.)	CN	Area x CN
Right-of-Way	29.32	82	2404.24
Residential Multi-Family	18.47	88	1625.75
Residential Single-Family	0.28	82	22.96
Undeveloped	9.87	74	730.38
Commercial	70.48	94	6625.12
Total Area	128.42		11408.45
Composite CN	89		
	•		
Prop Land Usage Subarea A	Area (ac.)	CN	Area x CN
Right-of-Way	0.00	82	0.00
Residential Single-Family	19.02	82	1559.75
Undeveloped	0.00	74	0.00
Commercial	0.00	94	0.00
Total Area	19.02		1559.75
Composite CN	82		
	_		
Ex Land Usage Subarea B	Area (ac.)	CN	Area x CN
Park	14.92	75	1118.65
Residential Single-Family	61.95	82	5080.24
Undeveloped	0.00	74	0.00
School	10.64	92	978.44
Total Area	87.50		7177.33
Composite CN	82		
Land Usage Subarea A + A1 + B	Area (ac.)	CN	Area x CN
Right-of-Way	29.32	82	2404.24
Park	14.92	75	1118.65
Residential Single-Family	81.25	82	6662.50
Residential Multi-Family	18.47	88	1625.36
Undeveloped	9.87	74	730.38
Commercial	70.48	94	6625.12
School	10.64	92	978.44
Total Area	234.94		20144.69
Composite CN	86		
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