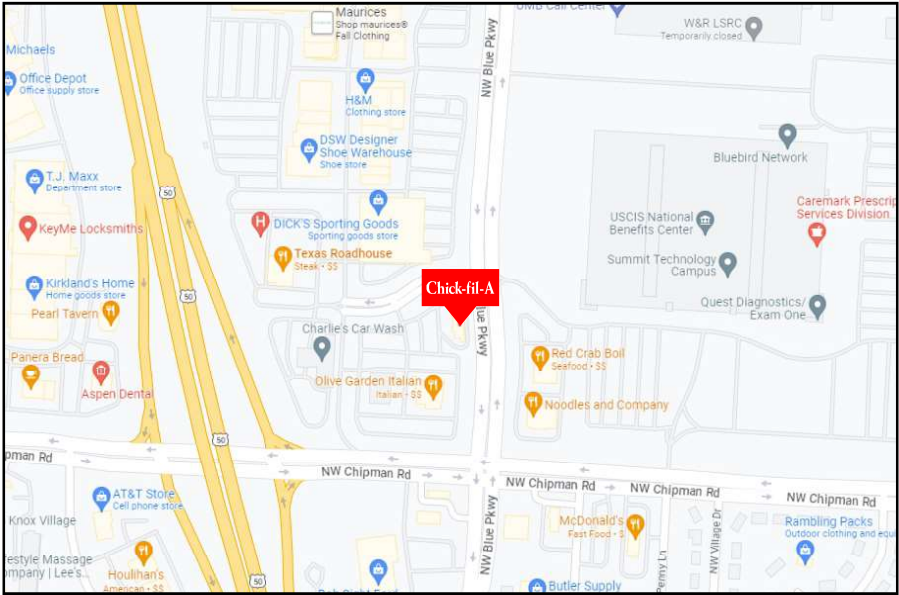




VICINITY MAP

N.T.S.



AERIAL VIEW



KRISTEN HAMILTON - 678-725-8852

KHamilton@chandler signs.com

TERRI BROWN - 682-204-6687

TBrown@chandler signs.com

Design #

0637033Ar3

Sheet 1 of 27

Client

#2859

Address

690 NW Blue Pkwy,
Lees Summit, MO

Account Rep. KRISTEN HAMILTON
TERRI BROWN

Designer LEAH LANSFORD

Date 9/29/23

Approval / Date

Client	
Sales	
Estimating	
Art	
Engineering	
Landlord	

Revision/Date

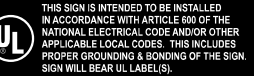
R1(12-22-23)LL: CHANGED SIZE OF PANELS ON THE STOP/DNE
R2(1/16/24)LL: ADDED STAMPED ENGINEERING
CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4
R3(02/28/2024)AM: UPDATED SP ADDED NOTE FOR SIGN A FOR CSI TO PROVIDE NEW STEEL AND FOUNDATION AND ADDED NOT FOR SIGN D FOR CSI TO REMOVE AND DISCARD EXISTING DIF DIRECTIONAL



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(678) 725-8852 Fax (210) 349-8724
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FINAL ELECTRICAL
CONNECTION BY
CUSTOMER



AERIAL VIEW

DocuSigned by:

Michael Young

0DCEC3135B2844E...

SITE PLAN 1 SCALE: 1/32" = 1'-0"

SIGN I-D LETTER	FACE A	FACE B
A		
B1 B2		N/A
C		
D		
E1 E2	 WITH BOLLARD	N/A
F	 WITH BOLLARD	N/A
G1 G2		N/A
H1-4		
I		N/A

SIGN I-D LETTER	FACE A	FACE B
		N/A
		N/A
		N/A

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0637033Ar3	
Sheet	2 of 27
Client	
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**FINAL ELECTRICAL
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SITE PLAN/KEY



A **D/F MONUMENT** SCALE: 1/2" = 1'-0"

ONE (1) REMOVAL REQUIRED - MANUFACTURE AND INSTALL 60 SQ. FT.



SPECS:

FABRICATED ALUM. FRAME WITH ALUMINUM CLADDING AND ALUM. FIN / FILLER PAINTED MATTHEWS #74155 DARK BRONZE, SEMI-GLOSS FINISH.

MAIN ID LOGO FACES

CABINET AND RETAINERS PAINTED MATTHEWS #74155 DARK BRONZE, SEMI-GLOSS. WHITE PLEX FACES WITH 3M #3630-53 CARDINAL RED TRANSLUCENT VINYL APPLIED 1ST SURFACE. INTERNALLY ILLUMINATED WITH 7100K WHITE LEDS AS REQUIRED.

READER BOARD DISPLAY

.080" ALUM. FACE PAN PANEL WITH ROUTED OUT OPENING FOR READER BOARD AND R.O.S.T. COPY READING "CLOSED SUNDAY", WITH HINGED LOCKABLE F-TRACK VANDAL COVER PAINTED MATTHEWS #74155 DARK BRONZE, SEMI-GLOSS. CLEAR LEXAN FACE, SECURED TO FACE OF ALUM. PANEL. BACKED WITH 3/16" WHITE PLEX. TRACK TO ACCOMMODATE THREE (3) LINES OF CHANGEABLE 6" COPY BLACK COMMERCIAL SET OF 334 LETTERS. INCLUDE CHANGER ARM.

INTERNALLY ILLUMINATED SAME AS ABOVE.

FOUNDATION SYSTEM

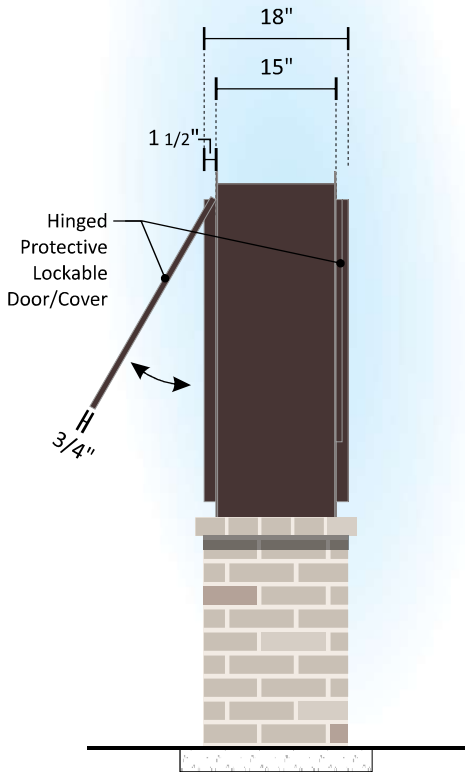
ONE (1) 4 1/2" O.D. x .237" WALL STEEL SUPPORT
ONE (1) 24" x 5'-0" DEEP CONCRETE PIER.

FOOTING AND 1" x 1" x .125" ALUM. FABRICATED BASE FRAME WITH 1/2" CEMENT BOARD.

MASONRY / BRICK: **BY G.C.**

SHALL MATCH THE BUILDING MATERIAL AND MORTAR FINISH.

PRIMARY ELECTRIC RUN THRU NEC APPROVED WEATHER-PROOF CONDUIT - COORDINATE PRIOR TO CONCRETE FOUNDATION / PAD POUR.



EXISTING CONDITIONS

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3 of 27

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CHANDLER SIGNS

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Chick-fil-A

A

11545 W. BERNARDO COURT
SUITE 201, SAN DIEGO, CA 92127
PROJECTMANAGER@SULLAWAYENG.COM
PHONE: 1-858-312-5150 FAX: 1-858-777-3534

PROJECT: CHICK-FIL-A - MONUMENT SIGN - 690 NW BLUE PKWY, LEES SUMMIT, MO

DATE: 1-9-2024

PROJECT #: 43787A

ENGINEER: JD

CLIENT: CHANDLER SIGNS

LAST REVISED:

GENERAL NOTES

1. DESIGN CODE: IBC 2018

2. DESIGN LOADS: ASCE 7-16

3. WIND VELOCITY: 110 MPH EXPOSURE C

4. CONCRETE 2500 PSI MIN.

5. PIPE STEEL ASTM A53, Fy= 35 KSI MIN.

6. PROVIDE PROTECTION AGAINST DISSIMILAR METALS USING ANTI-CORROSIVE PAINT OR NEOPRENE GASKETS.

7. LATERAL SOIL BEARING PER IBC CLASS 4 (150 PSF/FT)

8. ALL DIMENSIONS TO BE VERIFIED PRIOR TO FABRICATION.

11545 W. Bernardo Court, San Diego, CA 92127
projectmanager@sullawayeng.com
Phone: 858-312-5150 Fax: 858-777-3534

PROJECT: CHICK-FIL-A 2859

DATE: 1/9/24

PROJ. NO.: 43787A

ENGINEER: JD

CLIENT: CHANDLER SIGNS

units; pounds, feet unless noted otherwise

Applied Wind Loads; from ASCE 7-16

$F=q_z \cdot G \cdot C_f \cdot A_f$ with $q_z = 0.00256 K_z K_{zt} K_d V^2$ (29.3.2 & 29.4)

$C_f = 1.417$ (Fig. 29.3-1) max. height= 6.00

$K_{zt} = 1.0$ (26.8.2) (=1.0 unless unusual landscape) $s = 6.00$

$K_z =$ from table 28.3-1 Exposure= c

$K_d = 0.85$ for signs (table 26.6-1)

$V = 110$ mph

$G = 0.85$ (26.9)

$s/h = 1.000$

$B/s = 1.67$

weight= 0.600 kips

$M_{DL} = 0.00$ k-ft

Pole Loads	structure component	height at section c.g.	K_z	q_z	pressure $q_z \cdot G \cdot C_f$	A_f	shear	Wind Moment M_w
1		1.1	0.850	22.4	26.95	22.1	597	660
2		2.3046875	0.850	22.4	26.95	1.9	50	116
3		4.19791667	0.850	22.4	26.95	36.0	971	4077
sums:							60.0	1618
for s/h=1, add 10% (asce fig. 29.4-1):							x 1.10	5.34
$P_u = 0.72$ kip								$M = 5.34$ k-ft
$M_u = \text{sqrt}(1.2 M_{DL}^2 + 1.0 M_w^2) = 5.34$ k-ft								$M = \text{sqrt}(M_{DL}^2 + M_w^2)$

Pole Design section; pipe

$M_u \leq \phi M_n$ with $M_n = f_y Z$ $f_y = 35$ ksi $\phi = 0.9$

H	M_u (k-ft)	Z req'd. (in)	Size(in)	t (in)	Z	USE
at grade	5.3	2.03	3	0.216	2.2	4 STD. PIPE, Mn= 10.6 k-ft

Footing Design footprint: round

$\omega = 1.3$ IBC 1806.3.2 IBC Table 1806.2, sections 1806.3.4, 1807.3.2 $S = (1.3 \times 2 \times)$

$P = 1.26$ kip $S1 = S \times d / 3$ $A = 2.34 \times P / (S1 \times b)$ $S = 400$

$S1 = 586$ $d = 0.5 \times A (1 + (1 + 4.36 \times h/A)^{.5})$ IBC 1807.3.2.1

$A = 2.52$

footing: 2' - 0" dia. 4' - 5" deep
USE 5' DEEP

Design #

0637033Ar3

Sheet 4 of 27

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TERRI BROWN

Designer

LEAH LANSFORD

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A



11545 W. Bernardo Court, San Diego, CA 92127

projectmanager@sullawayeng.com

Phone: 858-312-5150 Fax: 858-777-3534

PROJECT: CHICK-FIL-A 2859

DATE: 1/9/24

PROJ. NO.: 43787A

ENGINEER: JD

CLIENT: CHANDLER SIGNS

v6.5

units; pounds, feet unless noted otherwise

Check Buckling for Round HSS Section

Pole Design-AISC

section; pipe<=12"

weight= 0.6 kips

F_y= 35 ksi

= 0.9

E= 29,000 ksi

H

M_u(k-ft)

Size(in)

t (in)

Z

S

at grade

5.34

2.03

4.5

0.220

4

3

r= 1.52

A= 2.96

h (L) = 6

spec wt= 0.289 kcf

signage wt; 0.600 k

pipe weight 0.065 k

P= 0.665 k

P_r= 0.80 k

D/t= 20.4

KL/r= 95.0

K= 2

F_e= 32.8 ksi (E3-4)

4.71sqrt(E/f_y)= 137.9

for D/t < 0.07 E/F_y section is compact

for D/t < 0.31 E/F_y section is non-compact

F_{cr}= 22.39

F_{cr}= 28.74

use F_{cr}= 22.39

0.07 E/F_y= 58

0.31 E/F_y= 257

Section is compact

P_n=F_{cr}A_g= 66.3 k

M_n=(0.021E/(D/t) + F_y)S= 16.6 k (non-compact)

M_n=F_yZ= 11.8 k-ft (compact)

M_n=F_{cr}S= 5.6 k-ft (slender - slender sections NOT USED)

use M_n= 11.8 k-ft

M_c=φM_n= 10.6 k-ft

P_c=φP_n= 59.7 k

(F8-2)

P_r/P_c= 0.0134

P_r/2P_c= 0.0067

P_r/P_c + 8/9 * M_r/M_c = 0.461

For P_r/P_c<0.2; P_r/2P_c + M_r/M_c = 0.510

use 0.51

AISC Chap. E3

AISC Chap. H1

Round Pipe Torsion Capacity

Pipe

D= 4.5 in

t= 0.22041 in

L= 40 ft

J= 14

C= 6 in3

E= 29 x10e6 psi

C=2J/d

J=pie/32(d^4-(d-2t)^4)

T_n=F_{cr}C

φ= 0.9

AISC H3

F_{cr}=1.23E / (sqrt(L/D)(D/t)^1.25)

F_{cr}= 79.6 ksi max;

F_{cr}= 188.6 ksi

F_{cr}=0.6E / ((D/t)^1.5)

F_{cr}= 188.6 ksi

F_{cr} < 0.6F_y

0.6F_y = 21 ksi

F_{cr}= 21.0 ksi

T_u= 3.2 k-ft

φT_n= 114 k-in

10 k-ft

(T_u/φT_n)²= 0.115

P_u/φP_n +M_u/φM_n +(T_u/φT_n)²= 0.63

ok

Design #

0637033Ar3

Sheet 5 of 27

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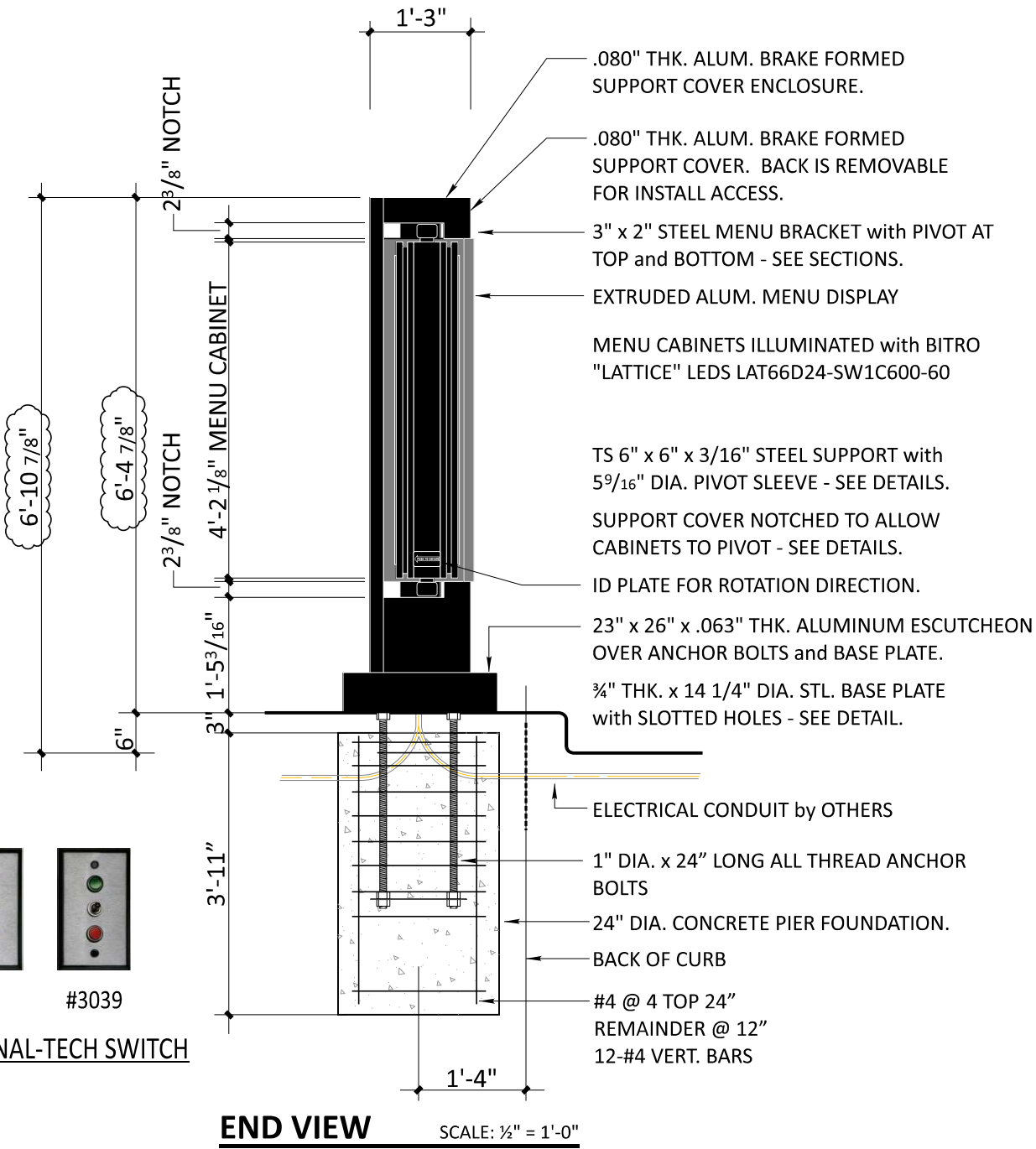
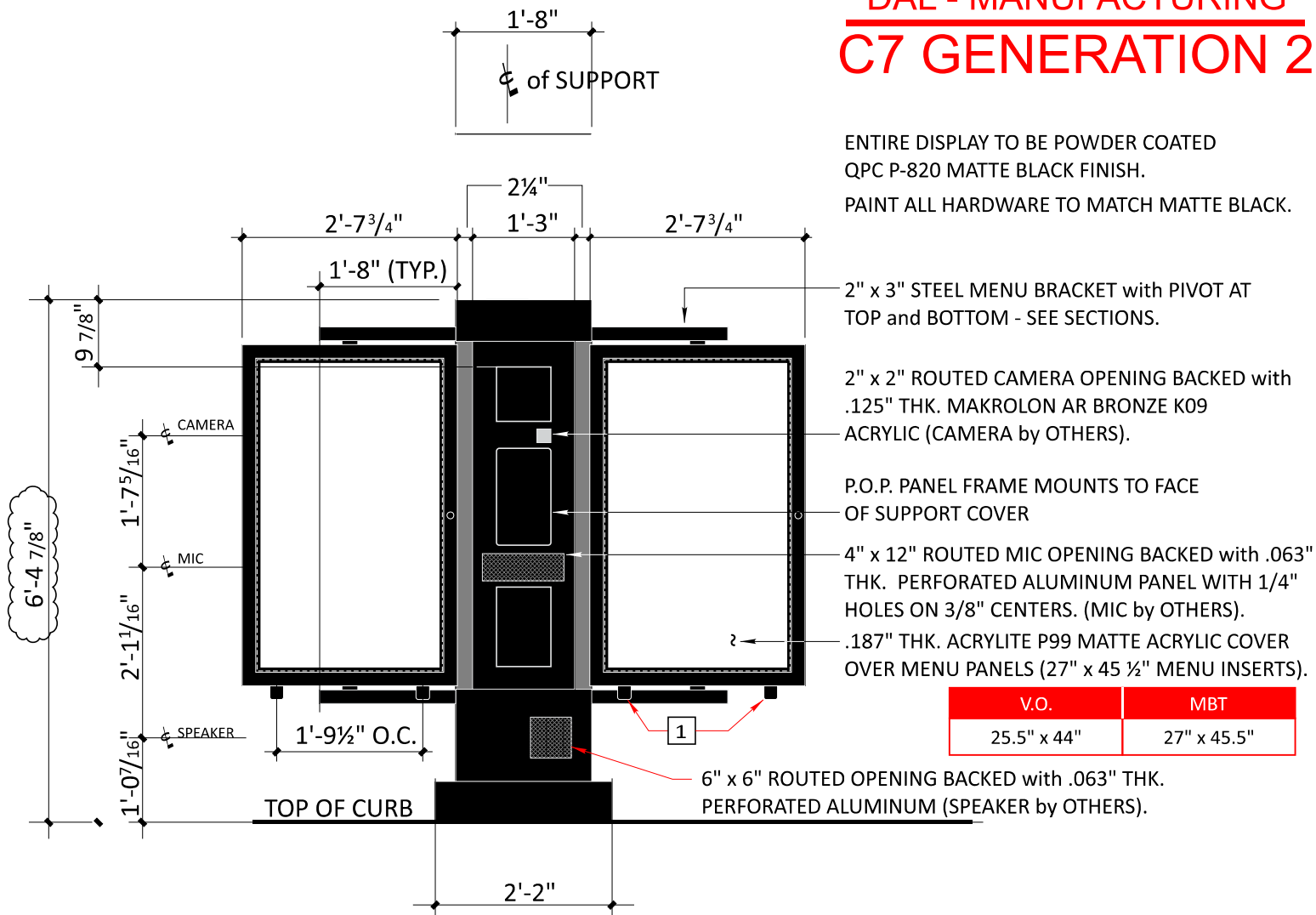


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A

DAL - MANUFACTURING
C7 GENERATION 2



B1 B2

CFA - C7 GEN 2 ORDERING STATION W/O CANOPY

SCALE: 1/2" = 1'-0"

TWO (2) REMOVALS REQUIRED - MANUFACTURE & INSTALL

G.C. TO REMOVE AND DISCARD EXISTING C7'S.

MANUFACTURE AND INSTALL TWO NEW C7'S IN NEW LOCATION.

G.C. TO CONFIRM ELECTRICAL.



INTERIOR SIGNAL-TECH SWITCH



EXISTING CONDITIONS

2014/2017 NEC
COMPLIANT LABEL

DANGER!

INTERNAL ENERGIZED PARTS
TURN OFF POWER AT
BREAKER PANEL

POWER SOURCE FOUND

FLOOR _____

BREAKER PANEL _____

BREAKER # _____

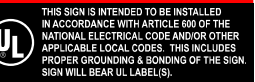
WARNING LABEL/
BREAKER LOCATION

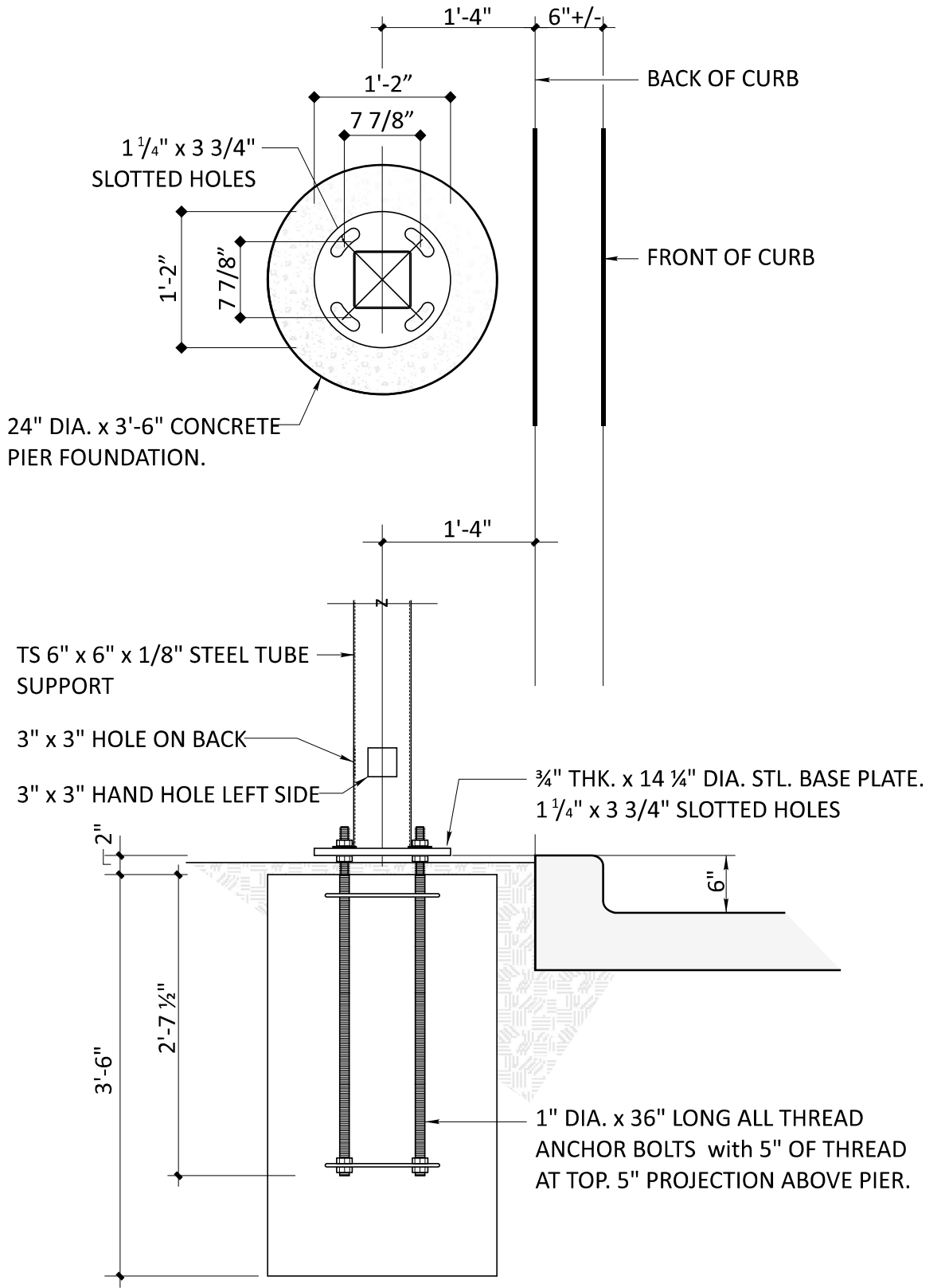
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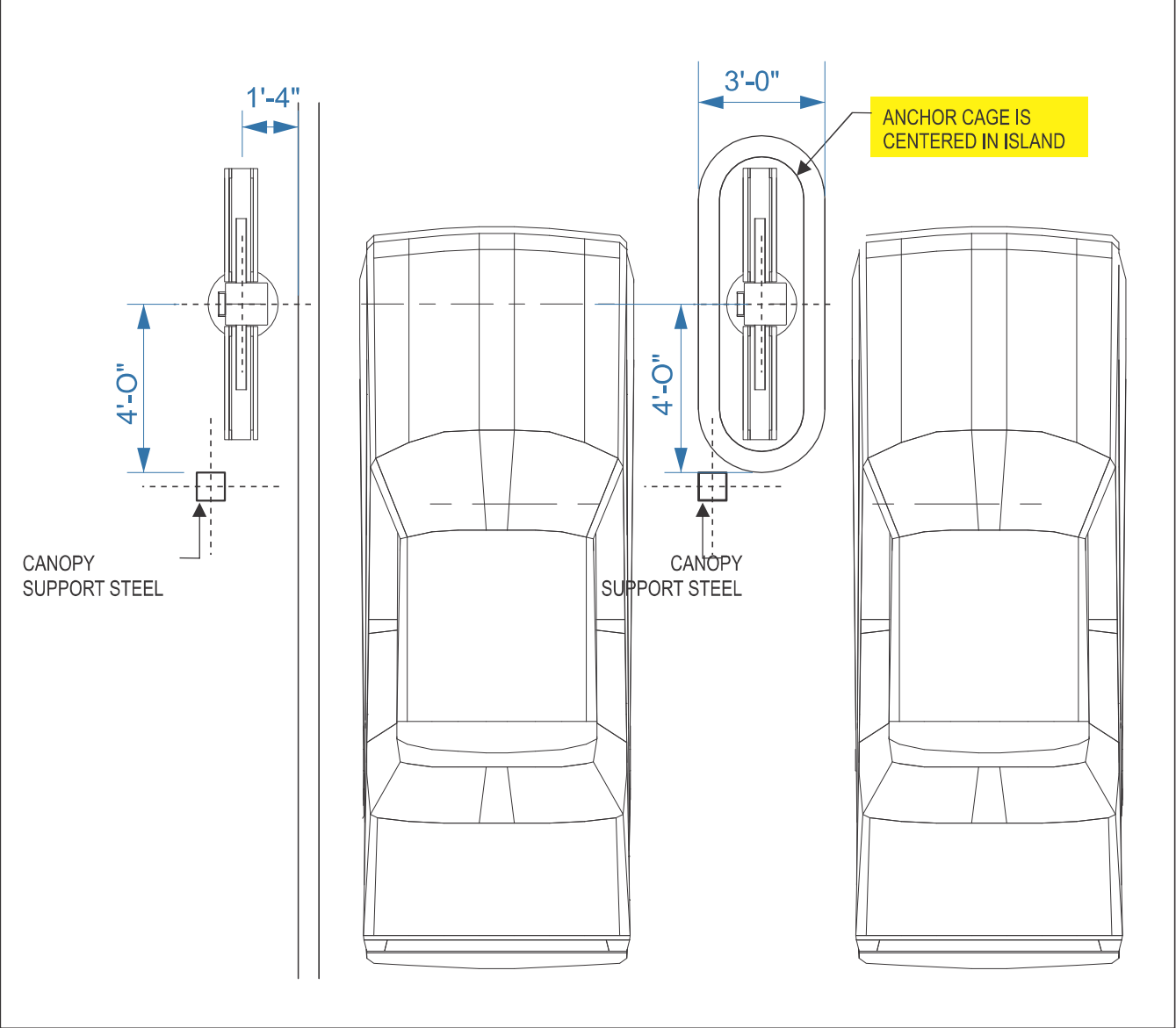
FINAL ELECTRICAL
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CUSTOMER





BASE PLATE AND ANCHOR DETAIL

3/4" = 1'-0"



CHANDLER SIGNS TO PROVIDE ORDERING STATIONS.
CHANDLER SIGNS TO PROVIDE TEMPLATES AND ANCHOR BOLTS.
GEN. CONTRACTOR TO SET ANCHOR BOLTS AND POUR CONCRETE.
CHANDLER SIGNS TO INSTALL ORDERING STATIONS.

- General Notes:**
- MINIMUM CONCRETE RESISTANCE OF 3600 PSI AFTER 28 DAYS
 - THE GROUND MUST NOT BE ALTERED AND MUST BE WELL DRAINED
 - FOUNDATION IS BASE ON SAFE LATERAL SOIL BEARING PRESSURE MINIMUM OF 150 PSF PER FOOT OF DEPTH. SOIL REPORT WAS NOT FURNISHED. ALLOWABLE BEARING PRESSURE SHOULD BE VERIFIED PRIOR TO PLACEMENT OF CONCRETE. DO NOT PLACE FOUNDATION FILL.
 - ALL BACKFILLED TO BE PLACE IN COMPACTED LAYERS COMPACTED TO 95% MODIFIED PROCTOR DENSITY
 - ELECTRICAL CONDUIT TO BE AS PER CITY CODE
 - ALL VOIDS BETWEEN COLUMN BASE PLATE AND FOUNDATION SURFACE SHALL BE COMPLETELY FILLED WITH HIGH STRENGTH, NON-SHRINK GROUT

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**FINAL ELECTRICAL
CONNECTION BY
CUSTOMER**





10815 Rancho Bernardo RD., SD, CA 92127
 projectmanager@sullawayeng.com
 Phone: 858-312-5150 Fax: 858-777-3534

PROJECT: CHICK-FIL-A
 PROJ. NO.: 43787B
 CLIENT: CHANDLER SIGNS

DATE: 1/9/24
 ENGINEER: SB/TH(IH)

V5.5
units: pounds, feet unless noted otherwise

Applied Wind Loads; from ASCE 7-16

$F = q_z \cdot G \cdot C_f \cdot A_f$ with $q_z = 0.00256 K_z K_{zt} K_d V^2$ (29.3.2 & 29.4)
 $C_f =$ (Fig. 29.3-1) 1.00 max. height= 6.7
 $K_{zt} =$ 1.0 (26.8.2) (=1.0 unless unusual landscape)
 $K_z =$ from table 28.3-1 Exposure= c
 $K_d =$ 0.85 for signs (table 26.6-1)
 $V =$ 110 mph
 $G =$ 0.85 (26.9)
 $s/h =$
 $B/s =$

$weight =$ 0.341 kips
 $M_{DL} =$ 0.00 k-ft

Pole Loads	structure component	height at section c.g.	K_z	q_z	pressure $q_z \cdot G \cdot C_f$	A_f	shear	Wind Moment M_w
	1	0.13	0.850	22.4	31.45	0.0	0	0
	2	0.50	0.850	22.4	31.45	1.1	34	17
	3	1.22	0.850	22.4	31.45	1.6	49	59
	4	1.77	0.850	22.4	31.45	0.8	26	46
	5	1.89	0.850	22.4	31.45	0.2	6	12
	6	4.01	0.850	22.4	31.45	28.9	909	3644
	7	6.14	0.850	22.4	31.45	0.2	5	30
	8	6.26	0.850	22.38	31.45	0.8	26	164
	9	6.50	0.850	22.38	31.45	0.5	17	108
sums:							34.1	1072
								4.08 (M_w) k-ft arm= 3.8
								M= 4.08 k-ft $M = \sqrt{M_{DL}^2 + M_w^2}$

$P_u =$ 0.41 kip
 $M_u = \sqrt{(1.2M_{DL})^2 + (1.0M_w)^2} =$ 4.08 k-ft

Pole Design

$M_u \leq \phi M_n$ with $M_n = f_y Z$
 $f_y =$ 46 ksi
 $\% \sqrt{f_c} =$ 0.9

H	M_u (k-ft)	Z req'd. (in)	Size (in)	t (in)	Z	USE
at 3' below grade	4.08	1.18	2.5	0.188	1.3	6x6x1/8" SQ.HSS, $\phi M_n = 15.6$ k-ft

Footing Design

$\phi =$ 1.3 IBC 1605.3.2
 $P =$ 0.84 kip
 $S_1 =$ 519
 $A =$ 1.88

footprint: round
 IBC Table 1806.2, sections 1806.3.4, 1807.3.2
 $S_1 = S \times d / 3$
 $d = 0.5 \times A \cdot (1 + (1 + 4.36 \times h/A)^{0.5})$
 $S = (1.3 \times 2 \times 150 \text{ psf/ft})$
 $A = 2.34 \times P / (S_1 \times b)$
 IBC 1807.3.2.1

footing: 2' - 0" dia.

3' - 11" deep

Design #	
0637033Ar3	
Sheet	8 of 27
Client	
#2859	
Address	
690 NW Blue Pkwy, Lees Summit, MO	
Account Rep.	KRISTEN HAMILTON TERRI BROWN
Designer	LEAH LANSFORD
Date	9/29/23
Approval / Date	
Client	
Sales	
Estimating	
Art	
Engineering	
Landlord	
Revision/Date	
R1(12/22/23)LL: CHANGED SIZE OF PANELS ON THE STOPLINE	
R2(1/16/24)LL: ADDED STAMPED ENGINEERING	
CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4	
R3(02/26/2024)AM: UPDATED SP, ADDED NOTE FOR SIGN A FOR CSI TO PROVIDE NEW STEEL AND FOUNDATION AND DISCARD NOT FOR SIGN D FOR CSI TO REMOVE AND DISCARD EXISTING D/F DIRECTIONAL	
	
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B1-2	

Anchor Designer™
Software
Version 3.2.2309.2

Company:		Date:	1/9/2024
Engineer:		Page:	1/6
Project:			
Address:			
Phone:			
E-mail:			

1. Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General

Design method: ACI 318-19
Units: Imperial units

Anchor information:

Anchor type: Cast-in-place
Material: AB
Diameter (inch): 1.000
Effective Embedment depth, h_{ef} (inch): 24.000
Anchor category: -
Anchor ductility: Yes
 $f_{t,AB}$ (inch): 26.83
 C_{coar} (inch): 6.00
 S_{min} (inch): 6.00

Base Material

Concrete: Normal-weight
Concrete thickness, h (inch): 47.00
State: Cracked
Compressive strength, f_c (psi): 2500
 λ : 1.0
Reinforcement condition: Supplementary reinforcement not present
Supplemental edge reinforcement: Not applicable
Reinforcement provided at corners: No
Ignore concrete breakout in tension: No
Ignore concrete breakout in shear: No
Ignore ϕ requirement: No
Build-up grout pad: No

Base Plate

Diameter x Thickness (inch): 14.00 x 0.75
Yield stress: 36000 psi

Profile type/size: H556X6X1/8

Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB8 (1"Ø)



Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility

Simpson Strong-Tie Company Inc. 3856 W. Las Positas Boulevard Pleasanton, CA 94588 Phone: 925.560.8000 Fax: 925.847.3871 www.strongtie.com

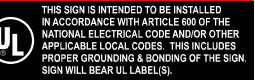


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B1-2



Company:		Date:	1/9/2024
Engineer:		Page:	2/6
Project:			
Address:			
Phone:			
E-mail:			

Load and Geometry

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: No

Strength level loads:

N_{ux} [lb]: 0

V_{ux} [lb]: 0

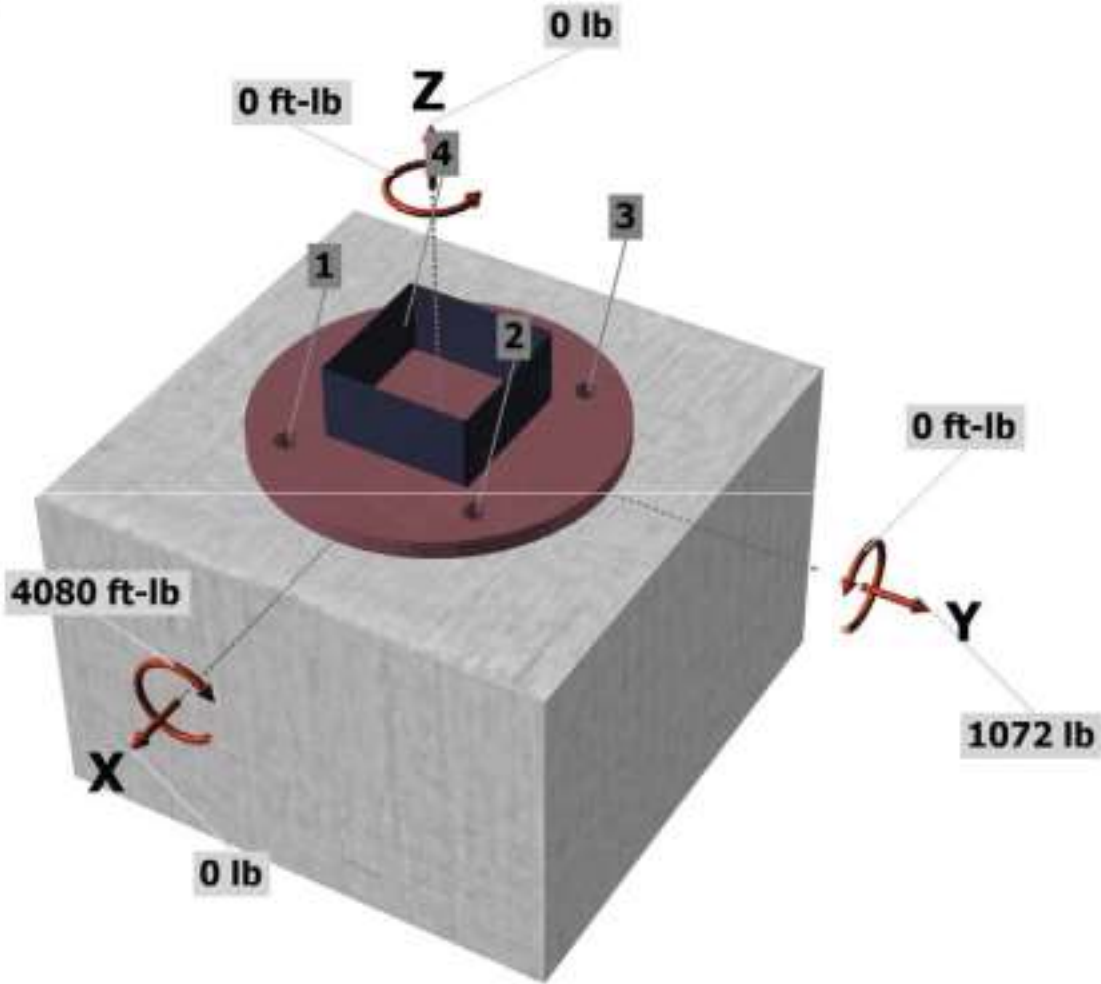
V_{uy} [lb]: 1072

M_{ux} [ft-lb]: -4080

M_{uy} [ft-lb]: 0

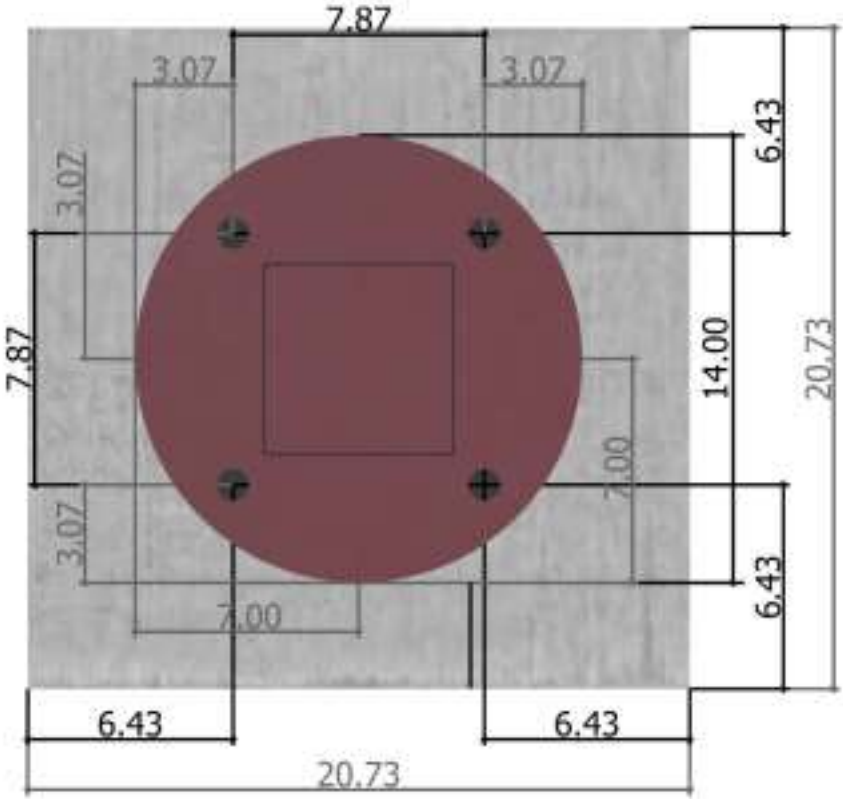
M_{ux} [ft-lb]: 0

<Figure 1>



Company:		Date:	1/9/2024
Engineer:		Page:	3/6
Project:			
Address:			
Phone:			
E-mail:			

<Figure 2>



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Design #

0637033Ar3

Sheet 10 of 27

Client

#2859

Address

690 NW Blue Pkwy,
Lees Summit, MO

Account KRISTEN HAMILTON
Rep. TERRI BROWN

Designer LEAH LANSFORD

Date 9/29/23

Approval / Date

Client	
Sales	
Estimating	
Art	
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Landlord	

Revision/Date

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B1-2

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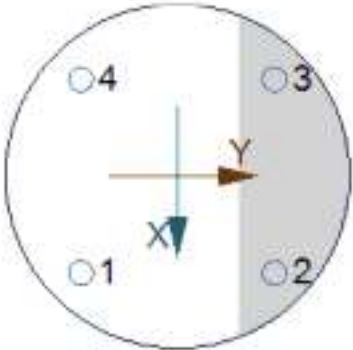
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Company:		Date:	1/9/2024
Engineer:		Page:	4/6
Project:			
Address:			
Phone:			
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3. Resulting Anchor Forces				
Anchor	Tension load, N _{ax} (lb)	Shear load x, V _{ax} (lb)	Shear load y, V _{ay} (lb)	Shear load combined, √(V _{ax}) ² +(V _{ay}) ² (lb)
1	2704.5	0.0	268.0	268.0
2	0.0	0.0	268.0	268.0
3	0.0	0.0	268.0	268.0
4	2704.5	0.0	268.0	268.0
Sum	5409.0	0.0	1072.0	1072.0

Maximum concrete compression strain (‰): 0.07
Maximum concrete compression stress (psi): 307
Resultant tension force (lb): 5409
Resultant compression force (lb): 5409
Eccentricity of resultant tension forces in x-axis, e'_{tx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{ty} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.6.1)		
N _{ax} (lb)	φ	φN _{ax} (lb)
35150	0.75	26363

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.6.2)

$N_b = 16\lambda\sqrt{f_c}h_{ef}^{3/2}$ (Eq. 17.6.2.2.1)

λ	f_c (psi)	h_{ef} (in)	N_b (lb)
1.00	2500	9.533	34290

$\phi N_{brg} = \phi (A_{brg} / A_{brk}) \zeta_{ec,N} \zeta_{en,N} \zeta_{cs,N} \zeta_{cm,N} N_b$ (Sec. 17.5.1.2 & Eq. 17.6.2.1a)

A_{brg} (in ²)	A_{brk} (in ²)	$c_{ax,min}$ (in)	$\zeta_{ec,N}$	$\zeta_{en,N}$	$\zeta_{cs,N}$	$\zeta_{cm,N}$	N_b (lb)	ϕ	ϕN_{brg} (lb)
429.73	817.96	6.43	1.000	0.835	1.00	1.000	34290	0.70	10528

6. Pullout Strength of Anchor in Tension (Sec. 17.6.3)				
φN _{pn} = φγ _{cr,N} N _b = φγ _{cr,N} 6A _{brg} f _c (Sec. 17.5.1.2, Eq. 17.6.3.1 & 17.6.3.2.2a)				
γ _{cr,N}	A _{brg} (in ²)	f _c (psi)	φ	φN _{pn} (lb)
1.0	5.15	2500	0.70	72156

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Company:		Date:	1/9/2024
Engineer:		Page:	5/6
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Address:			
Phone:			
E-mail:			

7. Side-Face Blowout Strength of Anchor in Tension (Sec. 17.6.4)							
φN _{sf} = φ[(1+c _{ax} /c _{ax1})/4](1+s/5c _{ax1})N _b = φ[(1+c _{ax} /c _{ax1})/4](1+s/5c _{ax1})(160c _{ax} √A _{brg})λ√f _c (Sec. 17.5.1.2, Eq. 17.6.4.1 & 17.6.4.2)							
s (in)	c _{ax} (in)	c _{ax1} (in)	A _{brg} (in ²)	λ	f _c (psi)	φ	φN _{sf} (lb)
7.87	6.43	6.43	5.15	1.00	2500	0.70	49211

8. Steel Strength of Anchor in Shear (Sec. 17.7.1)			
V _{ax} (lb)	φ _{grout}	φ	φ _{grout} φV _{ax} (lb)
21090	1.0	0.65	13709

9. Concrete Breakout Strength of Anchor in Shear (Sec. 17.7.2)								
Shear perpendicular to edge in y-direction:								
$V_{by} = \min[7(l_e/d_s)^{3/2}\sqrt{d_s}\lambda\sqrt{f_c}c_{ax}^{1/3}; 9\lambda\sqrt{f_c}c_{ax}^{1/2}]$ (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)								
l_e (in)	d_s (in)	λ	f_c (psi)	c_{ax} (in)	V_{by} (lb)			
8.00	1.000	1.00	2500	14.30	24334			
$\phi V_{edge} = \phi (A_{brg}/A_{brk})\zeta_{ec,V}\zeta_{en,V}\zeta_{cs,V}\zeta_{cm,V}V_{by}$ (Sec. 17.5.1.2 & Eq. 17.7.2.1b)								
A_{brg} (in ²)	A_{brk} (in ²)	$\zeta_{ec,V}$	$\zeta_{en,V}$	$\zeta_{cs,V}$	$\zeta_{cm,V}$	V_{by} (lb)	ϕ	ϕV_{edge} (lb)
444.66	920.21	1.000	0.790	1.000	1.000	24334	0.70	6502

Shear parallel to edge in x-direction: $V_{by} = \min[7(l_e/d_s)^{3/2}\sqrt{d_s}\lambda\sqrt{f_c}c_{ax}^{1/3}; 9\lambda\sqrt{f_c}c_{ax}^{1/2}]$ (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)								
l_e (in)	d_s (in)	λ	f_c (psi)	c_{ax} (in)	V_{by} (lb)			
8.00	1.000	1.00	2500	6.43	7337			
$\phi V_{edge} = \phi(2)(A_{brg}/A_{brk})\zeta_{ec,V}\zeta_{en,V}\zeta_{cs,V}\zeta_{cm,V}V_{by}$ (Sec. 17.5.1.2, 17.7.2.1(c) & Eq. 17.7.2.1b)								
A_{brg} (in ²)	A_{brk} (in ²)	$\zeta_{ec,V}$	$\zeta_{en,V}$	$\zeta_{cs,V}$	$\zeta_{cm,V}$	V_{by} (lb)	ϕ	ϕV_{edge} (lb)
199.94	186.05	1.000	1.000	1.000	1.000	7337	0.70	11039

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.7.3)									
φV _{prg} = φk _{tr} N _{brg} = φk _{tr} (A _{brg} /A _{brk})ζ _{ec,N} ζ _{en,N} ζ _{cs,N} ζ _{cm,N} N _b (Sec. 17.5.1.2 & Eq. 17.7.3.1b)									
k _{tr}	A _{brg} (in ²)	A _{brk} (in ²)	ζ _{ec,N}	ζ _{en,N}	ζ _{cs,N}	ζ _{cm,N}	N _b (lb)	φ	φV _{prg} (lb)
2.0	429.73	165.38	1.000	1.000	1.000	1.000	9049	0.70	32921

11. Results				
Interaction of Tensile and Shear Forces (Sec. 17.8)				
Tension	Factored Load, N _{ax} (lb)	Design Strength, φN _t (lb)	Ratio	Status
Steel	2704	26363	0.10	Pass
Concrete breakout	5409	10528	0.51	Pass (Governs)
Pullout	2704	72156	0.04	Pass
Side-face blowout	5409	49211	0.11	Pass
Shear				
Shear	Factored Load, V _{ax} (lb)	Design Strength, φV _t (lb)	Ratio	Status
Steel	268	13709	0.02	Pass
T Concrete breakout y+	1072	6502	0.16	Pass (Governs)
Concrete breakout x-	536	11039	0.05	Pass (Governs)

Design #
0637033Ar3

Sheet 11 of 27

Client
#2859

Address
690 NW Blue Pkwy,
Lees Summit, MO

Account Rep.
KRISTEN HAMILTON
TERRI BROWN

Designer
LEAH LANSFORD

Date
9/29/23

Approval / Date

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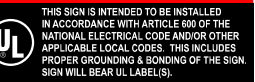
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B1-2

Anchor Designer™
Software
Version 3.2.2309.2

Company:

Engineer:

Project:

Address:

Phone:

E-mail:

Date:

Page:

Pryout

1072

32921

0.03

Pass

Interaction check

$N_{u,s}/\phi N_n$

$V_{u,s}/\phi V_n$

Combined Ratio

Permissible

Status

Sec. 17.8.1

0.51

0.00

51.4%

1.0

Pass

PAB8 (1"Ø) with hef = 24.000 inch meets the selected design criteria.

12. Warnings

- Designer must exercise own judgement to determine if this design is suitable.

Design #

0637033Ar3

Sheet

12 of 27

Client

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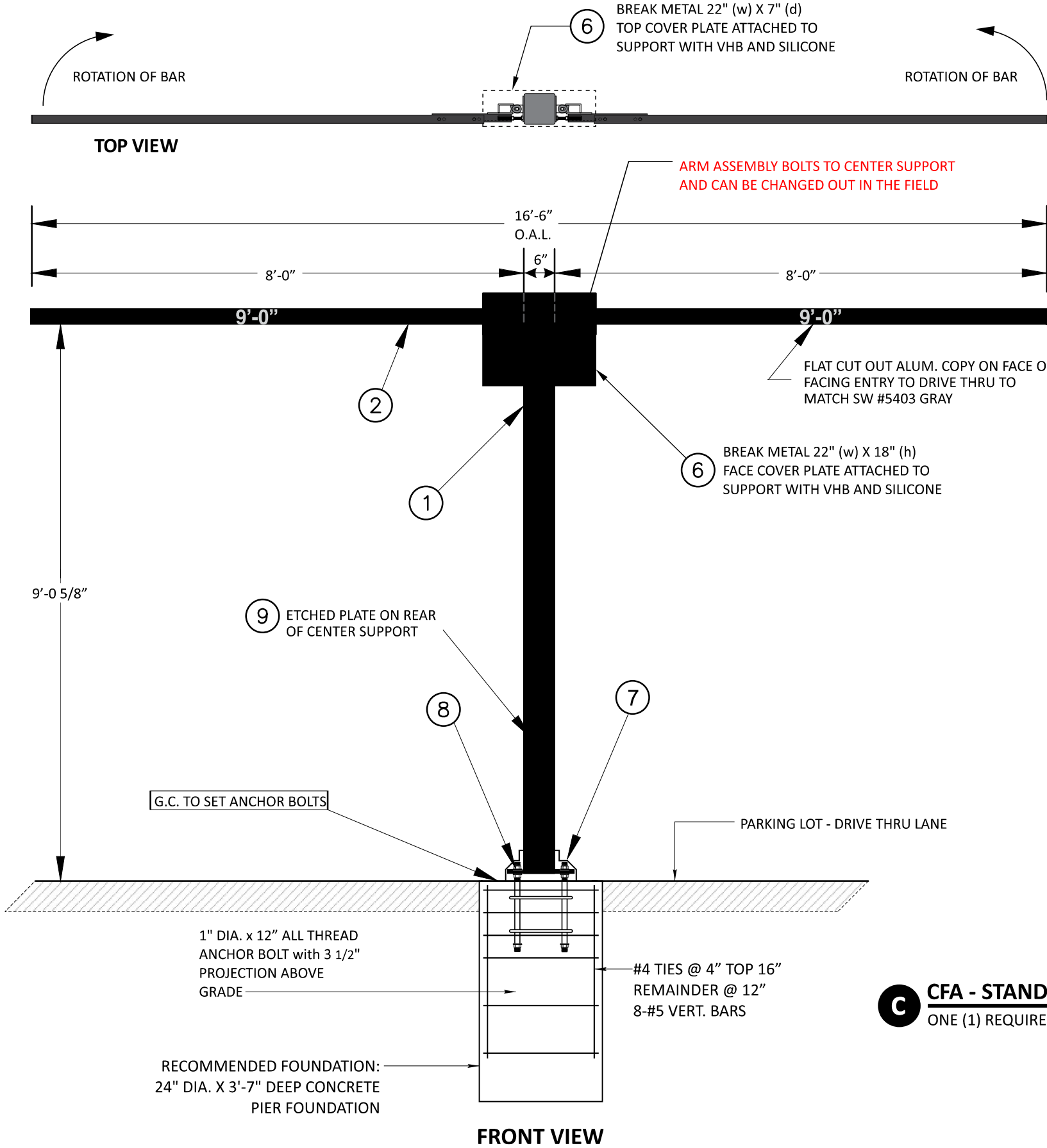
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PROPER GROUNDING & BONDING OF THE SIGN.
SIGN WILL BEAR UL LABEL(S).

Chick-fil-A

B1-2



ITEM	QUANTITY	DESCRIPTION
1	1	CENTER POST ASSEMBLY, 6"X 6" STEEL
2	2	CLEARANCE BAR ASSEMBLY, 2" X 2" ALUM ANGLE
6	1	TOP COVER, .125" ALUM, BREAK FORMED
7	1	BASE COVER, .08" ALUM, BREAK FORMED
8	4	1" X 36" LONG, ALL TREAD ANCHORS, INCLUDING NUTS AND WASHERS
9	1	CLEARANCE BAR ID PLATE

- Notes:
- ENTIRE CLEARANCE BAR AND HARDWARE TO BE POWDER-COATED P-820 MATTE BLACK FINISH
 - CHANDLER TO PROVIDE ALL-THREAD ANCHORS WITH FENDER WASHERS AND HEX BOLTS

CFA - STANDARD DUAL 9' ARM CLEARANCE BAR - MATTE BLACK SCALE: 1/2" = 1'-0"
ONE (1) REQUIRED - MANUFACTURE AND INSTALL

Design #
0637033Ar3

Sheet 13 of 27

Client
#2859

Address
690 NW Blue Pkwy,
Lees Summit, MO

Account Rep. KRISTEN HAMILTON
TERRI BROWN

Designer LEAH LANSFORD

Date 9/29/23

Approval / Date

Client

Sales

Estimating

Art

Engineering

Landlord

Revision/Date

R1(12-22-23)LL: CHANGED SIZE OF PANELS ON THE STOPPINE

R2(1/16/24)LL: ADDED STAMPED ENGINEERING

CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4

R3(02/26/2024)AM: UPDATED SP ADDED NOTE FOR SIGN A FOR CSI TO PROVIDE NEW STEEL AND FOUNDATION AND ADDED NOT FOR SIGN D FOR CSI TO REMOVE AND DISCARD EXISTING DIF DIRECTIONAL

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C



PROJECT: CFA-2859

PROJ. NO.: 43787C

CLIENT: CHANDLER SIGNS

DATE: 1/09/24

ENGINEER: JC(IH)

VSS

units: pounds, feet unless noted otherwise

Applied Wind Loads; from ASCE 7-16

$F = q_z \cdot G \cdot C_f \cdot A_f$

with $q_z = 0.00256 K_z K_{zt} K_d V^2$ (29.3.2 & 29.4)

$C_f =$ (Fig. 29.3-1) 1.00 max. height= 9.53

$K_{zt} =$ 1.0 (26.8.2) (=1.0 unless unusual landscape)

$K_z =$ from table 28.3-1 Exposure= c

$K_d =$ 0.85 for signs (table 26.6-1)

$V =$ 110 mph

$G =$ 0.85 (26.9)

$s/h =$

$B/s =$

$weight =$ 0.083 kips

$M_{OL} =$ 0.00 k-ft

Pole Loads	structure component	height at section c.g.	K_z	q_z	pressure $q_z \cdot G \cdot C_f$	A_f	shear	Wind Moment M_w
	1	0.25	0.850	22.4	43.66	0.5	21	5
	2	4.68	0.850	22.4	43.66	4.2	183	855
	3	8.96	0.850	22.4	43.66	0.3	15	134
	4	9.14	0.850	22.4	43.66	2.7	120	1097
	5	9.38	0.850	22.4	43.66	0.6	25	234
				sums:	8.3	363	2.33	(M_w) k-ft arm= 6.4
				$P_U =$ 0.10 kip			$M =$ 2.33 k-ft	$M = \sqrt{(M_{OL}^2 + M_w^2)}$
				$M_U = \sqrt{(1.2M_{OL}^2 + 1.0M_w^2)} =$ 2.33 k-ft				

Pole Design

section: tube

$M_u \leq \phi M_n$ with $M_n = f_y Z$

$f_y =$ 46 ksi

$\% \gamma =$ 0.9

H	M_u (k-ft)	Z req'd. (in)	Size (in)	t (in)	Z	USE
at grade	2.33	0.67	2	0.25	1.0	6x6x1/8" SQ. HSS, $\phi M_n = 15.6$ k-ft

Footing Design

footprint: round

$\omega =$ 1.3 IBC 1606.3.2 IBC Table 1606.2, sections 1806.3.4, 1807.3.2 $S = (1.3 \times 2 \times 150 \text{ psf/ft})$

$P =$ 0.28 kip $S_1 = S \times d / 3$ $A = 2.34 \times P / (S_1 \times b)$ $S = 400$

$S_1 =$ 388 $d = 0.5 \times A (1 + (1 + 4.36 \times b/A)^{0.5})$ IBC 1807.3.2.1

$A =$ 0.86

footing: 2' - 0" dia.

2' - 11" deep min.

Design # 0637033Ar3	
Sheet	14 of 27
Client #2859	
Address 690 NW Blue Pkwy, Lees Summit, MO	
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Designer	LEAH LANSFORD
Date	9/29/23
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Landlord	
Revision/Date	
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R2(1/16/24)LL: ADDED STAMPED ENGINEERING	
CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4	
R3(02/26/2024)AM: UPDATED SP. ADDED NOTE FOR SIGN A FOR CSI TO PROVIDE NEW STEEL AND FOUNDATION AND ADDED NOTE FOR SIGN D FOR CSI TO REMOVE AND DISCARD EXISTING D/F DIRECTIONAL	
 CHANDLER SIGNS	
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C	



PROJECT: CFA-2859
 PROJ. NO.: 43787C
 CLIENT: CHANDLER SIGNS

DATE: 1/09/24
 ENGINEER: JC(IH)

Check 2"x2"x0.125" Sq. Aluminum Tube

(ADM 2015 - Ch F)

	Mu =	4.453 k-in (See Page#3)	d	t
Yielding: (Governs)			2	0.125
(ADM 15, F.2)	Mn = Z Fcy =	23.1 k-in	welded?	NO
	Mn = 1.5 St Fty =	29.0 k-in	Fcy = Fty =	35 ksi
			Z =	0.660 in ³
	PMn =	20.8 k-in OK	St =	0.552 in ³
LB:			P =	0.9
(ADM 15 F.3.1)	Bp =	45.0 ksi	8 =	1 ksi
	Dp =	0.30 ksi	E =	10100 ksi
	Cp =	61.4	k1c =	0.35
			k2c =	2.27
	91 = Bp-Fcy/1.6Dp =	20.8	k1f =	0.5
	92 = k1 Bp/1.6Dp =	15.2	k2f =	2.04
			b/t =	14.0
since b/t < 91: Fc = Fcy =		35.00	m =	0.65
			I =	0.552 in ⁴
	Bbr =	66.8 ksi	ccf =	0.938 in
	Dbr =	0.67 ksi	ccw =	1.0 in
	Cbr =	67		
	91 = Bbr-1.5 Fcy/mDbr =	33.0		
	92 = k1 Bbr/mDbr =	77.2		
since b/t < 91: Fc = 1.5 Fcy =		52.50		
Mnlb = Fc If / ccf + Fb lw / ccw =		49.57 k-in		
PMnlb =		44.61 k-in OK		

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units; pounds, feet unless noted otherwise

Check HSS6X6X.125 for torsion and combined forces (AISC 14 H3)

$T_r =$	6.99 k-in (See Page#3)	$F_y =$	46 ksi
$h/t =$	48.7	$h =$	5.65 in ³
$2.45 (E/F_y)^{1/2} =$	61.52	$t =$	0.116 in ³
$3.07 (E/F_y)^{1/2} =$	77.08	$E =$	29000 ksi
		$L =$	in
		$C =$	8.03 in ³
$F_{cr} =$	27.6 ksi	$\phi =$	0.9
$T_c \approx T_n = \phi F_{cr} C =$			
	199.5 k-in OK		
$M_r/M_c + (T_r/T_c)^2 =$	0.15 < 1 OK	$(eq'n. H3-6)$	
		(See Page #2 for M_r & M_c)	



Company:		Date:	1/9/2024
Engineer:		Page:	1/6
Project:			
Address:			
Phone:			
E-mail:			

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 35.00
State: Cracked
Compressive strength, f_c (psi): 2500
 λ : 1.0
Reinforcement condition: Supplementary reinforcement not present
Supplemental edge reinforcement: Not applicable
Reinforcement provided at corners: No
Ignore concrete breakout in tension: No
Ignore concrete breakout in shear: No
Ignore f_{td} requirement: No
Build-up grout pad: No

Length x Width x Thickness (inch): 13.00 x 13.00 x 0.75

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB8 (1"Ø)

()



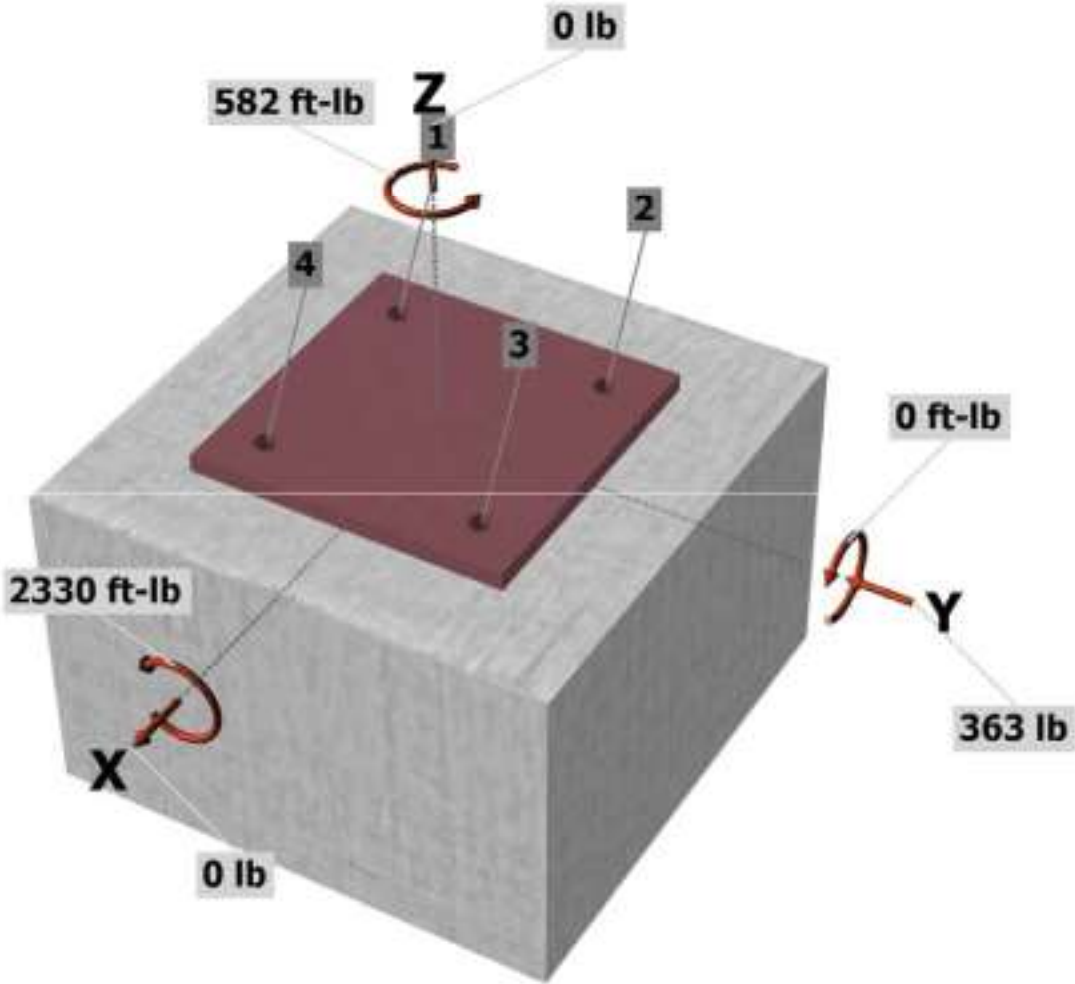
Company:		Date:	1/9/2024
Engineer:		Page:	2/6
Project:			
Address:			
Phone:			
E-mail:			

Load and Geometry
Load factor source: ACI 318 Section 5.3
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: Not applicable
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Strength level loads:

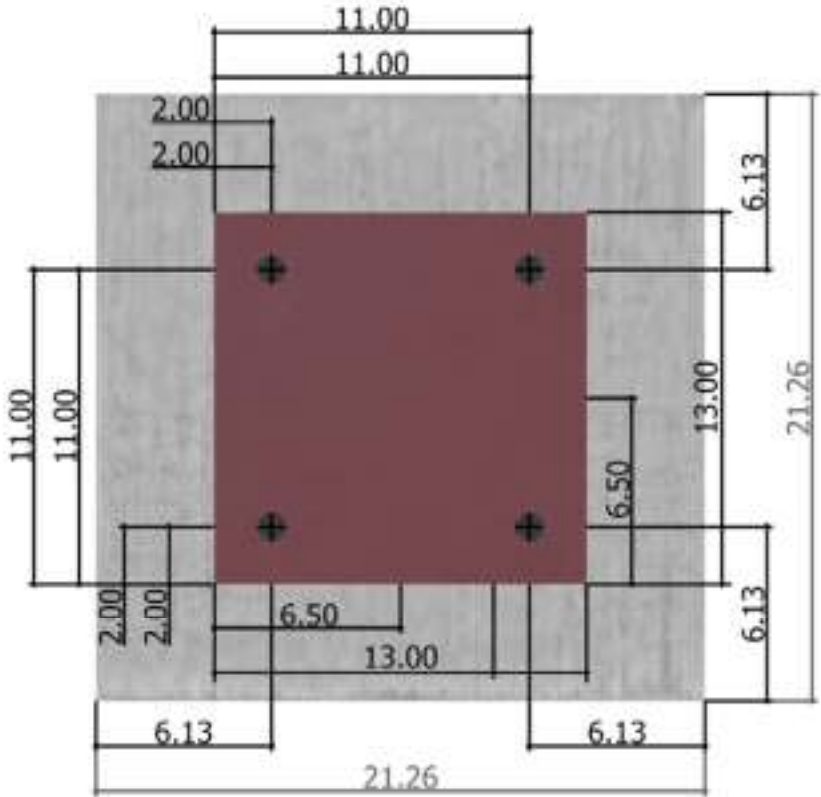
N_{ux} [lb]: 0
V_{uxx} [lb]: 0
V_{uyy} [lb]: -363
M_{ux} [ft-lb]: 2330
M_{uy} [ft-lb]: 0
M_{uz} [ft-lb]: 582

<Figure 1>



Company:		Date:	1/9/2024
Engineer:		Page:	3/6
Project:			
Address:			
Phone:			
E-mail:			

<Figure 2>



Design #

0637033Ar3

Sheet 17 of 27

Client

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C



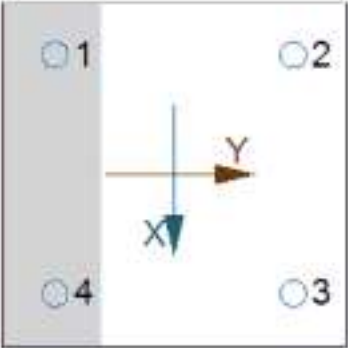
Company:		Date:	1/9/2024
Engineer:		Page:	4/6
Project:			
Address:			
Phone:			
E-mail:			

3. Resulting Anchor Forces

Anchor	Tension load, N _{ax} (lb)	Shear load x, V _{ax} (lb)	Shear load y, V _{ay} (lb)	Shear load combined, √(V _{ax}) ² + (V _{ay}) ² (lb)
1	0.0	194.0	-284.7	344.5
2	1432.0	-194.0	-284.7	344.5
3	1432.0	-194.0	103.2	219.8
4	0.0	194.0	103.2	219.8
Sum	2864.0	0.0	-363.0	1128.6

Maximum concrete compression strain (‰): 0.03
Maximum concrete compression stress (psi): 119
Resultant tension force (lb): 2864
Resultant compression force (lb): 2864
Eccentricity of resultant tension forces in x-axis, e'_{tx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{ty} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.6.1)

N _{ax} (lb)	φ	φN _{ax} (lb)
35150	0.75	26363

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.6.2)

N_b = 16.1λ√f_ch_{ef}^{3/2} (Eq. 17.6.2.2.1)

λ	f _c (psi)	h _{ef} (in)	N _b (lb)
1.00	2500	10.087	37671

φN_{bx} = φ (A_{nc} / A_{no}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} √f_{cz} N_b (Sec. 17.5.1.2 & Eq. 17.6.2.1a)

A _{nc} (in ²)	A _{no} (in ²)	λ _{ci} (in)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	N _b (lb)	φ	φN _{bx} (lb)
451.99	915.67	6.13	1.000	0.822	1.00	1.000	37671	0.70	10694

6. Pullout Strength of Anchor in Tension (Sec. 17.6.3)

φN_{ux} = φ √f_{ci} √f_{ct} √f_{cy} √f_{cz} √f_{cz} A_{sq} √f_c (Sec. 17.5.1.2, Eq. 17.6.3.1 & 17.6.3.2.2a)

√f _{ci}	A _{sq} (in ²)	f _c (psi)	φ	φN _{ux} (lb)
1.0	5.15	2500	0.70	72156



Company:		Date:	1/9/2024
Engineer:		Page:	5/6
Project:			
Address:			
Phone:			
E-mail:			

8. Steel Strength of Anchor in Shear (Sec. 17.7.1)

V _{ax} (lb)	φ _{gross}	φ	φ _{gross} V _{ax} (lb)
21090	1.0	0.65	13709

9. Concrete Breakout Strength of Anchor in Shear (Sec. 17.7.2)

Shear perpendicular to edge in x-direction:

V_{ax} = min[7(l_e / d_s)²√d_sλ√f_cd_{cr}^{1.5}; 9.1λ√f_cd_{cr}^{1.5}] (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)

l _e (in)	d _s (in)	λ	f _c (psi)	d _{cr} (in)	V _{ax} (lb)
8.00	1.000	1.00	2500	15.13	26483

φV_{axg} = φ (A_{vc} / A_{vo}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} V_{ax} (Sec. 17.5.1.2 & Eq. 17.7.2.1b)

A _{vc} (in ²)	A _{vo} (in ²)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	V _{ax} (lb)	φ	φV _{axg} (lb)
482.50	1030.13	1.000	0.781	1.000	1.000	26483	0.70	6782

Shear perpendicular to edge in y-direction:

V_{ay} = min[7(l_e / d_s)²√d_sλ√f_cd_{cr}^{1.5}; 9.1λ√f_cd_{cr}^{1.5}] (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)

l _e (in)	d _s (in)	λ	f _c (psi)	d _{cr} (in)	V _{ay} (lb)
8.00	1.000	1.00	2500	15.13	26483

φV_{ayg} = φ (A_{vc} / A_{vo}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} V_{ay} (Sec. 17.5.1.2 & Eq. 17.7.2.1b)

A _{vc} (in ²)	A _{vo} (in ²)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	V _{ay} (lb)	φ	φV _{ayg} (lb)
482.50	1030.13	1.000	0.781	1.000	1.000	26483	0.70	6782

Shear parallel to edge in x-direction:

V_{ax} = min[7(l_e / d_s)²√d_sλ√f_cd_{cr}^{1.5}; 9.1λ√f_cd_{cr}^{1.5}] (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)

l _e (in)	d _s (in)	λ	f _c (psi)	d _{cr} (in)	V _{ax} (lb)
8.00	1.000	1.00	2500	6.13	6830

φV_{axg} = φ (2)(A_{vc} / A_{vo}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} V_{ax} (Sec. 17.5.1.2, 17.7.2.1(c) & Eq. 17.7.2.1b)

A _{vc} (in ²)	A _{vo} (in ²)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	V _{ax} (lb)	φ	φV _{axg} (lb)
195.49	169.10	1.000	1.000	1.000	1.000	6830	0.70	11054

Shear parallel to edge in y-direction:

V_{ay} = min[7(l_e / d_s)²√d_sλ√f_cd_{cr}^{1.5}; 9.1λ√f_cd_{cr}^{1.5}] (Eq. 17.7.2.2.1a & Eq. 17.7.2.2.1b)

l _e (in)	d _s (in)	λ	f _c (psi)	d _{cr} (in)	V _{ay} (lb)
8.00	1.000	1.00	2500	6.13	6830

φV_{ayg} = φ (2)(A_{vc} / A_{vo}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} V_{ay} (Sec. 17.5.1.2, 17.7.2.1(c) & Eq. 17.7.2.1b)

A _{vc} (in ²)	A _{vo} (in ²)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	V _{ay} (lb)	φ	φV _{ayg} (lb)
195.49	169.10	1.000	1.000	1.000	1.000	6830	0.70	11054

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.7.3)

φV_{ax} = φ k_{ap} N_{ux} = φ k_{ap} (A_{nc} / A_{no}) √f_{ci} √f_{ct} √f_{cy} √f_{cz} N_b (Sec. 17.5.1.2 & Eq. 17.7.3.1a)

k _{ap}	A _{nc} (in ²)	A _{no} (in ²)	√f _{ci}	√f _{ct}	√f _{cy}	√f _{cz}	N _b (lb)	φ	φV _{ax} (lb)
2.0	113.00	915.67	0.822	1.000	1.000	1.000	37671	0.70	5347

11. Results

Interaction of Tensile and Shear Forces (Sec. 17.8)

Design #

0637033Ar3

Sheet 18 of 27

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CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4
R3(02/26/2024)AM: UPDATED SP ADDED NOTE FOR SIGN A FOR CSI TO PROVIDE NEW STEEL AND FOUNDATION AND ADDED NOT FOR SIGN D FOR CSI TO REMOVE AND DISCARD EXISTING DIF DIRECTIONAL

CHANDLER
SIGNS

National Headquarters

14201 Sovereign Road #101
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San Antonio

17319 San Pedro Ave
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Georgia

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Dawsonville, GA 30534
(678) 725-8852 Fax (210) 349-8724

South Texas

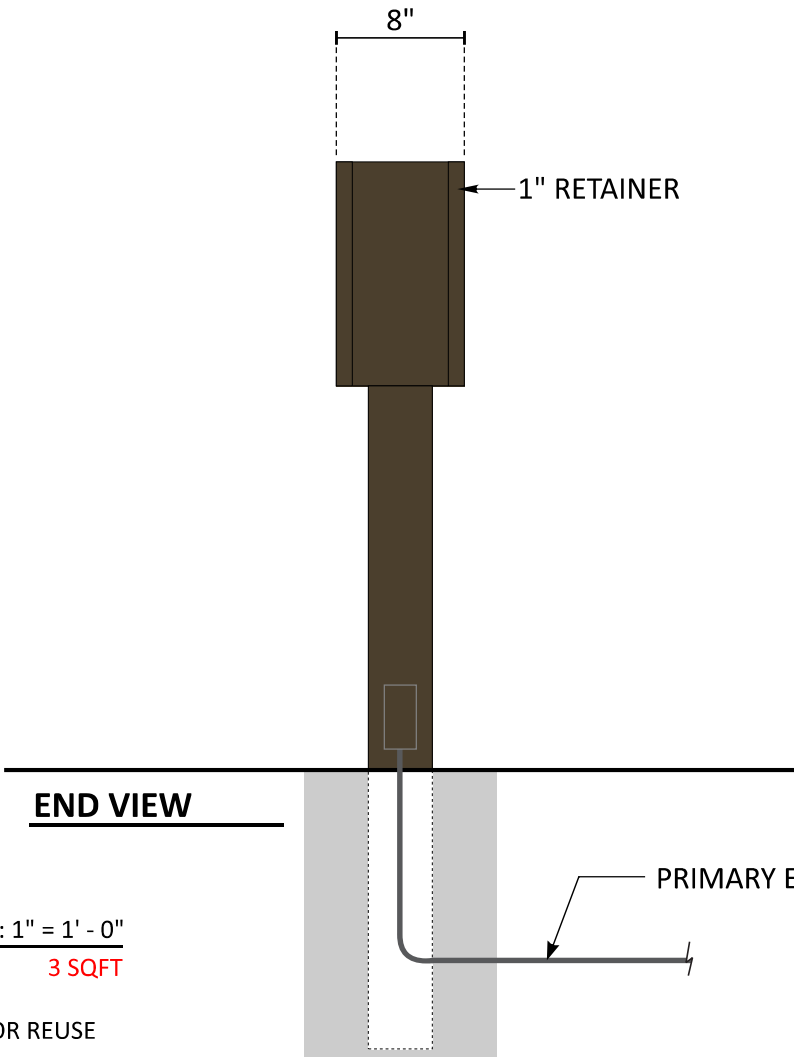
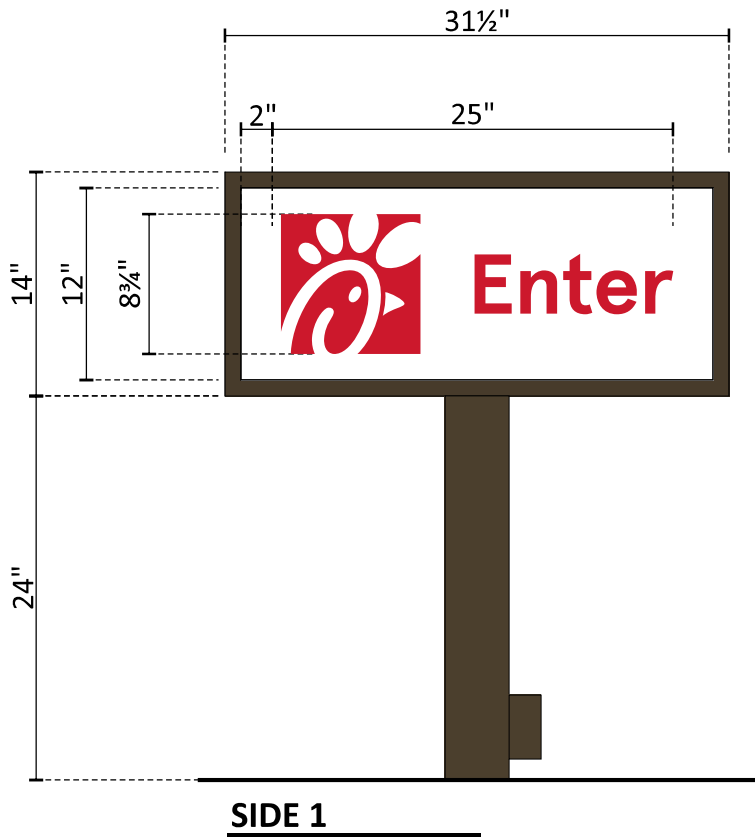
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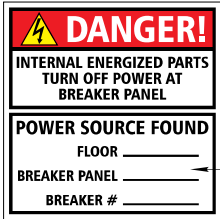
THIS SIGN IS INTENDED TO BE INSTALLED
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SIGN WILL BEAR UL LABEL(S).

C

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2014/2017 NEC
COMPLIANT LABEL



WARNING LABEL/
BREAKER LOCATION

D CFA - D/F DIRECTIONAL SCALE: 1" = 1' - 0"
ONE (1) REMOVAL REQUIRED - MANUFACTURE & INSTALL 3 SQFT

CSI TO REMOVE AND DISCARD EXISTING D/F DIRECTIONAL. CAP ELECTRICAL FOR REUSE

MANUFACTURE AND INSTALL ONE NEW D/F VIS 22 DIRECTIONAL.
REUSE EXISTING ELECTRICAL.

GENERAL SPECIFICATIONS

D/F ALUMINUM SIGN CABINET INTERNALLY ILLUMINATED WITH 6500K
WHITE LEDS.

FILLER, RETAINER AND SUPPORT PAINTED MATTHEWS #20181 DK
BRONZE, SATIN.

ACRYLIC FACES

#7328 WHITE ACRYLIC DECORATED WITH **AVERY UC900-440-T RED
TRANSLUCENT VINYL (BRAND REQ.)** APPLIED 1ST SURFACE.

TEXT TO BE APERCU SENTENCE CASE BOLD

STEEL POLE

4" x 4" STEEL SQUARE TUBE SUPPORT



EXISTING CONDITIONS

Design #
0637033Ar3

Sheet 20 of 27

Client
#2859

Address
690 NW Blue Pkwy,
Lees Summit, MO

Account Rep. KRISTEN HAMILTON
TERRI BROWN

Designer LEAH LANSFORD

Date 9/29/23

Approval / Date

Client

Sales

Estimating

Art

Engineering

Landlord

Revision/Date

R1(12-22-23)LL: CHANGED SIZE OF PANELS ON THE STOPPONE

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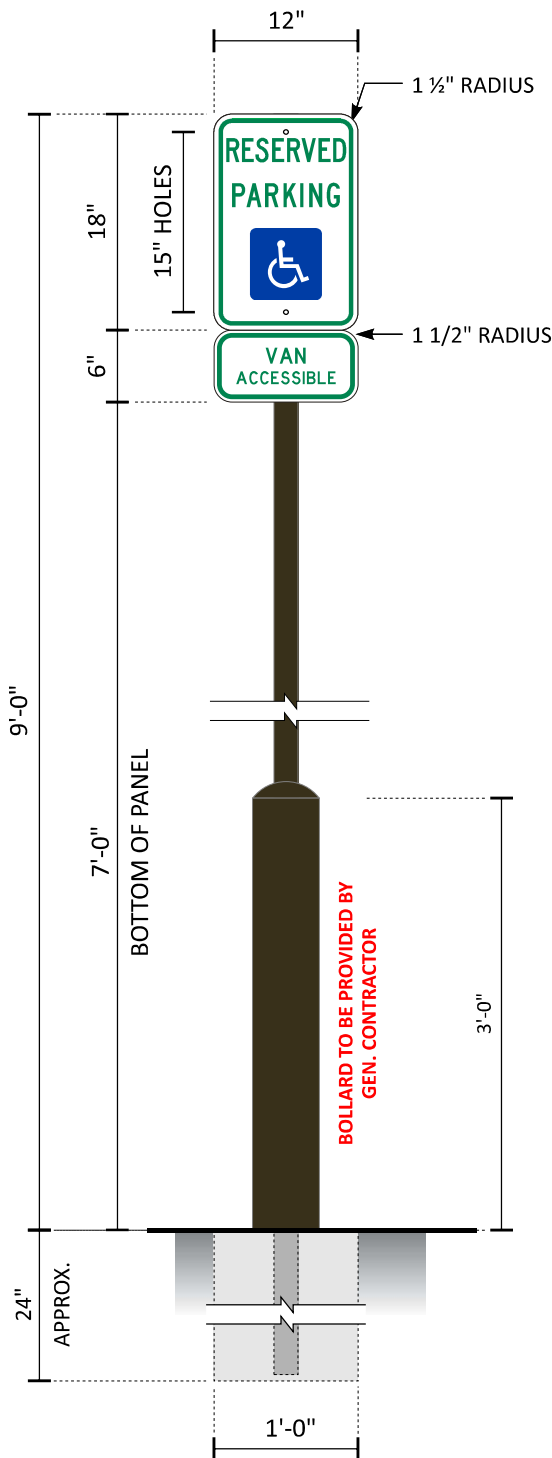
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FINAL ELECTRICAL
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CUSTOMER

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D



BOLLARD MOUNTED HANDICAP SIGNS

SPECIFICATIONS

SIGN PANELS

.080 ALUMINUM WITH BACKS PAINTED MATTHEWS
#20181 DARK BRONZE, SATIN AND REFLECTIVE VINYL
GRAPHICS APPLIED 1ST SURFACE.

**SIGN PANELS ARE TO BE SECURED TO SIGN POST WITH
NUTS AND BOLTS PAINTED TO MATCH VINYL BACKGROUND**

SIGN POST

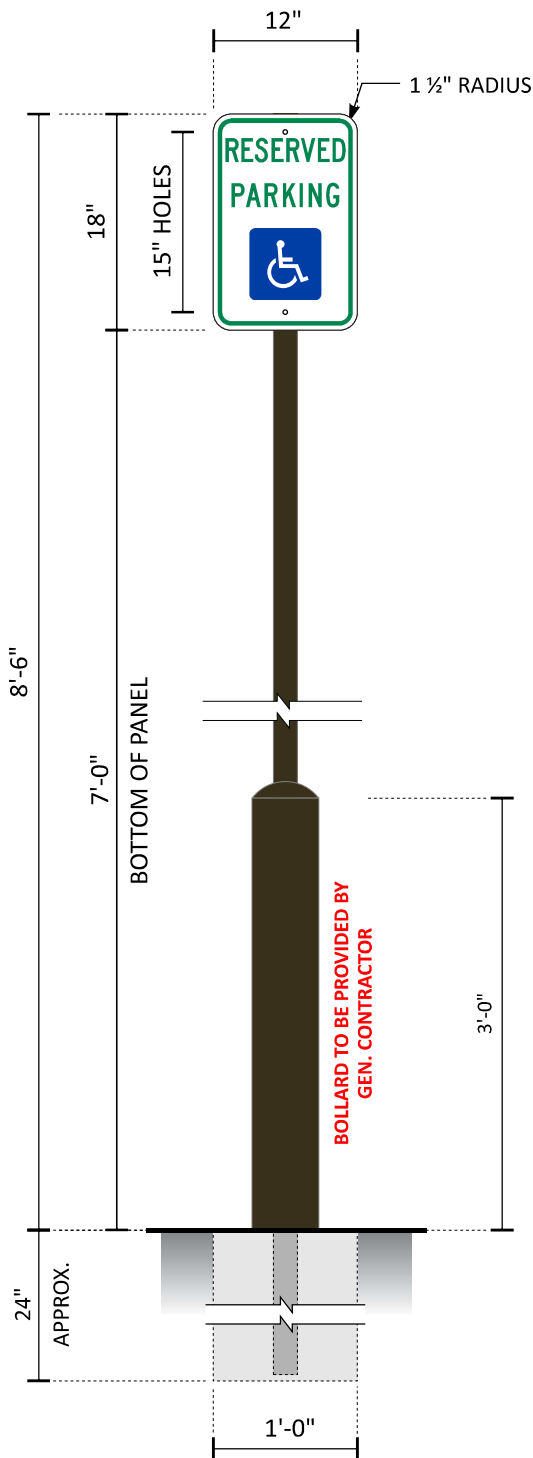
2" x 2" x .125"(WALL) ALUMINUM SQ. TUBE, CAPPED ON TOP WITH
PUSH IN PLASTIC CAP PAINTED MATTHEWS #20181
DARK BRONZE, SATIN.
CAP IS A BUYOUT FROM MCMASER CARR #9565K31
INVENTORY #02948

BOLLARD - TO BE PROVIDED BY GEN.CONTRACTOR
5 9/16" O.D. x .280 WALL THICKNESS STEEL PIPE.

BOLLARD AND CONCRETE TOP TO BE PAINTED
MATTHEWS #20181 DARK BRONZE, SATIN.
INSTALLER TO PROVIDE PAINT.

DAL - MANUFACTURING

MUTCD PANEL - UPPERCASE



E1 E2

E2

CFA - S/F HCVA SIGN

TWO (2) REQUIRED - MANUFACTURE AND INSTALL

SCALE: $3/4" = 1'-0"$

2 SQ. FT.

F

CFA - S/F HC SIGN

ONE (1) REQUIRED - MANUFACTURE AND INSTALL

SCALE: 3/4" = 1'-0"

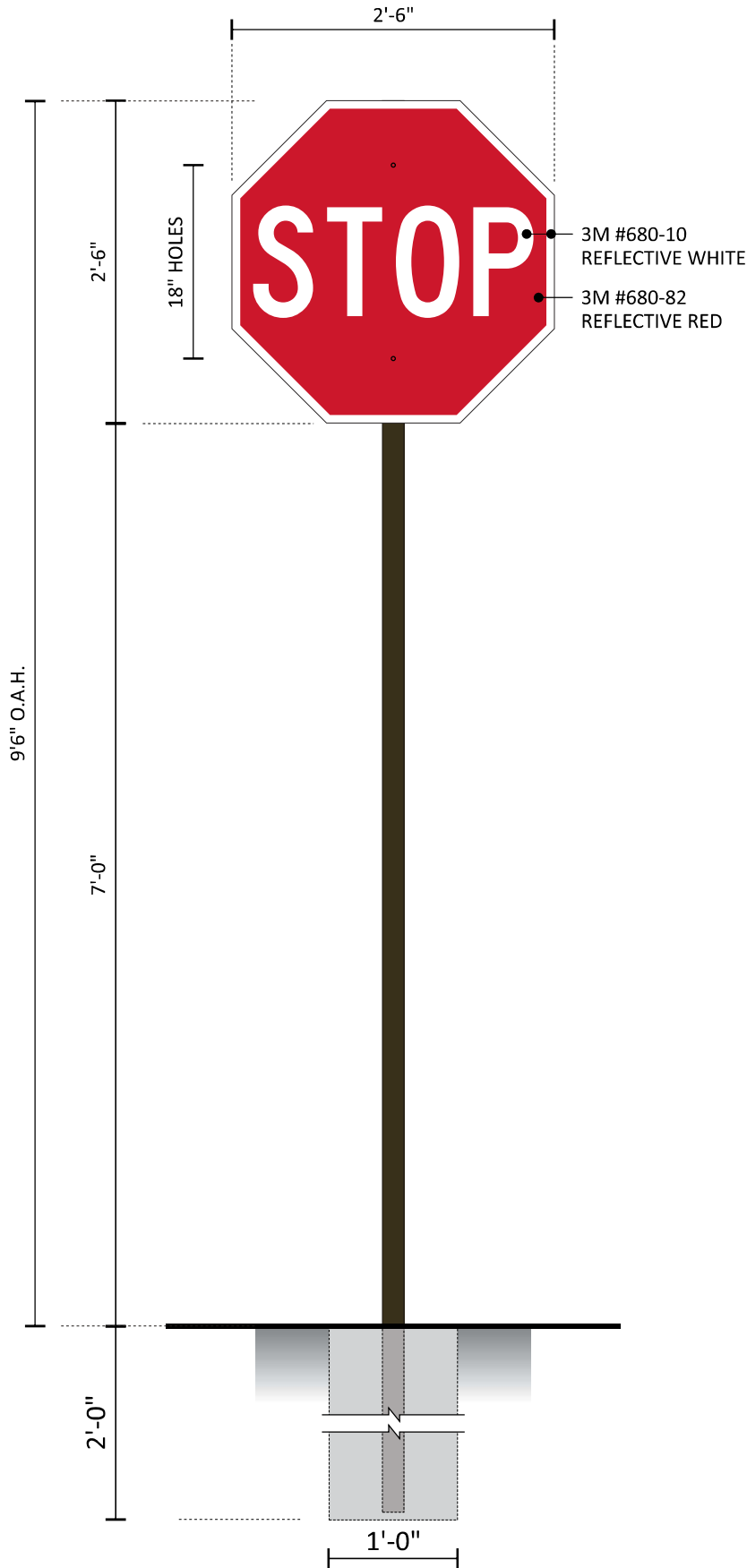
1.5 SQ. FT.

DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

Design #	
0637033Ar3	
Sheet	21 of 27
Client	
#2859	
Address	
690 NW Blue Pkwy, Lees Summit, MO	
Account Rep.	KRISTEN HAMILTON TERRI BROWN
Designer	LEAH LANSFORD
Date	9/29/23
Approval / Date	
Client	
Sales	
Estimating	
Art	
Engineering	
Landlord	
Revision/Date	
R1(1/2-2-23)LL: CHANGED SIZE OF PANELS ON THE STOPDNE	
R2(1/16/24)LL: ADDED STAMPED ENGINEERING	
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17319 River Road Ste 201 Louisville, KY 40206 (502) 897-9800 Cell (502) 554-2575	
111 Woodstone Place Dawsonville, GA 30534 (678) 725-8852 Fax (210) 349-8724	
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E1-2, F



G1 G2

CFA - DOT S/F STOP SIGN

SCALE: 3/4" = 1'-0"

TWO (2) REMOVALS REQUIRED - MANUFACTURE AND INSTALL

5 SQ. FT.

G.C. TO REMOVE AND DISCARD EXISTING STOP SIGNS IN PARKING LOT LANDSCAPING.

MANUFACTURE AND INSTALL TWO NEW S/F VIS 22 STOP SIGNS.

SPECIFICATIONS

SIGN PANELS

.080 ALUMINUM PANELS WITH BACKS PAINTED MATTHEWS
#20181 DK. BRONZE, SATIN AND REFLECTIVE VINYL
GRAPHICS APPLIED 1ST SURFACE.

SIGN PANEL IS TO BE SECURED TO SIGN POST WITH
NUTS AND BOLTS PAINTED TO MATCH VINYL BACKGROUND

SIGN POST

2" x 2" x .125"(WALL) ALUMINUM SQ. TUBE, CAPPED ON TOP WITH
PUSH IN PLASTIC CAP PAINTED MATTHEWS #20181
DARK BRONZE, SATIN.
CAP IS A BUYOUT FROM MCMASTER CARR #9565K31
INVENTORY #02948

NOTE:
IF SIGN IS LOCATED ON SIDEWALK, THEN IT IS THE
RESPONSIBILITY OF THE GENERAL CONTRACTOR
TO INSTALL A PVC SLEEVE INTO THE CONCRETE WHEN
THE SIDEWALK IS POURED PRIOR TO INSTALLATION OF
THE SIGN.

DAL - MANUFACTURING
MUTCD PANEL - UPPERCASE



EXISTING CONDITIONS



EXISTING CONDITIONS

DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

Design #

0637033Ar3

Sheet

22 of 27

Client

#2859

Address

690 NW Blue Pkwy,
Lees Summit, MO

Account Rep.

KRISTEN HAMILTON
TERRI BROWN

Designer

LEAH LANSFORD

Date

9/29/23

Approval / Date

Client

Sales

Estimating

Art

Engineering

Landlord

Revision/Date

R1(12-22-23)LL: CHANGED SIZE OF PANELS ON THE STOP/DONE

R2(1/16/24)JLL: ADDED STAMPED ENGINEERING CORRECTION(01/17/2024)AM: REVISED DETAIL SECTION AND ADDED THE WORD G.C. IN FRONT OF REMOVALS FOR SIGNS B1-2, C, D, G1-2 AND H1-4

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CHANDLER SIGNS

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FINAL ELECTRICAL
CONNECTION BY
CUSTOMER

UL

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Chick-fil-A

G1-2

H1-4

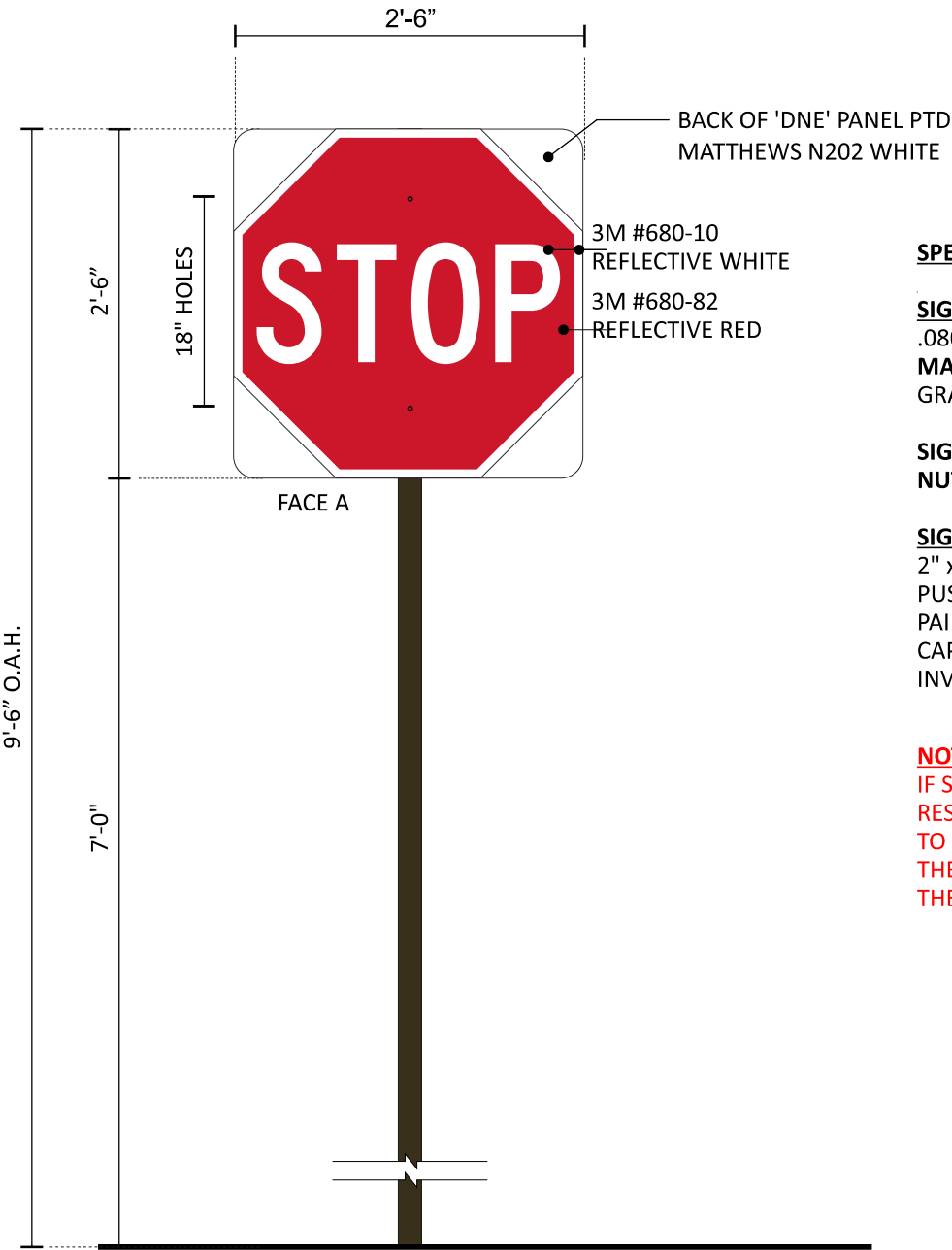
D/F STOP/DNE POST AND PANEL

FOUR (4) REMOVALS REQUIRED - MANUFACTURE AND INSTALL

MANUFACTURE AND INSTALL FOUR (4) NEW STOP/DNE SIGNS.

SCALE: 3/4" = 1'-0"

4 SQ. FT.



SPECIFICATIONS

SIGN PANELS

.080 ALUMINUM PANELS WITH BACKS PAINTED MATTHEWS N202 WHITE, SATIN AND REFLECTIVE VINYL GRAPHICS APPLIED 1ST SURFACE.

SIGN PANEL IS TO BE SECURED TO SIGN POST WITH NUTS AND BOLTS PAINTED TO MATCH VINYL BACKGROUND

SIGN POST

2" x 2" x .125"(WALL) ALUMINUM SQ. TUBE, CAPPED ON TOP WITH PUSH IN PLASTIC CAP.
PAINTED MATTHEWS #20181 DARK BRONZE, SATIN.
CAP IS A BUYOUT FROM MCMASTER CARR #9565K31
INVENTORY #02948

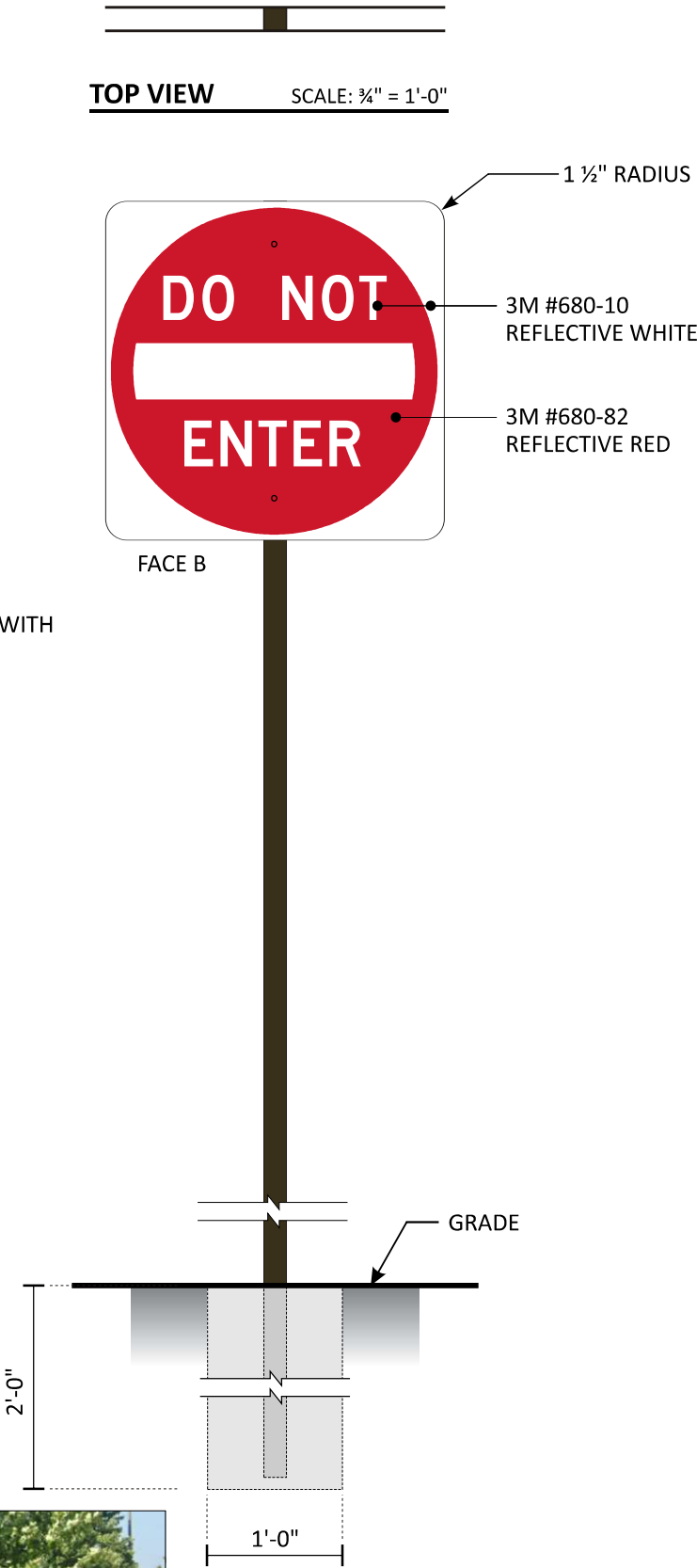
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DAL - MANUFACTURING
MUTCD PANEL - UPPERCASE



EXISTING CONDITIONS



DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

Design #

0637033Ar3

Sheet

23 of 27

Client

#2859

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Account Rep.

KRISTEN HAMILTON
TERRI BROWN

Designer

LEAH LANSFORD

Date

9/29/23

Approval / Date

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Landlord

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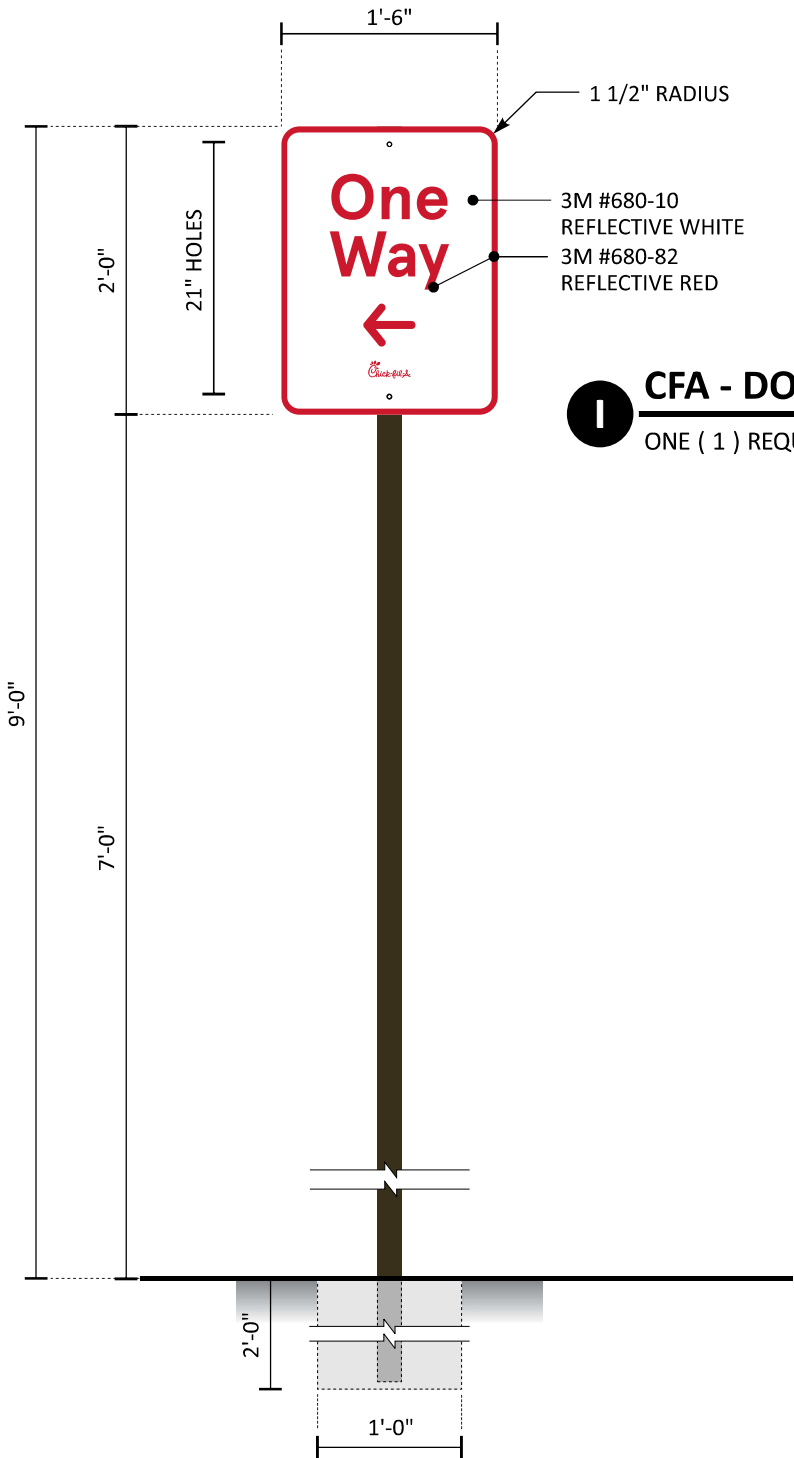
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Chick-fil-A

H1-4

DAL - MANUFACTURING
NEW CFA WAYFINDING PANELS



I CFA - DOT S/F DRIVE THRU WITH ARROW POST AND PANEL SCALE: 3/4" = 1'-0"
ONE (1) REQUIRED - MANUFACTURE AND INSTALL 7 SQ. FT.

SPECIFICATIONS

SIGN PANEL
.080 ALUMINUM PANEL WITH BACK PAINTED MATTHEWS
#20181 DK. BRONZE, SATIN AND REFLECTIVE VINYL
GRAPHICS APPLIED 1ST SURFACE.

**SIGN PANEL IS TO BE SECURED TO SIGN POST WITH
NUTS AND BOLTS PAINTED TO MATCH VINYL BACKGROUND**

SIGN POST
2" x 2" x .125"(WALL) ALUMINUM SQ. TUBE, CAPPED ON TOP WITH
PUSH IN PLASTIC CAP PAINTED MATTHEWS #20181
DARK BRONZE, SATIN.
CAP IS A BUYOUT FROM MCMASTER CARR #9565K31
INVENTORY #02948

NOTE:
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TO INSTALL A PVC SLEEVE INTO THE CONCRETE WHEN
THE SIDEWALK IS POURED PRIOR TO INSTALLATION OF
THE SIGN.

DAL - MANUFACTURING
MUTCD PANEL - UPPERCASE

DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

Design #	
0637033Ar3	
Sheet	24 of 27
Client	
#2859	
Address	
690 NW Blue Pkwy, Lees Summit, MO	
Account Rep.	KRISTEN HAMILTON TERRI BROWN
Designer	LEAH LANSFORD
Date	9/29/23
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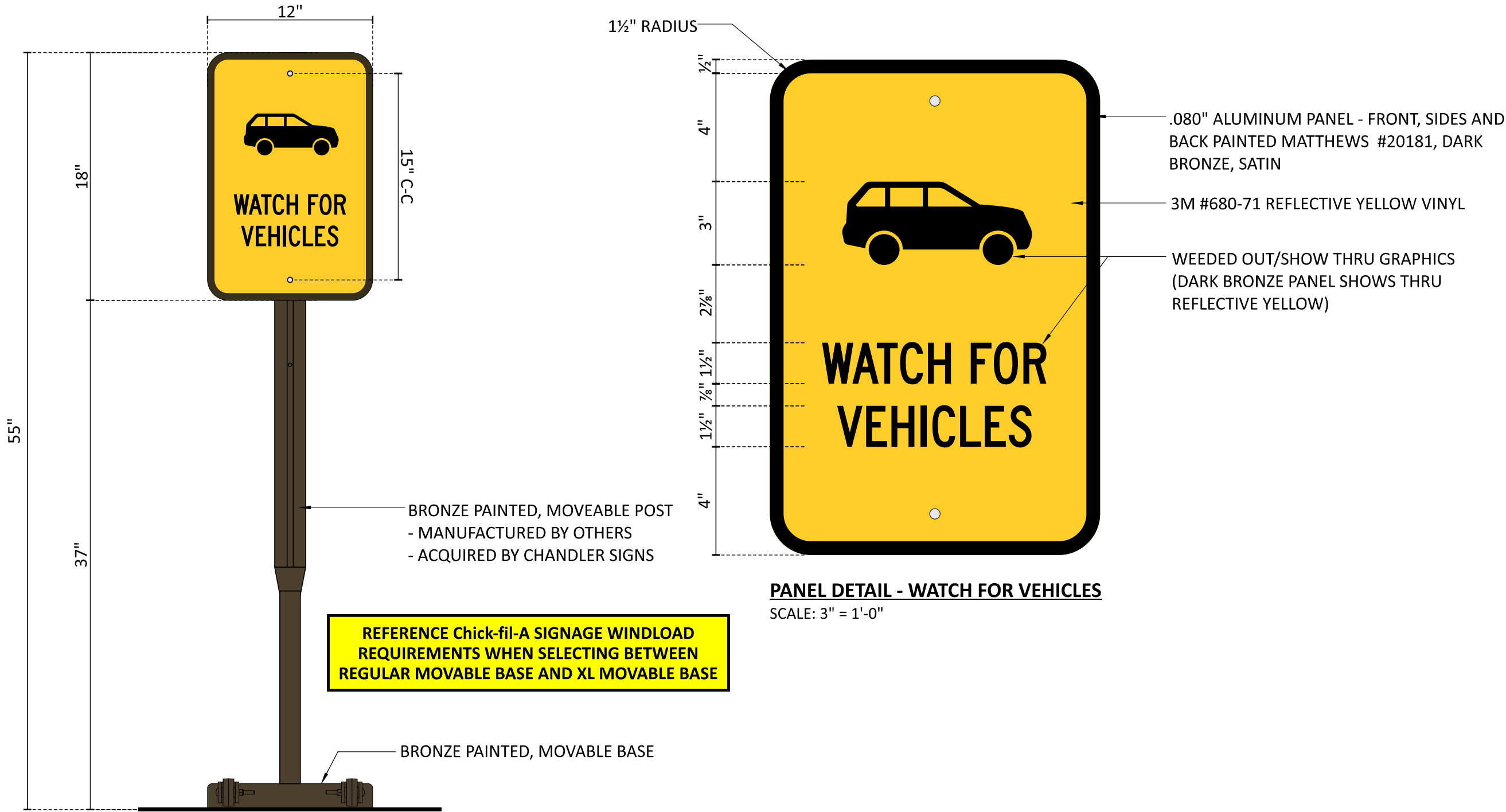
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I



K

SAFETY SIGN - WATCH FOR VEHICLES

ONE (1) REQUIRED - MANUFACTURE & INSTALL

SCALE: 1-1/2" = 1'-0"

PLEASE NOTE: PORTABLE BASE AND POST PROVIDED BY PATTISON.

PANEL DETAIL - WATCH FOR VEHICLES
SCALE: 3" = 1'-0"

DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

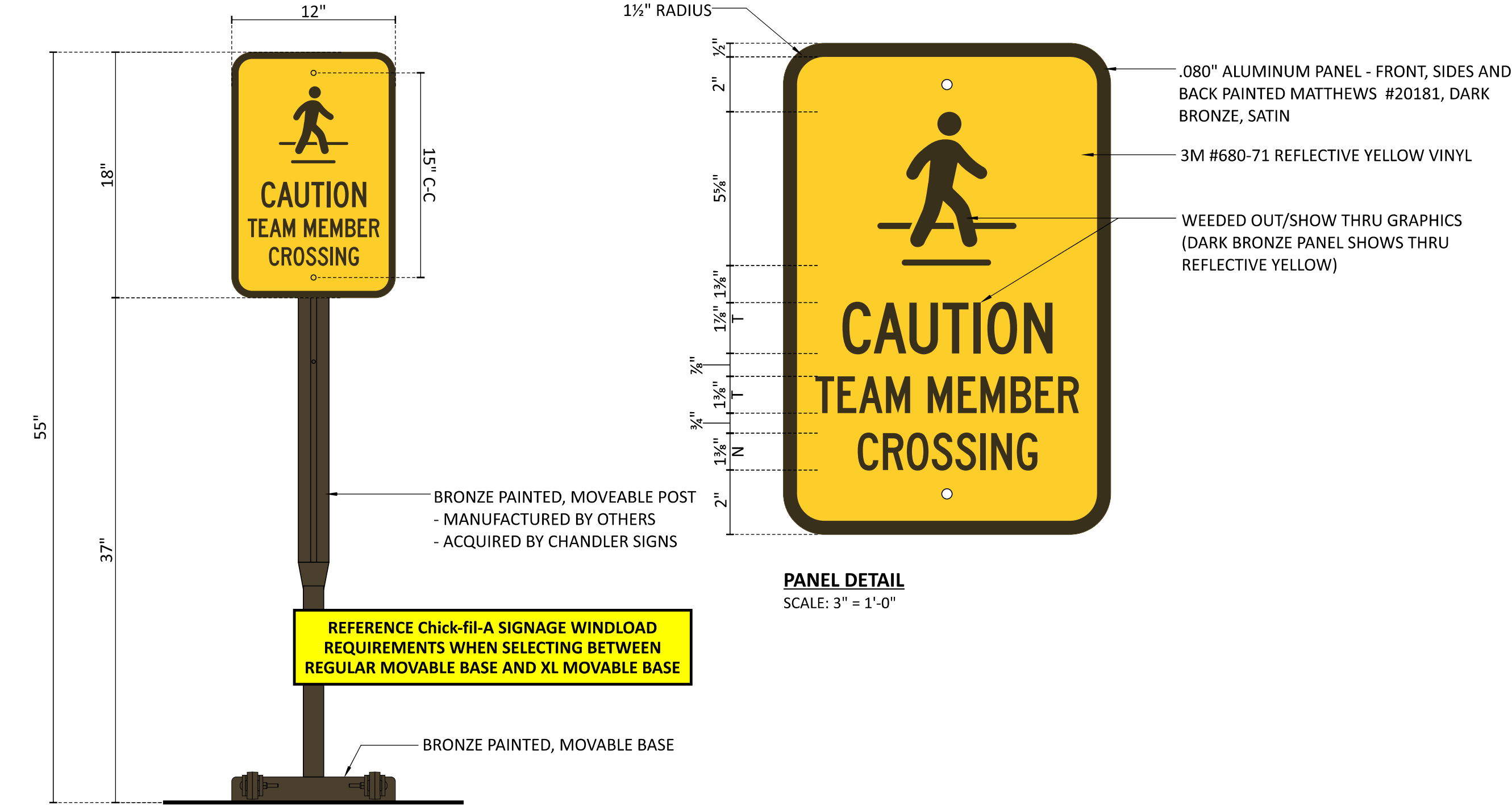
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L1 L2 SAFETY SIGN - TEAM MEMBER CROSSING SCALE: 1-1/2" = 1'-0"
TWO (2) REQUIRED - MANUFACTURE & INSTALL

PLEASE NOTE: PORTABLE BASE AND POST PROVIDED BY PATTISON.

DocuSigned by:
Michael Young
0DCEC3135B2844E...

DFW MANUFACTURING / NEW VIS 2022 MUTCD PANEL

Design #

0637033Ar3

Sheet

27 of 27

Client

#2859

Address

690 NW Blue Pkwy,
Lees Summit, MO

Account Rep.

KRISTEN HAMILTON
TERRI BROWN

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LEAH LANSFORD

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