GOVERNMENTAL AGENCIES

BUILDING DEPARTMENT

AGENCY: CITY OF LEE'S SUMMIT DEVELOPMENT SERVICES DEPARTMENT

PHONE #: 816.969.1200

DEVTECH@CITYOFLS.NET

FIRE MARSHALL

AGENCY: CITY OF LEE'S SUMMIT FIRE DEPARTMENT ADDRESS: 207 SE DOUGLAS, LEE'S SUMMIT, MO 64063 **CONTACT:** CHIEF JIM EDEN **PHONE #:** 816.969.1300

JIM.EDEN@CITYOFLS.NET

BUILDING DATA

PLUMBING CODE 2018 INTERNATIONAL PLUMBING CODE MECHANICAL CODE 2018 INTERNATIONAL MECHANICAL CODE 2018 INTERNATIONAL FUEL GAS CODE ELECTRIC CODE: 2017 NATIONAL ELECTRICAL CODE

ACCESSIBILITY CODE: 2009 ICC/ ANSI A117.1 ENERGY CODE: 2018 INTERNATIONAL ENERGY CONSERVATION CODE FIRE CODE: 2018 INTERNATIONAL FIRE CODE

EXIST. BUILDING OCCUPANCY EXIST. BLDG. CONSTRUCTION TYPE

EXIST. BUILDING AREA:

A2 (NO CHANGES) VB (SPRINKLERED, NO CHANGES 4,161 GSF (NO CHANGES)

135 OCCUPANTS (CHANGES)

EXISTING BLDG OCCUPANCY LOAD

OCCUPANT LOAD CALCULATION

DINING AREA: 1,539 SF / 15 SF/PERSON = 103

ORDER AREA:

KITCHEN / DT / SERVING / MULTI-PURPOSE **BUSINESS AREA (OFFICE)**

69 SF / 150 SF/PERSON = 1

137 OCCUPANTS

113 SF / 5 SF/PERSON = 23

1,936 SF / 200 SF/PERSON = 10

NEW TOTAL OCCUPANCY LOAD

PROPOSED NEW F2F CANOPY AREA:

PROPOSED NEW OMD CANOPY AREA:

SCOPE OF WORK

THESE DOCUMENTS REPRESENT AN ADDITION OF A NEW DUAL LANE OUTSIDE MEAL DELIVERY CANOPY ADDITION & DUAL LANE FACE TO FACE CANOPY AND PLAY AREA CONVERSION TO

ITEMS OF IMPORTANCE

- REFER TO CIVIL PLANS FOR EXTENT OF SITE WORK
- 2. EXISTING SITE ITEMS TO REMAIN UNLESS NOTED OTHERWISE.
- 3. F2F & OMD CANOPIES BY LANE
- 4. NO CHANGES TO BUILDING FOOTPRINT & OCCUPANCY TYPE. 5. EXISTING CANOPY AT DRIVE THRU SIDE TO BE REMOVED.

PROJECT GENERAL NOTES

- 1. ELECTRICAL WORK WILL BE PERFORMED UNDER THIS CONTRACT. ALL TO REMAIN UNLESS NOTED
- 2. ALL WORK SHALL BE IN COMPLIANCE WITH APPLICABLE FEDERAL, STATE AND LOCAL BUILDING CODES, REGULATIONS, ORDINANCES, STANDARDS INCLUDING ADA, OTHER HANDICAP ACCESSIBILITY CODES AND INSURANCE RATING BOARDS. NO WORK SHALL COMMENCE UNTIL ALL JURISDICTIONAL PERMITS AND APPROVALS ARE OBTAINED.
- 3. GENERAL CONTRACTOR SHALL COORDINATE WITH THE OWNER'S VENDORS REGARDING SCHEDULING AND SEQUENCING OF THE WORK.
- 4. THE CONSTRUCTION NOTES AND DRAWINGS ARE SUPPLIED TO ILLUSTRATE THE DESIGN AND GENERAL TYPE OF CONSTRUCTION DESIRED AND ARE INTENDED TO IMPLY THE FINEST QUALITY OF CONSTRUCTION. MATERIALS AND WORKMANSHIP THROUGHOUT AND SHALL CONFORM TO THE APPROPRIATE NATIONAL TRADE PUBLICATION.
- 5. IT SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO FULLY EXAMINE THE SITE SPACE PRIOR TO THE START OF CONSTRUCTION. THE G.C. SHALL VERIFY ALL DIMENSIONS, (VERTICAL, HORIZONTAL AND OTHERWISE), AS WELL AS TO VERIFY THE CONDITIONS AND NATURE OF THE PROPOSED CONSTRUCTION, MATERIALS, AVAILABLE UTILITIES AND STRUCTURAL ELEMENTS. THE G.C. SHALL NOTIFY THE OWNER'S REPRESENTATIVE (OWNER'S REP), IN WRITING OF ANY AND ALL DISCREPANCIES BETWEEN THE EXISTING CONDITIONS AND THE CONSTRUCTION DOCUMENTS.
- 6. IT SHALL BE THE JOINT RESPONSIBILITY OF THE G.C. AND ALL SUBCONTRACTORS AND SUPPLIERS OF MATERIALS TO SECURE ALL NECESSARY ADAPTATIONS AS MAY BE REQUIRED FOR THEIR RESPECTIVE WORK, PRIOR TO ORDERING, FABRICATION OR INSTALLATION OF ANY MATERIALS, EQUIPMENT OR COMPONENTS WHICH ARE TO BE INTEGRATED INTO THE WORK. NO CLAIMS FOR ADDITIONAL COMPENSATION SHALL BE MADE OR SHALL BE VALID UNLESS WRITTEN NOTIFICATION IS RECEIVED BY THE OWNER'S REP AND THE ADDITIONAL COMPENSATION IS APPROVED IN ADVANCE OF PROCEEDING WITH THE WORK.
- 7. REFERENCE ALL DRAWINGS FOR A COMPLETE DESCRIPTION OF THE WORK 8. COMMENCEMENT OF WORK IN ANY AREA BY THE CONTRACTOR SHALL BE CONSTRUED THAT THE CONTRACTOR HAS CHECKED THE EXISTING CONDITIONS AND FOUND THEM TO BE SATISFACTORY TO ACCEPT THIS PORTION OF THE WORK.
- 9. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL EXISTING UTILITIES WHETHER SHOWN IN THE DRAWINGS OR NOT & TO PROTECT THEM FROM DAMAGE DURING THE WORK. THE CONTRACTOR SHALL BEAR ALL EXPENSES OF REPAIR OR REPLACEMENT OF UTILITIES OR OTHER PROPERTY DAMAGED BY OPERATIONS IN CONJUNCTION WITH THE PERFORMANCE OF THE WORK.
- 10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE COMPLETE SECURITY OF THE SITE WHILE JOB IS IN PROGRESS & UNTIL JOB IS COMPLETED.
- 11. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS & SHALL MAINTAIN THE STRUCTURAL INTEGRITY OF ALL WORK.
- 12. RESTAURANT REFUSE/DUMPSTER SHALL NOT BE USED FOR CONSTRUCTION DEBRIS. 13. CAP AND SEAL OFF ANY PLUMBING/ELECTRICAL PENETRATIONS AS NECESSARY. DO NOT ABANDON ANY
- UTILITIES OR MATERIALS WITHIN THE SPACE REMOVE BACK TO THE SOURCE. 14. COVER RETURN AIR DUCTS AS NECESSARY BEFORE AND DURING CONSTRUCTION



5200 BUFFINGTON ROAD ATLANTA, GEORGIA 30349-2998 PHONE: (404) 765-8000 FAX: (404) 684-8550

S08N-104-R **CUSTOM PROJECT SOLUTIONS** DUAL LANE OUTSIDE MEAL DELIVERY CANOPY & DUAL LANE FACE TO FACE CANOPY ADDITION. PLAY AREA CONVERSION TO DINING

SUMMIT FAIR FSR #02859 690 NW BLUE PARKWAY,

LEE'S SUMMIT, MO 64086 **AUGUST 2023**

REVIS	REVISION SCHEDULE								
REVISION NUMBER	REVISION DATE	ISSUE DESCRIPTION	CHANGE DESCRIPTION	AFFECTED SHEETS					
1	02/19/24	PLAY AREA REMOVAL	-	G-000, ASP-1.1, D-201, D-221, A-005, A-201, A-211, A-221, A-601, A-620, M-1.1, M-2.1, F-201, F-211, F-701					
-	-	-	-	-					

ARCHITECT:

CIVIL

ENGINEER:

GBC DESIGN, INC

AKRON, OH 44320

PHONE: (330) 836-0228

565 WHITE POND DRIVE

CONTACT: JACK MEANEY, P.E.

INTERPLAN LLC. 220 E CENTRAL PKWY, SUITE 4000 ALTAMONTE SPRINGS, FL 32701 **AOR:** LAUREL MARTIN, R.A., NCARB **CONTACT:** JESSICA CHERKASSKY PHONE (407) 645-5008 FAX (407) 629-9124 EMAÎL: JCHERKASSKY@INTERPLANLLC.COM

ENGINEER: INTERPLAN LLC SUITE 4000

ELECTRICAL

220 E CENTRAL PKWY, ALTAMONTE SPRINGS, FL 32701 PHONE: (407) 645-5008 ENGINEER OF RECORD: STACY HENSON

CANOPY

SUPPLIER

PLUMBING MECHANICAL ENGINEER: ENGINEER:

INTERPLAN LLC

STACY HENSON

SUITE 4000

FL 32701

220 E CENTRAL PKWY,

ALTAMONTE SPRINGS

PHONE: (407) 645-5008

ENGINEER OF RECORD:

220 E CENTRAL PKWY, SUITE 4000 ALTAMONTE SPRINGS, PHONE: (407) 645-5008 ENGINEER OF RECORD: STACY HENSON CONTACT: MARYANA IBRAHIM CONTACT: MARYANA IBRAHIM CONTACT: MARYANA IBRAHIM

INTERPLAN LLC

LANE SUPPLY, INC. 120 FAIRVIEW ARLINGTON, TX 76010 CONTACT: LARRY TOLBERT PHONE: (817) 261-9116

DRAWING INDEX

ARCHITECTURAL

COVER SHEET

ARCHITECTURAL SITE PLAN- F2F CANOPY

DEMOLITION FLOOR PLAN DEMOLITION REFLECTED CEILING PLAN

FINISH SCHEDULE PROPOSED FLOOR PLAN

PROPOSED REFLECTED CEILING PLAN INTERIOR DETAILS

MECHANICAL

MECHANICAL FLOOR PLAN MECHANICAL SPECIFICATIONS & SCHEDULES

PLUMBING

OMD GAS PLUMBING PLAN F2F GAS PLUMBING PLAN PLUMBING DETAILS

ELECTRICAL

CANOPY POWER & LIGHTING PLAN CANOPY ELECTRICAL DETAILS

FUŘŇIŤUŘĚ

FURNITURE FLOOR PLAN FURNITURE CORE DRILL PLAN DECOR ELEVATIONS

F2F CANOPY

CANOPY FOOTING LOCATIONS

CANOPY FOOTINGS CANOPY FRAMING PLAN

CANOPY SECTIONS CANOPY ELEVATION PLAN

OMD CANOPY

CANOPY FOOTING LOCATIONS

CANOPY LIGHT LAYOUT

CANOPY FOOTINGS CANOPY FOOTINGS

CANOPY FRAMING PLAN CANOPY SECTIONS

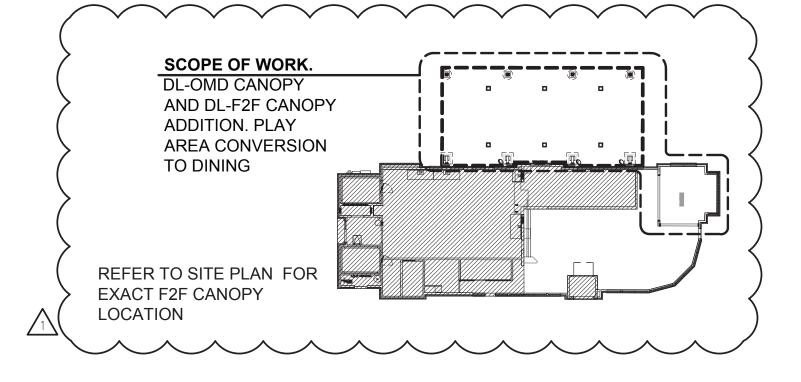
CANOPY SECTIONS

CANOPY ELEVATION PLAN









KEY PLAN





Atlanta, Georgia 30349-2998

5200 Buffington Road

INTERPLAN

ARCH COA #2015008774

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 3270 407.645.5008

ENG COA #2005026904



LAUREL R MARTIN - ARCHITECT

FSR#02859

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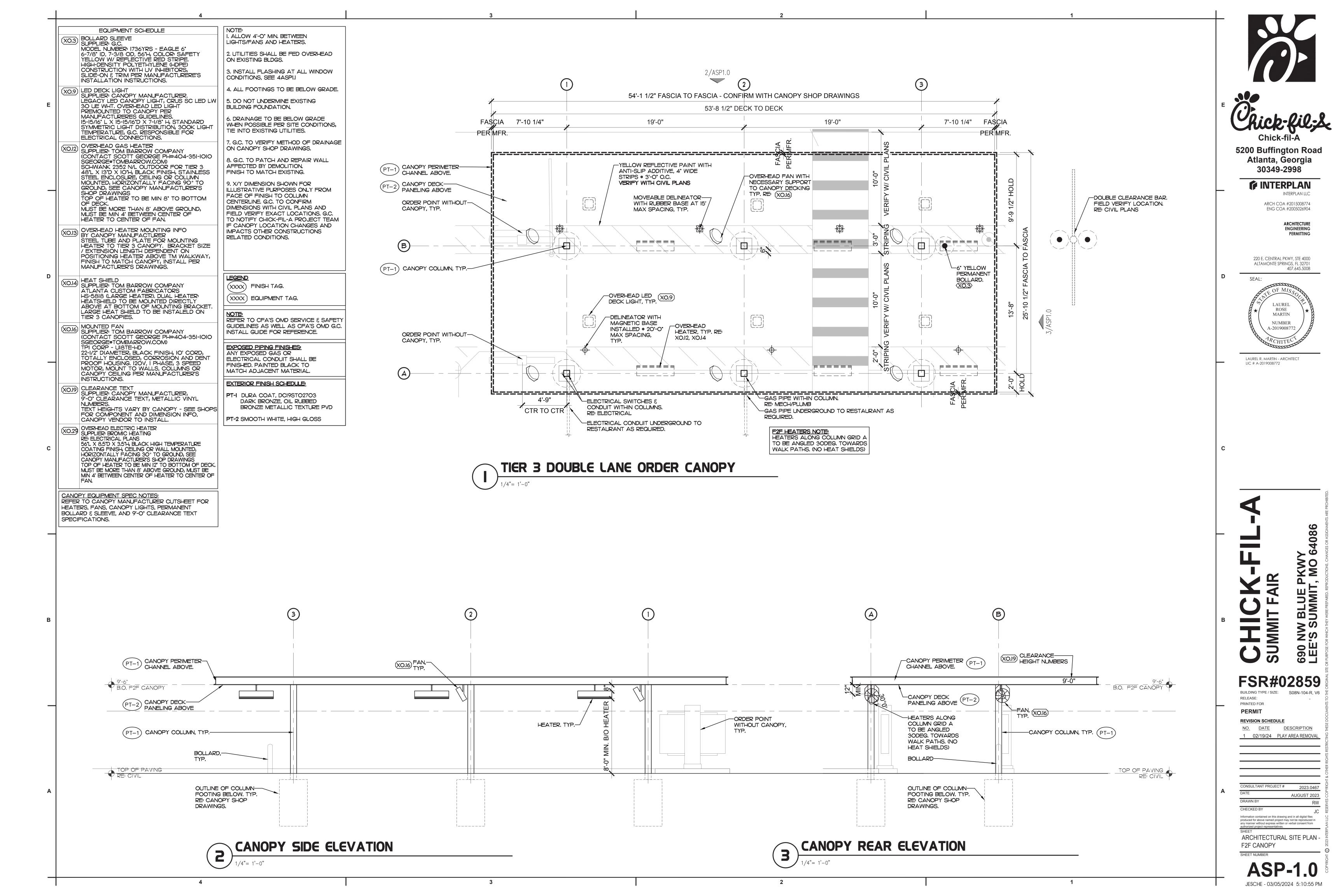
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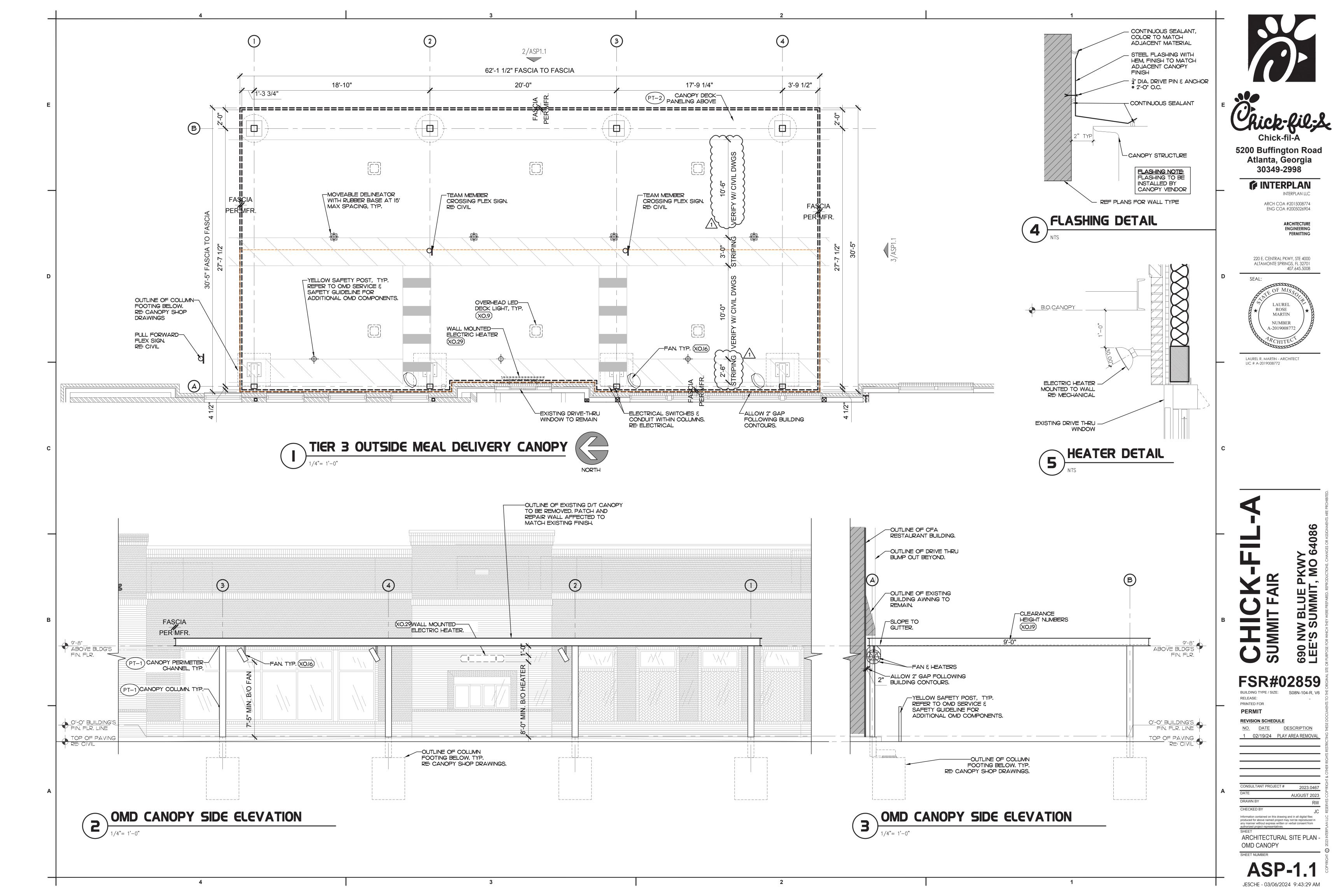
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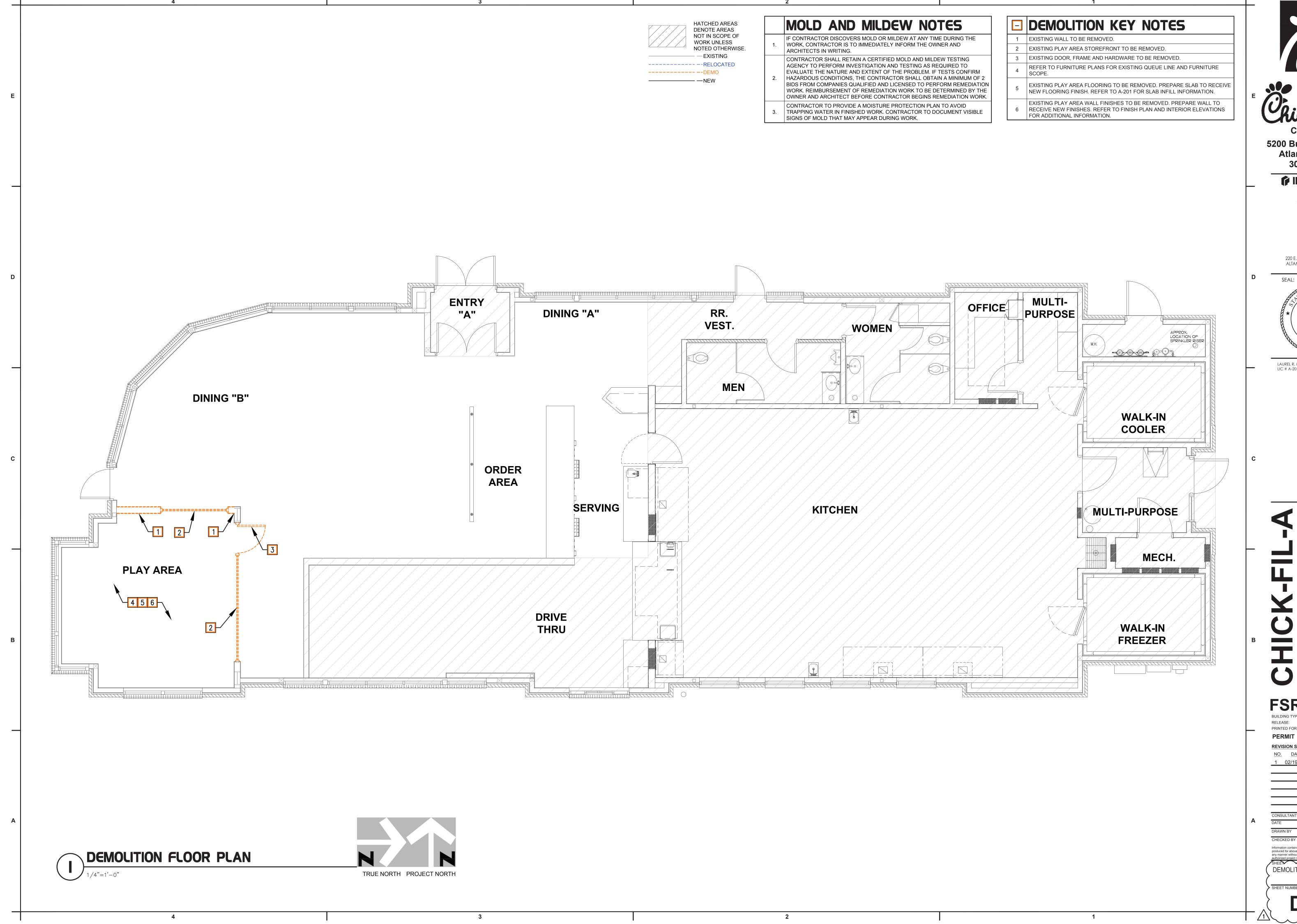
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COVER SHEET

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INTERPLAN

ARCH COA #2015008774 ENG COA #2005026904

ARCHITECTURE

PERMITTING

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008

MARTIN NUMBER

LAUREL R. MARTIN - ARCHITECT LIC # A-2019008772

FSR#02859

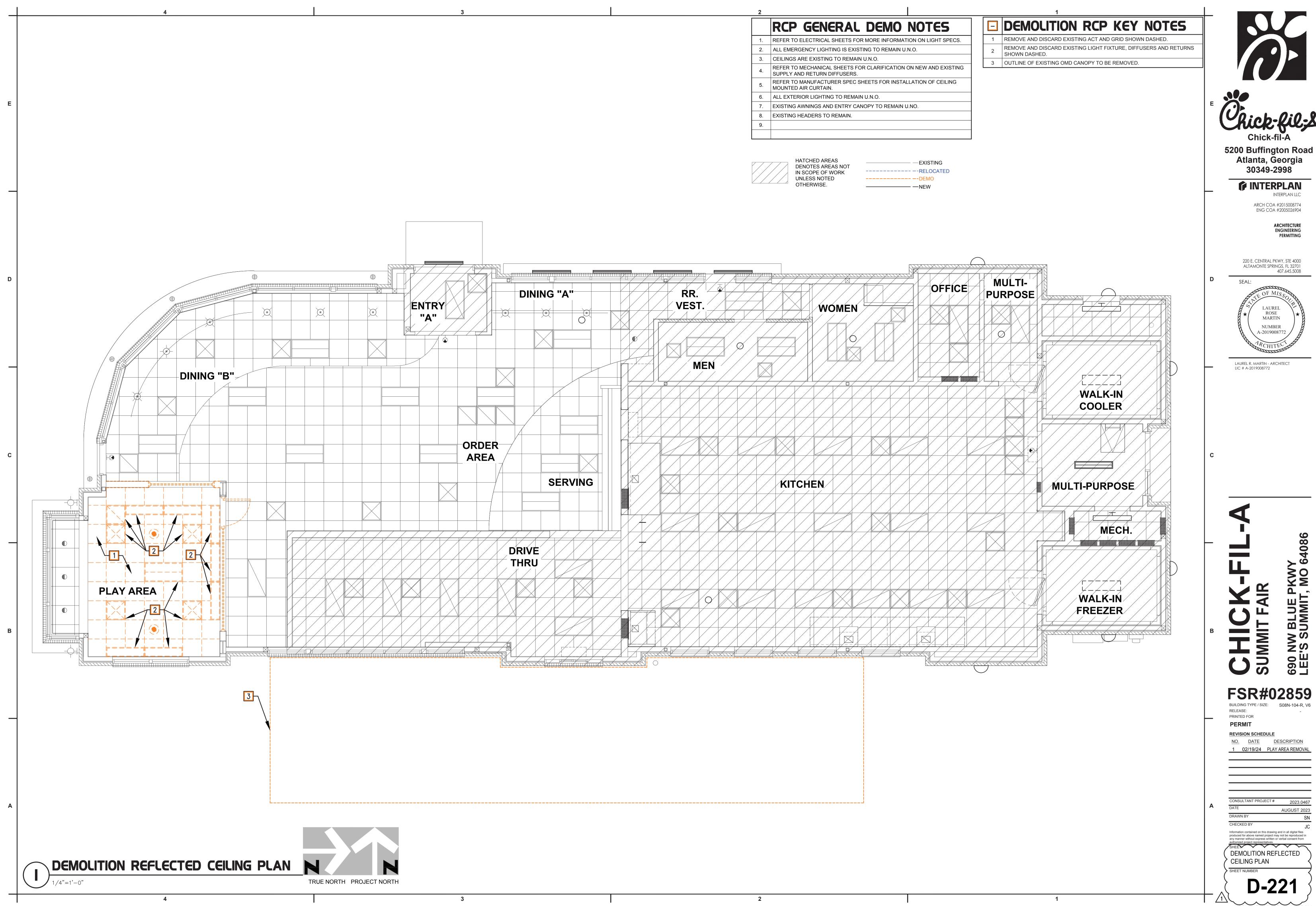
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NO. DATE DESCRIPTION

DEMOLITION FLOOR PLAN



Atlanta, Georgia 30349-2998

INTERPLAN LLC

ARCH COA #2015008774

PERMITTING



DEMOLITION REFLECTED

•	INITCDIOD CINICII CCIICDIII C		
	INTERIOR FINISH SCHEDULE		FLOOD FINISHES
	CEILING FINISHES ACOUSTICAL CEILING TILE		FLOOR FINISHES
ACT-2	CERTAINTEED CEILING TILE CERTAINTEED CEILINGS, PERFORMA SYMPHONY M, #1222BF-IOF-1, 24" X 24" X 3/4" WHITE GRID: ELITE NARROW REVEAL (CORNER BEVEL) 9/16" GRID, WHITE [VERIFY EXISTING ACT SPECIFICATION, SEE NOTE BELOW]	G-1	FLOOR TILE GROUT (T-3 AND T-4, USE WITH PORCELAIN TILE) MAPEI, ULTRA COLOR GROUT 47 / CHARCOAL
2T-1A	PRIMARY INTERIOR CEILING PAINT SHERWIN WILLIAMS, PRO MAR 200 ZERO VOC PAINT SW-7011 / NATURAL CHOICE, FINISH: FLAT (SEMI-GLOSS ON HARDIE PANEL)	T-3	PORCELAIN TILE CREATIVE MATERIALS CORPORATION LAVA LIGHT GRAY, 12"X12" GROUT: G1, JOINT WIDTH: 3/16"
	PRIMARY INTERIOR CEILING PAINT SHERWIN WILLIAMS, PRO MAR 200 ZERO VOC PAINT		MISCELLANEOUS FINISHES
PT-3A	SW7600/ BOLERO, FINISH: FLAT		ROLLER SHADE PHIFER SHEERWEAVE 4000 U61 ECO/GREYSTONE, 5% OPENNESS - NOTCHLESS 4" FASCIA,
	WALL FINISHES	RS-1	DARK BRONZE TO MATCH STOREFRONT COLOR, ROLLEASE SKYLINE CLUTCH, (HEAT SEALED
	PRIMARY INTERIOR WALL PAINT		INTERNAL POCK HEM BAR), 110LB STAINSTEEL ROLLEASE CHAIN, CHAIN LOCATED AT JAMB ONLY, NOT IN CENTER WINDOW RE: INTERIOR ELEVATIONS
PT-1B	SHERWIN WILLIAMS, PRO MAR 200 ZERO VOC PAINT SW-7011 / NATURAL CHOICE, FINISH: EGGSHELL		
WD-3	WAINSCOTING PER NATIONAL ACCOUNT 1/4" PLYWOOD (RED OAK, PLAIN CUT LAUAN CORE WITH METAL TRIM) CUSTOM, FINISH: RED OAK STAINED MINWAX DRIFTWOOD. RE: DETAILS AND SHOP DRAWINGS FROM MANUFACTURER.		
	WALL BASES	1	
T-4	PORCELAIN TILE COVE BASE CREATIVE MATERIALS CORPORATION LAVA LIGHT GRAY, 6"X12" COVE BASE GROUT: G1, JOINT WIDTH: 3/16"	_	
	INTERIOR FINISH NOTES		EXTERIOR FINISH NOTES
R(PI W	ROVIDE 5" HIGH BAND OF 1/2" CEMENTITIOUS BOARD AT BASE OF ALL WALLS IN DINING DOMS AND VESTIBULES, 12" HIGH AT BASE OF KITCHEN WALLS. FOR ALL WALLS WITH TILE - ROVIDE FULL COVERAGE OF CEMENT BOARD SUBSTRATE FROM FLOOR TO THE HEIGHT OF YALL TILE. CEMENTITIOUS BOARD SHALL BE "DUROCK" BY U.S. GYPSUM. RE: INTERIOR LEVATIONS.	ACTU 2. REF	SHES LISTED IN THIS SCHEDULE DO NOT REPRESENT ORIGINAL PROTOTYPE FINISHES. CONFIRM AL FINISHES TO MATCH ON SITE. ER TO EXTERIOR ELEVATIONS FOR AWNING TYPES AND CORRESPONDING FINISH.
W	OLLER SHADE WIDTH DIMENSIONS TO BE 2" LESS THAN THE FINISHED DIMENSION OF EACH INDOW TO ACCOUNT FOR WAINSCOT TOP CAP RETURNING TO STOREFRONT - VALENCE WILL AINTAIN FULL LENGTH & ROLLER SHADE WILL BE 2" LESS THAN TOTAL MEASUREMENT.	TO EX	C. TO OBTAIN PAINT, COLOR, BRICK, MATERIAL SAMPLES AND TAKE PHOTOS OF SAMPLES NEXT ISTING BUILDING IN FIELD. SEND PICTURES OF SAMPLES TO ARCHITECT, CFA CONSTRUCTION AGER, AND CHICK-FIL-A DESIGN TEAM FOR APPROVAL BEFORE START OF CONSTRUCTION AS TO DELAY THE PROJECT.
	T T-2/CT-45 OUTSIDE CORNERS IN PUBLIC AREAS. USE BLANKE (RE: TR-1) TRIM STRIP. SEE ATIONAL ACCOUNTS FOR ORDERING INFORMATION.		NOTES: MANUFACTURER, COLOR, AND MODEL NUMBERS WITH EXTERIOR FINISH SCHEDULE
IN	OR WAINSCOTING WHERE GRAPHIC MESSAGE EXTENDS ABOVE TOP HORIZONTAL TRIM CAP, ISTALLER TO FIELD CUT VERTICAL BATTENS AND TOP CAP AT GRAPHICS AS REQUIRED. OORDINATE WITH CHARTER HOUSE.	1. B 1.1. 1.2. 1.3.	SITE SIGNAGE (MAIN ID, SECONDARY ID, DIRECTIONAL, VERIFY OTHER POSSIBLE SIGNAGE) NEW CANOPIES AT MAIN ENTRANCE AND DRIVE-THRU AWNING FRAMES (VERIFY FABRIC WITH EXTERIOR FINISH SCHEDULE)\
	OR CEILING FINISHES, IF PATCHING AND REPAIRING ACT, VERIFY EXISTING SPECIFICATION RIOR TO ORDERING.	1.4. 1.5.	DRIVE-THRU ORDER POINTS/MENU BOARDS DRIVE-THRU CLEARANCE BARS
Ν	OR EXISTING RESTAURANTS THAT NEED 6 INCH TILE FOR REPAIR, THE INSTALLER SHOULD SPECIFY EEDING A COVE BASE (DAL TILE LAVA LIGHT GREY SPEC) WITH A 6 INCH HEIGHT AND ORDER IRECTLY FROM DALTILE (CHICK-FIL-A@DALTILE.COM).		ARK BRONZE SITE METALS, NOT MENTIONED ABOVE, INCLUDING BUT NOT LIMITED TO: BOLLARDS, DUMPSTER GATE POSTS, LIGHT POLES, HANDRAILS BUILDING METALS, NOT MENTIONED ABOVE, INCLUDING BUT NOT LIMITED TO: LIGHT FIXTURES, DOWNSPOUTS, SCUPPERS NEW BUILDING PARAPET COPINGS (IF APPLICABLE) EXISTING BUILDING PARAPET COPINGS (REPAINT TO MATCH NEW) - IF APPLICABLE

> **INTERPLAN** INTERPLAN LLC

> > ARCH COA #2015008774 ENG COA #2005026904

ARCHITECTURE ENGINEERING PERMITTING

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008



LAUREL R. MARTIN - ARCHITECT LIC # A-2019008772

690 NW BLUE PKWY LEE'S SUMMIT, MO 64086

FSR#02859
BUILDING TYPE / SIZE: S08N-104-R, V6 RELEASE:

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REVISION SCHEDULE

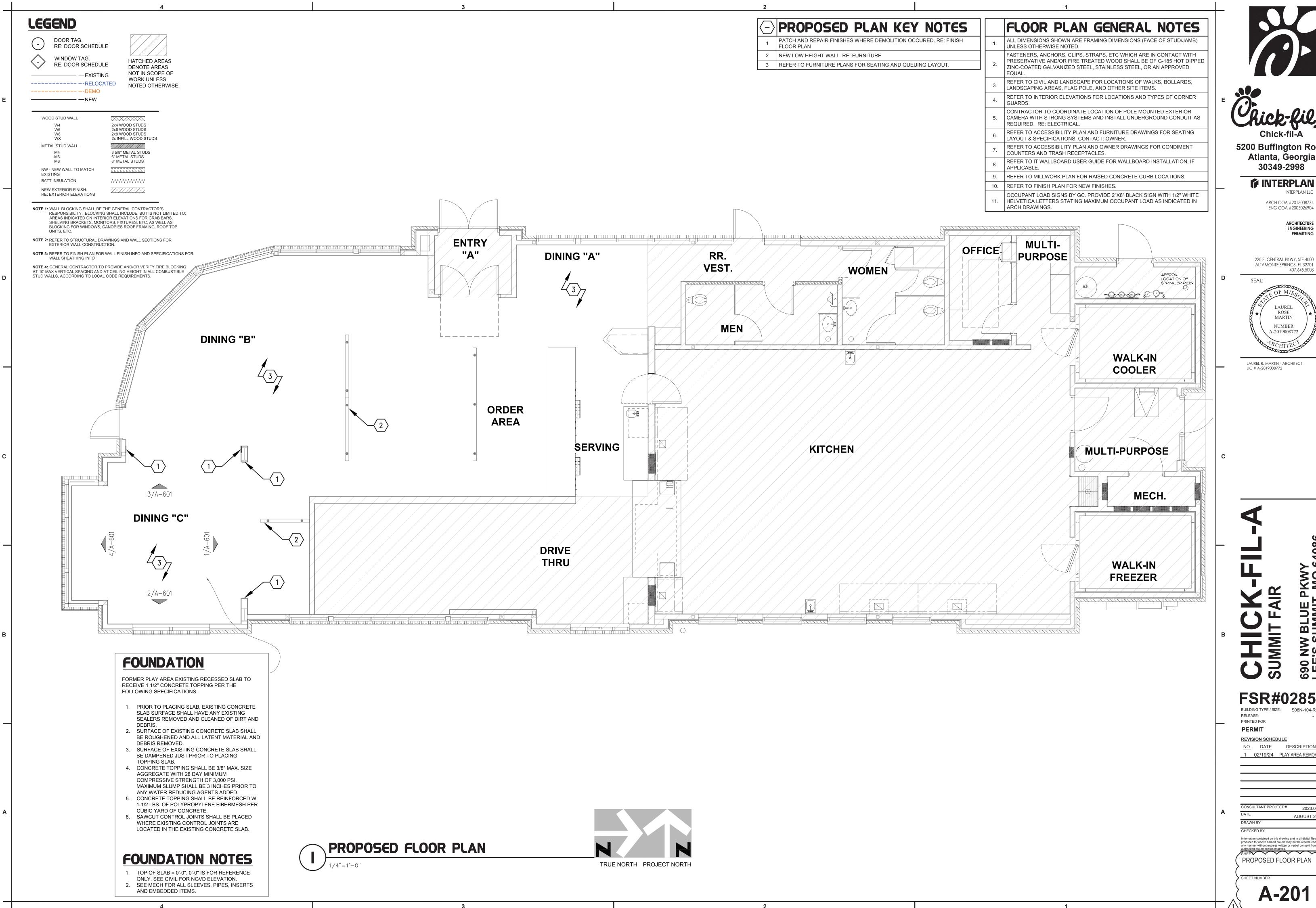
NO. DATE DESCRIPTION 1 02/19/24 PLAY AREA REMOVAL

CONSULTANT PROJECT # 2023.0467

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SHEET

FINISH SCHEDULE



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ARCHITECTURE

PERMITTING

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701



LAUREL R. MARTIN - ARCHITECT LIC # A-2019008772

FSR#02859

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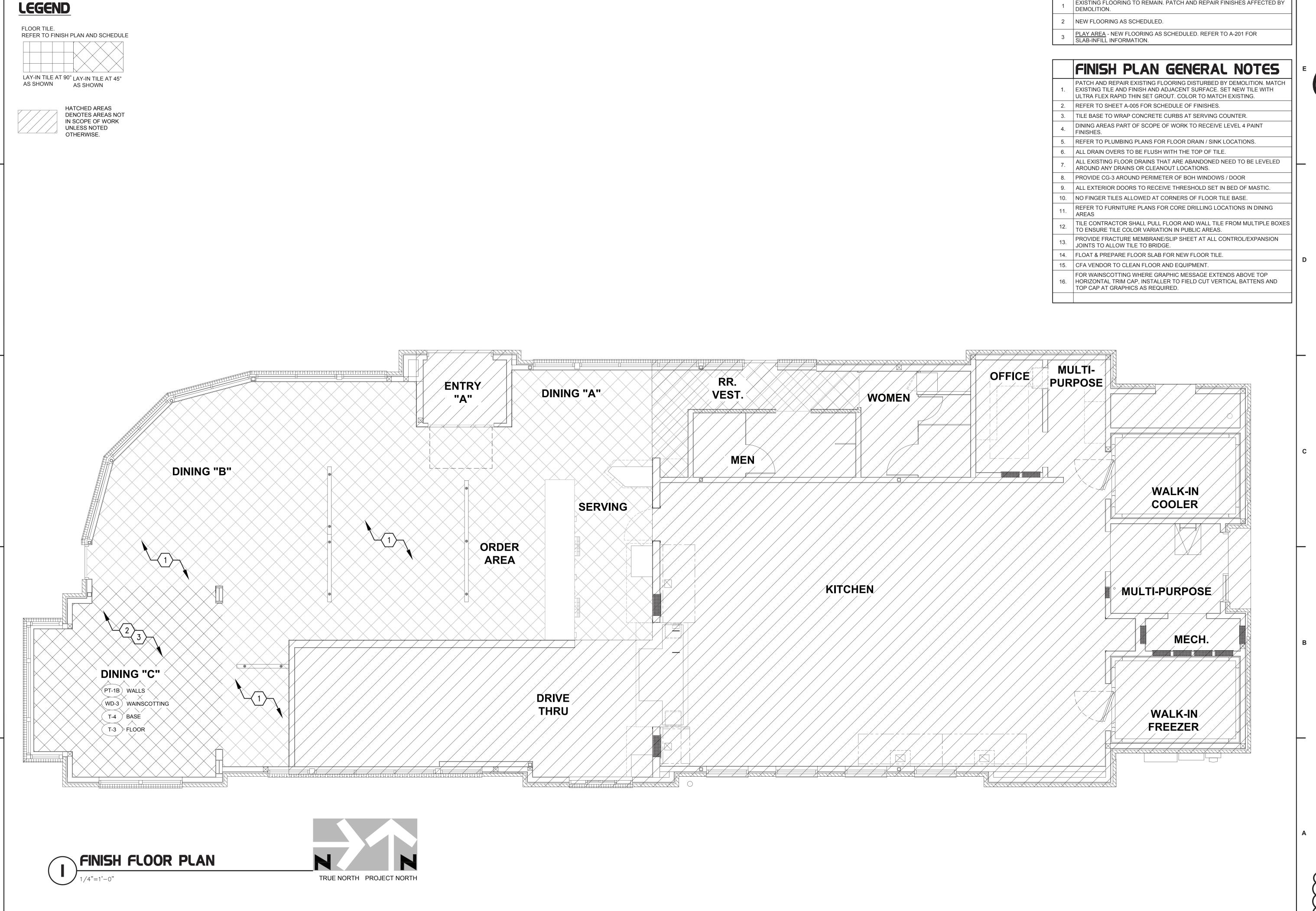
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PROPOSED FLOOR PLAN





FINISH PLAN KEY NOTES

EXISTING FLOORING TO REMAIN. PATCH AND REPAIR FINISHES AFFECTED BY

5200 Buffington Road Atlanta, Georgia 30349-2998

> **INTERPLAN** INTERPLAN LLC

> > ARCH COA #2015008774 ENG COA #2005026904

> > > ARCHITECTURE

220 E. CENTRAL PKWY, STE 4000

ALTAMONTE SPRINGS, FL 32701 407.645.5008



LAUREL R. MARTIN - ARCHITECT LIC # A-2019008772

690 NW BLUE PKWY LEE'S SUMMIT, MO 64086

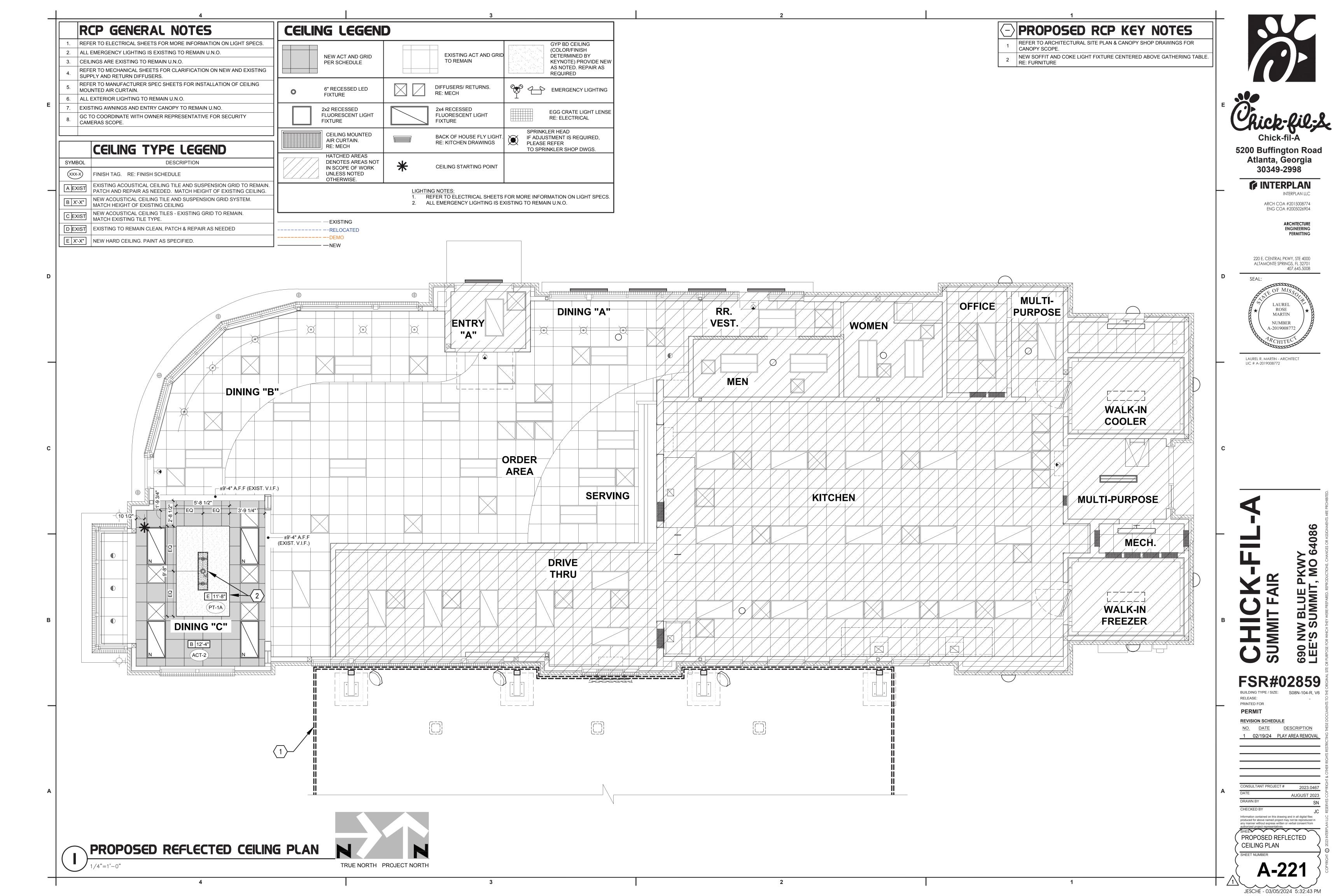
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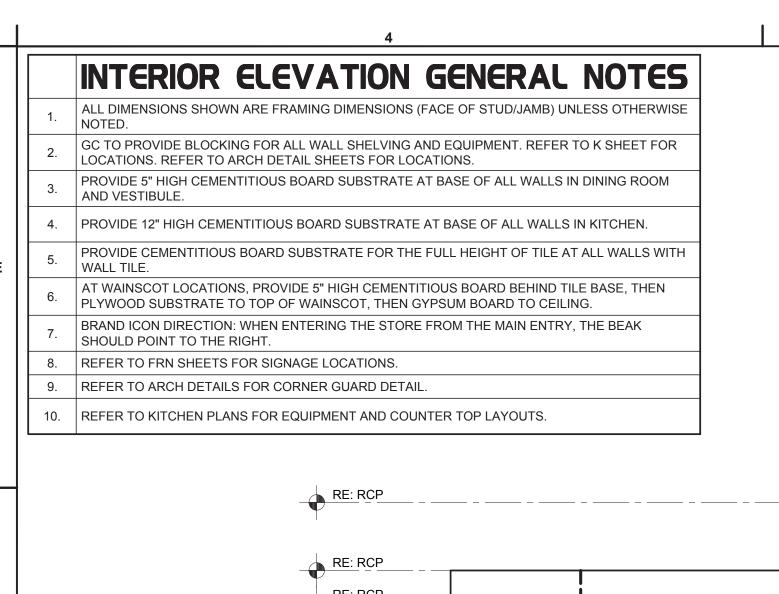
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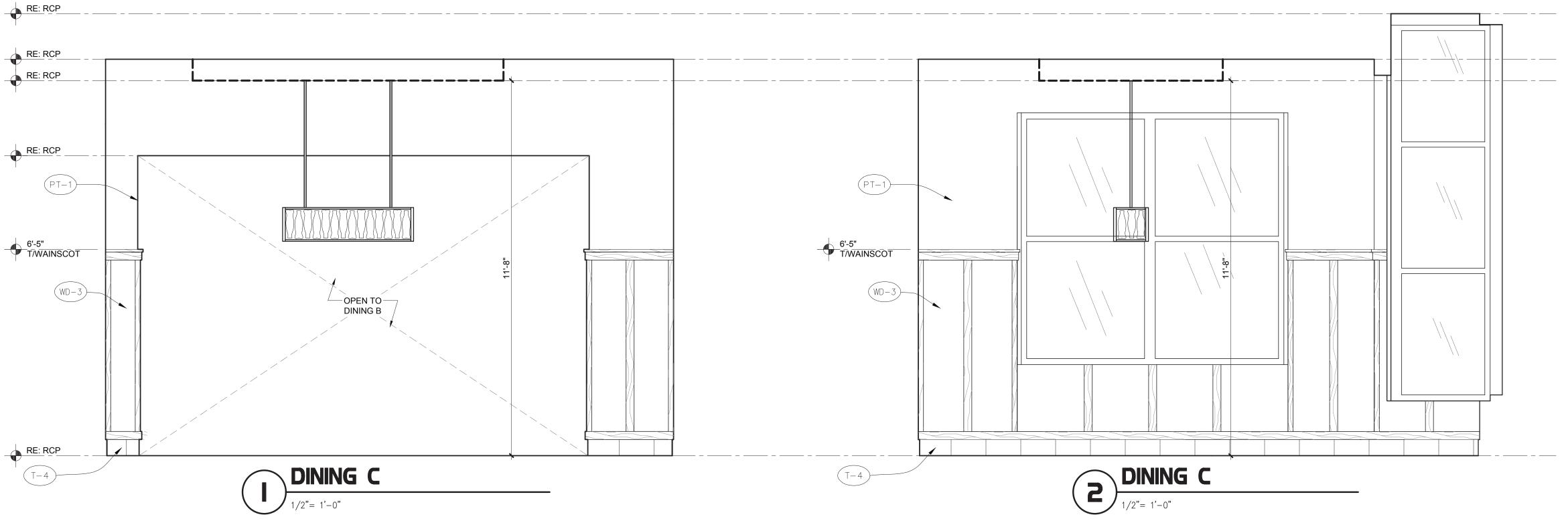
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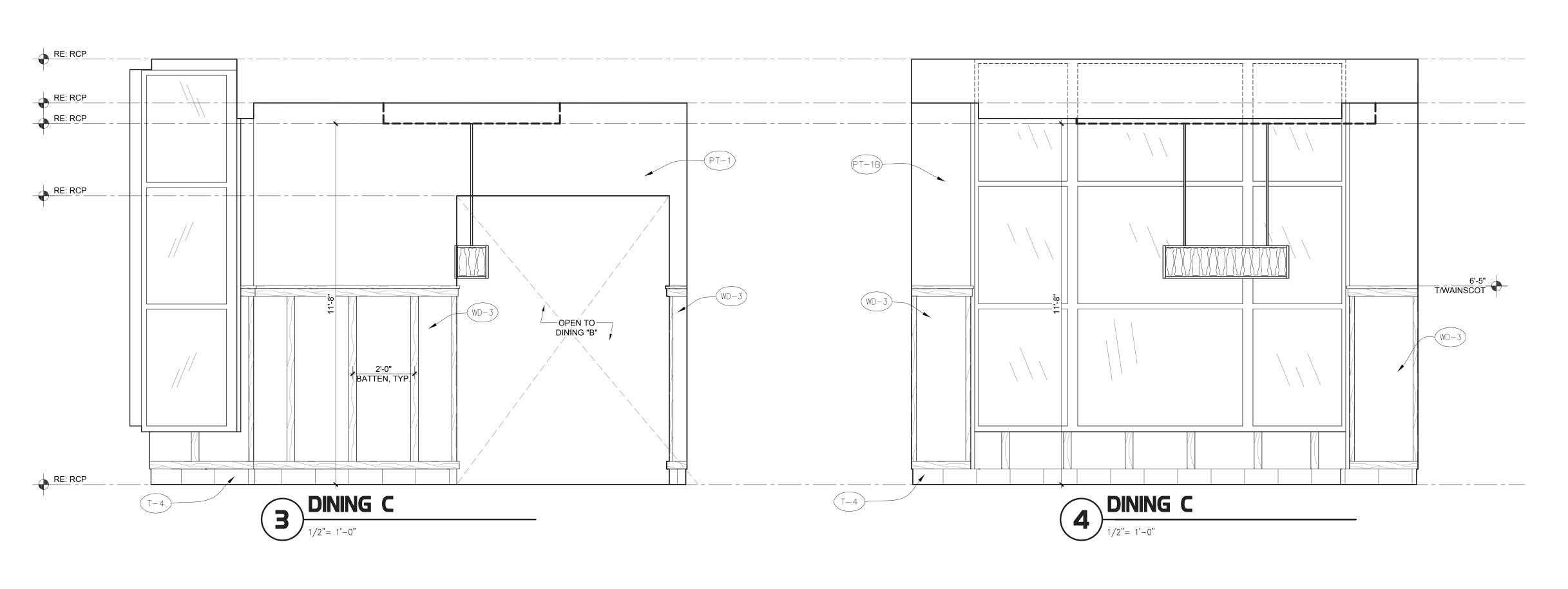
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Chick-fil-A

5200 Buffington Road Atlanta, Georgia 30349-2998

INTERPLAN

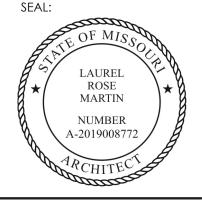
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ARCHITECTURE ENGINEERING

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008

407.645.500



LAUREL R. MARTIN - ARCHITECT LIC # A-2019008772

CHICK-FIL-A
SUMMIT FAIR

FSR#02859

SUILDING TYPE / SIZE: S08N-104-R, V6

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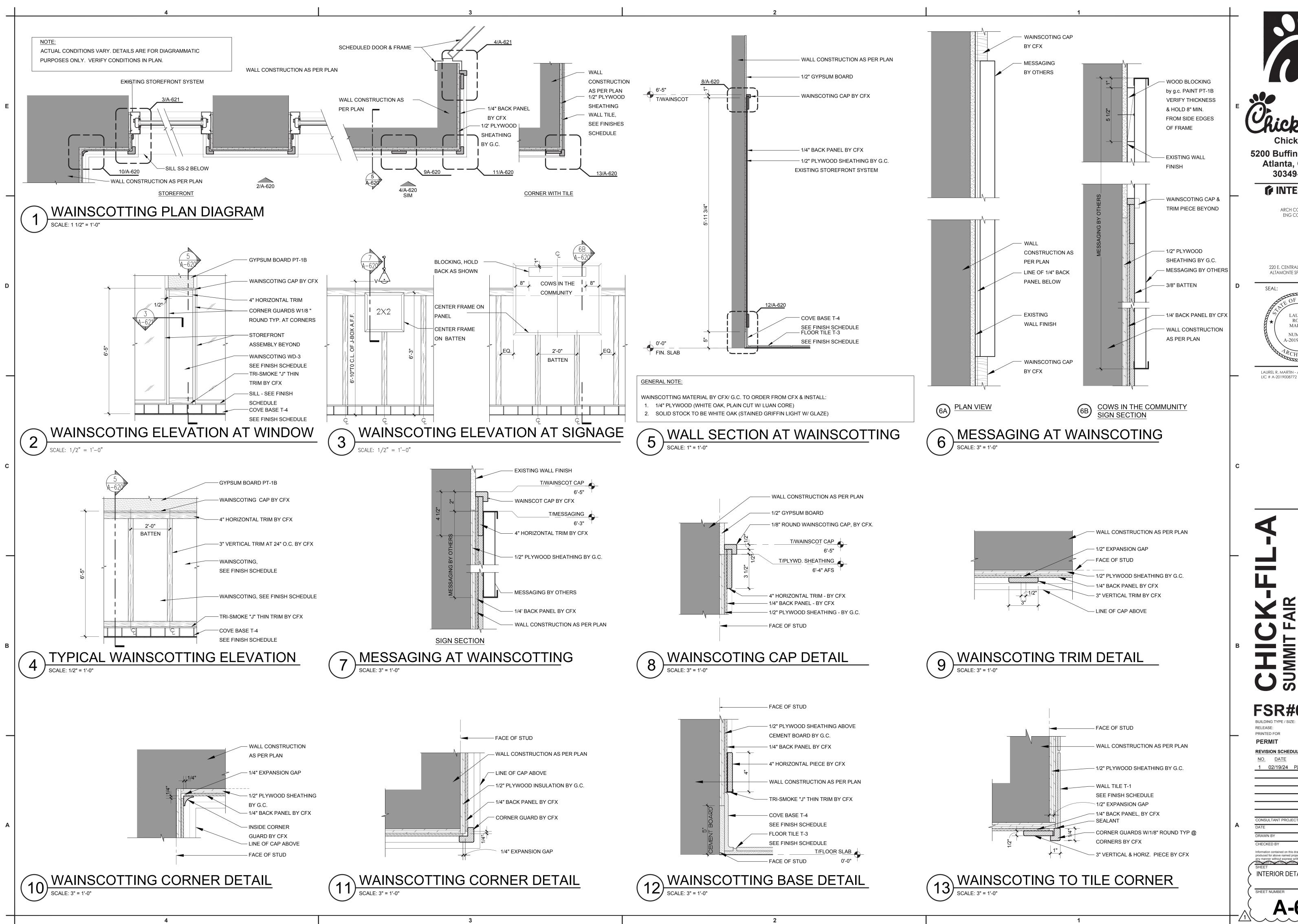
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SHEEN

INTERIOR ELEVATIONS

A-601

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ARCHITECTURE ENGINEERING PERMITTING

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LAUREL R. MARTIN - ARCHITECT

690 NW BLUE PKWY LEE'S SUMMIT, MO 64086

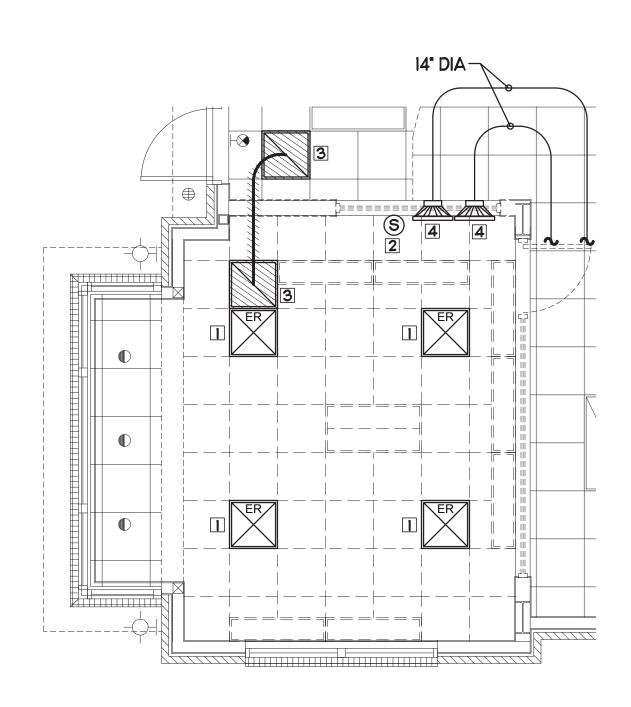
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CONSULTANT PROJECT # 2023.0467

authorized project representatives INTERIOR DETAILS SHEET NUMBER

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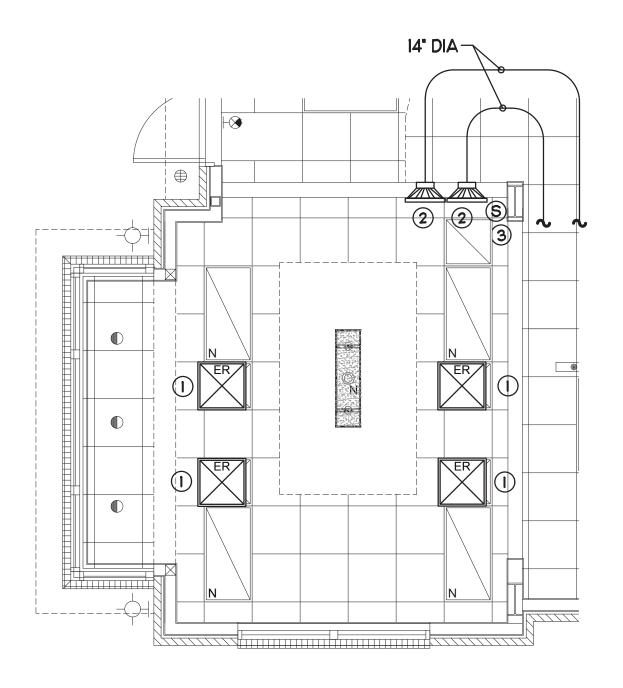


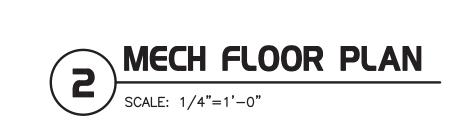
DEMOLITION KEY NOTES

- ☐ EXISTING AIR DEVICE TO BE RELOCATED.
- 2 EXISTING REMOTE TEMPERATURE SENSOR TO BE RELOCATED.
- 3 DEMOLISH EXISTING TRANSFER AIR GRILLS.
- 4 EXISTING AIR DEVICE TO REMAIN.

DEMO	DLITION LEGEND
	EXISTING EQUIPMENT, DUCT, AIR DEVICES ETC. TO REMAIN INTACT.
	EXISTING EQUIPMENT, DUCT, AIR DEVICES ETC. TO BE DEMOLISHED.

	HVAC LEG	END	
A-12-400	TYPE - NECK SIZE - CFM	EF#I	EXHAUST FAN #I (TYP.)
—	SPIN-IN FITTING WITH MANUAL BALANCING DAMPER, WITHOUT SCOOP	AC#I	AIR CONDITIONING UNIT #I
Ф—✓≫	□ □ ○ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □		RETURN/EXHAUST (TYP.)
Ф—√⊠	EXISTING EQUIPMENT, DUCT, ξ AIR DEVICE	\boxtimes	SUPPLY DIFFUSER, SQ FACE
Ф—√⊠	NEW EQUIPMENT, DUCT, & AIR DEVICE	①	PLAN NOTE REFERENCE
\bigcirc	THERMOSTAT	-	MANUAL VOLUME DAMPER





MECH. KEY NOTES

- 1 EXISTING AIR DEVICE TO BE RELOCATED.
- 2 EXISTING AIR DEVICE TO BE REMAIN.
- 3 RELOCATE AC#3 THERMOSTAT WALL MOUNTED AT 5'-O" AFF, ROUTE WIRING BACK TO SUNCOAST CONTROL PANEL.



Atlanta, Georgia 30349-2998

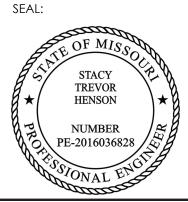
INTERPLAN LLC

ARCH COA #2015008774 ENG COA #2005026904

> ARCHITECTURE ENGINEERING PERMITTING

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008

05.41



STACY HENSON - P.E. LIC # PE-2016036828

CHICK-FIL-A SUMMIT FAIR

FSR#02859

BUILDING TYPE ARELEASE:
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NO. DATE DESCRIPTION
01 02/19/24 PLAY AREA REMOVAL

CONSULTANT PROJECT # 2023.0467

DATE

AUGUST 2023

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SHEET

MECHANICAL FLOOR PLAN

SHEET NUMBER

M1.1

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		LOGATION	1 = 01 / 01 = =	E4.0E.0ITE		DE 44 D 40
MARK	DESCRIPTION	LOCATION	NECK SIZE	FACE SIZE	FRAME TYPE	REMARKS
A	PRICE MODEL APDC ALUMINUM SUPPLY AIR DIFFUSER WITH INDIVIDUALLY ADJUSTABLE CURVED AIR PATTERN CONTROLLERS.	DINING AREA KITCHEN TEAM MEMBER	SEE PLAN	24X24	LAY-IN	l,2
NOTES	MECHANICAL CONTRACTOR SHALL PURCHAS COMPANY, CONTACT MR, SCOTT GEORGE AT NOT PURCHASED THRU TOM BARROW COMPA	404-351-1010, FO	R PRICING A			CES

. SECTION CI5000 - MECHANICAL SPECIFICATIONS

PART I - GENERAL

- A. IT IS THE RESPONSIBILITY OF CONTRACTOR TO READ ALL SPECIFICATIONS AND CONSULT ALL DRAWINGS WHICH MAY AFFECT THE INSTALLATION AND COORDINATION OF HIS WORK WITH OTHER TRADES, CONTRACTOR SHALL COORDINATE AND MAKE MINOR ADJUSTMENTS IN LOCATION OF EQUIPMENT AND MATERIALS AS NECESSARY TO SECURE COORDINATION.
- B. COMPLETED INSTALLATION SHALL CONFORM TO ALL APPLICABLE FEDERAL, STATE AND LOCAL CODES AND ORDINANCES, INCLUDING BUT NOT LIMITED TO THE LATEST APPROVED EDITIONS OF NFPA-96, NFPA-90A, NFPA-54, SMACNA, ASHRAE 90.1 AND ASHRAE 62.
- C. SYSTEM LAYOUT IS SCHEMATIC AND EXACT LOCATIONS SHALL BE DETERMINED BY STRUCTURAL CONDITIONS, COORDINATION WITH OTHER TRADES, COORDINATION WITH FINISHES AND OTHER CONDITIONS, STRUCTURAL SUPPORTS SHALL NOT BE CUT OR ALTERED TO ASSURE FIT OF HVAC SYSTEM. TEN FOOT CLEARANCE SHALL BE MAINTAINED BETWEEN OUTSIDE AIR INTAKES AND EXHAUST FANS AND PLUMBING VENT TERMINALS.
- D. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEFECTS, REPAIRS AND REPLACEMENTS IN MATERIALS AND WORKMANSHIP FOR A PERIOD OF ONE (1) YEAR AFTER FINAL PAYMENT IS APPROVED. CONTRACTOR SHALL HONOR FACTORY WARRANTIES ON ALL EQUIPMENT PROVIDED AS PART OF THIS SYSTEM.
- E. UPON COMPLETION OF PROJECT, ALL SYSTEM EQUIPMENT AND MATERIALS SHALL BE IN NEW, CLEAN CONDITION WITH ALL DAMAGE RESTORED TO CONDITION ACCEPTABLE TO THE OWNERS REPRESENTATIVE. ALL EQUIPMENT, COMPONENTS AND DUCTWORK SHALL BE INSPECTED AND THOROUGHLY CLEANED, READY FOR USE, AT COMPLETION OF JOB, ALL MISCELLANEOUS TOOLS, SCAFFOLDING, SURPLUS MATERIALS, RUBBISH AND DEBRIS SHALL BE REMOVED BY CONTRACTOR.
- F. CONTRACTOR SHALL PROVIDE TWO SETS OF 2" MERV 8 OR HIGHER THROW AWAY TYPE FILTERS. A CLEAN SET SHALL BE PROVIDED PRIOR TO TEST AND BALANCE AND AGAIN PRIOR TO OPENING.

- 2.01 DUCTWORK (C15735)
- A. ACCEPTABLE MANUFACTURERS OF INSULATION ARE MANVILLE, OWENS CORNING OR KNAUF.
- B. ALL DUCTWORK SHALL BE SHEET METAL, UNLESS NOTED OTHERWISE (U.N.O.).
- C. DUCT DIMENSIONS SHOWN ARE INSIDE CLEAR DIMENSIONS, U.N.O.
- D. CONSTRUCTION OF DUCTWORK SHALL MEET SMACNA I' W.C. PRESSURE CLASS STANDARD AND RECOMMENDATIONS. SMACNA SHALL BE FOLLOWED WITH RESPECT TO GAGE THICKNESS, JOINTS, REINFORCING, CONSTRUCTION, INSTALLATION AND SUPPORT FOR PRESSURE CLASS STATED. ALL TRANSVERSE JOINTS IN RECTANGULAR AND ROUND DUCT INCLUDING DUCT CONNECTION TO AIR DEVICE COLLAR SHALL BE SEALED PER SMACNA SEAL CLASS C WITH U.L. DUCT MASTIC SEALANT APPROVED FOR INTENDED USE. DUCT TAPE IS NOT AN ACCEPTABLE SUBSTITUTE FOR MASTIC UNLESS EQUAL TO HARDCAST FOIL-GRIP 1402 BUTYL RUBBER ADHESIVE TAPE.
- E. DUCT SHALL BE SUPPORTED AT BASE OF DUCT DROPS. CURB DUCT RAILS ARE NOT INTENDED TO AND SHALL NOT SUPPORT THE WEIGHT OF THE DUCT.
- F. ALL DUCT INSULATION SHALL MEET MINIMUM R-VALUE REQUIRED BY ASHRAE 90.1 LATEST EDITION. ALL DUCT WRAP SHALL BE MINIMUM 2" THICK, 3/4 PCF AND 5.6 R-VALUE INSTALLED WITH EITHER A VAPOR BARRIER WITH MAXIMUM PERMEANCE 0.05 OR A MINIMUM 2 MIL ALUMINUM REINFORCED FOIL/KRAFT FACING.
- G. ALL DUCT DROPS FROM THE ROOFTOP UNITS SHALL BE EXTERNALLY INSULATED.
- H. SUPPLY AND RETURN AIR DUCTWORK SERVING ALL AREAS SHALL BE EXTERNALLY INSULATED.
- ALL AIR CONVEYANCE COMPONENTS SUCH AS, BUT NOT LIMITED TO DUCT, DUCT PLENUMS, GRILLES/DIFFUSERS, BACK PANS, AND BOOTS SHALL BE INSULATED. INSULATION TYPE IS COVERED ELSEWHERE IN THIS SPECIFICATION.
- J. RESTROOM RECTANGULAR EXHAUST AIR DUCTWORK SHALL BE LINED WITH I' THICK, I-1/2 PCF INSULATION.

- K. TRUNK DUCTS SHALL BE ISOLATED FROM UNIT VIBRATION WITH THE USE OF NFPA AND U.L. APPROVED FLEXIBLE CONNECTORS INSTALLED AT THE TOP OF BOTH SUPPLY AND RETURN DROPS.
- L. INSULATED FLEXIBLE DUCT MAY BE UTILIZED FOR RUNOUTS TO GRILLES AND DIFFUSERS ONLY IN THE HORIZONTAL POSITION AND IN MAXIMUM LENGTHS OF 4'-O", NO EXCEPTIONS. SEE TAKE-OFF DETAIL ON DRAWING M3.1.
- M. CONSTRUCTION OF FLEXIBLE DUCTWORK SHALL INCLUDE SPIRAL METAL HELIX BONDED TO A POLYESTER CORE, FIBERGLASS INSULATION WITH POLYETHYLENE OR MYLAR VAPOR BARRIER, ALL COMPONENTS SHALL HAVE APPROPRIATE U.L. APPROVAL AND SHALL BE EQUIVALENT TO THERMAFLEX MKE.
- N. FLEXIBLE DUCT SHALL BE INSTALLED PER THE "ADC FLEXIBLE DUCT PERFORMANCE AND INSTALLATION STANDARDS, 4TH ED" USING FOIL TAPE AND DRAWBAND ON THE INNER CORE AND TAPE OR DRAWBAND ON THE OUTER JACKET.
- O. DUCT TAPE SHALL BE EQUAL TO FASSON 181-B FX, 2-1/2" WIDE.
- P. SINGLE THICKNESS TURNING VANES SHALL BE INSTALLED AT 90 DEGREE TURNS IN SUPPLY DUCTWORK WHERE ANY ONE DIMENSION IS GREATER THAN 12".
- Q. RADIUSED ELBOWS MAY BE SUBSTITUTED FOR 90 DEGREE ELBOWS AT THE DISCRETION OF THE CONTRACTOR. CENTERLINE RADIUS EQUAL TO, R-W PER FIGURE NO. 2-2 IN SMACNA HVAC DUCT CONSTRUCTION STANDARDS.
- R. EXTERNAL INSULATION ON BOTTOM OF DUCTS 24" OR WIDER SHALL BE SUPPORTED WITH STICK PINS ON 18" CENTERS. STICK PIN WASHERS SHALL BE COVERED WITH DUCT TAPE OR MASTIC.

PART III - EXECUTION

ON DRAWINGS.

- A. FURNISH AND INSTALL SYSTEM IN ACCORDANCE WITH REFERENCED STANDARDS, APPLICABLE CODES, MANUFACTURER'S RECOMMENDATIONS AND AS INDICATED
- B. OWNER SHALL TEST AND BALANCE MECHANICAL SYSTEM IN ACCORDANCE WITH NCI OR AABC STANDARDS TO ASSURE CONFORMANCE WITH DESIGN, G.C. WILL MAKE MECHANICAL CONTRACTOR AVAILABLE DURING TEST AND BALANCE TO ASSIST TESTING AGENCY AND TO MAKE CORRECTIONS IMMEDIATELY NECESSARY. CONTRACTOR SHALL CORRECT ITEMS ON WRITTEN TEST AND BALANCE REPORT.
- C. CONTRACTOR SHALL INSTRUCT THE OWNER'S REPRESENTATIVE IN ALL MATTERS PERTAINING TO THE PROPER MAINTENANCE OF EQUIPMENT FURNISHED UNDER THIS CONTRACT THROUGH DEMONSTRATION AND EXPLANATION OF OPERATING & MAINTENANCE MANUALS.
- D. CONTRACTOR SHALL PROVIDE A "SAMPLE MAINTENANCE PROPOSAL" TO THE OWNER'S REPRESENTATIVE IN ALL MATTERS PERTAINING TO THE PROPER MAINTENANCE OF EQUIPMENT FURNISHED UNDER THIS CONTRACT.
- E. CONTRACTOR SHALL COMPLETE A/C EQUIPMENT STARTUP DOCUMENTATION PROVIDED BY OWNER.

FIELD VERIFY ALL CONDITIONS

NOTE: AS NOTED IN THE SPECIFICATIONS, ALL WIRING LAYOUTS, LAYOUTS ARE SCHEMATIC. EXACT LOCATIONS SHALL BE DETERMINED BY THE CONSTRUCTION AND STRUCTURE OF THE BUILDING AND SHALL BE VERIFIED AND COORDINATED IN THE FIELD, EACH TRADE CONTRACTOR SHALL VERIFY WITH THE GENERAL CONTRACTOR THAT HE HAS THOROUGHLY REVIEWED AND COORDINATED ALL LOCATIONS AND ROUTINGS WITH ALL OTHER TRADES PRIOR TO FABRICATION OF CONDUITS, DUCTS, OR PIPING, AND START OF INSTALLATION OF SAME (INCLUDING SPRINKLER PIPING WHEN PRESENT ON JOB), ANY INSTALLATION OR CONSTRUCTION CONFLICTS WHICH OCCUR IN THE FIELD SHALL BE RESOLVED BY THE TRADE CONTRACTOR TO THE SATISFACTION OF THE OWNER AND ARCHITECT AND AT NO EXPENSE TO THE OWNER, ARCHITECT AND/OR GENERAL CONTRACTOR.

THE CONTRACTOR SHALL CONTACT THE ARCHITECT, ENGINEER OR OWNER PRIOR TO BIDDING FOR INTERPRETATIONS AND CLARIFICATIONS OF THE DESIGN AND INCLUDE IN HIS BID ALL COSTS TO MEET THE DESIGN INTENT. CLARIFICATIONS MADE BY THE ARCHITECT, ENGINEER OR OWNER AFTER BIDDING WILL BE FINAL AND SHALL BE IMPLEMENTED AT CONTRACTORS COST.

BIDDING CONTRACTORS SHALL HAVE A WORKING KNOWLEDGE OF LOCAL CODES AND ORDINANCES AND SHALL INCLUDE IN THEIR BIDS THECOSTSFOR ALL WORK INSTALLED IN STRICT ACCORDANCE WITH GOVERNING CODES, THE PLANS AND SPECIFICATIONS NOT WITHSTANDING. THE CONTRACTOR SHALL ALERT ARCHITECT, ENGINEER OR OWNER OF ANY APPARENT DISCREPANCIES BETWEEN GOVERNING CODES AND DESIGN INTENT.

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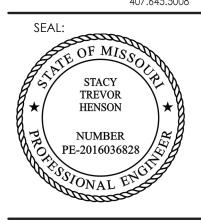
INTERPLAN

ARCHITECTURE ENGINEERING

PERMITTING

ARCH COA #2015008774 ENG COA #2005026904

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701



STACY HENSON - P.E. LIC # PE-2016036828

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FSR#02859

BUILDING TYPE / SIZE: PRINTED FOR

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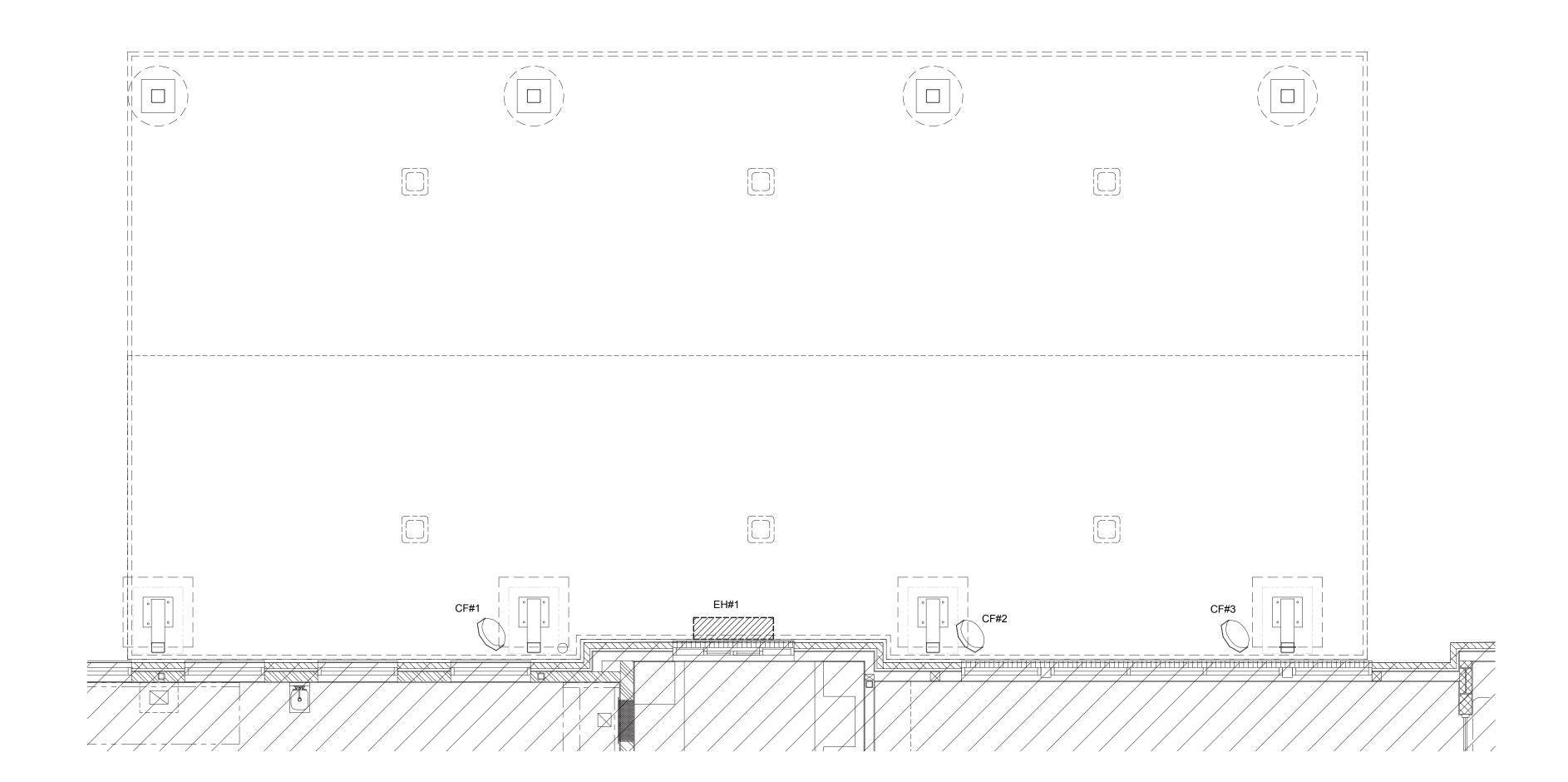
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MECH. SPECIFICATIONS & SCHEDULES

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NATIONAL ACCOUNTS

- PRICE AIR DEVICES THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE AIR DEVICES DIRECTLY FROM TOM BARROW COMPANY. CONTACT MR. SCOTT GEORGE AT 404-351-1010 FOR PRICING AND AVAILABILITY. AIR DEVICES NOT PURCHASED THRU TOM BARROW COMPANY WILL NOT BE ACCEPTED.
- AIR DOORS THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE AIR DOORS DIRECTLY FROM TOM BARROW COMPANY, CONTACT MR. SCOTT GEORGE AT 404-35HOIO FOR PRICING AND AVAILABILITY. AIR DOORS NOT PURCHASED THRU TOM BARROW COMPANY WILL NOT





GENERAL NOTES

- COORDINATE NEW WORK WITH EXISTING CONDUIT, STRUCTURE, AND PIPING. FIELD VERIFY EXISTING CONDITIONS PRIOR TO START OF
- 2. COORDINATE LOCATION AND RESPONSIBILITIES FOR UNDERGROUND PIPING AND ASSOCIATED TRENCHING WITH GENERAL CONTRACTOR PRIOR TO START OF WORK.
- 3. EXPOSED GAS PIPING SHALL BE PAINTED BY GENERAL CONTRACTOR. USE ANTI-CORROSIVE PAINT AND COORDINATE WITH CFA CONSTRUCTION MANAGER.

FIELD VERIFY ALL CONDITIONS

NOTE! AS NOTED IN THE SPECIFICATIONS, ALL WIRING LAYOUTS, PIPING LAYOUTS AND DUCT LAYOUTS ARE SCHEMATIC. EXACT LOCATIONS SHALL BE DETERMINED BY THE CONSTRUCTION AND STRUCTURE OF THE BUILDING AND SHALL BE VERIFIED AND COORDINATED IN THE FIELD. EACH TRADE CONTRACTOR SHALL VERIFY WITH THE GENERAL CONTRACTOR THAT HE HAS THOROUGHLY REVIEWED AND COORDINATED ALL LOCATIONS AND ROUTINGS WITH ALL OTHER TRADES PRIOR TO FABRICATION OF CONDUITS, DUCTS, OR PIPING, AND START OF INSTALLATION OF SAME (INCLUDING SPRINKLER PIPING WHEN PRESENT ON JOB). ANY INSTALLATION OR CONSTRUCTION CONFLICTS WHICH OCCUR IN THE FIELD SHALL BE RESOLVED BY THE TRADE CONTRACTOR TO THE SATISFACTION OF THE OWNER AND ARCHITECT AND AT NO EXPENSE TO THE OWNER, ARCHITECT AND/OR GENERAL CONTRACTOR.

THE CONTRACTOR SHALL CONTACT THE ARCHITECT, ENGINEER OR OWNER PRIOR TO BIDDING FOR INTERPRETATIONS AND CLARIFICATIONS OF THE DESIGN AND INCLUDE IN HIS BID ALL COSTS TO MEET THE DESIGN INTENT. CLARIFICATIONS MADE BY THE ARCHITECT, ENGINEER OR OWNER AFTER

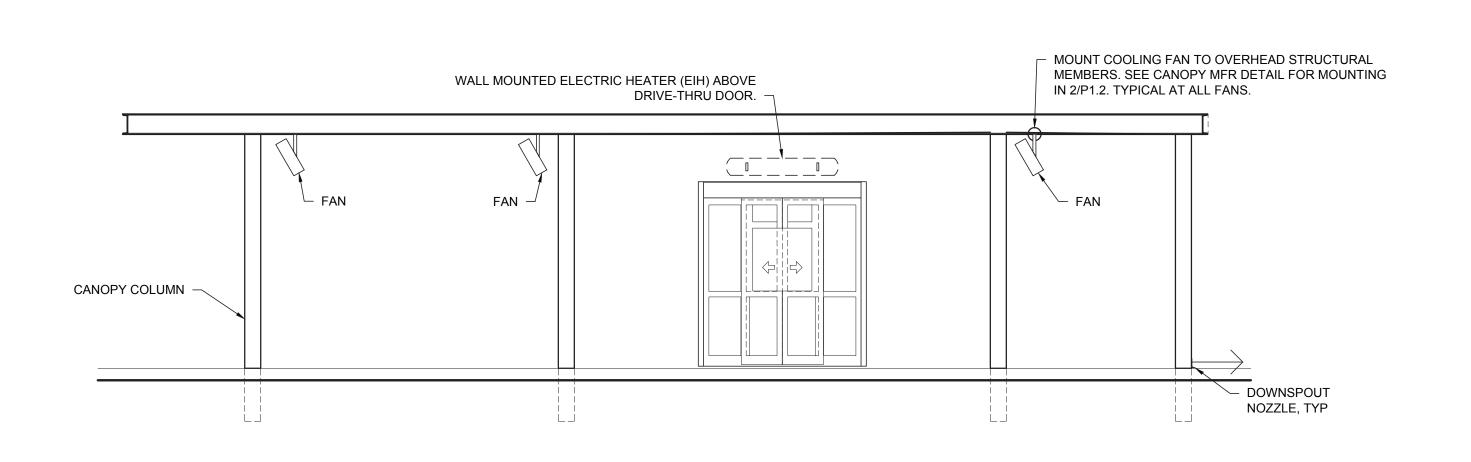
BIDDING WILL BE FINAL AND SHALL BE IMPLEMENTED AT CONTRACTORS COST.

BIDDING CONTRACTORS SHALL HAVE A WORKING KNOWLEDGE OF LOCAL CODES AND ORDINANCES AND SHALL INCLUDE IN THEIR BIDS THE COSTS FOR ALL WORK INSTALLED IN STRICT ACCORDANCE WITH GOVERNING CODES, THE PLANS AND SPECIFICATIONS NOT WITHSTANDING. THE CONTRACTOR SHALL ALERT ARCHITECT, ENGINEER OR OWNER OF ANY APPARENT DISCREPANCIES BETWEEN GOVERNING CODES AND DESIGN INTENT.

NATIONAL ACCOUNTS

- 1. SCHWANK INFRARED HEATER PACKAGE THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE HEATER PACKAGE DIRECTLY FROM TOM BARROW COMPANY. CONTACT MR. SCOTT GEORGE AT 404-351-1010 FOR PRICING AND AVAILABILITY. HEATERS NOT PURCHASED THRU TOM BARROW COMPANY WILL NOT BE ACCEPTED.
- COOK FAN PACKAGE THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE FAN PACKAGE DIRECTLY FROM TOM BARROW COMPANY. CONTACT MR. SCOTT GEORGE AT 404-351-1010 FOR PRICING AND AVAILABILITY. FANS NOT PURCHASED THRU TOM BARROW COMPANY WILL NOT BE ACCEPTED.

	LEGEND
CF#1	CIRCULATING FAN #1 (TYP)
EH#1	ELECTRIC HEATER #1 (TYP)
	NEW GAS PIPING ABOVE GRADE
	NEW GAS PIPING BELOW GRADE
B/G	BELOW GRADE
EC	ELECTRICAL CONTRACTOR
MC	MECHANICAL CONTRACTOR



HEATER FAN SECTION

NO SCALE

E Chick-fil-A

5200 Buffington Road Atlanta, Georgia 30349-2998

♠ INTERPLAN

ARCH COA #2015008774 ENG COA #2005026904

ARCHITECTURE

220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008

SEAL:

STACY
TREVOR
HENSON

NUMBER
PE-2016036828

ORDER

TREVOR
HENSON

NUMBER
PE-2016036828

STACY HENSON - P.E. LIC # PE-2016036828

SUMMIT FAIR
690 NW BLUE PKWY

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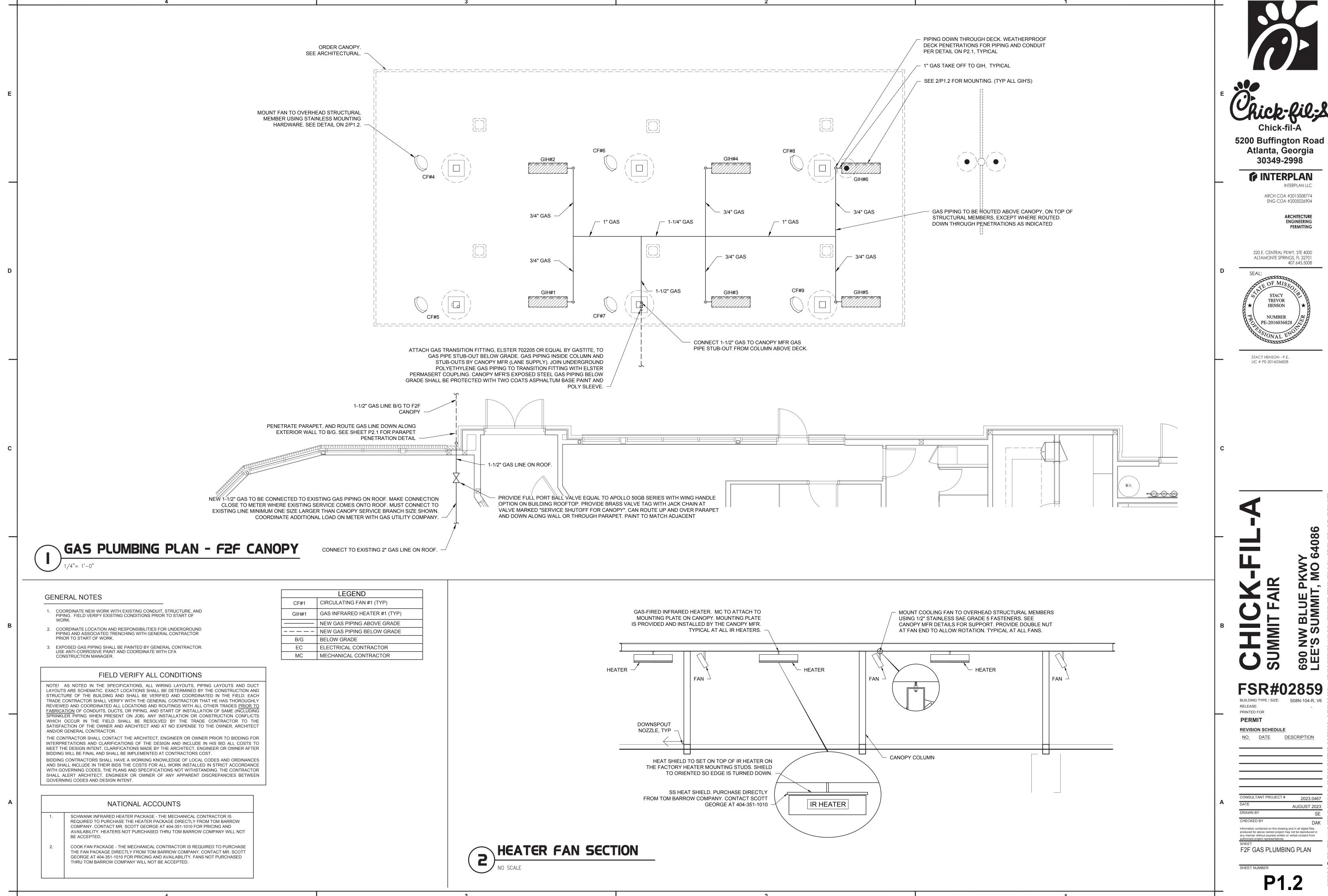
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GAS CONNECTION SCHEDULE **EQUIPMENT** GAS LOAD **EXISTING AC#1** 480,000 BTU'S 150,000 BTU'S EXISTING AC#2 240,000 BTU'S EXISTING AC#3 150,000 BTU'S EXISTING AC#4 EXISTING WATER HEATER 80,000 BTU'S (6) 50,000 BTU'S NEW GAS HEATERS (6) TOTAL CONNECTED LOAD 1,400,000 BTU'S REMARKS: . EQUIVALENT TO 1,400 CFH @ pressure drop 0.5 IN. W.C. W/ DEVELOP LENGTH OF 279 FT (METER TO GIH#6) 2. 7" w.c. DELIVERY PRESSURE.

		GAS FIR	ED INF	RARED	HEATER SCHE	DULE	
MADK	INDLIT (MRH)	FRAME SIZE			MOUNTING TYPE	MODEL	MANUFACTURE
IVIARK	IIVI OT (IVIDIT)	LENGTH	WIDTH	DEPTH	MOONTING TIPE	WIODEL	MANUFACTURE
GIH	50.0	48"	13"	10"	BRACKET	2352-NG	SCHWANK
		, ,	MARK INPUT (MBH) LENGTH	MARK INPUT (MBH) FRAME SIZE LENGTH WIDTH	MARK INPUT (MBH) FRAME SIZE LENGTH WIDTH DEPTH	MARK INPUT (MBH) FRAME SIZE LENGTH WIDTH DEPTH MOUNTING TYPE	MARK INPUT (MBH) LENGTH WIDTH DEPTH MOUNTING TYPE MODEL

REMARKS 1. STEEL BURNER WITH CERAMIC BURNER TILES.

2. STAINLESS STEEL LENS WITH BLOCK EMISSIVE COATING.

3. PROVIDE ENGRAVED PLASTIC LABEL AT EACH UNIT WITH UNIT DESIGNATION IN 1" HIGH WHITE LETTERS ON A BLACK BACKGROUND. MOUNT TO CANOPY DECK, FACING DOWNWARD, 12" LATERALLY FROM THE SIDE OF THE HEATER

3. VERIFY GAS LOAD OF EXISTING EQUIPMENT.

4. MOUNTING BRACKET PROVIDED AND INSTALLED BY CANOPY MFR.

PROVIDE HEAT SHIELD ABOVE EACH HEATER AT THE BOTTOM OF THE BRACKET.

CIRCULATING FAN SCHEDULE									
MARK	CFM	RPM	HP	MODEL	MANUFACTURER				
CF	5,750	1,625	1/8	U18TE-HD	TPI				
REMARKS	1. ALUMINUM	1. ALUMINUM PADDLE WITH STEEL HUB/SPIDER PROPELLER							
	2. 360° ROTAT	2. 360° ROTATING HEAD HORIZONTALLY AND VERTICALLY							
	3. OSHA COMI	PLIANT DOU	BLE LOCKING, COATE	D STEEL WIRE	GUARD				
	4. 3-SPEED, TOTALLY ENCLOSED, PERMANENTLY LUBRICATED BALL BEARING MOTOR								
	5. FACTORY P	RE-WIPED P	OWER CORD						
	6. PROVIDE FA		LL MOUNTING BRACK STRUCTIONS	ET. SEE DETA	L 3/M2.1 FOR				
7. PROVIDE ENGRAVED PLASTIC LABEL AT EACH UNIT WITH UNIT DESIGNAT IN 1" HIGH WHITE LETTERS ON A BLACK BACKGROUND. MOUNT TO UNDERS OF CANOPY OR EXISTING OVERHANG, FACING DOWNWARD, 12" LATERALLY FROM THE FAN LOCATION									
	8. REMOVE PL	JLL CHAIN EX	XTENSION AT ON/OFF	SWITCH IN FI	ELD				
	9. FACTORY C	ERTIFIED FO	R OUTDOOR INSTAL	LATION.					

CONTRACTOR TO VERIFY EXISTING GAS SYSTEM CAN HANDLE NEW GAS LOAD. RESIZE AND INSTALL NEW GAS PIPING AS REQUIRED IF EXISTING GAS PIPING IS UNDERSIZED FOR NEW GAS LOAD AND PIPE LENGTH. FIELD VERIFY EXACT CONDITIONS PRIOR TO BID.

PIPING CROSSING OVER CONDENSATE PIPING.

NON ADJUSTABLE MODEL DB610 PIPE STAND TO BE USED FOR NON-ELEVATED PIPING INSTALLED

PROVIDE MODEL DBE 10-8 OR DBE 10-12 OR DBE 10-16 AS NEEDED FOR ELEVATING PIPING FOR GAS

NATIONAL ACCOUNTS SCHWANK INFRARED HEATER PACKAGE - THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE HEATER PACKAGE DIRECTLY FROM TOM BARROW COMPANY. CONTACT MR. SCOTT GEORGE AT 404-351-1010 FOR PRICING AND AVAILABILITY. HEATERS NOT PURCHASED THRU TOM BARROW COMPANY WILL NOT BE ACCEPTED. TPI FAN PACKAGE - THE MECHANICAL CONTRACTOR IS REQUIRED TO PURCHASE THE FAN PACKAGE DIRECTLY FROM TOM BARROW COMPANY. CONTACT MR. SCOTT GEORGE AT

404-351-1010 FOR PRICING AND AVAILABILITY. FANS NOT PURCHASED THRU TOM BARROW

IMPORTANT NOTE - PLEASE READ

NUMBERS OF GAS INFRARED HEATERS AND CIRCULATING FANS WILL BE DETERMINED BY SITE-SPECIFIC CANOPY LAYOUT AND EQUIPMENT LOCATIONS, AS INDICATED ON ARCHITECTURAL PLANS.

GENERAL NOTES

1. COORDINATE NEW WORK WITH EXISTING CONDUIT, STRUCTURE AND PIPING. FIELD VERIFY EXISTING CONDITIONS PRIOR TO START OF WORK.

2. COORDINATE LOCATION AND RESPONSIBILITIES FOR UNDERGROUND PIPING AND ASSOCIATED TRENCHING WITH GENERAL CONTRACTOR PRIOR TO START OF WORK.

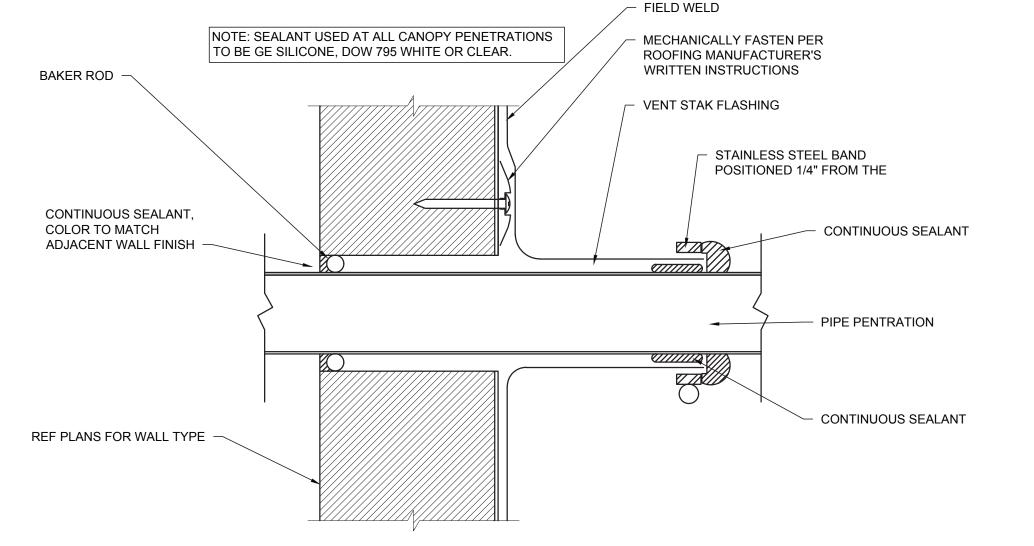
3. EXPOSED GAS PIPING SHALL BE PAINTED BY GENERAL CONTRACTOR.

COMPANY WILL NOT BE ACCEPTED.

				ELE	CTRIC HEATE	R SCHEDULI			
MARK	OUTPUT (kW)	FRAME SIZE		MOUNTING TYPE	MODEL	MANUFACTURER	VOLTAGE		
IVIARK	OOTI OT (KVV)	LENGTH	WIDTH	DEPTH	I MOONTING TIPE	IVIODEL	MANOFACTORER	VOLTAGE	
EIH	5.4-5.9	56"	8.5"	3.5"	BRACKET	BH04200-35(33)	BROMIC	208V(230-240V) / 60Hz / 28.4A(25A)	
REMARKS	1 DROVIDE BOTARY TIMER SWITCH (TORK#C502H 2 HOLID MAY) TO BE MOLINTED INSIDE DRIVE THRU AREA NEVT TO								
	5. PROVIDE 2	-POLE 40-AI	MP BREAK	ER IN A P	ANEL WITH AVAILA	BLE CAPACITY.			

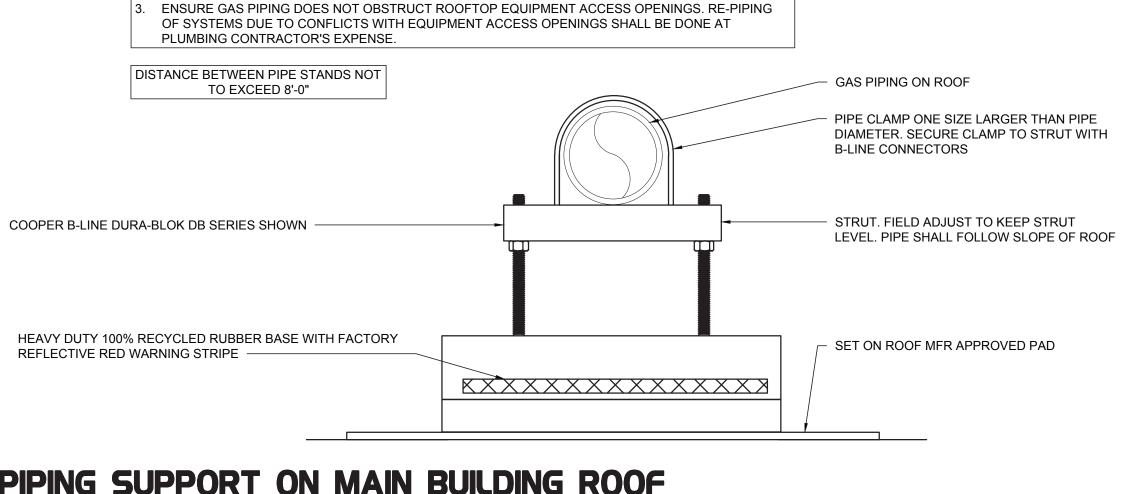
DISTANCE BETWEEN PIPESTANDS

NOT TO EXCEED 8'-0".



PARAPET PENETRATION DETAIL

GAS PIPING AND CONDUIT ON ROOF

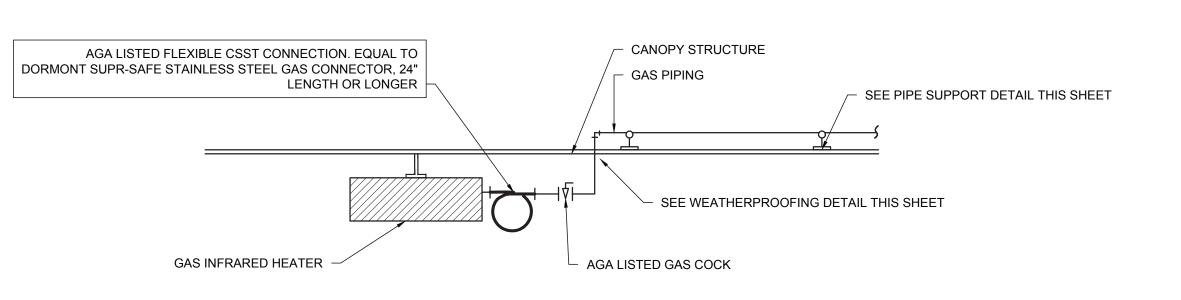


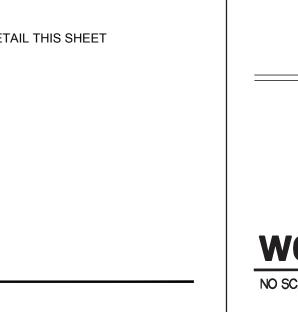
PIPING SUPPORT ON MAIN BUILDING ROOF

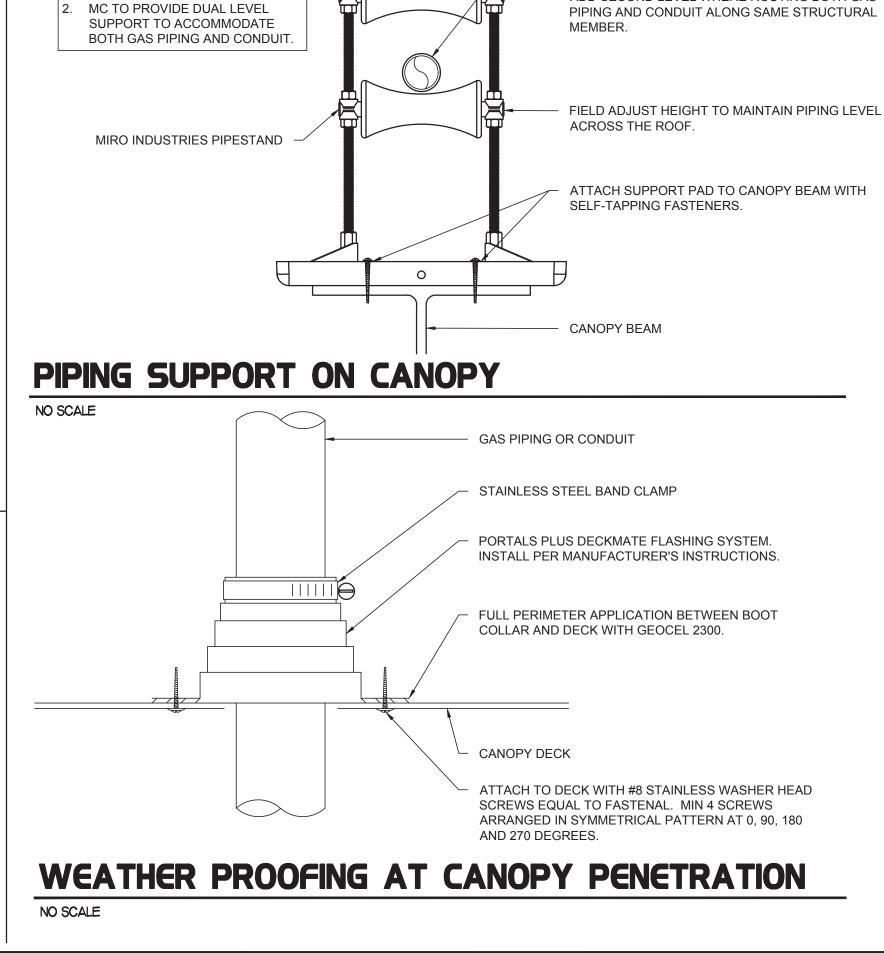
GAS CONNECTION AT APPLIANCE

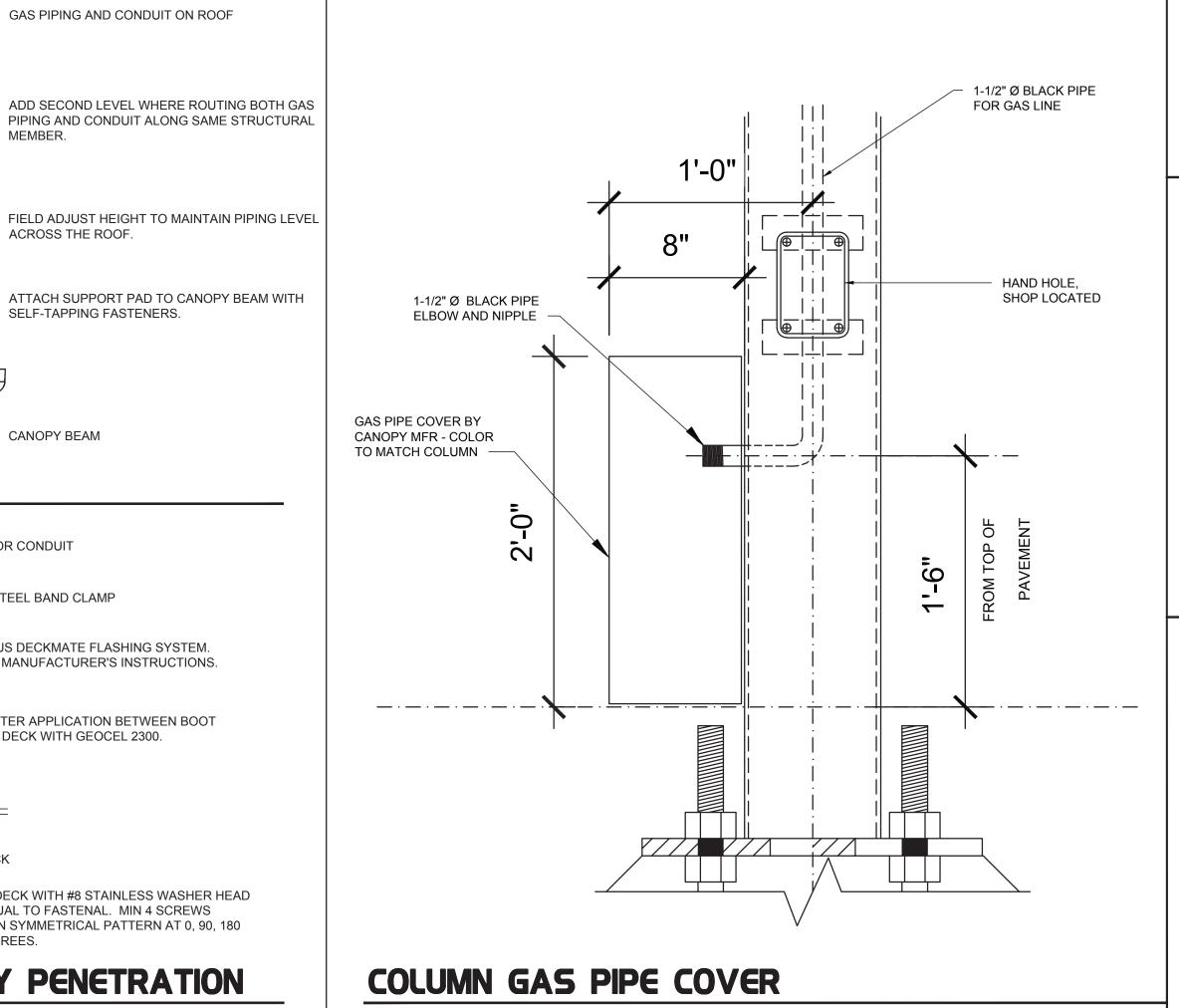
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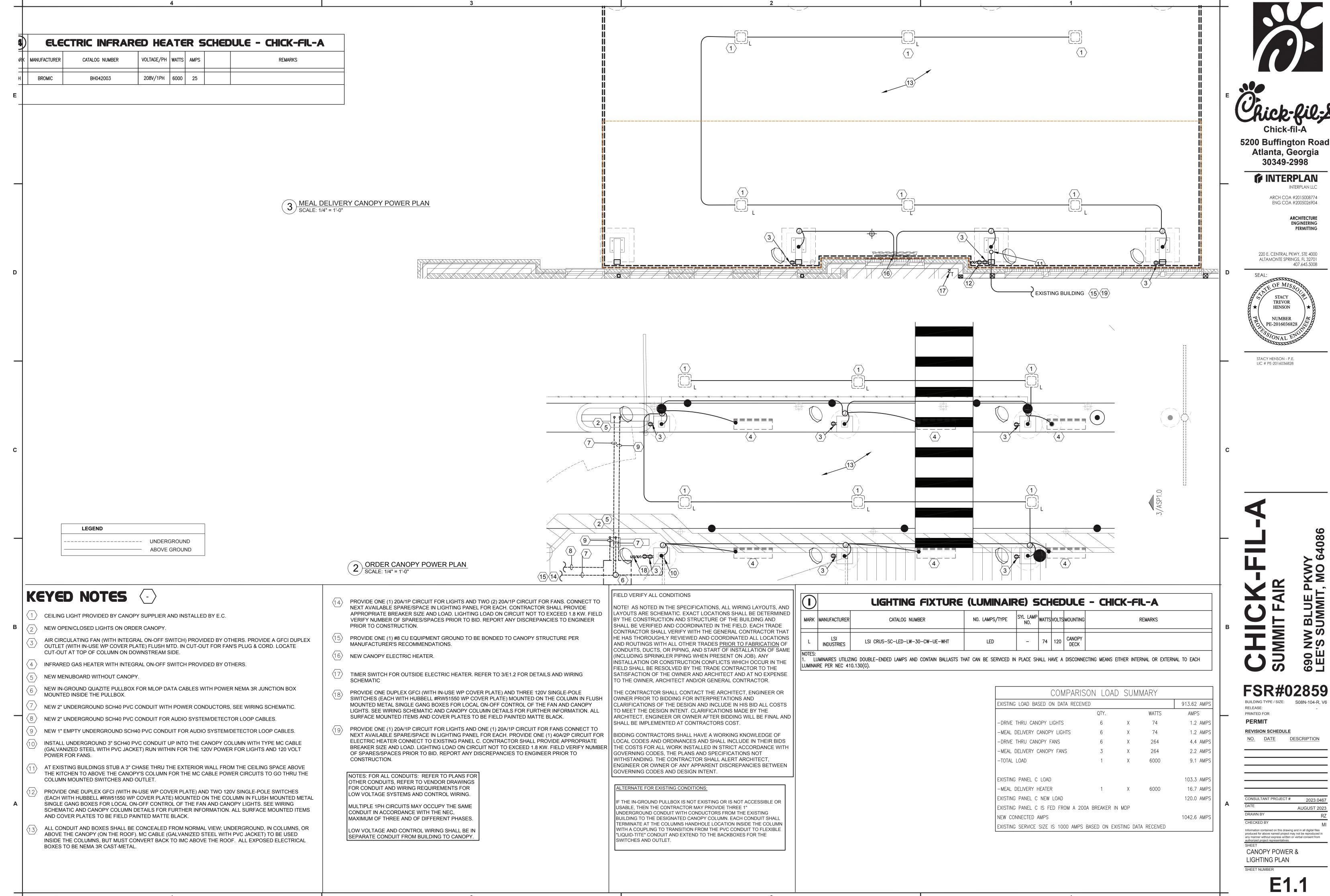


Atlanta, Georgia 30349-2998 **INTERPLAN** ARCH COA #2015008774 ENG COA #2005026904 **ARCHITECTURE** 220 E. CENTRAL PKWY, STE 4000 ALTAMONTE SPRINGS, FL 32701 407.645.5008 HENSON PE-2016036828 STACY HENSON - P.E. LIC # PE-2016036828

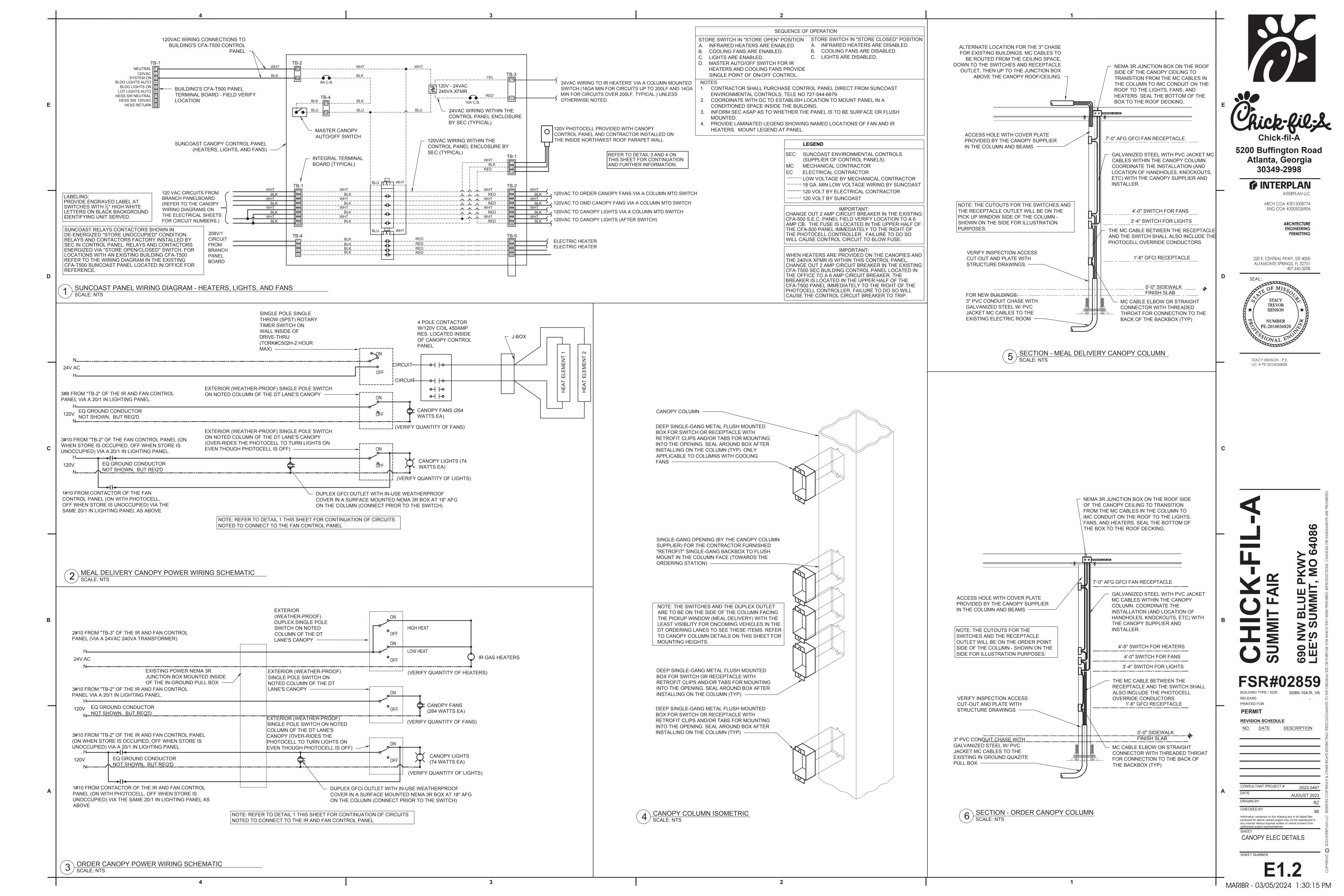
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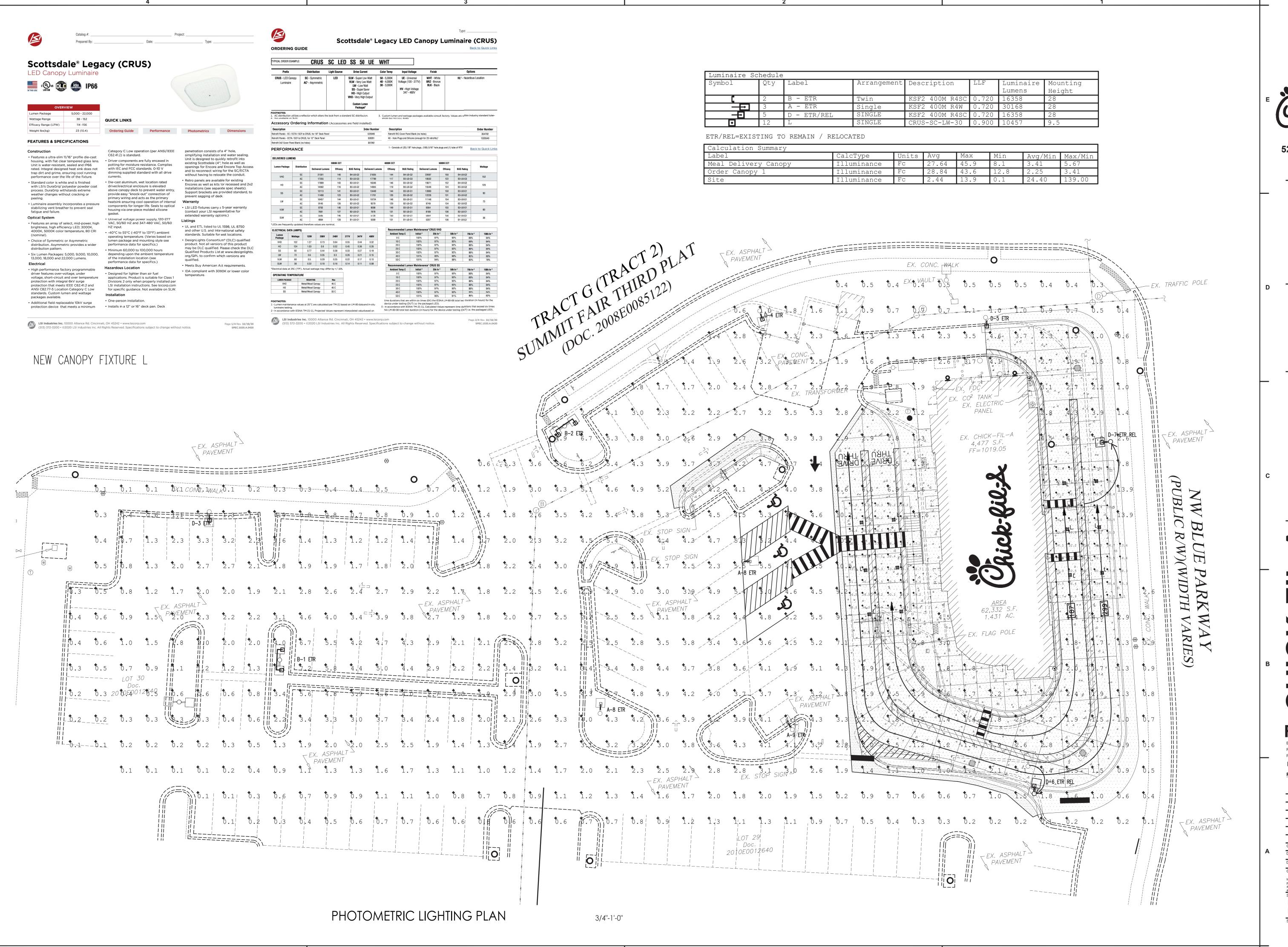
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PLUMBING DETAILS



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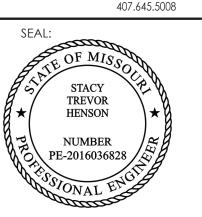
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> > > **ARCHITECTURE**

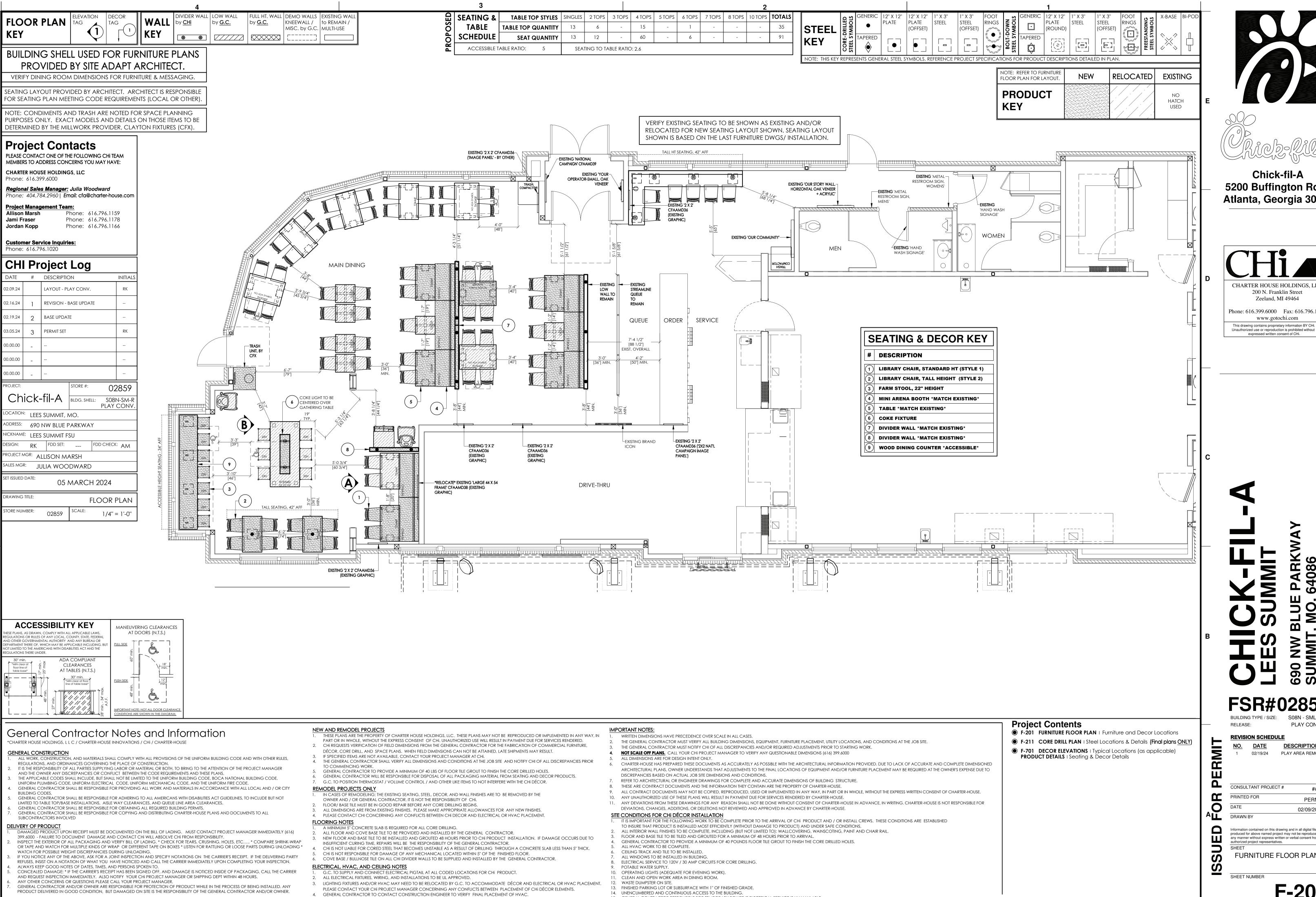
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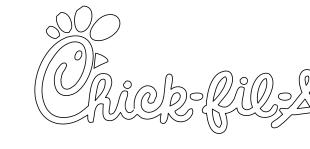
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15. GENERAL CONTRACTOR RESPONSIBLE FOR TEMPORARY POWER IF ELECTRICAL SERVICE IS UNAVAILABLE.

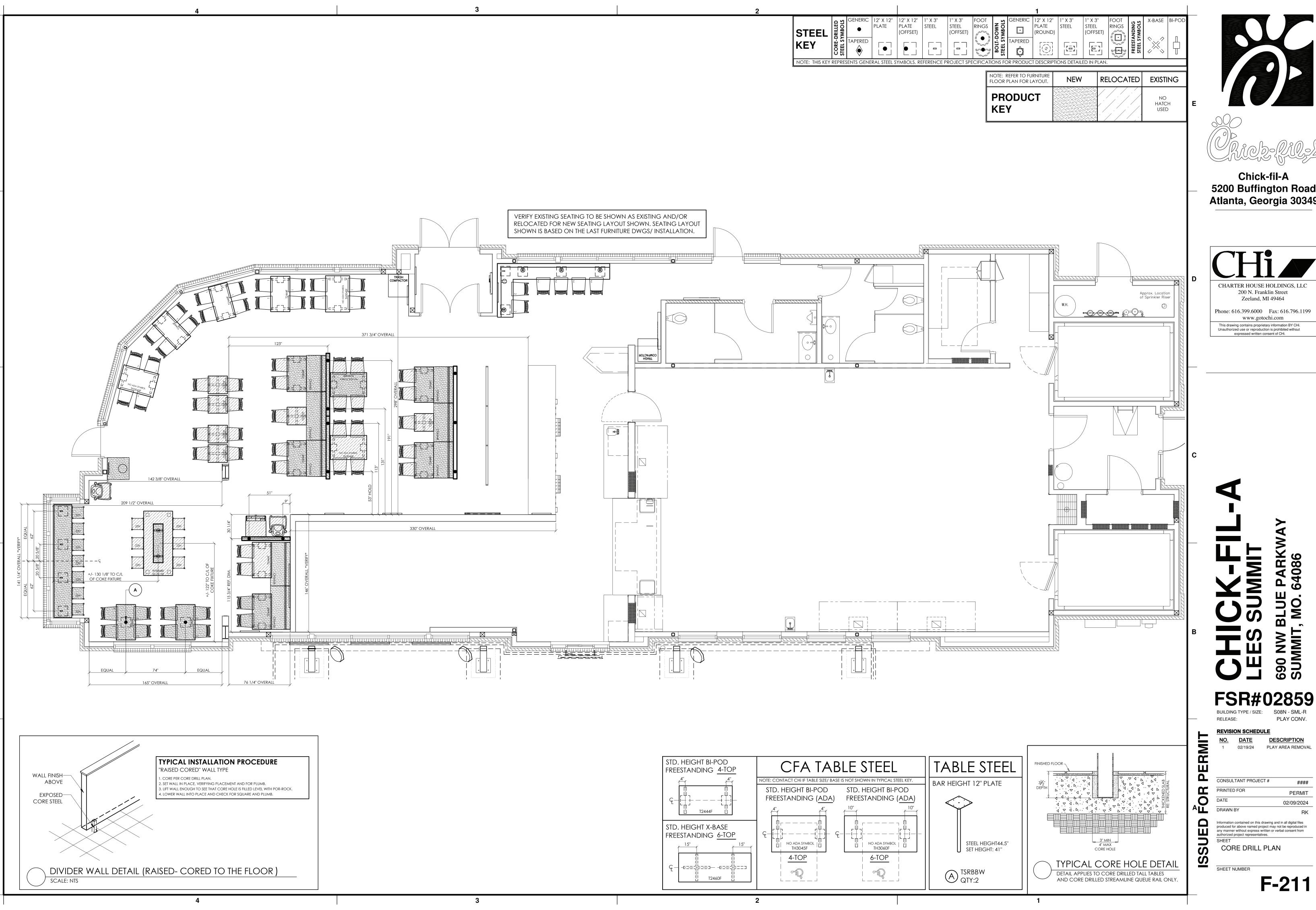


Chick-fil-A **5200 Buffington Road** Atlanta, Georgia 30349



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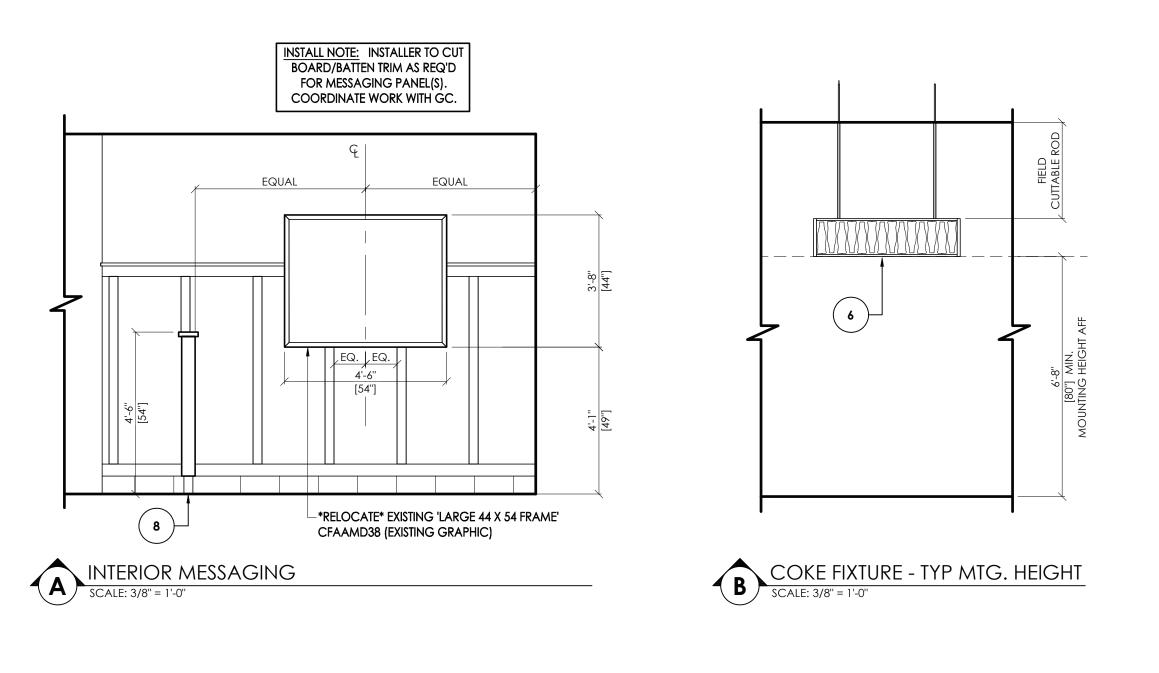




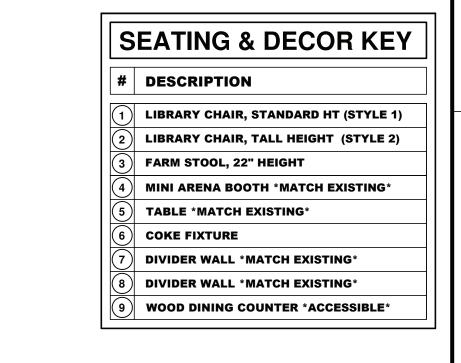
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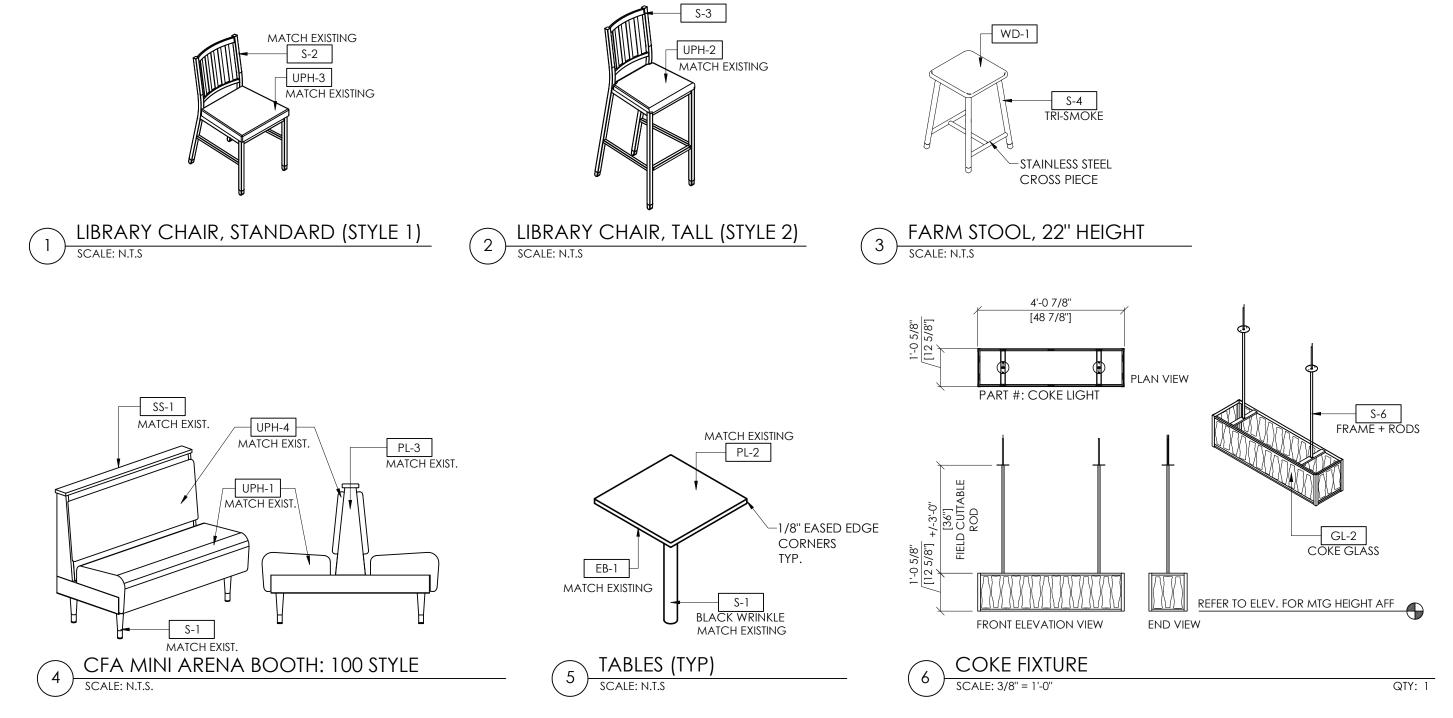
F-211

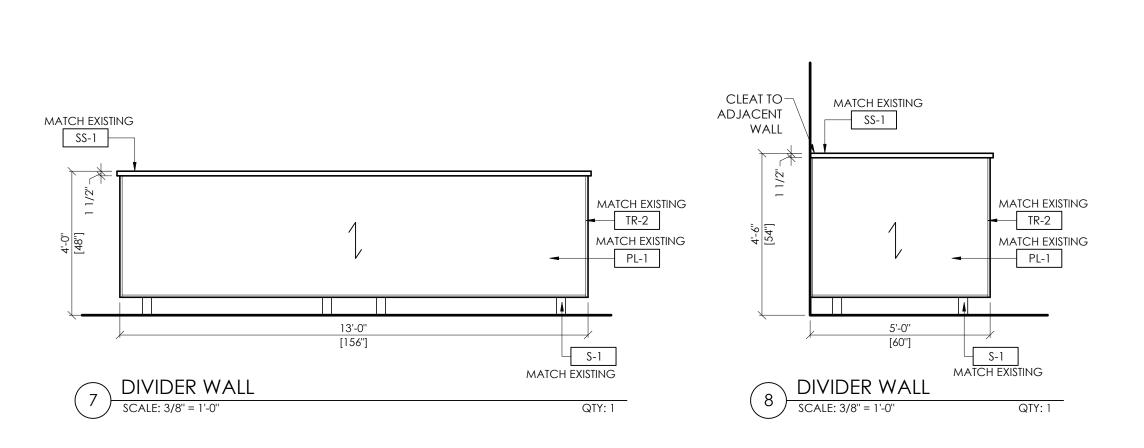


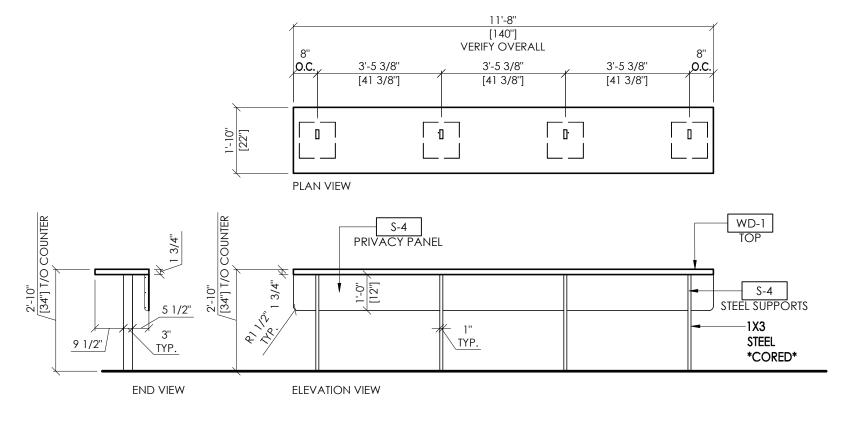
		I						
MATERIAL	CODE	MANUFACTURER	PRODUCT SPECIFICATION	SIZE	CONTACT / ADDITIONAL INFORMATION	SUPPLIER	INSTALLER	REVISIO
STEEL								
	S-1	N/A	BLACK WRINKLE	N/A	CHI MANUFACTURING	CHI	N/A	
	S-2	N/A	RESOLVE SILVER METALLIC	N/A	CHI MANUFACTURING	CHI	N/A	
	S-3	N/A	DARK CHERRY	N/A	CHI MANUFACTURING	CHI	N/A	
	S-4	N/A	TRI-SMOKE MINI TEX. #T1-7060	N/A	CHI MANUFACTURING	CHI	N/A	
	S-5							
	S-6	N/A	TIGER 89/80419 RAL 9011-FINE TEXTURE	N/A	CHI MANUFACTURING	CHI	N/A	
UPHOLSTERY	'			'	<u> </u>	1	-	
	UPH-1	CF STINSON	SLEEK, SLK38, CHARISMA (VINYL)	N/A	CHI UPHOLSTERY DISTRIBUTOR	СНІ	N/A	
	UPH-2	ARC COM	DURANGO, AC-67567 RED (VINYL)	N/A	CHI UPHOLSTERY DISTRIBUTOR	CHI	N/A	
	UPH-3	CF STINSON	MONTANA, CFASB, SABLE BROWN (VINYL)	N/A	CHI UPHOLSTERY DISTRIBUTOR	CHI	N/A	
	UPH-4	MOMENTUM	FOLD	N/A	CHI UPHOLSTERY DISTRIBUTOR	CHI	N/A	
PLASTIC LAMINATE								
	PL-1	WILSONART	CAFELLE 7933-38	N/A	LOCAL DISTRIBUTOR	CHI	N/A	
	PL-2	PIONITE	CAVALCADE SOUTH, AT650	N/A	LOCAL DISTRIBUTOR	CHI	N/A	
	PL-3	WILSONART	PINNACLE WALNUT, 7992-38	N/A	LOCAL DISTRIBUTOR	CHI	N/A	1
SOLID SURFACE				l .				
	SS-1	AVONITE	F1-9144, PALERMO	N/A	LOCAL DISTRIBUTOR	СНІ	N/A	
	NOTE: DA	ARK SOLID SURFACES SHOW N	MORE WEAR OVER TIME	·		L	-	
EDGE BAND								
	EB-1	N/A	REHAU, NUBIAN BROWN	N/A	CHI MANUFACTURING	CHI	N/A	
DECORATIVE BOARD	1	ı			I		1	
	DB-1	NOT USED						
TRIMS		1			I			
	TR-1	NOT USED						
	TR-2	N/A	FURNITURE GRADE DURANODIC	N/A	CHI MANUFACTURING	CHI	N/A	+
WOOD		1					- I	
	WD-1	N/A	SOLID WHITE OAK	N/A	CHI MANUFACTURING	СНІ	N/A	$\overline{}$
GLASS	1	'	11. 2 2	1. 4		1	1 ***	
-	GL-1	NOT USED						
	GL-2	N/A	COKE GLASS - SMART GLASS JEWELRY	N/A	CHI MANUFACTURING	CHI	N/A	











9 WOOD DINING COUNTER WITH PRIVACY PANEL (ACCESSIBLE HEIGHT) *CORED*





Chick-fil-A 5200 Buffington Road Atlanta, Georgia 30349



FSR#02859

PLAY CONV.

	<u>NO.</u>	DATE	DESCRIPTION
Σ	1	02/19/24	PLAY AREA REMOVA
₹			
Ш			
	CONSU	LTANT PROJE	CT # """
		LIANTINOUL	####
	DDINTE	D EOD	

REVISION SCHEDULE

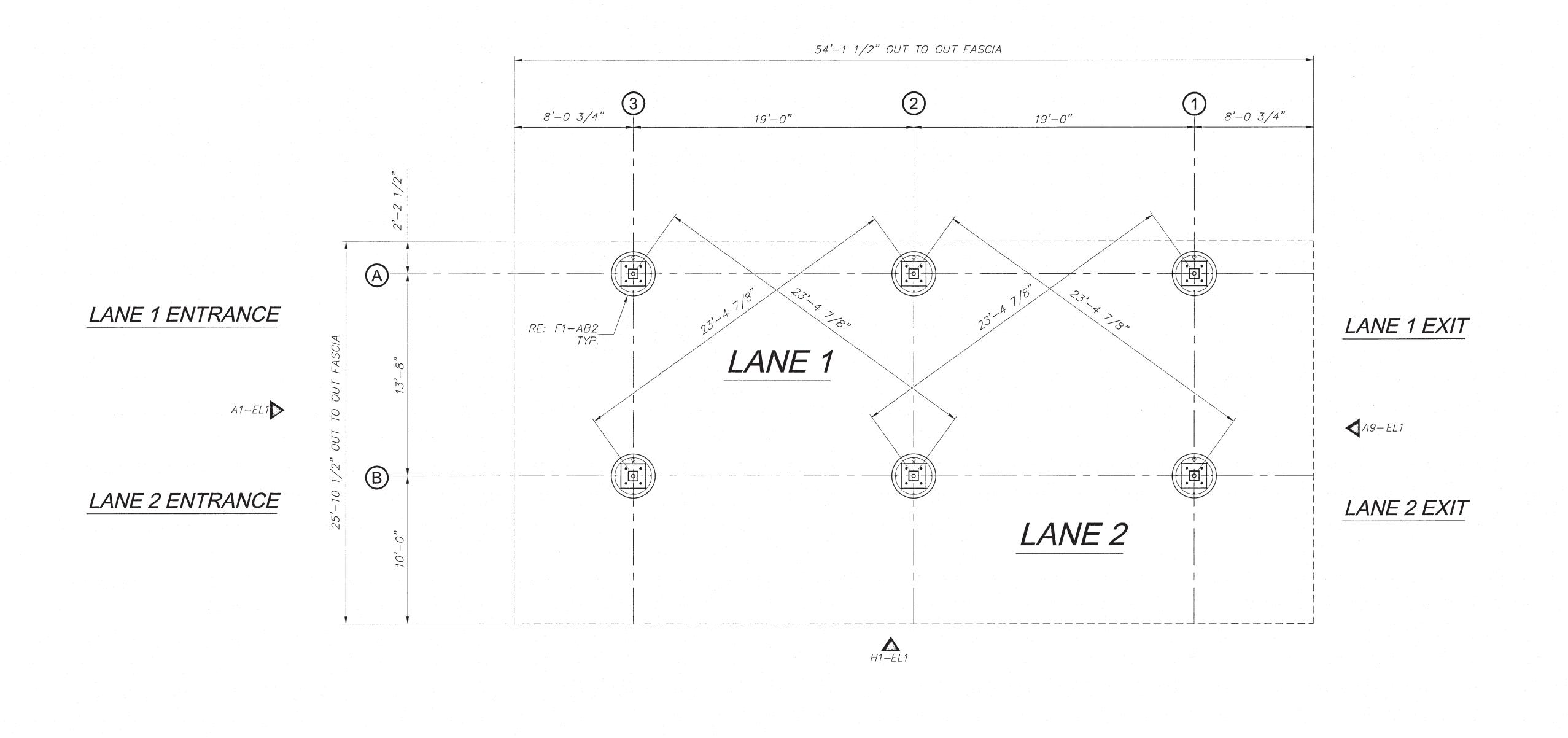
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PRINTED FOR	PERMIT
DATE	02/09/2024
DRAWN BY	RK
Information contained on this draw produced for above named project	ving and in all digital files

DECOR ELEVATIONS PRODUCT DETAILS

SHEET NUMBER

ISSUE

F-701

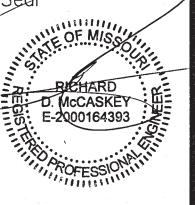


$DEAD\ LOAD = 3\ p.s.f.(DECK + LIGHTS) +$ WEIGHT OF STRUCTURAL COMPONENTS $LIVE\ LOAD\ =\ 20\ p.s.f.$ VERY IMPORTANT: $SNOW LOAD = 20^{\circ} p.s.f.$ WIND LOAD V,ULT = 116 m.p.h. EXP. CSURVEY ROD AFTER FOOTINGS ARE POURED PLEASE WIND V.ASD = 90 m.p.h. EXP C OR TAPE PROVIDE LANE CO. WITH THE FOOTING BLDG CODE = MISSOURI BUILDING CODE 2018 ELEVATIONS ON THE ELEVATION SHEET ADOPTING 2018 INTERNATIONAL BUILDING CODE ATTACHED. EQUIVALENT LATERAL FORCE PROCEDURE _TRANSIT LATERAL FORCE RESISTING SYSTEM = CANTILEVERED HIGHEST POINT OF DRIVE COLUMN SYSTEM-ORDINARY STEEL MOMENT FRAME Pf = 20 p.s.f. Ce = 1.2 Ct = 1.2 ls = 1.0W = DRIFT LOADS NOT CONSIDEREDPd = DRIFT LOADS NOT CONSIDERED TOP OF - FOOTING * SITE CLASS = DSs(0.2) = 0.099S1(1.0) = 0.068 $\dot{S}DS' = 0.11$ SD1 = 0.11Fa = 1.60Fv = 2.40imes must provide this information. R = 1.25IMPORTANCE FACTOR = 1.0RISK CATEGORY = II SEISMIC DESIGN CATEGORY = D CS = 0.084CONSTRUCTION TYPE = IIB Sheet OCCUPANCY CATEGORY = A2TOTAL SEISMIC BASE SHEAR BOTH DIRECTIONS = 0.84 KIPS DESIGN LOADS

5200 Buffington R Atlanta Georgia, 30349—2998

Revisions:

Mark Date



SEP 07 2023

C.O.A. 2001015838

I A NIE SERVE MALE NO. 12 AND ADDRESS. SUPPLY, INC. 120 FAIRVIEW ARLINGTON, TX. 76010 (817) 261-9116

IOTICE: THIS DOCUMENT IS THE PROPERTY OF LANE COMPANY, IETHER THIS DOCUMENT NOR ANY DATA OR INFORMATION IETHER THIS DOCUMENT NOR ANY DATA OR INFORMATION REPRODUCED IN ANY MANNER, DANED OTHERWISE DISPOSED OF, OR USED FOR ANY PURPOSE ANTICOLOR WITHOUT THE PROPOSED FOR WHITE PERMISSION OF LANE OMPANY, IF THE DOCUMENT IS LOANED BY OR WITH THE COMPANY, IF THE DOCUMENT, IN EDITOR OF THE PROPOSED OF LANE OF THE PROPERTY OF THE PROPOSED TO THE PROPOSED OF THE PROPOSED OF THE PROPOSED OF THE SPECIFICALLY AUTHORIZED WORK FOR HIGH OF THE SPECIFICALLY AUTHORIZED WORK FOR HIGH IF WEST USED.

Chick-fil-A #02859 690 NW BLUE PARKWAY. LEE'S SUMMIT,MO

SHEET TITLE

CANOPY FOOTING LOCATIONS

Job No.: <u>LSC: 75966</u> : <u>02859</u> Store . 8.30.23

Drawn By Checked By: RM

F2FC-I

ABI OF 2

COLUMN AND FOOTING LOCATIONS

1/4" = 1'-0"

N. T. S.

. ALL FOUNDATION WORK BY OTHERS AND SUBJECT TO LOCAL APPROVAL

2. THE FOUNDATION DESIGN IS BASED UPON SECTION 1807.3.2.2-IBC 2018 EDITION. THE DESIGN CRITERIA SELECTED ASSUMES: SITE CLASS D MATERIAL OR BETTER, SOIL BEARING CAPACITY OF 1,500 p.s.f. AND A PASSIVE SOIL PRESSURE OF 100 p.s.f. PER FOOT OF DEPTH.

DRILLED SHAFT FOOTINGS SHALL BE INSTALLED PER ACI STD. 336. CONCRETE DESIGN AND CONSTRUCTION SHALL CONFORM TO ACI STANDARD 318-14 "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE.

5. MINIMUM COMPRESSIVE STRENGTH OF CONCRETE (F'C) AT THE END OF 28 DAYS SHALL BE 2500 PSI MIN.

6. REINFORCING STEEL SHALL BE GRADE 60 AND CONFORM TO ASTM A615 LATEST REVISION.

DETAILING, FABRICATION AND PLACEMENT OF REINFORCING BARS SHALL COMPLY WITH ACI 315, ACI 318 AND CRSI STANDARDS.

ANCHOR BOLTS SHALL CONFORM TO ASTM F1554-GR36. LANE IS NOT RESPONSIBLE FOR FOOTING POURED PRIOR

TO PERMITTING. 10. FOOTINGS ARE DESIGNED TO BE CONSTRAINED AT THE TOP BY A 6" SLAB. IF THEY ARE NOT, PLEASE NOTIFY LANE SUPPLY CO.

11. POUR FOOTINGS TO SAME TOP ELEVATION. 12. USE MASTER FLOW 928 NON-SHRINK GROUT OR EQUIVALENT F'm=5000 p.s.i.

13. G.C. TO ENSURE THAT FOOTINGS DO NOT INTERFERE WITH UNDERGROUND UTILITIES

FOUNDATION NOTES

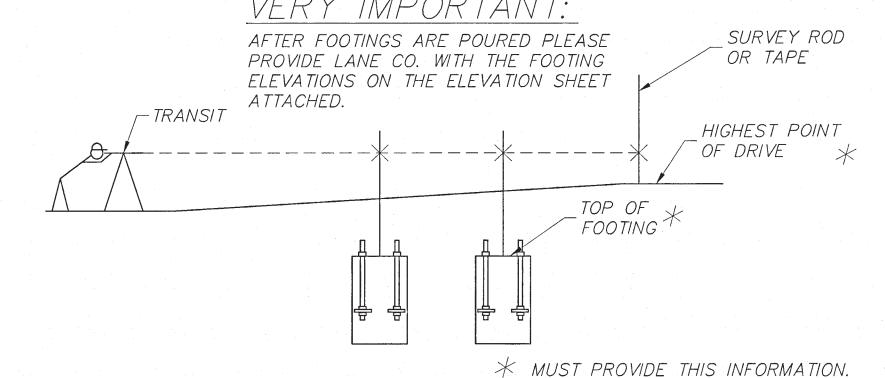
TOP OF ALL CANOPY FOOTINGS ARE TO BE POURED A MINIMUM OF 12" BELOW FINISHED GRADE OR AS REQUIRED BY LOCAL CODES AND ORDINANCES.

2. IT IS THE OWNERS RESPONSIBILITY TO CONVEY TO ALL CONTRACTORS THAT IT IS THEIR RESPONSIBILITY TO INSURE THAT THE SITE IS PROPERLY EXCAVATED AND GRADED. DURING CONCRETE FORMING PRIOR TO AND AFTER THE POUR, THE CONCRETE SHOULD BE CHECKED FOR PROPER ELEVATION.

SQUARE AND CORRECT DIMENSIONS. 3. MEASUREMENTS FOR ANCHOR BOLTS ARE EXACT AND SHOULD BE RECHECKED TO INSURE PROPER LOCATION.

4. CORRECTION OF LOCATION, OF ELEVATION AND OF DIMENSIONAL ERRORS MUST BE MADE PRIOR TO THE ARRIVAL OF THE ERECTION CREW AND PRIOR TO THE ERECTION OF THE STRUCTURE.

5. AFTER THE FORMS HAVE BEEN REMOVED, ALL TRENCHES, HOLES AND UNEVEN SITE CONDITIONS MUST BE LEVELED TO INSURE A SAFE WORKING AND ACCESS AREA ACCEPTABLE TO LOCAL, STATE, FEDERAL AND OSHA



AGENCIES.

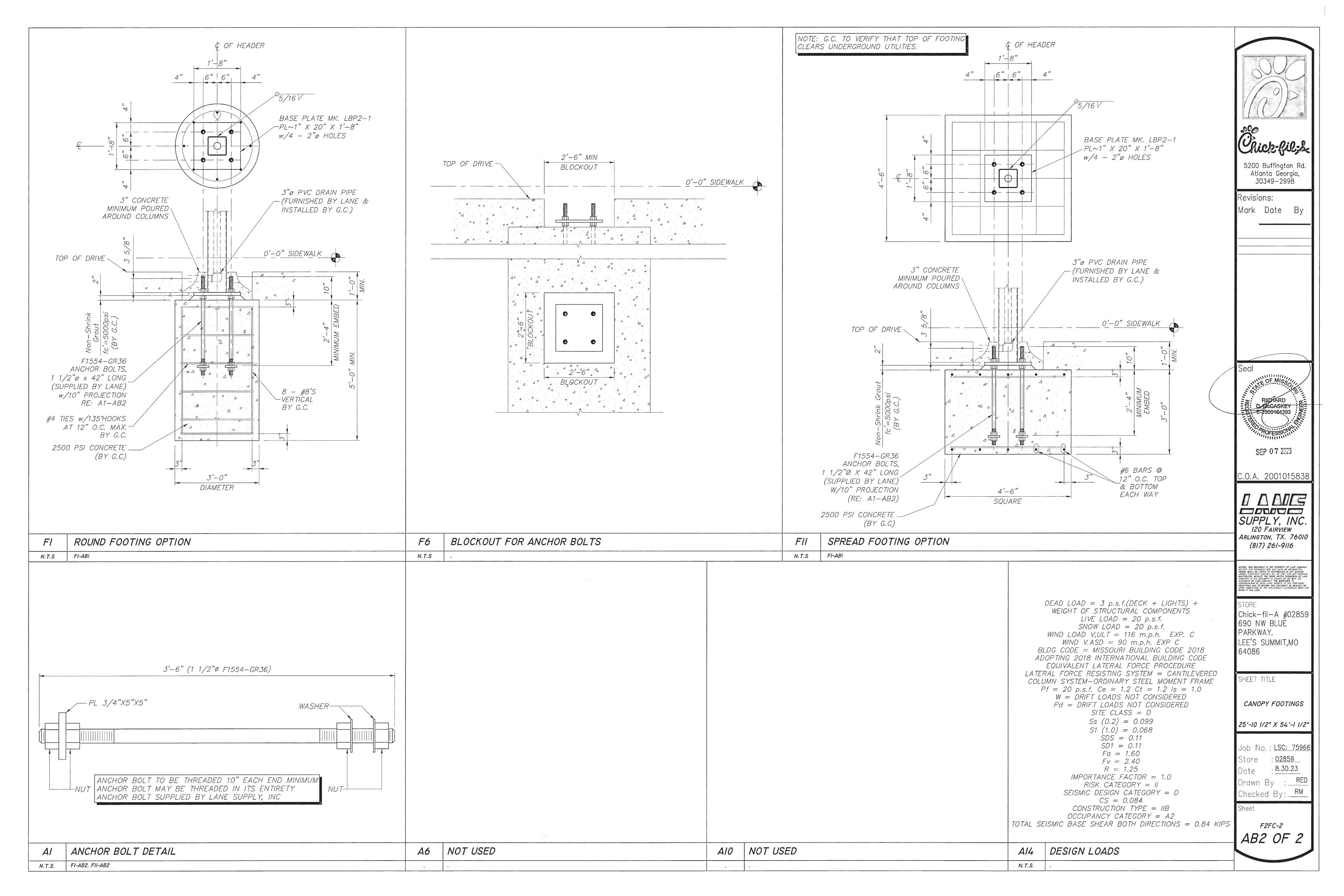
GENERAL NOTES

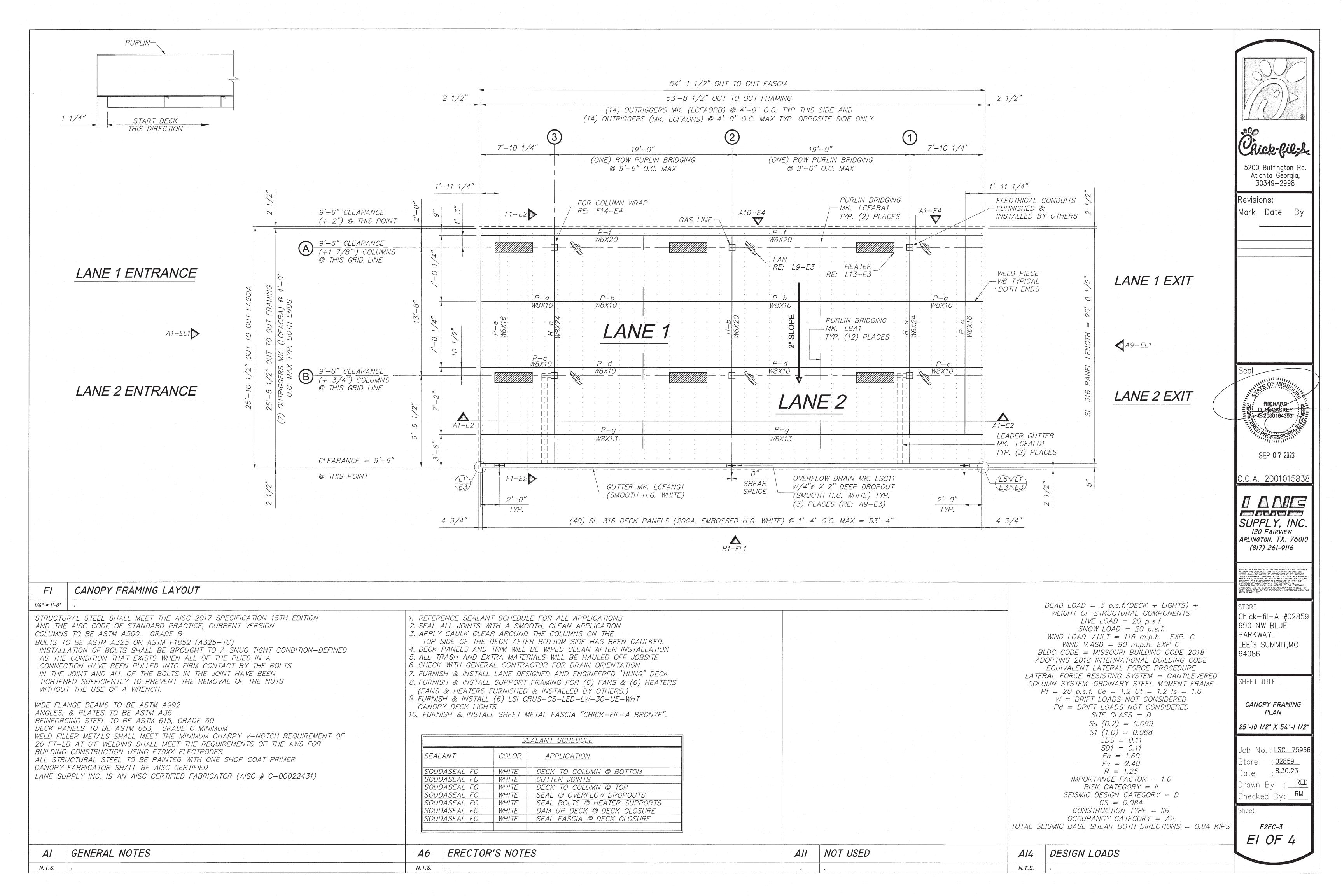
N. T. S.

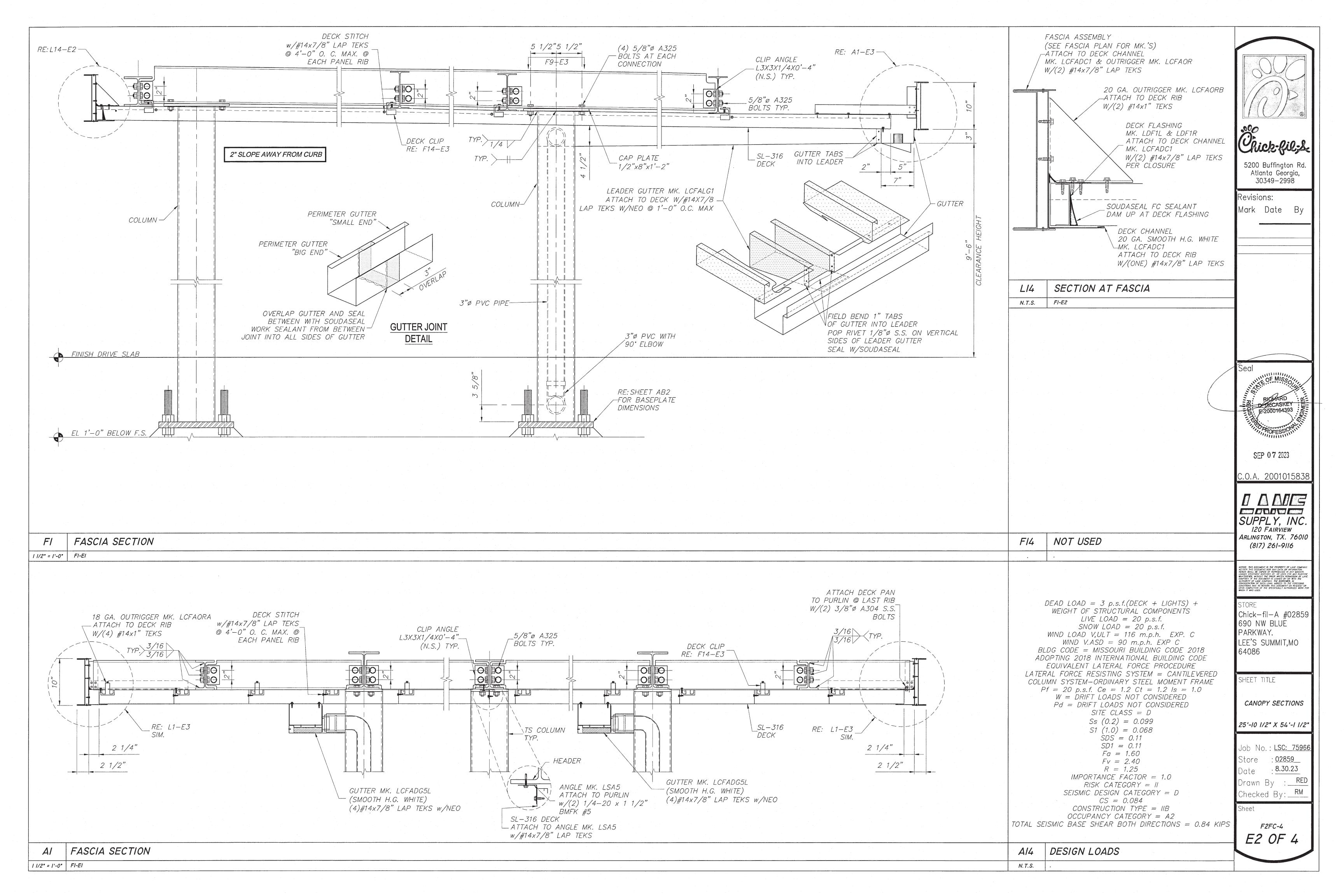
FOOTING ELEVATIONS

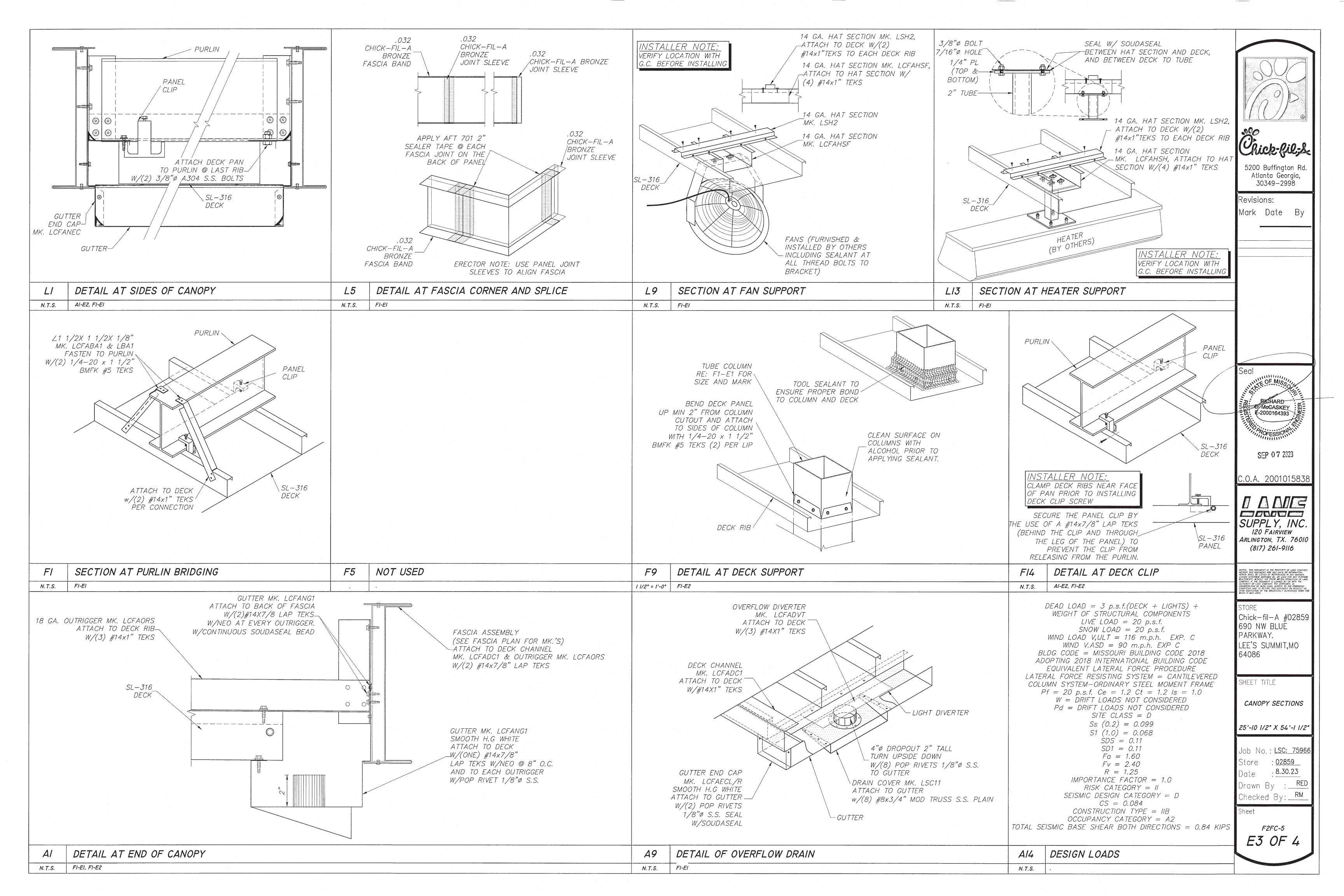
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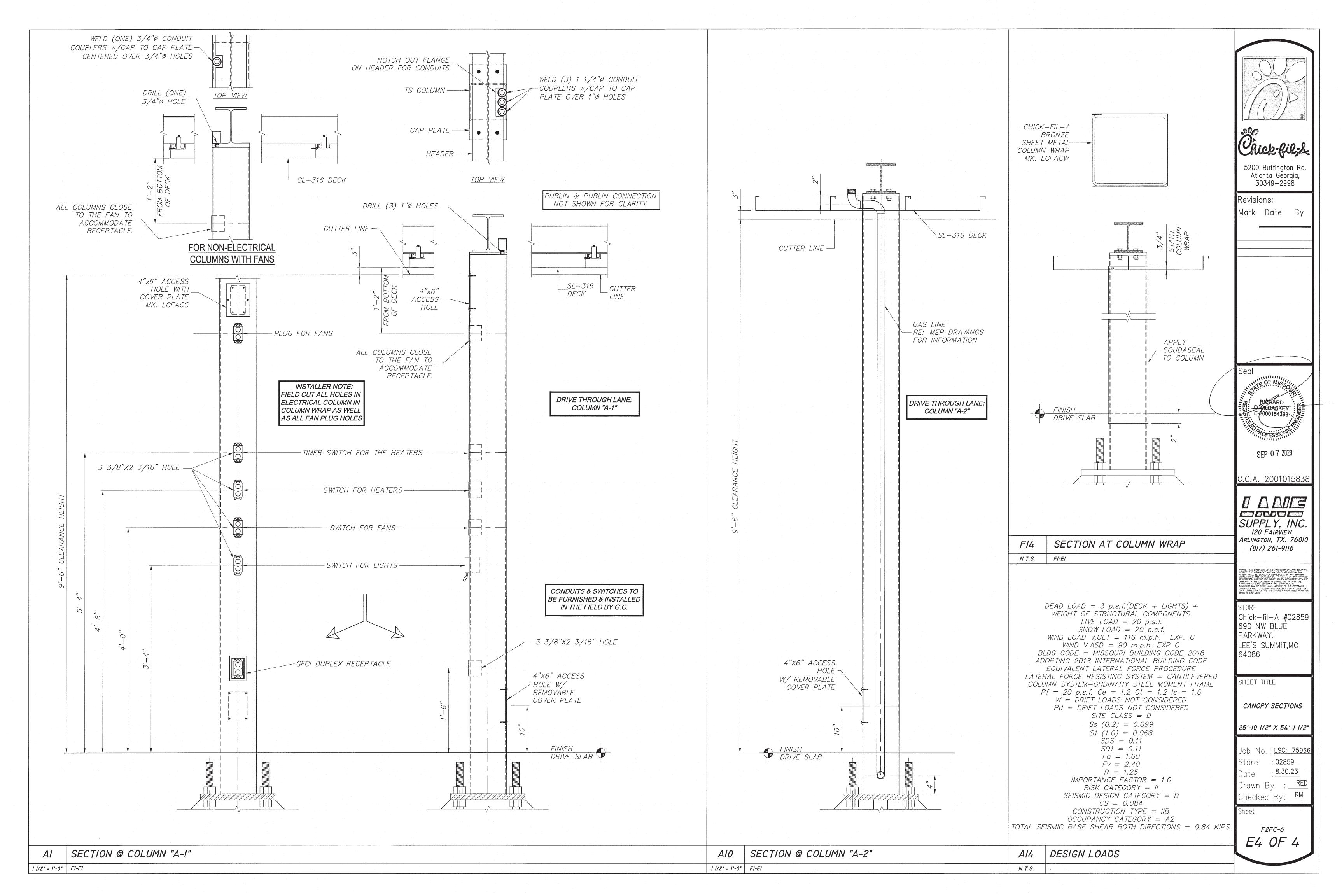
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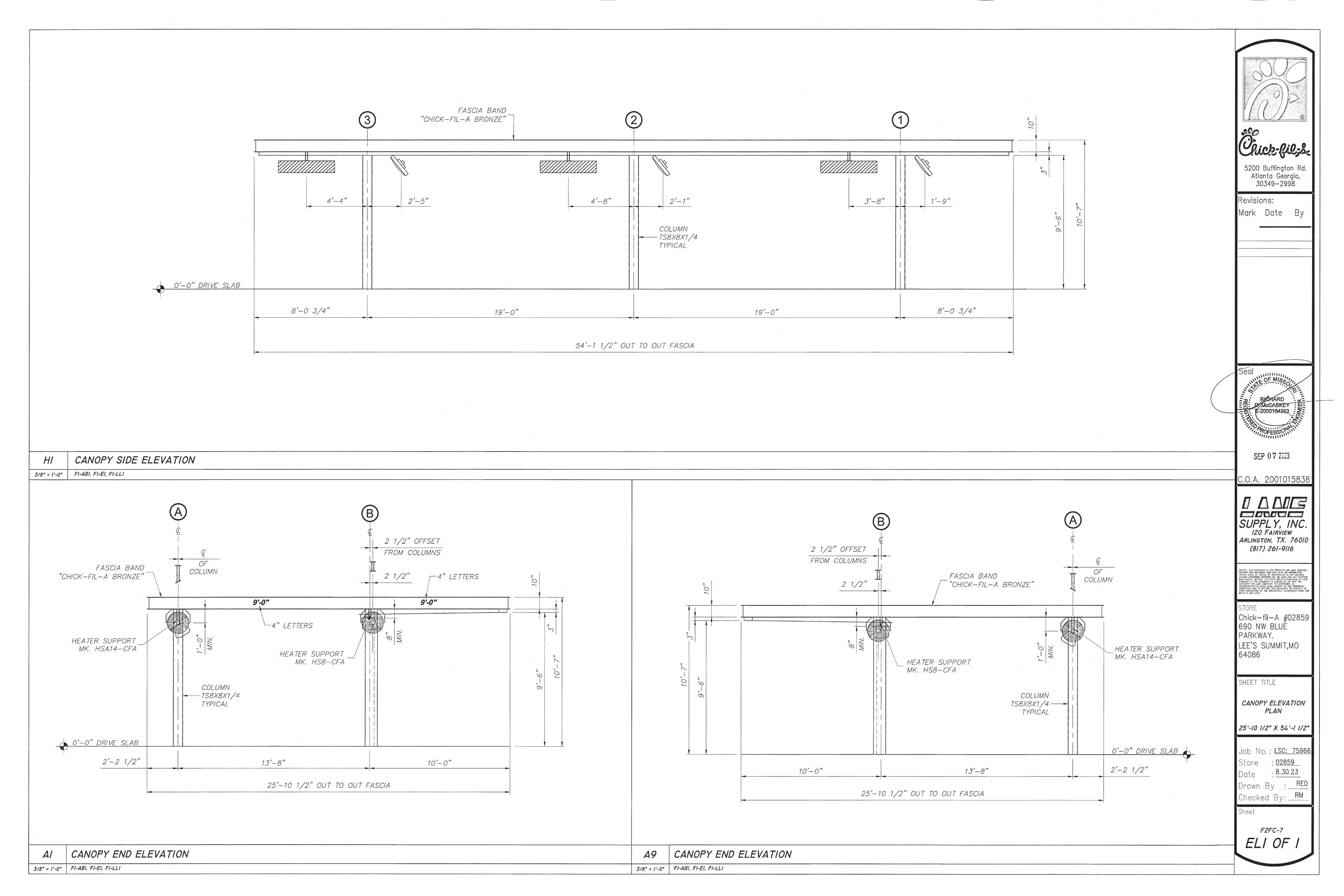


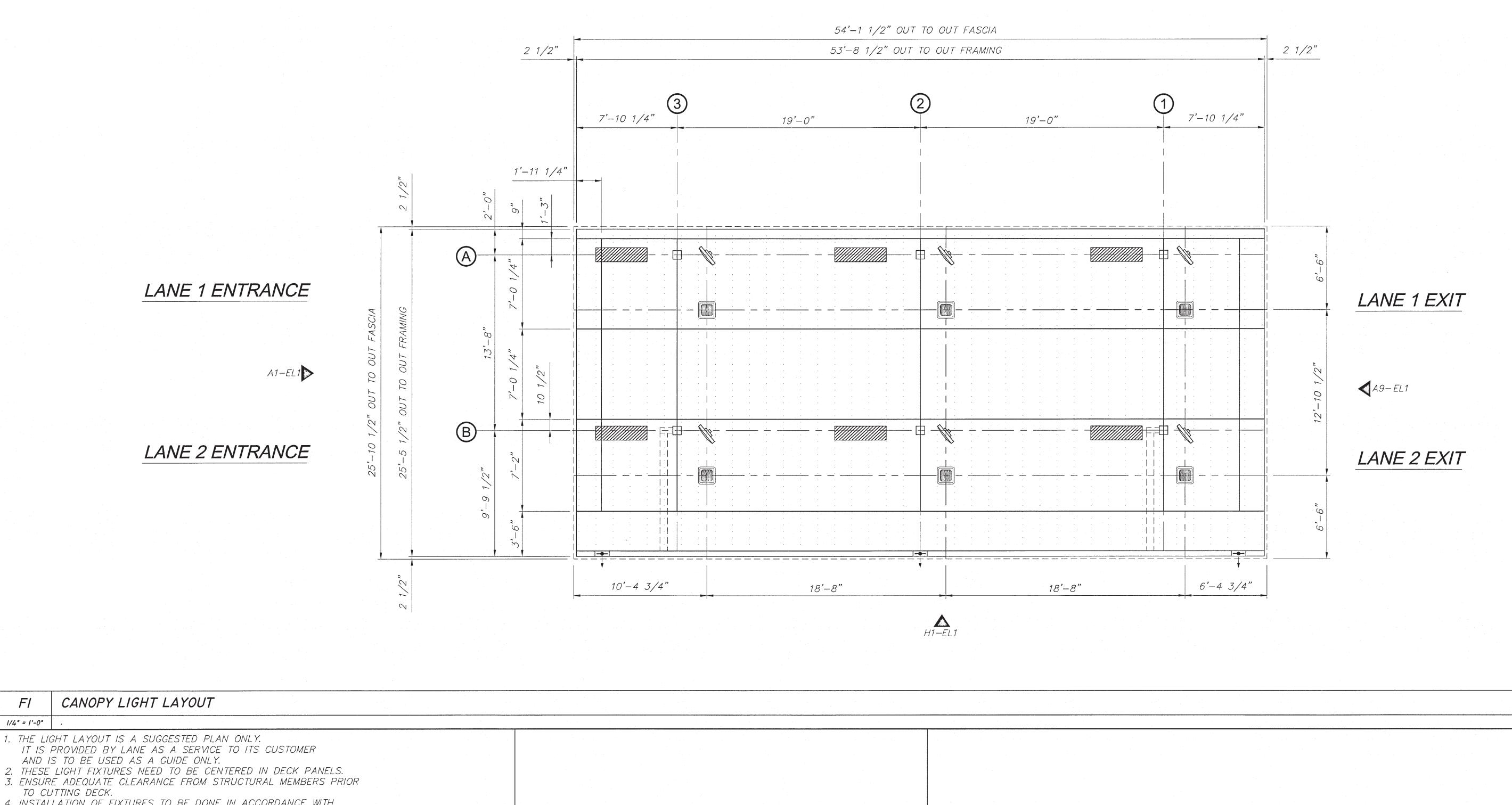


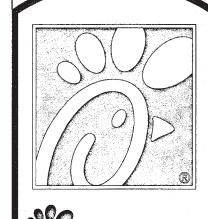






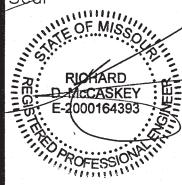






Revisions:

Mark Date By



SEP 07 2023

C.O.A. 2001015838

I A NIE SUPPLY, INC.
120 FAIRVIEW
ARLINGTON, TX. 76010 (817) 261-9116

Chick-fil-A #02859 690 NW BLUË PARKWAY. LEE'S SUMMIT,MO

SHEET TITLE

CANOPY LIGHT LAYOUT

25'-10 1/2" X 54'-1 1/2"

Job No.: <u>LSC: 75966</u> : <u>02859</u> 8.30.23

Drawn By : RE

Checked By: RM

LLI OF I

1/4" = 1'-0"

1. THE LIGHT LAYOUT IS A SUGGESTED PLAN ONLY. IT IS PROVIDED BY LANE AS A SERVICE TO ITS CUSTOMER

3. ENSURE ADEQUATE CLEARANCE FROM STRUCTURAL MEMBERS PRIOR

4. INSTALLATION OF FIXTURES TO BE DONE IN ACCORDANCE WITH MANUFACTURES INSTRUCTIONS AND RECOMMENDATIONS.

5. IF LIGHTS INTERFERE WITH LEADER GUTTERS MOVE ROW LIGHTS TO THE NEXT DECK.

LEGEND:

INDICATES LSI CRUS-SC-LED-LW-30-CW-UE-WHT CANOPY DECK LIGHTS.

INDICATES DECK STITCHING.

MOUNTED FANS/HEATERS (BY OTHERS) RE: SHEET É3 FOR MOUNTING SUPPORT

N. T. S.

INDICATES MOUNTED FAN

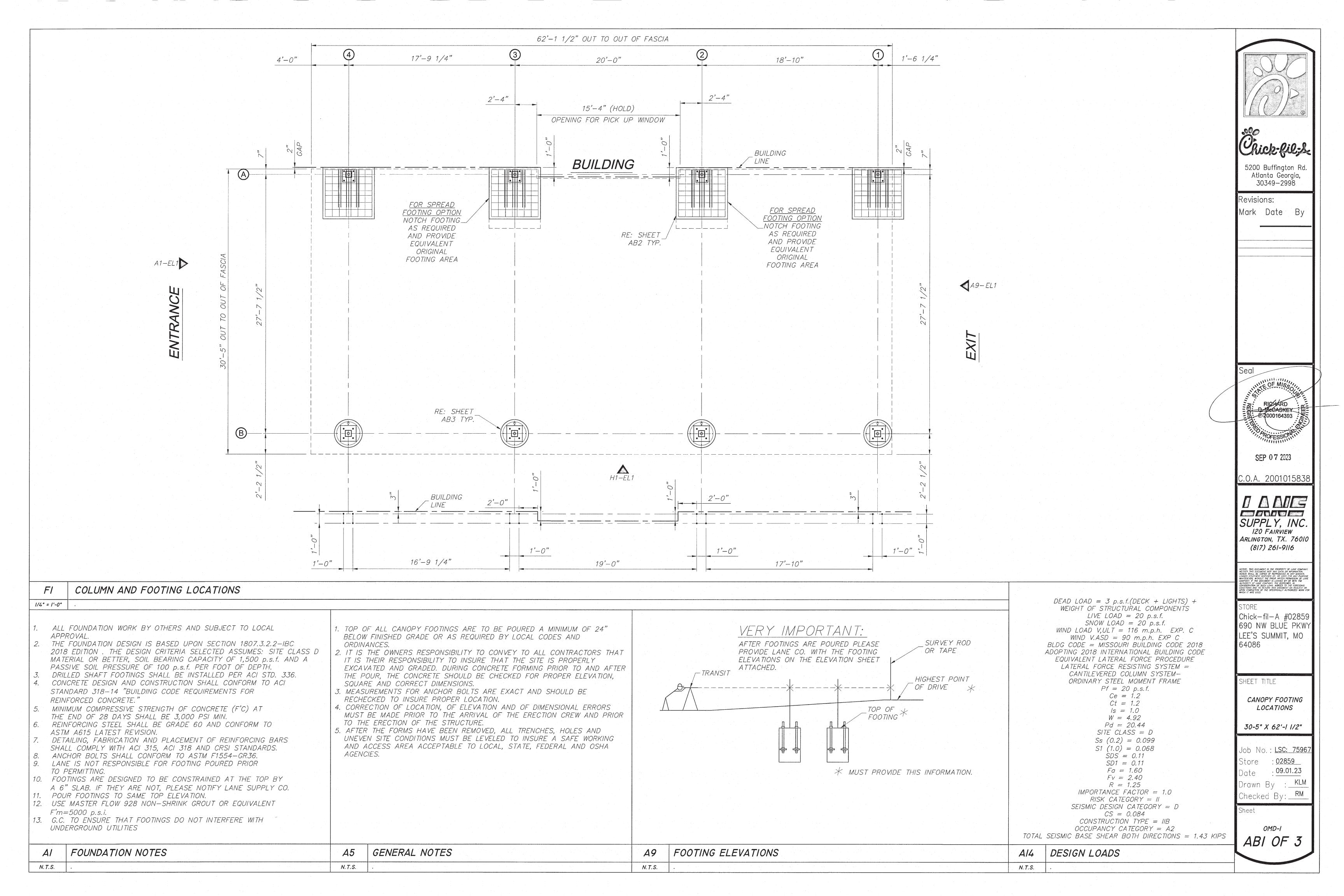


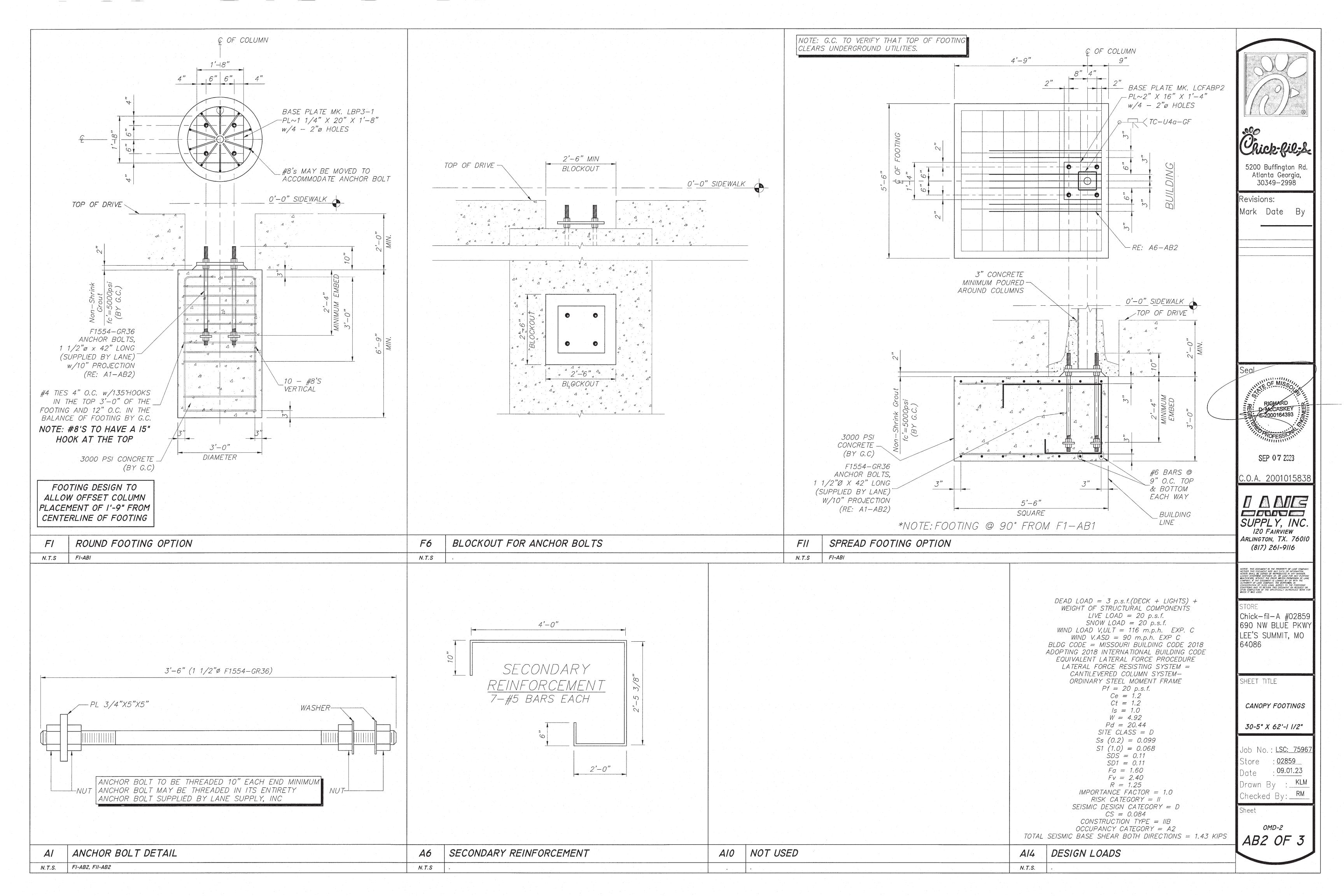
INDICATES MOUNTED HEATER

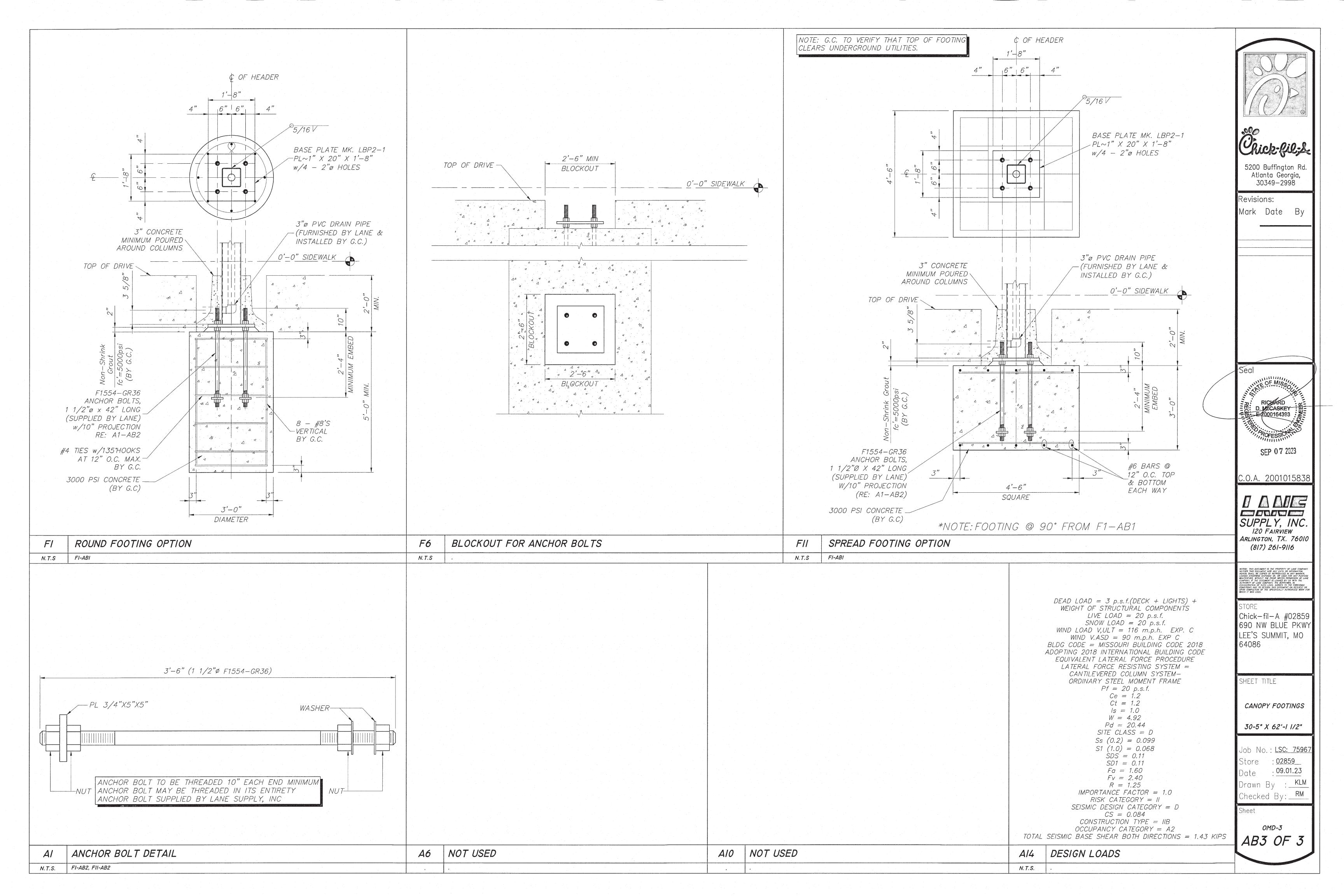
GENERAL NOTES

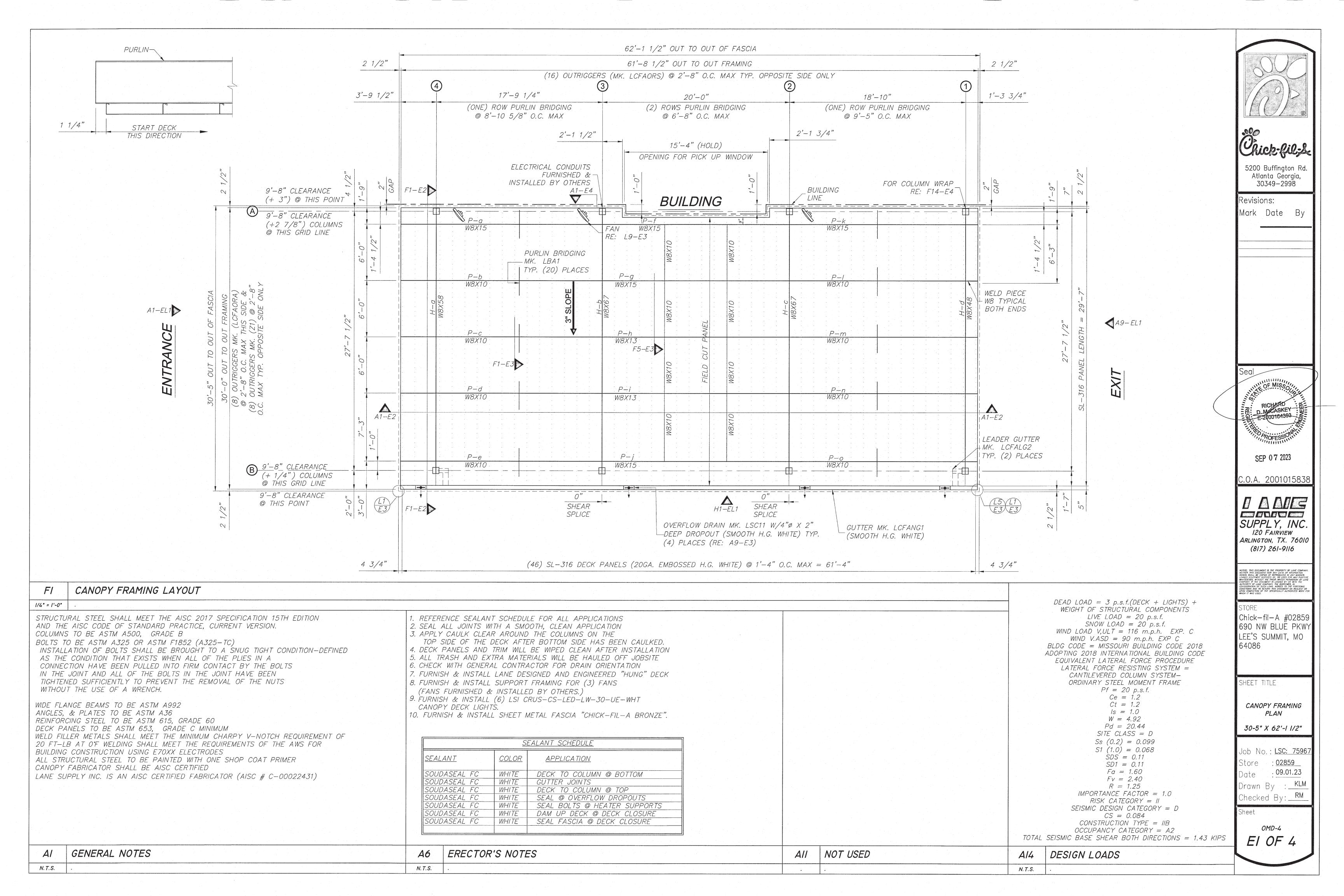
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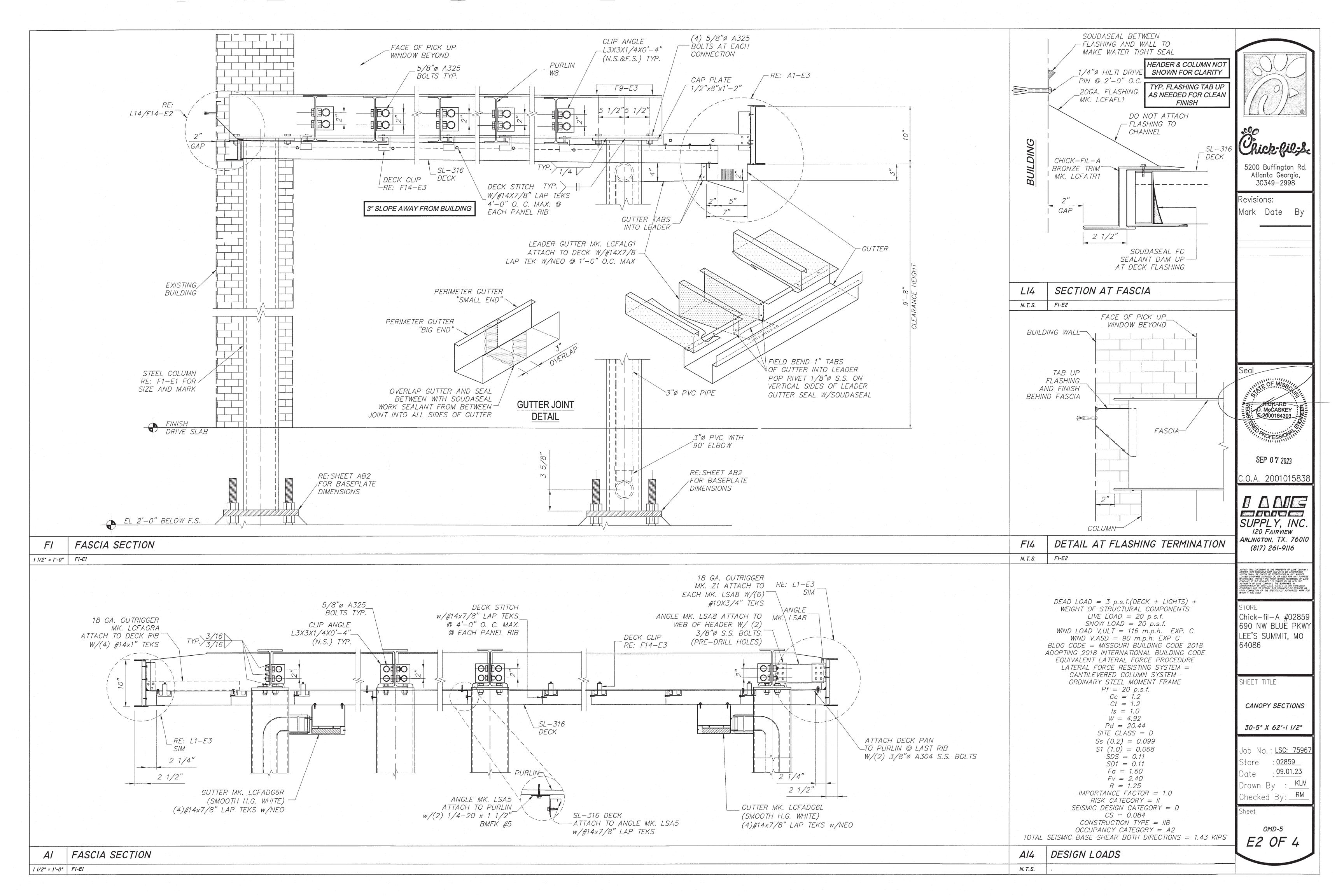
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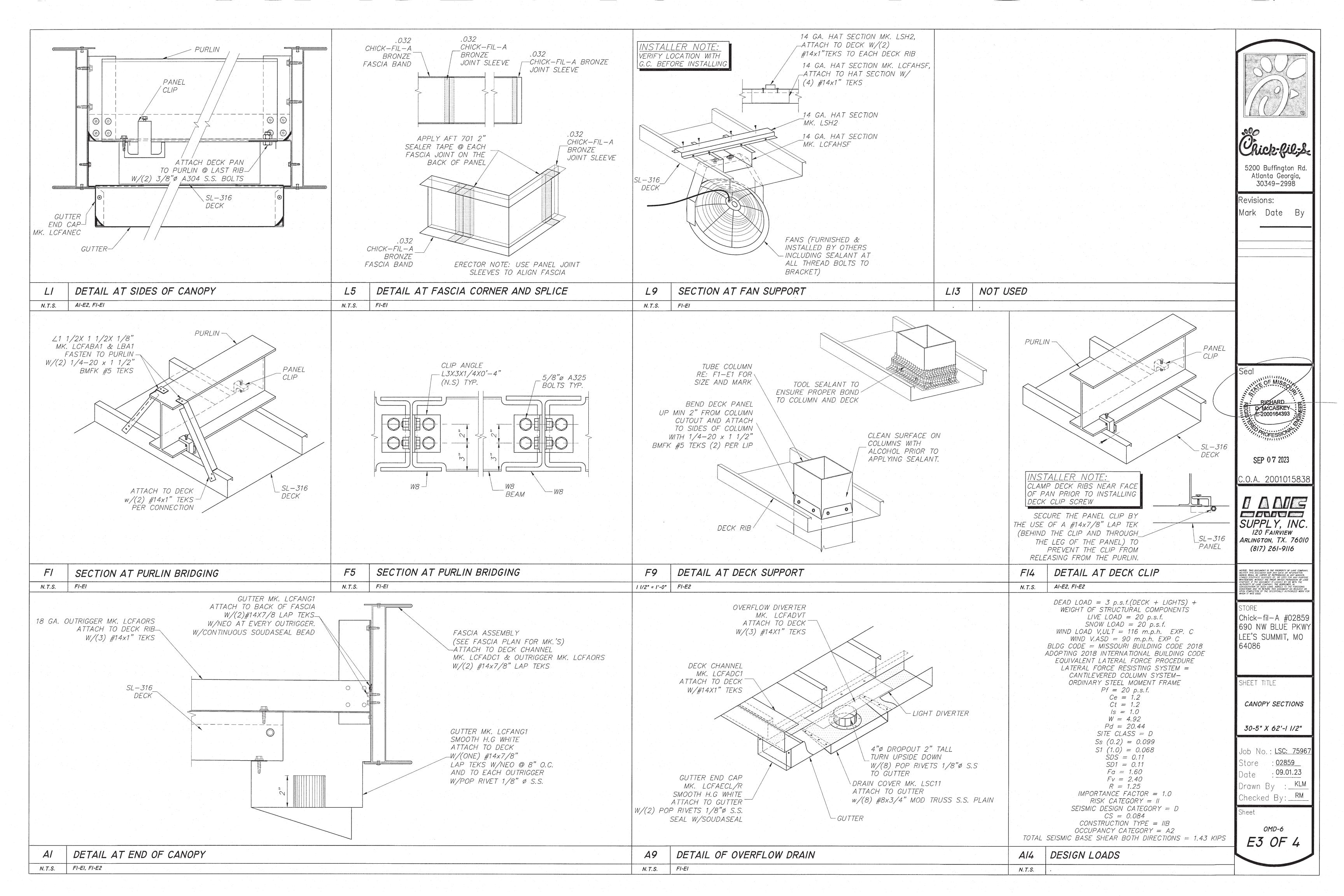


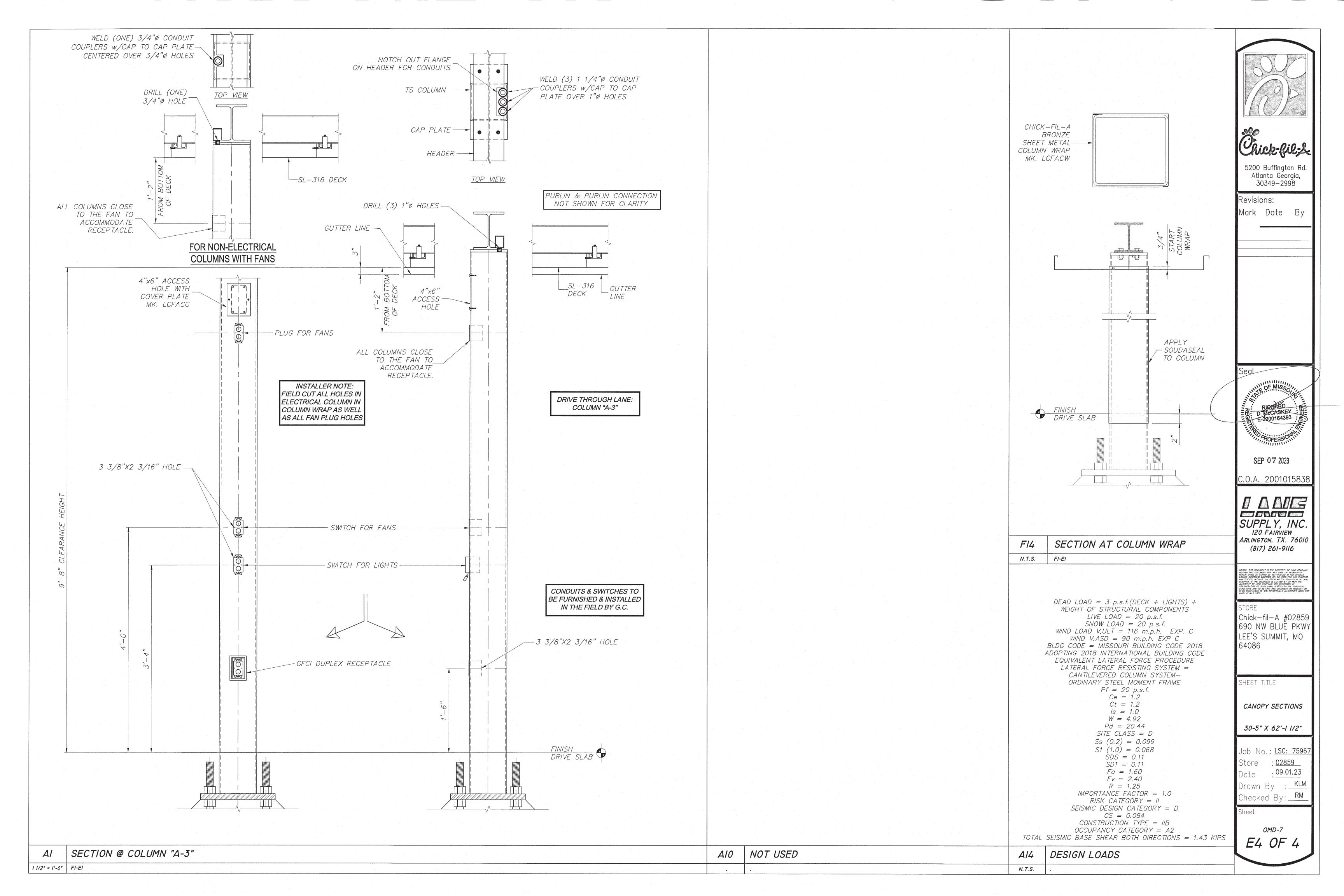


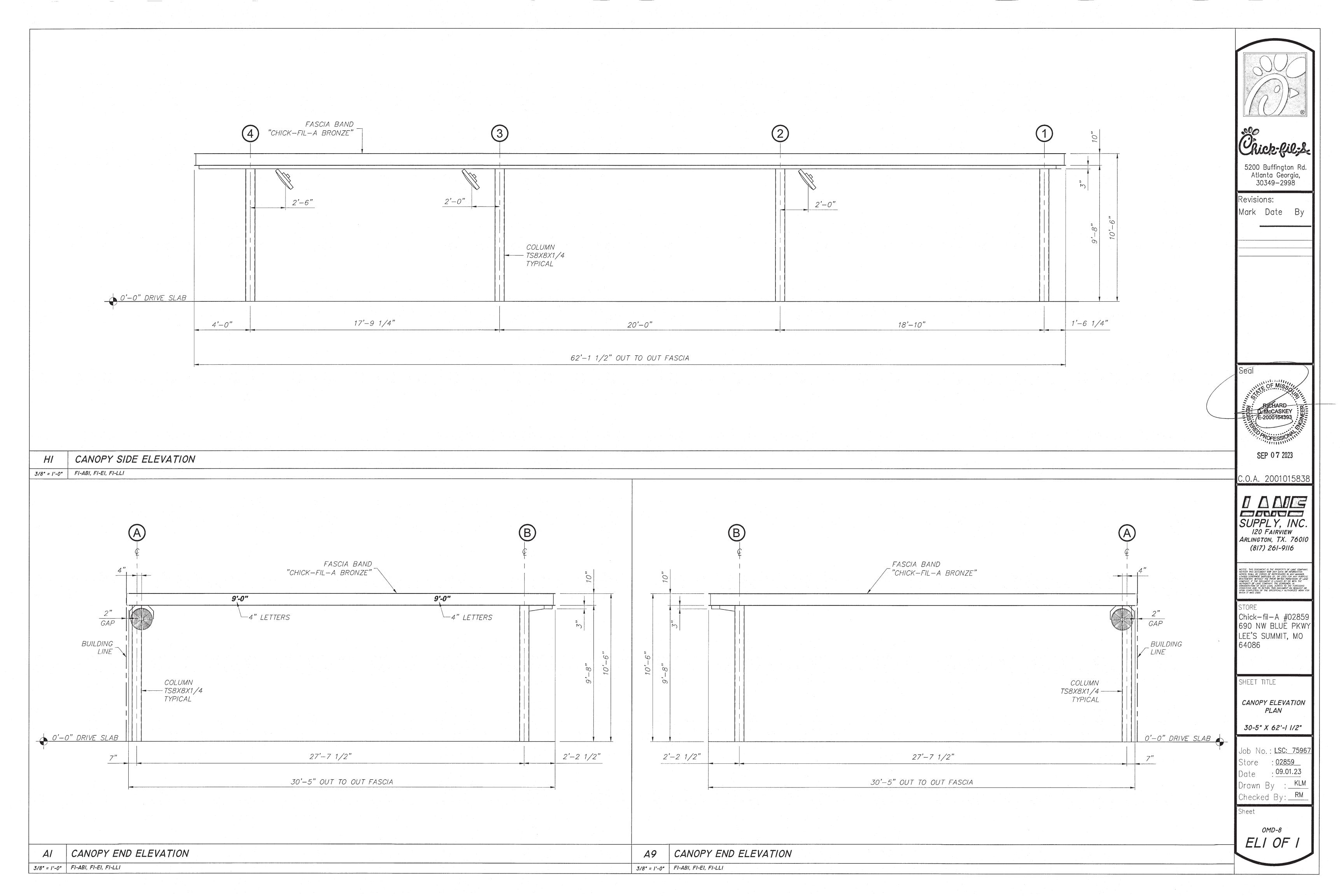


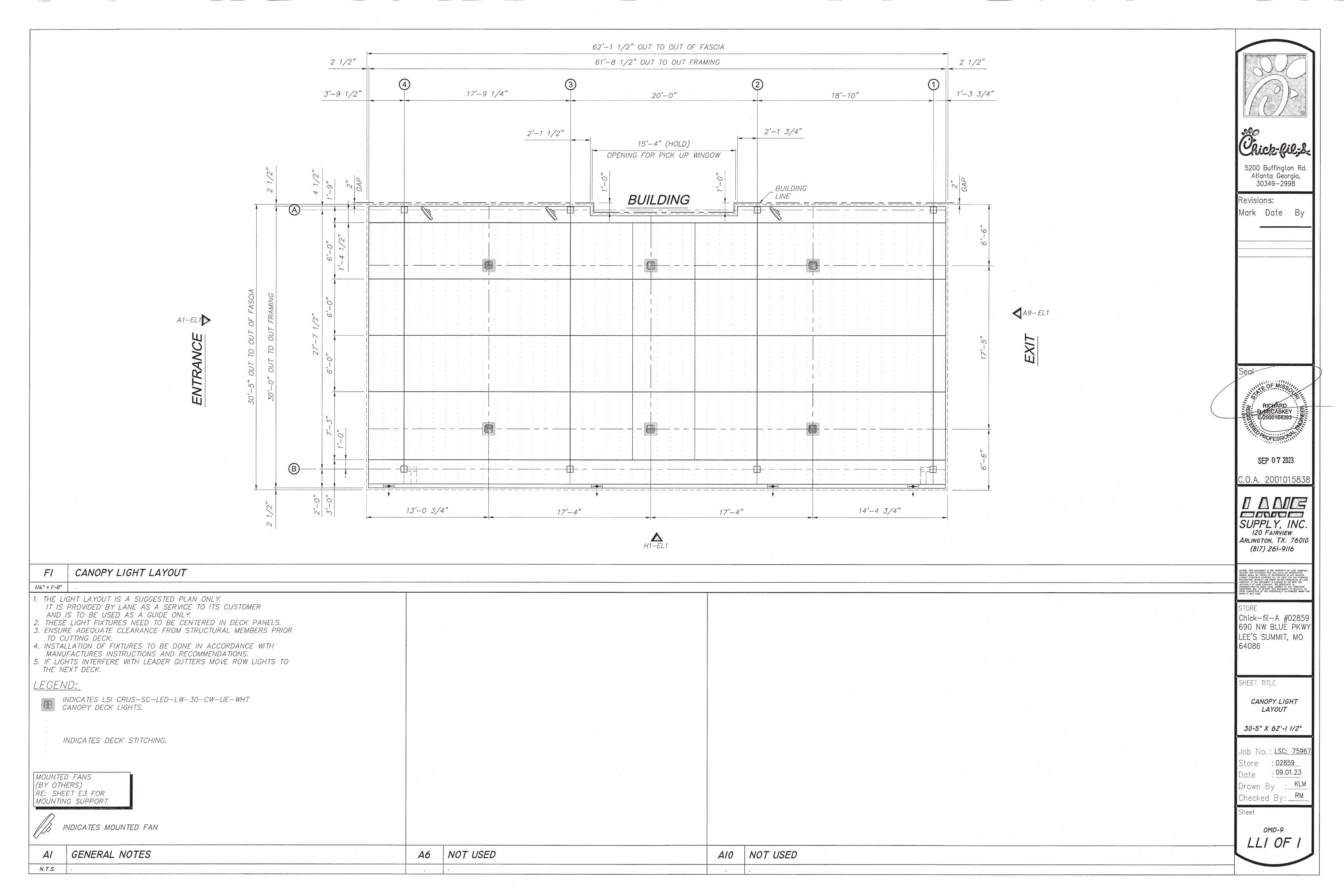














LANE SUPPLY, INC.

120 Fairview Arlington, TX 76010 817-261-9116

DESIGN CALCULATIONS FOR:

Chick-fil-A #02859 Order Canopy 690 NW Blue Parkway Lee's Summit, MO

Six-Column Canopy:

25'-5" X 53'-9" Canopy

Lane Reference Number :

LSC-75966

Date:

01-Sep-23

TABLE OF CONTENTS:

Canopy Calculations:

Design Loads: 1-2

Deck Design: 3

Purlin Design: 4-8

Header Design: 9-10

Column & Foundation Design:

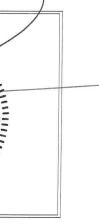
11-12

Attachments:

Lane St.-316 Deck Panel Properties
Lane Standard Base Plate Design

Design Sketch

Engineer's Seal:



C.O.A. 2001015838

SEP 07 2023

McGASKEY 2000164393 Calculations By: Lane Supply, Inc. LSC -75966 Customer: Chick-fil-A #02859 Order Canopy By: JO Project: 25'-5" X 53'-9" Canopy Check:

Code:

Missouri Building Code 2018 2018 International Builling Code

Roof Loads:

Dead Load = 3.00 psf (SL-316 Deck) Live/Snow Load = 20.00 psf

TOTAL = 23.00 psf

Fascia Load:

Height = 10.00 in. plf

Dead Load = 5.83

Wind Loads:

Risk Category = 11 V, ULT Speed = 116 m.p.h. Exp C V, ASD Speed = 90 m.p.h. Exp C Height = 15 Kd = 0.85 Kh = 0.85 G= 0.85 14.93 psf

Lateral Load = $1.0 (H) \cdot qz =$ 16.00 psf Deck Uplift = $-1.7 (V) \cdot G \cdot qz =$ -21.58 psf Frame Uplift = $-1.1 (V) \cdot G \cdot qz =$ -13.96 psf

qz =

Base Shear: V =

 $CS \cdot W =$

0.084 · W

Site Class = D Ss(0.2) =0.099 S1(1.0) =0.068 Fa = 1.60 Fv = 2.40 SM1 = Fv•S1 = 0.16 SMS = Fa·Ss = 0.16 SD1 = 2/3·SM1 = 0.11 SDS = 2/3.SMS = 0.11 1.25 R= Risk Category = 11

CS = (SDS/R) =0.084 (12.8-2)

B

Seismic Design Category Based on SDS: A Seismic Design Category Based on SD1: В

Design Category:

Section 7.1--Symbols & Notation

```
Ce =
           1.2
                    Exposure Factor as determined from Table 7-2
Ct =
           1.2
                    Thermal factor as determined from Table 7-3
 D = Snow Density in pcf as determined from Eq. 7-4
      Height of balanced snow load determined by dividing Pf by D, in feet.
hd = Height of snow drift, in feet
hc = Clear height from top of balanced snow to top of parapet, ft
hr =
          0.83
                     = Fascia height, ft
ls =
           1.0
                     = Importance factor (see Table 7-4).
Pf = Snow load on flat roofs, psf.
Pg =
                     =ground snow, psf.
           20
Pd = Maximum intensity of drift surcharge load, psf.
         25.875
                    = Length of roof upwind of the drift, feet
lu =
 w = Width of snow drift, in feet
```

Section 7.3--Flat-Roof Snow Loads, Pf

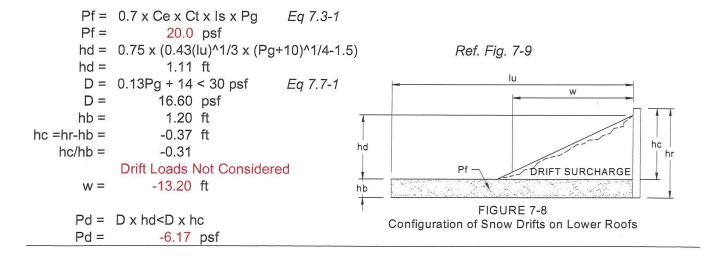
The snow load, Pf, on a roof with a slope equal to or less than 15° shall be calculated in psf using equation 7.3-1, but not less than the following minimum values for low slope roofs: where Pg is 20 psf or less Pf = I(Pg), where Pg exceeds 20 psf, Pf = 20 (I).

Section 7.7 & Section 7.8

The geometrey of the surcharge load due to snow drifting shall be approximated by a triangle as shown in figure 7-8. Drift loads shall be superimposed on the balanced snow load. If hc/hb is less than 0.2, drift loads are not required to be applied. The height of such drifts shall be taken as 0.75 x hd as determined from Fig 7-9, with lu equal to the length of the roof upwind of the projection or parapet wall. If the side of a roof projection is less than 15 ft long, a drift load is not required to be applied to that side. If the height, hd, is equal to or less than hc, the drift width shall equal 4hd and the drift height shall equal hd. If this height exceeds hc, the drift width, w, shall equal 4 hd²/hc and the drift height shall equal hc. However, the drift width w shall not exceed 8hc. The maximum intensity of the drift surcharge load, pd, equals hd x D where the snow density, D, is defined by Eq 7.7-

Section 7.10--Rain-On-Snow Surcharge Load

For locations where Pg is 20 psf or less but not zero, all roofs with a slope less than W/50, shall have a 5 psf rain-on-snow surcharge load appled to establish the design snow loads. This rain-on-snow augmented design load applies only to the balanced load case and need not be used in combination with drift, sliding, unbalanced, or partial loads.



P1					P2
V	o 23.00	psf	0		V
^A	B^		^C	_)^
X1> L1	> <	L2	> <	L3	> < X2>
Wd=	3.00 psf		X1= 0.75		
WI=	20.00 psf		L1= 7.02		
Deck: Ww=	-21.58 psf		L2= 7.02		
Frame : Ww=	-13.96 psf		L3= 7.17		
P1= P2=	5.83 plf		X2= 3.50	π	
P2-	5.83 plf		D A -d	40.0	C If
			RAd= RAI=		6 plf 1 plf
			Frame : RAW=	-60.0	
			Deck: RAw=	-92.8	()
MAd=	5.22 ft-lbs/ft		RA(d+l)=	105.3	
MAI=	5.63 ft-lbs/ft		Frame : RA(d+w)=	-40.6	
Deck : MAw=	-6.07 ft-lbs/ft		Deck : RA(d+w)=	-73.4	The second secon
MA(d+1)=	10.84 ft-lbs/ft	-	200111111(0111)	7011	. р
Deck: MA(d+w)=	-0.85 ft-lbs/ft		RBd=	20.3	2 plf
			RBI=	140.4	
			Frame: RBw=	-97.4	7 plf
			Deck : RBw=	-150.6	
MAB(d+I)=	139.12 ft-lbs/ft		RB(d+l)=	160.7	5 7
Deck: MAB(d+w)=	-114.04 ft-lbs/ft		Frame : RB(d+w)=	-77.1	•
•			Deck : RB(d+w)=	-130.3	1 plf
MBC(d+l)=	141.71 ft-lbs/ft		RCd=	15.8	7 plf
Deck : MBC(d+w)=	-114.47 ft-lbs/ft		RCI=	141.88	B plf
			Frame : RCw=	-87.1	1 plf
			Deck: RCw=	-134.63	
MCD(d+I)=	128.90 ft-lbs/ft		RC(d+I)=	157.74	1. A. C.
Deck: MCD(d+w)=	-77.16 ft-lbs/ft		Frame : RC(d+w)=	-71.24	•
			Deck : RC(d+w)=	-118.76	6 plf
			RDd=	32.50) plf
MDd=	38.79 ft-lbs/ft		RDI=	158.76	•
MDI=	122.50 ft-lbs/ft		Frame: RDw=	-110.83	
Deck: MDw=	-132.17 ft-lbs/ft		Deck: RDw=	-171.29	
MD(d+l)=	161.29 ft-lbs/ft		RD(d+l)=	191.26	6 plf
Deck: MD(d+w)=	-93.37 ft-lbs/ft		Frame : RD(d+w)=	-78.34	
			Deck : RD(d+w)=	-138.79	9 plf
USE 20 GAUGE G				*	
+S=.3961 in^3 -S=.30	36 in^3 FY=40 ksl				

BEAM DESI	GN:	P-a						
Wd=		1.5			P			
WI=	140.42	? plf			V	170.74	plf	-
Ww=		•			-	^A	B^	
Pd=					<>	<	L>	
PI=		lbs						
Pw=		lbs	Defle	ctions:	(inches)	Overhang	Midspan	_
L=				DL=		0.000	0.000	
X=	1.94	ft		L+LL=		-0.002	0.004	
			(+dov	vnward,	, -upward)			
MA(d) =		ft-lbs				RAd=		
MA(I) =		ft-lbs				RAI=	732	lbs
MA(w) =		ft-lbs	_			RAw=		lbs
MA(d+l) =	399	ft-lbs lu=		1.33	ft	RA(d+l)=	944	lbs
MA(d+w) =	-47	ft-lbs lu=		1.94	ft	RA(d+w)=	-296	lbs
						RBd=	67	lbs
						RBI(Max)=	415	lbs
						RBw=	-257	lbs
MAB(d+I)=		ft-lbs lu=		5.92	ft	RB(d+l)=	482	lbs
MAB(d+w)=	-271	ft-lbs lu=		1.33	ft	RB(d+w)=	-191	lbs
<u></u>	USE:	W8X10		Fy =	50	ksi		
DE 414 DE016								
BEAM DESIG		P-b	16					
	Wd=							
	WI=	140.42	•					
	Ww=	-97.47	100					
	L=	19.00	π					
		170.74	~ I£					
		170.74	рп					
			1	>	Dd-	200	llaa	
		<	L		Rd=	288		
	Md=	1368.2	ft lbo		RI=	1334		
	MI=	6336.3		-	Rw=	-926		
,	Mw=	-4398.2			R(d+l)= R(d+w)=	1622 -638		
	10100-	-4330.2	It-IDS		K(u+w)-	-030	IDS	
	M(d+l)=	7704.5	ft_lhe		Lu=	9.50	ft	ОК
	M(d+w)=	-3030.1			Lu=	1.33		OK
	W(G · W)-	-0000.1	ונ-וטס		Lu-	1.33	11	
	USE:	W8X10		Fy =	50	ksi		
_		Deflections	in al	\	N4: ala			
		Deflections: (inches)	Midspan			
		DL=			0.100			
		DL+LL= (+downward,	TIPLE	-4)	0.560			

BEAM DESIGN	N:	P-c							
Wd=	25.87				IP		The state of the s		
WI=	141.88	B plf			V	167.74	l plf		
Ww=	-87.11	plf				^A	B [']	١	
Pd=	36.39	lbs			<>	<	L>	1	
PI=	0.00	lbs							
Pw=	0.00	lbs	Defle	ctions:	inches)	Overhang	Midspan		
L=	5.92	! ft		DL=		0.000	0.000		
X=	1.94	ft		L+LL=		-0.002	0.004		
			(+dov	vnward,	-upward)				
MA(d) =	119	ft-lbs				RAd=	183	lbs	
MA(I) =	266	ft-lbs				RAI=	740	lbs	
MA(w) =	-164	ft-lbs				RAw=		lbs	
MA(d+l) =		ft-lbs lu=		1.33	ft	RA(d+l)=		lbs	
MA(d+w) =		ft-lbs lu=		1.94		RA(d+w)=			
						()			
						RBd=	56	lbs	
						RBI(Max)=		lbs	
						RBw=			
MAB(d+l)=	676	ft-lbs lu=		5.92	ft	RB(d+l)=		lbs	
MAB(d+w)=		ft-lbs lu=		1.33		RB(d+w)=			
(,		11 100 10		1.00		(Carw)	17.7	100	
	USE:	W8X10		Fy =	50	ksi			
BEAM DESIGN	l:	P-d							
	Wd=	25.87	plf						
	WI=	141.88	plf						
	Ww=	-87.11	plf						
	L=	19.00	ft						
		167.74	plf						
		٨		٨					
		<	L	>	Rd=	246	lbs		
					RI=	1348	lbs		
	Md=	1167.3	ft-lbs		Rw=	-828	lbs		
	MI=	6402.1	ft-lbs	-	R(d+I)=	1594			
	Mw=	-3930.9			R(d+w)=	-582			
					,				
	M(d+l)=	7569.4	ft-lbs		Lu=	9.50	ft	OK	
	M(d+w)=	-2763.6	ft-lbs		Lu=	1.33		OK	
17.0	USE:	W8X10		Fy =	50	ksi			
		D (1 .:							
			inches'		Midspan				
		Deflections: (IIICHES,						
	_	DL=	iiiciies,		0.085				

		Λ	B A	ES	AOI	١.
-	_	Δ	11//	 -	11-11	

Р-е

P1d =	212.11	lbs		P1	P	2
P1I =	732.00	lbs	۸ ===	▼	▼	p
P1w =	-508.10	lbs				В
P2d =	183.17	lbs		X1	X2	X3
P2I =	739.60	lbs			L	
P2w =	-454.12	lbs				-
				X1 =	7.02	ft
Wd =	16.00	plf		X2 =	7.02	ft
WI =	0.00	plf		X3 =	7.17	ft
Ww =	0.00	plf		L =	21.21	ft

RAd = RAI =	373 740	lbs	
RAw =	-493	10000 01	
RA(d+I) =	1113	lbs	
RA(d+w) =	-120	lbs	181
RBd =	361	lbs	
RBI =	732	lbs	
RBw =	-469	lbs	
RB(d+I) =	1093	lbs	
RB(d+w) =	-108	lbs	

MAB(dI) =	2301	ft-lbs			
MAB(II) =	5246	ft-lbs			
MAB(wl) =	-3464	ft-lbs			
MAB(dI+II) =	7520	ft-lbs	lu =	 7.17	ft
MAB(dl+wl) =	-1236	ft-lbs	lu =	7.17	ft

Deflection

dI = 0.202 in dI+II = 0.665 in

USE: W6X16	Fy =	50 ksi

P1d= P1I=	25.09 lbs 0.00 lbs	V		P2				
P1w=	0.00 lbs	¥				Λ Λ		P
P2d=	373.46 lbs		X1	I	X2	A A	X3	В
P2I=	739.60 lbs	<		-		unikinin.	^3	
P2w=	-493.36 lbs							
Wd =	39.36 plf			RAd=	1272.	12 lbs		
WI =	86.01 plf			RAI=		17 lbs		
Ww=	-60.04 plf			RAw=	-1786.4			
			-	RAd+I=		29 lbs		
				RAd+w=		36 lbs		
X1=	1.94 ft							
X2=	5.92 ft			RBd=	183.3	34 lbs		
X3=	19.00 ft			RBI=		15 lbs		
				RBw=		32 lbs		
				RBd+l=		19 lbs		
				RBd+w=		97 lbs		
				, , , , , , , , , , , , , , , , , , , ,	100.0	71 150		
	MA(d)=	3621 ft-lbs						
	1VI/ ((CI)	7000 511						

MA(d)=	3621	ft-lbs				
MA(I)=	7029	ft-lbs				
MA(w)=	-4771	ft-lbs				
MA(d+I)=	10649	ft-lbs lu	=	1.33	ft	
MA(d+w)=	-1150	ft-lbs lu	=	5.92	ft	
MAB(d+I)=	1557	ft-lbs lu	=	9.50	ft	
MAB(d+w)=	-439	ft-lbs lu	=	1.33	ft	

Deflections

	ОН	SPAN
dl (in)=	0.221	-0.023
dl+ll (in) =	0.616	-0.045

USE:	W6X20	Fy =	50 ksi	

P1d=	46.30 II	bs	P1		P2				
P1I=	0.00 II	bs			1				
P1w=	0.00 II	bs	<u></u>				Λ Λ		В
P2d=	361.16 II	bs		X1		X2	A A	Х3	
P2 =	732.00 II	bs	<	7(1	> -	7,2	D	7.0	
P2w=	-468.87 II	bs							
Wd =	45.50 p	olf			RAd=	1402.4	7 lbs		
WI =	158.76 p	olf			RAI=	3972.8	2 lbs		
Ww =	-110.83 p	olf			RAw=	-2718.2	0 lbs		
					RAd+l=	5375.2	9 lbs		
					RAd+w=	-1315.7	3 lbs		
X1=	1.94 ft								
X2=	5.92 ft				RBd=	226.7	5 lbs		
X3=	19.00 ft				RBI=	1022.5	4 lbs		
					RBw=	-726.9	8 lbs		
					RBd+l=	1249.2	9 lbs		
					RBd+w=	-500.2	3 lbs		
	B A A / II	0004 6 11							

MA(d)=	3904	ft-lbs				
MA(I)=	9228	ft-lbs				
MA(w)=	-6193	ft-lbs				
MA(d+l)=	13132	ft-lbs	lu =	1.33	ft	_
MA(d+w)=	-2289	ft-lbs	lu =	5.92	ft	
MAB(d+I)=	3803	ft-lbs	lu =	9.50	ft	
MAB(d+w)=	-1915	ft-lbs	lu =	1.33	ft	

Deflections

	ОН	SPAN
dl (in)=	0.239	-0.018
dl+ll (in) =	0.624	0.067

USE: W8X13 Fy =	50	ksi
-----------------	----	-----

P1d =		2 lbs		P1			P2	1.5	-3		P4
P1I =	2602	2 lbs		Γ			_' _	Ι,	,		1, 4
P1w =	-1786	3 lbs	,								
P2d =	358	5 lbs		1	manana a	_z A		1	В	A	
P2I =	1749	9 lbs		X	1	X2		X3	X4 B	/////X5	
P2w =	-1183	3 lbs							-		
P3d =		2 lbs					X1 =	1.25	5 ft		
P3I =		B lbs					X2 =	5.77			
P3w =	-1058						X3 =	7.02			
P4d =		2 lbs					X4 =	0.88			
P4I =	3973						X5 =	6.29			
P4w =	-2718						V2 -	0.28	7 11		
P4W =	-2/10	Sui									
Wd =	24.00	•									
WI =) plf									
Ww=	0.00) plf									
	RAd=	=	1128	lbs				RBd=	271	3 lbs	
	RAI=		2135	lbs				RBI=	795	7 lbs	
	RAw=	=	-1450	lbs				RBw=	-529	3 lbs	
-	RAd+l=		3263	lbs		-		RBd+l=	1067) lbs	
	RAd+w=		-322	lbs				RBd+w=	-258	3 lbs	
MA(DL):	-1608.9	ft-lbs									
MA(LL):	-3252.7										
MA(WL):	2233.1								Deflection		
MA(DL+LL):	-4861.6		lu =		1.25	ft		DL =		2 in	
MA(DL+WL):		ft-lbs			1.25			DL+LL =		in	
MA(DL: WL).	024.2	11-103	iu –		1.20	11		DL ILL -	0.00)	
		0544	-								
	1001.0	SPAN	Commence of the Commence of th		= 00				Deflection		
M(DL+LL):	-4861.6				7.02			DL =	-0.06		
M(DL+WL):	624.2	ft-lbs	lu =		7.02	ft		DL+LL =	-0.08	3 in	
MB(DL):	-9298.9	ft_lhe									
MB(LL):	-24995.6										
	17102.0								Deflection		
MB(WL): MB(DL+LL):	-34294.5		lu =		6.29	£4		DI -		l lm	
								DL =	0.11		
MB(DL+WL):	7803.1	IL-IDS	iu =		6.29	П		DL+LL =	0.38	s in	
	USE:	W8X2	1		Fy =		50 ks	oi			
_	OOL.	110/12			' y -		JU K	31	<u> </u>		
	The second secon										

P1d = P1l = P1w =	89	7 lbs 4 lbs 9 lbs	,	P1			P2	2	Р3			P4
P2d = P2l = P2w =	57 266	6 lbs 8 lbs 2 lbs		>	<17///	A X2		Х3	-	х ⁴	/// X5	
P3d = P3l =	492	2 lbs 2 lbs 6 lbs					X1 = X2 =		5 ft 7 ft			
P3w =							X3 =		2 ft			
P4d =	453	3 lbs					X4 =		8 ft			
P4I =	204	5 lbs					X5 =		9 ft			
P4w =	-1454	4 lbs										
Wd =	20.00											
WI =) plf										
Ww=	0.00) plf										
	RAd=		690					RBd:	=	1622	lbs	
	RAI=		1749					RBI:	=	6554		
	RAw=		-1204			_		RBw:		-4396		
	RAd+I=		2438					RBd+l		8177		
	RAd+w=	-	-514	lbs				RBd+w	=	-2774	lbs	
MA(DL):	-474.0	ft-lbs										
MA(LL):												
MA(WL):		ft-lbs				_			De	eflection		
MA(DL+LL):			lu =		1.25			DL =		-0.00	in	
MA(DL+WL):	324.3	ft-lbs	lu =		1.25	ft		DL+LL =		-0.00	in	
		SPAN	I						De	flection		
M(DL+LL):	4724.0				7.02	ft		DL =		-0.01	in	
M(DL+WL):	-1549.8				7.02			DL+LL =		0.01		
MP(DL):	-3249.1	ft lbo										
MB(DL):	-3249.1											
MB(LL):	9147.8								D	flootice		
MB(WL): MB(DL+LL):	-16116.1		lu =		6.29	ft		DL =	ь	flection	in	
MB(DL+UL):	5898.7				6.29			DL = DL+LL =		0.06		
WID(DL ' VV L).	3030.7	פטו-זו	iu –		0.23	ıt		DLTLL -		0.30	1[1	
	USE:	W6X2	0		Fy =		50 k	si				
									_			

Column Des	ign			AISC	15th ed, Use I	First Order An	alysis Criteria
	P DL = 2	.71	kips		Clr. Ht.=	9.50	ft
	P LL = 7	.96	kips		Fascia Ht.=	1.00	ft
	PWL = -5	.30	kips		Col. Trib=	19.27	ft
E	Base Shear = 0	.20	kips		Wind Load=	16.00	psf
Total E	Base Shear = 0	.84	kips		# of COL.=	2	_
MWL =	w(Fascia Ht•2.5•Col Trib./#	of co	ol•L)+ w(Wrap•1/	2 Clr. Ht^2)	Max All. Defl =	1.20	in
M Seis =	Base Shear x L			N	Max Defl Ratio =	L/	100
M Unbal =	Live Load x Col. Trib.x (Car	ору	Width/2)^2/2		Max Defl. =	0.13	in, OK
L =	Clr. Ht. + Fascia Ht/2						
Pr =	10.67 kips 1.6F	r<0	.5Py First-Or	der Analysis A	Allowed (A-7-1	1)	
Py =	326.60 kips						
N =	0.00 •Yi (A-7-	2)		Use:	TS8X8X1/4	FERENCE	
B2 =	1.05 OK, A-8-	6		Fy =	46.00	ksi	
MWL =	4.58 kip-ft			K =	1.00		
M Seis =	1.98 kip-ft			L, Col =	10.00	ft	
M DL(Nod) =	0.11 kip-ft			A =	7.10	in^2	
M LL(Nod) =	0.33 kip-ft			l =	70.70	in^4	
M Unbal DL=	0.00 kip-ft			Cm =	1.00		
M Unbal LL=	0.00 kip-ft			Pe1 =	447.31	kips	
M Unbal WL=	0.00 kip-ft			B1 =	1.04	(A-8-3)	
				P,AII =	177.38	kips	
,	1		_ 1	M, All =	44.10	kip-ft	
	Load Combination		Pr, Kips	Mr, Kip-ft	Equation	Result	
	D+L		10.67	0.47	0.04	OK	
	D+W		2.71	4.88	0.12	OK	
	D+0.7E		2.71	1.56	0.04	OK	
	D+0.75W+0.75L		8.68	3.95	0.11	OK	
	D+0.525E+0.75L		8.68	1.46	0.06	OK	

Top Connection :	Standard Cap Plate	Base Plate :	LBP 8 - 20	

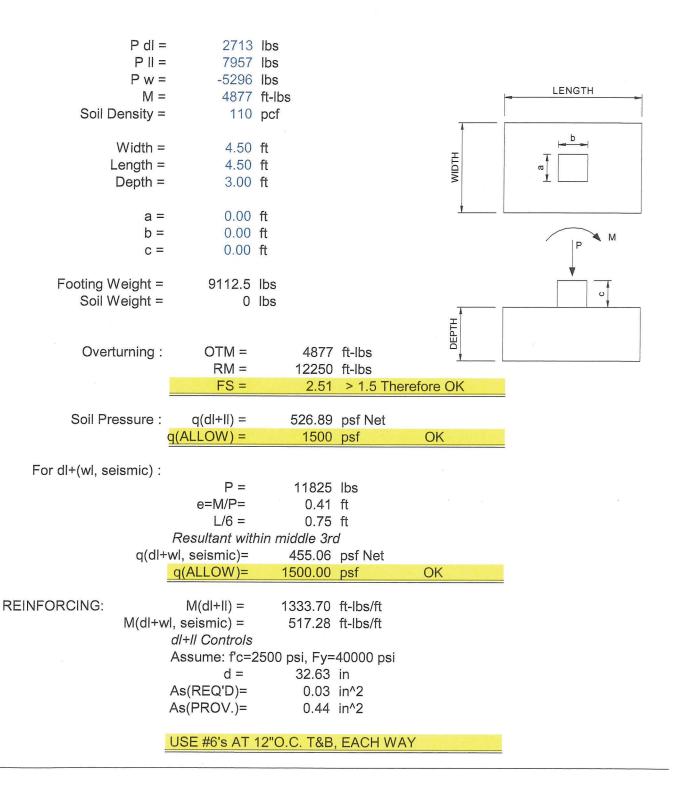
Foundation: (Restrained at Grade)

d^2=(4.25*M)/(S3*b)

M(MAX)=4877 ft-lbs Pmax= 10.67 kips S3= 100 PCF X d Footing Area= 7.07 ft^2 b= 3.000 ft Bearing= 1509.44 psf d= 4.103 ft Footing= Round USE: 3.00 FT.RND. X 5.00 ft deep footing

As=12*M/(jd*24000)= 0.0653 in^2

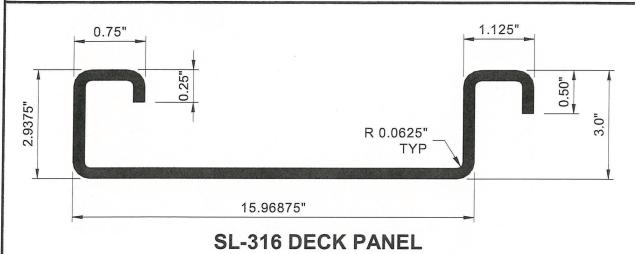
USE: 8 #8's (RND. Cage) w/ #4 Ties @ 12" O.C. w/135 hooks





LANE SUPPLY, INC.

120 Fairview Arlington, Texas 76010 817-261-9116



				Section F	Properties				
Gage	Wt, psf	Thickness, in	ASTM 653	+I, in ⁴	-I, in ⁴	+S, in ³	-S, in ³	+M, ft-lbs/ft	-M, ft-lbs/ft
20	2.20	0.0359	Grade 40	0.9346	0.4680	0.3961	0.3036	592.70	454.44
20	2.20	0.0000	Grade 50	0.9208	0.4522	0.3879	0.2880	725.86	538.92
18	2.93	0.0478	Grade 40	1.2486	0.6827	0.5329	0.4377	797.77	655.28
10	2.90	0.0470	Grade 50	1.2129	0.6518	0.5141	0.4296	962.09	803.92

Notes:

- 1 Designed per AISI Cold Formed Steel Manual, 2016 ed.
- 2 Complete calculations are available upon request.
- 3 ± M is allowable bending moment.

Issued 12-5-17



120 Fairview Arlington, Texas 76010 817-261-9116 FAX 817-275-1660

STANDARD BASE PLATE DESIGN

LE	3P	#	M	P _{BOLT}	Bolt Dia.	t REQ'D	t ACTUAL	Weld Req'd	Weld Actual	Base Plate
(D		M)	(ft-k)	(k)	(in)	(in)	(in)	(1/16 in)	(in)	Mark
8	_	10	10	5.58	1 1/2	0.72	3/4	1.52	1/4	LBP 1
8	-	20	20	10.91	1 1/2	0.99	1	3.03	5/16	LBP 2
8	-	30	30	16.00	1 1/2	1.17	1 1/4	4.55	5/16	LBP 3
8	-	40	40	20.87	1 1/2	1.32	1 1/2	6.06	F.P.	LBP 4
8	-	50	50	26.09	1 1/2	1.46	1 1/2	7.58	F.P.	LBP 5

TS 8 X 8 COLUMN:

D= 8 in.

e= 2 in.

b,d= 8 in.

CONSTANTS:

A36 Steel Plate

E70xx Electrode

A307 Anchor Bolts

Fy = 36 ksi

Fw = 0.928 k/in/16th

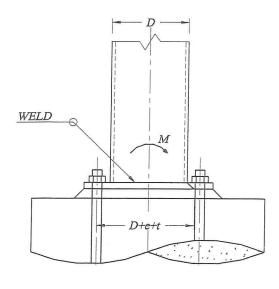
Ft = 20 ksi

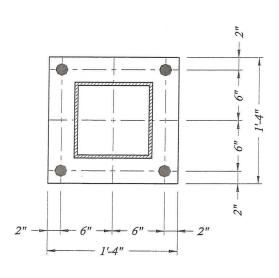
EQUATIONS:

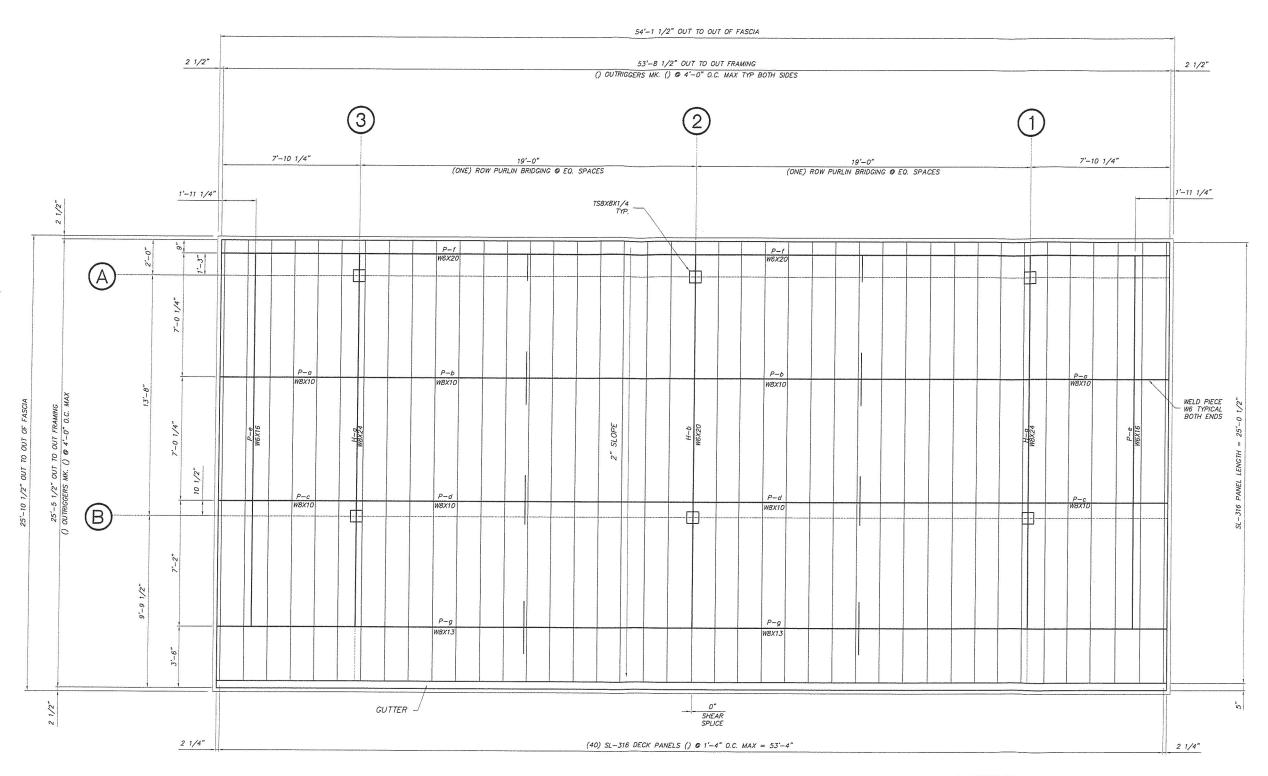
$$P_{BOLT} = \frac{M \times 12 \text{ in/ft}}{2 \text{ bolts } (D+e+t)}$$

$$Weld = \frac{M \times 12 \text{ in/ft}}{S_{\text{weld}} \times F_{\text{W}}} = \frac{M \times 12 \text{ in/ft}}{F_{\text{W}} (bd+d^{2}/3)}$$

$$t_{RBQD} = \sqrt{\frac{6 \times P \times e \times 2 \text{ bolts}}{0.75 \times Fy \times (D+2t)}}$$







DESIGN LOADS:

DEAD LOAD = 3 p.s.f.(DECK + LIGHTS) + WEIGHT OF STRUCTURAL COMPONENTS
LIVE. LOAD = 20 p.s.f.
SNOW LOAD = 20 p.s.f.
WHID LOAD V.LLT = 116 m.p.h. EXP. C
WIND V.ASD = 90 m.p.h. EXP. C
BLOC CODE = MISSOURI BUILDING CODE 2018
ADDPTING 2018 INTERNATIONAL BUILDING CODE
EQUIVALENT LATERAL FORCE PROCEDURE

LATERAL FORCE RESISTING SYSTEM = CANTILLEYRED COLUMN SYSTEM-ORDINARY STEEL MOMENT FRAME
Pf = 20 p.s.f.
Ce = 1.2
LT = 1.2
S = 1.0
W = DRIFT LOADS NOT CONSIDERED
Pd = DRIFT LOADS NOT CONSIDERED
Pd = DRIFT LOADS NOT CONSIDERED
SITE CLASS = 0
SS (0.2) = 0.099
S1 (1.0) = 0.058
SD = 0.11
SD = 0.11
F0 = 1.60
FY = 2.40
R = 1.52
IMPORTANCE FACTOR = 1.0
RISK CATEGORY = II
SEISMIC DESIGN CATEGORY = II
CONSTRUCTION TYPE = IIB
COLUMNIC BASE SHEAR BOTH DIRECTIONS = 0.84 KIPS



LANE SUPPLY, INC.

120 Fairview Arlington, TX 76010 817-261-9116

DESIGN CALCULATIONS FOR:

Chick-fil-A #02859 Outside Meal Delivery Canopy 690 NW Blue Parkway Lee's Summit, MO

Eight-Column Canopy:

30'-0" X 61'-9" Canopy

Lane Reference Number:

LSC-75967

Date:

04-Sep-23

TABLE OF CONTENTS:

Canopy Calculations:

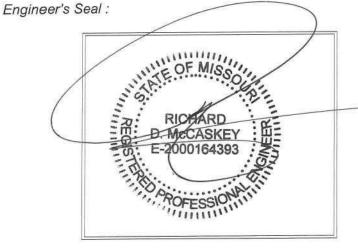
Design Loads: 1-2
Deck Design: 3-6
Purlin Design: 7-14
Header Design: 15-18

Column & Foundation Design:

19-23

Attachments:

Lane SL-316 Deck Panel Properties Lane Standard Cap Plate Design Lane Offset Base Plate Design Design Sketch



C.O.A. 2001015838

SEP 07 2023

Calculations By: Lane Supply, Inc. LSC -75967 Customer: Chick-fil-A #02859 Outside Meal Delivery Canopy By: JO-Project: 30'-0" X 61'-9" Canopy Check: Code: Missouri Building Code 2018 2018 International Builling Code Roof Loads: (SL-316 Deck) Dead Load = 3.00 psf Live/Snow Load = 20.00 psf TOTAL = 23.00 psf Fascia Load: Height = 10.00 in. Dead Load = 5.83 plf Wind Loads: Risk Category = 11 V, ULT Speed = 116 m.p.h. Exp C V, ASD Speed = 90 m.p.h. Exp C Height = 15 Kd = 0.85 Kh = 0.85 G = 0.85 qz =14.93 psf Lateral Load = $1.0 (H) \cdot qz =$ 16.00 psf Deck Uplift = $-1.7 (V) \cdot G \cdot gz =$ -21.58 psf Frame Uplift = -1.1 (V)•G•qz = -13.96 psf Base Shear: V = CS · W = 0.084 · W Site Class = D Risk Category = 11 Ss(0.2) =0.099 S1(1.0) =0.068 Fa = 1.60 Fv = 2.40 SMS = Fa·Ss = 0.16 (11.4-1) SM1 = Fv•S1 = 0.16 (11.4-2) SDS = 2/3•SMS = 0.11 (11.4-3) SD1 = 2/3·SM1 = 0.11 (11.4-4) R= 1.25 CS = (SDS/R) =0.084 (12.8-2) Seismic Design Category Based on SDS: A Seismic Design Category Based on SD1: В Design Category: B

Section 7.1.2--Symbols & Notation

```
Ce =
           1.2
                    Exposure Factor as determined from Table 7.3-1
Ct =
           1.2
                    Thermal factor as determined from Table 7.3-2
 D = Snow Density in pcf as determined from Eq. 7.7-1
hb = Height of balanced snow load determined by dividing Pf by D, in feet.
hd = Height of snow drift, in feet
hc = Clear height from top of balanced snow to top of parapet, ft
hr =
          6.00
                    = Fascia height, ft
          1.0
s =
                    = Importance factor (see Table 1.5-2).
Pf = Snow load on flat roofs, psf.
Pg =
           20
                    =ground snow, psf.
Pd = Maximum intensity of drift surcharge load, psf.
                    = Length of roof upwind of the drift, feet
lu =
         30.42
w = Width of snow drift, in feet
```

Section 7.3--Flat-Roof Snow Loads. Pf

The snow load, Pf, on a roof with a slope equal to or less than 5° shall be calculated in psf using equation 7.3-1, but not less than the following minimum values for low slope roofs: where Pg is 20 psf or less Pf = I(Pg), where Pg exceeds 20 psf, Pf = 20 (I).

Section 7.7 & Section 7.8

The geometrey of the surcharge load due to snow drifting shall be approximated by a triangle as shown in figure 7.7-2. Drift loads shall be superimposed on the balanced snow load. If hc/hb is less than 0.2, drift loads are not required to be applied. The height of such drifts shall be taken as 0.75 x hd as determined from Fig 7.6-1, with lu equal to the length of the roof upwind of the projection or parapet wall. If the side of a roof projection is less than 15 ft long, a drift load is not required to be applied to that side. If the height, hd, is equal to or less than hc, the drift width shall equal 4hd and the drift height shall equal hd. If this height exceeds hc, the drift width, w, shall equal 4 hd²/hc and the drift height shall equal hc. However, the drift width w shall not exceed 8hc. The maximum intensity of the drift surcharge load, pd, equals hd x D where the snow density, D, is defined by Eq 7.7-

Section 7.10--Rain-On-Snow Surcharge Load

For locations where Pg is 20 psf or less but not zero, all roofs with a slope less than W/50, shall have a 5 psf rain-on-snow surcharge load applied to establish the design snow loads. This additional load applies only to the slped roof (balanced) load case and need not be used in combination with drift, sliding, unbalanced, or partial loads.

```
Pf = 0.7 \times Ce \times Ct \times Is \times Pa
                                          Eq 7.3-1
       Pf =
                      20.0 psf
       hd = 0.75 x (0.43(lu)^1/3 x (Pg+10)^1/4-1.5) Ref. Fig. 7.6-1
       hd =
                      1.23 ft
        D = 0.13Pq + 14 < 30 psf
                                          Eq 7.7-1
        D=
                    16.60 psf
       hb =
                     1.20 ft
hc =hr-hb =
                     4.80 ft
    hc/hb =
                     3.98
                                                                                                        hc
                                                          hd
              Consider Drift
                                                                                     DRIFT SURCHARGE
                     4.92 ft
        w =
                                                          hb
                                                                            FIGURE 7.7-2
      Pd = Dxhd<Dxhc
                                                               Configuration of Snow Drifts on Lower Roofs
      Pd =
                    20.44 psf
```

P1							P2
v 23.00	PSF	0	0	0			V
^A		^B	^C	^D		^E	V0 -1
X1> L1		<lz></lz>	<	<l< td=""><td>4></td><td> <</td><td>X2> </td></l<>	4>	<	X2>
Wd=	3.00	nef	X1=	1.75	ft		
WI=	20.00		L1=	6.00			
Deck: Ww=	-21.58		L2=	6.00			
Frame : Ww=	-13.96		L3=	6.00			
P1=	5.83	700	L4=	7.25			
P2=	5.83	ARCOCK	X2=	3.00			
3		Protein .		0.00			
				RAd=	22.55	plf	
MAd=	14.80	ft-lbs/ft		RAI=	100.10		
MAI=	30.63	ft-lbs/ft	Fr	ame : RAw=	-69.88	9.5	
Deck : MAw=	-33.04	ft-lbs/ft	Sec. 3.	RA(d+l)=	122.65	-	
MA(d+I)=	45.43	ft-lbs/ft	Frame	: RA(d+w)=	-47.33	plf	
Deck: MA(d+w)=	-18.24	ft-lbs/ft					
				RBd=	15.53	plf	
				RBI=	120.00	plf	
MAB(d+I)=		ft-lbs/ft	Fr	ame: RBw=	-80.21	plf	12.00
Deck : MAB(d+w)=	-74.73	ft-lbs/ft		RB(d+I)=	135.53	plf	
12 10 10 10 10 10 10 10 10 10 10 10 10 10			Frame	: RB(d+w)=	-64.68	plf	
MBC(d+I)=	103.50						
Deck : MBC(d+w)=	-83.60	ft-lbs/ft		RCd=	18.00	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	\$1202000000	Service Name		RCI=	120.00		
MCD(d+I)=	103.50		Fra	ame: RCw=	-83.77		
Deck: MCD(d+w)=	-83.60	ft-lbs/ft	-	RC(d+I)=	138.00	A STATE OF THE PARTY OF	
MBEALIN	100.01	5. 11 . 15:	Frame	: RC(d+w)=	-65.77	plf	
MDE(d+I)=	136.01						
Deck: MDE(d+w)=	-91.25	π-lbs/π		RDd=	15.60		
			_	RDI=	132.50	13:04	
NAT d	24.00	£1 11 154	Fra	me: RDw=	-83.83		
MEd=		ft-lbs/ft	_	RD(d+l)=	148.10		
MEI=		ft-lbs/ft	Frame	: RD(d+w)=	-68.23	pit	
Deck: MEw=	-97.10			DE	00.00	10	
ME(d+l)=	121.00			REd=	29.98		
Deck : ME(d+w)=	-66.10	π-ids/π	-	REI=	144.91	A CONTRACTOR	
			r-ra	me : REw=	-101.17		
			From	RE(d+l)=	174.90	•	
			Frame	: RE(d+w)=	-71.18	pit	
USE 20 GAUG	SE GRADE C	DECK					
+S=.3961 in^3 -S							

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

wd=	3.00	psf		Wd		
ws=	20.00	psf	m1			
Deck: ww=	-21.58	psf	DRIFT SURCHARGE	P		
Frame: ww=	-13.96	25	PRII SCH			
P=	5.83	All the state of t	ns.	1		
(Drift Surcharge)Pm=	20.44	(12°)		- A		В
L=	6.00	173		YIIIIXIIII.	L	Williani.
X=	1.75			-1-		
(Drift Length) Wd=	4.92					
RAd=	22.55	plf		RBd=	6.53	plf
RAs=	151.33	•		RBs=	53.98	0.5
Frame: RAw=	-69.88	7.5		Frame : RBw=	-38.32	5. 5 .
Deck: RAw=	-108.00	plf		Deck: RBw=	-59.23	0.00000
RA(d+s)=	173.88	plf		RB(d+s)=	60.52	
Frame: RA(d+w)=	-47.33	plf		Frame : RB(d+w)=	-31.79	•
Deck: RA(d+w)=	-85.45	plf		Deck : RB(d+w)=	-52.69	There are
MAd =	-14.80	ft-lbs/ft				
MAs =	-58.21	ft-lbs/ft				
Deck: MAw =	33.04	ft-lbs/ft				
MA(d+s)=	-73.01	THE RESIDENCE OF THE PROPERTY OF		MAB(d+s)=	79.59	ft-lbs/ft
Deck: MA(d+w)=		ft-lbs/ft		Deck : MAB(d+w)=		ft-lbs/ft

USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

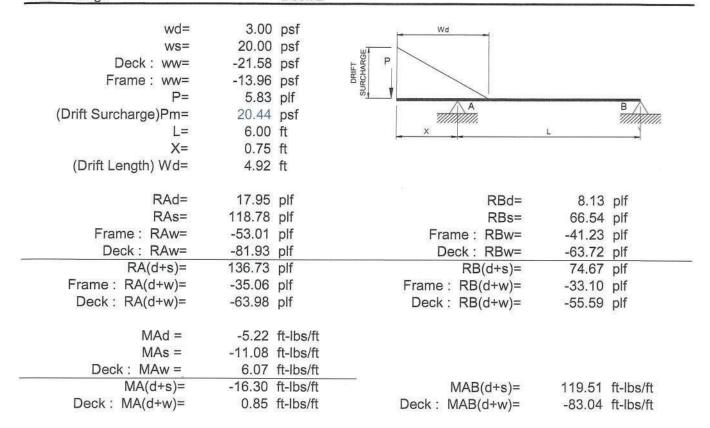
DECK DESIGN:

Wd=	3.00 psf	23.00 ps	f
WI=	20.00 psf	^A	B^
Deck: Ww=	-21.58 psf	< L	>
Frame: Ww=	-13.96 psf	*	3548
		Rd=	9.00 plf
L=	6.00 ft	RI=	60.00 plf
		Frame: Rw=	-41.89 plf
		Deck: Rw=	-64.73 plf
M(d+l)=	103.50 ft-lbs/ft	R(d+I)=	69.00 plf
Deck: M(d+w)=	-83.60 ft-lbs/ft	Frame: R(d+w)=	-32.89 plf
		Deck: R(d+w)=	-55.73 plf

USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

P1	_		_				P2
v 23.00 PS		0 ^B	^C	^D		^E	<u>V</u>
< X1> <l1< td=""><td>></td><td></td><td>•</td><td></td><td>1></td><td></td><td>X2> </td></l1<>	>		•		1>		X2>
The second secon	0.000.00 see 000.00 0.00 0.00 0.00 0.00		1. 50			1	72
Wd=	3.00	psf	X1=	0.75	ft		
VVI=	20.00		L1=	6.00			
Deck: Ww=	-21.58		L2=	6.00			
Frame: Ww=	-13.96	N. C. Constant	L3=	6.00			
P1=	5.83	17	L4=	7.25			
P2=	5.83	plf	X2=	3.00	ft		
				RAd=	17.95	plf	
MAd=	5.22	ft-lbs/ft		RAI=	75.94	plf	
MAI=	5.63	ft-lbs/ft	Fr	ame: RAw=	-53.01	plf	
Deck: MAw=	-	ft-lbs/ft		RA(d+I)=	93.89	plf	
MA(d+I)=		ft-lbs/ft	Frame	: RA(d+w)=	-35.06	plf	
Deck: MA(d+w)=	-0.85	ft-lbs/ft					
				RBd=	17.13		
				RBI=	120.00	plf	
MAB(d+l)=	100.91		Fra	ame : RBw=	-83.12	-7.	
Deck: MAB(d+w)=	-83.18	ft-lbs/ft	52304	RB(d+I)=	137.13		
	702 00	2 17 12	Frame	: RB(d+w)=	-65.99	plf	
MBC(d+I)=	103.50						
Deck : MBC(d+w)=	-83.60	ft-lbs/ft		RCd=	18.00	417.17.17.17.17.17.17.17.17.17.17.17.17.1	
MODALIN	400 50	5. 11 (5.	_	RCI=	120.00	19900	
MCD(d+1)=	103.50		Fra	ame : RCw=	-83.77		
Deck: MCD(d+w)=	-83.60	π-lbs/π	_	RC(d+l)=	138.00	1197/2004	
MDE(d.I)-	100.01	£ 11 /£	Frame	: RC(d+w)=	-65.77	plf	
MDE(d+l)=	136.01			DD-I	45.00		
Deck : MDE(d+w)=	-91.25	IL-IDS/IL		RDd= RDI=	15.60	0.53.4.77	
			E.		132.50		
MEd=	31.00	ft lbc/ft	FIE	RD(d+l)=	-83.83	110	
MEI=	90.00		Eramo	: RD(d+v)=	148.10 -68.23		
Deck : MEw=	-97.10		rrame	. ND(u+w)-	-00.23	pii	
$\frac{\text{ME}(d+l)=}{\text{ME}(d+l)=}$	121.00	10 A 10 A 20 A 20 A 20 A 20 A 20 A 20 A		REd=	29.98	nlf	
Deck : ME(d+w)=	-66.10			REI=	144.91		
Door Millian	00.10	100/10	Fra	me : REw=	-101.17		
			110	RE(d+l)=	174.90	-	
			Frame	: RE(d+w)=	-71.18	1.5	
			7 101110	(0.11)	71.10	Pii	
USE 20 GAUGE (GRADE C	DECK					
+S=.3961 in^3 -S=.30							



USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

DECK DESIGN:

Wd=	3.00	psf	23.00 p	sf	
WI=	20.00	psf	^A	B^	10
Deck: Ww=	-21.58	psf	< L	>	
Frame : Ww=	-13.96	psf		200.2	
			Rd=	9.00	plf
L=	6.00	ft	RI=	60.00	plf
			Frame : Rw=	-41.89	plf
			Deck: Rw=	-64.73	plf
M(d+l)=	103.50	ft-lbs/ft	R(d+l)=	69.00	plf
Deck: M(d+w)=	-83.60	ft-lbs/ft	Frame: R(d+w)=	-32.89	plf
			Deck: R(d+w)=	-55.73	plf

USE 20 GAUGE GRADE C DECK

+S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

Wd=		P-a						
	37.55	5 plf			IP			
WI=	151.33	5.5			v	188.88	plf	
Ww=	-69.88	A Commission				^A	B^	5
Pd=	29.20	200			<>	<	L>	
PI=) lbs				Programme and America	_	
Pw=) lbs		Deflections:	(inches)	Overhang	Midspan	
L=	17.77			DL=		-0.029	0.051	=
X=	3.79			DL+LL=		-0.160	0.268	
//-	5.73	, 10		(+downward		-0.100	0.200	
MA(d) =	201	ft-lbs		(+downward	, -upwaru)	DAd-	F07	These
\$31. \$ 20.						RAd=	527	
MA(I) =		ft-lbs				RAI=	1980	
MA(w) =		ft-lbs			6	RAW=	-914	
MA(d+1) =		ft-lbs		1.33		RA(d+I)=	2506	
MA(d+w) =	-122	ft-lbs	lu=	3.79	ft	RA(d+w)=	-388	lbs
						RBd=	312	lbs
						RBI(Max)=	1345	
						RBw=	-593	
MAB(d+1)=	7267	ft-lbs	lu=	8.89	ft	RB(d+l)=	1657	0.000.000
MAB(d+w)=	-1216			1.33		RB(d+w)=	-280	
m D(a m)	1210	16 100	10	1.00	**	NB(d·W)	-200	103
	USE:	W8X	15	Fy =	50	ksi		
BEAM DESIGN:		P-b						
MATERIAL PROPERTY OF THE PARTY	25.53	100	-		IP			
Wd=	25.53	plf			P	1/15 53	nlf	
Wd= Wl=	120.00	plf plf			P v	145.53		
Wd= WI= Ww=	120.00 -80.21	plf plf plf			v	^A	plf B^	
Wd= WI= Ww= Pd=	120.00 -80.21 33.51	plf plf plf lbs			P v			:
Wd= WI= Ww= Pd= PI=	120.00 -80.21 33.51 0.00	plf plf plf lbs lbs		Deflections	<>	^A <	B^ L>	:
Wd= WI= Ww= Pd= PI= Pw=	120.00 -80.21 33.51 0.00 0.00	plf plf plf lbs lbs		Deflections: (<>	^A < Overhang	B^ L> Midspan	
Wd= WI= Ww= Pd= PI= Pw= L=	120.00 -80.21 33.51 0.00 0.00 17.77	plf plf plf lbs lbs lbs ft		DL=	<>	^A < Overhang -0.028	B^ L> Midspan 0.052	
Wd= WI= Ww= Pd= PI= Pw=	120.00 -80.21 33.51 0.00 0.00	plf plf plf lbs lbs lbs ft		DL= DL+LL=	<x> inches)</x>	^A < Overhang	B^ L> Midspan	
Wd= WI= Ww= Pd= Pl= Pw= L= X=	120.00 -80.21 33.51 0.00 0.00 17.77 3.79	plf plf plf lbs lbs lbs ft		DL=	<x> inches)</x>	^A < Overhang -0.028 -0.190	B^ L> Midspan 0.052 0.321	
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79	plf plf plf lbs lbs ft ft		DL= DL+LL=	<x> inches)</x>	^A < Overhang -0.028 -0.190 RAd=	B^ L> Midspan 0.052 0.321	
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863	plf plf plf lbs lbs ft ft ft-lbs		DL= DL+LL=	<x> inches)</x>	^A < Overhang -0.028 -0.190 RAd= RAl=	B^ L> Midspan 0.052 0.321 375 1570	lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw=	B^ L Midspan 0.052 0.321 375 1570 -1049	lbs lbs
Wd= WI= Ww= Pd= PI= Pw= L= X= MA(d) = MA(I) = MA(V) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL=	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAl=	B^ L> Midspan 0.052 0.321 375 1570	lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw=	B^ L Midspan 0.052 0.321 375 1570 -1049	lbs lbs
Wd= WI= Ww= Pd= PI= Pw= L= X= MA(d) = MA(I) = MA(V) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAI= RAw= RA(d+I)= RA(d+w)=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675	lbs lbs lbs
Wd= WI= Ww= Pd= PI= Pw= L= X= MA(d) = MA(I) = MA(V) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAI= RAw= RA(d+I)= RA(d+w)= RBd=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675	lbs lbs lbs lbs
Wd= WI= Ww= Pd= PI= Pw= L= X= MA(d) = MA(I) = MA(V) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs		DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675 209 1066	lbs lbs lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173 -266	plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs	lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675 209 1066 -680	lbs lbs lbs lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) = MA(d+I) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173 -266	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs	lu= lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw= RB(d+I)=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675 209 1066 -680 1276	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173 -266	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs	lu= lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675 209 1066 -680	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) = MA(d+I) = MA(d+I) =	120.00 -80.21 33.51 0.00 0.00 17.77 3.79 311 863 -577 1173 -266	plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs	lu= lu= lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.190 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw= RB(d+I)=	B^ L> Midspan 0.052 0.321 375 1570 -1049 1944 -675 209 1066 -680 1276	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs

Wd=	28.00) plf		IP			
WI=	120.00	plf		v	148.00	plf	
Ww=	-83.77	Carlotte Control			^A	B [^]	=
Pd=	35.00	lbs		<>	<	L>	
PI=	0.00	Ibs		196.0	70	,	
Pw=	0.00	lbs	Deflections:	(inches)	Overhang	Midspan	
L=	17.77	ft	DL=		-0.031	0.058	-
X=	3.79	ft	DL+LL=		-0.193	0.326	
			(+downward	, -upward)			
MA(d) =	334	ft-lbs			RAd=	409	lbs
MA(I) =	863	ft-lbs			RAI=	1570	lbs
MA(w) =	-602	ft-lbs			RAw=	-1096	lbs
MA(d+l) =	1197	ft-lbs lu=	1.33	ft	RA(d+l)=	1979	
MA(d+w) =	-268	ft-lbs lu=	3.79		RA(d+w)=	-687	
8 1450							
					RBd=	230	lbs
					RBI(Max)=	1066	
					RBw=	-710	
MAB(d+l)=	5677	ft-lbs lu=	8.89	ft	RB(d+l)=	1296	
MAB(d+w)=		ft-lbs lu=	1.33		RB(d+w)=	-480	
	USE:	W8X10	Fy =	50	ksi		
-							
BEAM DESIGN:		P-d					
Wd=	25.60	plf		P			
Wd= WI=	132.50	plf		P v	158.10		
		plf	:	P v	158.10	plf B^	
WI= Ww= Pd=	132.50	plf plf	:	P v			
WI= Ww=	132.50 -83.83 35.03 0.00	plf plf lbs lbs	:	v	^A	B^	
WI= Ww= Pd=	132.50 -83.83 35.03 0.00 0.00	plf plf lbs lbs lbs	Deflections: (<>	^A	B^	8
WI= Ww= Pd= PI=	132.50 -83.83 35.03 0.00	plf plf lbs lbs lbs	Deflections: (<>	^A <	B^ L>	5
WI= Ww= Pd= PI= Pw=	132.50 -83.83 35.03 0.00 0.00	plf plf lbs lbs lbs ft		<>	^A < Overhang	B^ L> Midspan	
WI= Ww= Pd= PI= Pw= L=	132.50 -83.83 35.03 0.00 0.00 17.77	plf plf lbs lbs lbs ft	DL=	<> inches)	^A < Overhang -0.028	B^ L> Midspan 0.052	
WI= Ww= Pd= PI= Pw= L=	132.50 -83.83 35.03 0.00 0.00 17.77 3.79	plf plf lbs lbs lbs ft	DL= DL+LL=	<> inches)	^A < Overhang -0.028	B^ L> Midspan 0.052	lbs
WI= Ww= Pd= PI= Pw= L= X=	132.50 -83.83 35.03 0.00 0.00 17.77 3.79	plf plf lbs lbs lbs ft	DL= DL+LL=	<> inches)	^A < Overhang -0.028 -0.207	B^ L> Midspan 0.052 0.349	
WI= Ww= Pd= PI= Pw= L= X= MA(d) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79	plf plf lbs lbs lbs ft ft ft-lbs	DL= DL+LL=	<> inches)	^A < Overhang -0.028 -0.207 RAd=	B^ L> Midspan 0.052 0.349	lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603	plf plf lbs lbs lbs ft ft ft-lbs	DL= DL+LL=	<> inches) -upward)	^A < Overhang -0.028 -0.207 RAd= RAI=	B^ L> Midspan 0.052 0.349 377 1733	lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(W) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs	DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.207 RAd= RAI= RAw=	B^ L Midspan 0.052 0.349 377 1733 -1097	lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu=	DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.207 RAd= RAI= RAw= RA(d+I)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111	lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu=	DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.207 RAd= RAI= RAw= RA(d+I)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111	lbs lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu=	DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.207 RAd= RAI= RAw= RA(d+I)= RA(d+w)=	B^ L> Midspan 0.052 0.349 377 1733 -1097 2111 -719	lbs lbs lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu=	DL= DL+LL= (+downward,	<x> inches) -upward)</x>	^A < Overhang -0.028 -0.207 RAd= RAI= RAw= RA(d+I)= RA(d+w)= RBd=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719	lbs lbs lbs lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) = MA(w) = MA(d+I) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269 -286	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu=	DL= DL+LL= (+downward,	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.207 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719 210 1177	lbs lbs lbs lbs lbs lbs
WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+w) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269 -286	plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu= ft-lbs lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.207 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719 210 1177 -711	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs
WI= Ww= Pd= Pl= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+l) = MA(d+w) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269 -286	plf plf lbs lbs lbs ft ft ft ft-lbs ft-lbs ft-lbs lu= ft-lbs lu=	DL= DL+LL= (+downward, 1.33 3.79	<x> inches) -upward) ft ft</x>	^A < Overhang -0.028 -0.207 RAd= RAl= RAw= RA(d+I)= RA(d+W)= RBd= RBI(Max)= RBw= RB(d+I)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719 210 1177 -711 1387	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs
WI= Ww= Pd= Pl= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+l) = MA(d+w) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269 -286 6084 -2158	plf plf lbs lbs lbs ft ft ft ft-lbs ft-lbs ft-lbs lu= ft-lbs lu=	DL= DL+LL= (+downward, 1.33 3.79	v <> inches) -upward) ft ft	^A < Overhang -0.028 -0.207 RAd= RAl= RAw= RA(d+I)= RA(d+W)= RBd= RBI(Max)= RBw= RB(d+I)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719 210 1177 -711 1387	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs
WI= Ww= Pd= Pl= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+l) = MA(d+w) =	132.50 -83.83 35.03 0.00 0.00 17.77 3.79 317 952 -603 1269 -286 6084 -2158	plf plf lbs lbs lbs ft ft ft ft-lbs ft-lbs ft-lbs lu= ft-lbs lu= ft-lbs lu=	DL= DL+LL= (+downward, 1.33 3.79	v <> inches) -upward) ft ft	^A < Overhang -0.028 -0.207 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw= RB(d+I)= RB(d+W)=	B^ L Midspan 0.052 0.349 377 1733 -1097 2111 -719 210 1177 -711 1387	Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs Ibs

BEAM DESIGN:

BEAM DESIGN	l:	P-e										
Wd=	39.98	and the second				IP						
WI=	144.91					V		184.	90 pl	f		
Ww=	-101.17	100				3		^A		B^	9	
Pd=	42.27					<	X>		L	>		
PI=	0.00	lbs										
Pw=	0.00	lbs		Defle	ctions:	(inch	nes)	Overhan	g	Midspan		
L=	17.77	ft			DL=			-0.046		0.083		
X=	3.79	ft			L+LL=			-0.242		0.408		
				(+dov	vnward.	, -up	ward)					
MA(d) =	448	ft-lbs				E	9-2.00 -2-9 (No. 30.00 %)	RA	d= -	574	Ibs	
MA(I) =	1042	ft-lbs						RA	 =	1896	lbs	
MA(w) =	-727	ft-lbs						RAV	v=	-1323	lbs	
MA(d+I) =	1489	ft-lbs	lu=	_	1.33	ft		RA(d+l		2470	-	
MA(d+w) =	-280	ft-lbs	lu=		3.79			RA(d+w		-749		
								RBo	<u> </u>	330	lbs	
								RBI(Max		1288		
								RBv		-858		
MAB(d+l)=	7077	ft-lbs	lu=		8.89	ft		RB(d+l		1618		
MAB(d+w)=	-2277				1.33			RB(d+w	.00	-528		
	USE:	W8X	10		Fy =		50	ksi				
-	002.	110/1	10		' '		- 00	KOI				
BEAM DESIGN:		P-f										
	Wd=		32.95									
	WJ=		118.78	plf								
	Ww=		-53.01	plf								
	L=		20.00	ft								
	_	^	151.73	plf								
		•		200	^		_					
		<		L	>		Rd=		0 lbs			
			1047 -	51. 11.			RI=		8 lbs			
	Md=		1647.7		8-		Rw=		0 lbs			
	MI=		5938.8				R(d+l)=		7 lbs			
	Mw=	-2	2650.7	tt-lbs			R(d+w)=	-20	1 lbs			
	M(d+I)=		7586.4				Lu=		7 ft		ОК	
	M(d+w)=	-1	1003.0	ft-lbs			Lu=	1.3	3 ft		OK	
	HCE.	11/0/4	E		Ev		F0	lia:				
	USE:	W8X1	ט		Fy =		50	KSI				
		Deflec	tions: (inches)		dspan					
			DL=				.085					
			L+LL= nward,			0	.392					

BEAM DESIGN:	P-g	ā				
Wd		plf				K)
WI		191 2 1				
Ww						
L						
_	20.00	11.				
	158.67	plf				
	2000 Water	Δ	-		9900	
	<	L>	Rd=		lbs	
			RI=	1265		
Md=			Rw=	-831	The state of the s	
MI=	6326.8	ft-lbs	R(d+l)=	1587	lbs	
Mw=	-4156.0	ft-lbs	R(d+w)=	-510	lbs	
M(d+I)=	7933.4	ft lbs	Lu=	6.67	ft	ок
M(d+w)=						
M(d+w)-	-2549.5	IL-IDS	Lu=	1.33	П	OK
USE:	W8X15	Fy =	50	ksi		
	Deflections	(inches)	Midonon			
	Deflections:	(inches)	Midspan			
	DL=		0.083			
	DL+LL=	· velus exclosionistes e en	0.410			
	(+downward,	-upward)				
BEAM DESIGN:	P-h					
Wd=	21 00	nlf				
WI=	120.00	plf				
WI= Ww=	120.00 -83.77	plf plf				
WI=	120.00 -83.77	plf plf				
WI= Ww=	120.00 -83.77 20.00	plf plf ft				
WI= Ww=	120.00 -83.77	plf plf ft				
WI= Ww=	120.00 -83.77 20.00 151.00	plf plf ft plf	Dd-	210	lhe	
WI= Ww=	120.00 -83.77 20.00	plf plf ft plf	Rd=	310		
WI= Ww= L=	120.00 -83.77 20.00 151.00	plf plf ft plf L>	RI=	1200	lbs	
WI= Ww= L= Md=	120.00 -83.77 20.00 151.00 ^ <	plf plf ft plf 	RI= Rw=	1200 -838	lbs lbs	
WI= Ww= L= Md= MI=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0	plf plf ft plf L> ft-lbs ft-lbs	RI= Rw= R(d+I)=	1200 -838 1510	lbs lbs	
WI= Ww= L= Md=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0	plf plf ft plf L> ft-lbs ft-lbs	RI= Rw=	1200 -838	lbs lbs	
WI= Ww= L= Md= MI=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7	plf plf ft plf L> ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)=	1200 -838 1510 -528	lbs lbs lbs	ОК
WI= Ww= L= Md= MI= Mw= M(d+I)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0	plf plf ft plf L> ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)=	1200 -838 1510 -528 6.67	lbs lbs lbs lbs	OK OK
WI= Ww= L= Md= MI= Mw=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0	plf plf ft plf L> ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu=	1200 -838 1510 -528	lbs lbs lbs lbs	OK OK
WI= Ww= L= Md= MI= Mw= M(d+I)= M(d+w)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0 -2638.7	plf plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu=	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	
WI= Ww= L= Md= MI= Mw= M(d+I)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0	plf plf ft plf L> ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu=	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	
WI= Ww= L= Md= MI= Mw= M(d+I)= M(d+w)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0 -2638.7	plf plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu=	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	
WI= Ww= L= Md= MI= Mw= M(d+I)= M(d+w)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0 -2638.7	plf plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 Midspan	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	
WI= Ww= L= Md= MI= Mw= M(d+I)= M(d+w)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0 -2638.7 W8X13 Deflections: (plf plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 Midspan 0.097	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	
WI= Ww= L= Md= MI= Mw= M(d+I)= M(d+w)=	120.00 -83.77 20.00 151.00 ^ < 1550.0 6000.0 -4188.7 7550.0 -2638.7 W8X13 Deflections: (plf plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 Midspan	1200 -838 1510 -528 6.67 1.33	lbs lbs lbs lbs	

BEAM DESIGN:	P-i					
Wd=	THE RESERVE THE PERSON NAMED IN COLUMN	plf				
WI=						
Ww=						
L=	20.00	π				
	161.10	plf				
	at one	Α.		name and man	a version of	
	<	L>	Rd= RI=	286 1325	lbs	
Md-	1420.0	ft lbs				
Md=			Rw=	-838		
MI=			R(d+I)=	1611		
Mw=	-4191.7	ft-lbs	R(d+w)=	-552	lbs	
M(d+1)=	8055.0	ft-lhs	Lu=	6.67	ft	ок
M(d+w)=			Lu=	1.33		
W(d+w)−	-2/01./	II-IDS	Lu=	1.33	π	OK
	1440144					
USE:	W8X13	Fy =	50 ksi			
	Deflections:	(inches)	Midspan			
	DL=	(0.090			
	DL+LL=		0.505			
		upurard)	0.505			
DEAM DECION.	(+downward,	-upward)				
BEAM DESIGN:	P-j					
Wd=	44.98					
WI=	4 4 4 0 4	nlf				
	144.91					
Ww=	-101.17					
		plf				
Ww=	-101.17 20.00	plf ft				
Ww=	-101.17	plf ft				
Ww=	-101.17 20.00 189.90	plf ft	Dd-	450	lle s	
Ww=	-101.17 20.00 189.90	plf ft	Rd=	450		
Ww= L=	-101.17 20.00 189.90	plf ft^ 	RI=	1449	lbs	
Ww= L= Md=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs	RI= Rw=	1449 -1012	lbs lbs	
Ww= L= Md= Ml=	-101.17 20.00 189.90 ^ < 2249.2 7245.7	plf ft plf L> ft-lbs ft-lbs	RI=	1449 -1012 1899	lbs lbs	
Ww= L= Md=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs	RI= Rw=	1449 -1012	lbs lbs	
Ww= L= Md= Ml= Mw=	-101.17 20.00 189.90 ^ < 2249.2 7245.7 -5058.3	plf ft plf L> ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)=	1449 -1012 1899 -562	lbs lbs lbs lbs	OK
Ww= L= Md= Ml= Mw= M(d+I)=	-101.17 20.00 189.90 ^ < 2249.2 7245.7 -5058.3 9494.9	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu=	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	OK
Ww= L= Md= Ml= Mw=	-101.17 20.00 189.90 ^ < 2249.2 7245.7 -5058.3	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)=	1449 -1012 1899 -562	lbs lbs lbs lbs	ОК
Md= Ml= Ml= Mw= M(d+l)= M(d+w)=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu=	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	
Ww= L= Md= Ml= Mw= M(d+I)=	-101.17 20.00 189.90 ^ < 2249.2 7245.7 -5058.3 9494.9	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu=	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	
Md= Ml= Ml= Mw= M(d+l)= M(d+w)=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 ksi	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	
Md= Ml= Ml= Mw= M(d+l)= M(d+w)=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 ksi	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	
Md= Ml= Ml= Mw= M(d+l)= M(d+w)=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= Lu= Midspan 0.116	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	
Md=	-101.17 20.00 189.90 ^ <	plf ft plf L> ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs	RI= Rw= R(d+I)= R(d+w)= Lu= Lu= 50 ksi	1449 -1012 1899 -562 6.67	lbs lbs lbs lbs	

Wd=	27 5	5 plf	Sales and the sales of the sale	IP			
		4.4					
WI=	151.33	9		V	188.88		_
Ww=	-69.88	3 plf			^A	B [^]	<u> </u>
Pd=	29.20) lbs		<>	<	L>	
PI=	0.00) lbs					
Pw=	0.00) lbs	Deflections:	(inches)	Overhang	Midspan	
L=	18.83	3 ft	DL=		-0.016	0.074	
X=	1.31	ft	DL+LL=		-0.083	0.379	
			(+downward				
MA(d) =	71	ft-lbs	A == 11131/=11=1		RAd=	436	lbs
MA(I) =		ft-lbs			RAI=	1631	
MA(w) =		ft-lbs			RAw=	-753	
MA(d+1) =		ft-lbs lu=	1 33	ft	RA(d+I)=		
MA(d+w) =		ft-lbs lu=	1.31		RA(d+w)=		
1VIA(a · VV) —	10	It-IDS IU-	1.51	п	KA(u+w)-	-317	ibs
					DD4-	250	lbo
					RBd=	350	
					RBI(Max)=	1425	
MADIALIN	0000	G. Hand	0.10	<i>r</i> .	RBw=	02078030	53000000
MAB(d+l)=		ft-lbs lu=	9.42		RB(d+l)=		
MAB(d+w)=	-1439	ft-lbs lu=	1.33	π	RB(d+w)=	-305	lbs
	1105	MOVAE	100	-			
<u> </u>	USE:	W8X15	Fy =	50	ksi		
BEAM DESIGN:			Fy =	50	ksi	8 5	
BEAM DESIGN:		P-I	Fy=		ksi		-
Wd=	25.53	P-I plf	Fy =	50	22 0000000000	w)E	
Wd= WI=	25.53 120.00	P-I plf plf	Fy =		145.53	plf	
Wd= WI= Ww=	25.53 120.00 -80.21	P-I plf plf plf	Fy =	P v	145.53 ^A	B^	
Wd= WI= Ww= Pd=	25.53 120.00 -80.21 33.51	P-I plf plf plf plf lbs	Fy =	P v	145.53	B^	
Wd= Wl= Ww= Pd= Pl=	25.53 120.00 -80.21 33.51 0.00	P-I plf plf plf lbs lbs		P v <>	145.53 ^A <	B^ L>	
Wd= WI= Ww= Pd= PI= Pw=	25.53 120.00 -80.21 33.51 0.00 0.00	P-I plf plf plf lbs lbs	Deflections: (P v <>	145.53 ^A < Overhang	B^ L> Midspan	
Wd= WI= Ww= Pd= Pl= Pw= L=	25.53 120.00 -80.21 33.51 0.00 0.00 18.83	P-I plf plf plf lbs lbs lbs ft	Deflections: (P v <>	145.53 ^A < Overhang -0.017	B^ L> Midspan 0.078	:
Wd= WI= Ww= Pd= PI= Pw=	25.53 120.00 -80.21 33.51 0.00 0.00	P-I plf plf plf lbs lbs lbs ft	Deflections: (DL= DL+LL=	P v <> inches)	145.53 ^A < Overhang	B^ L> Midspan	
Wd= Wl= Ww= Pd= Pl= Pw= L= X=	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31	P-I plf plf plf lbs lbs lbs ft	Deflections: (P v <> inches)	145.53 ^A < Overhang -0.017 -0.100	B^ L> Midspan 0.078 0.454	
Wd= Wl= Ww= Pd= Pl= Pw= L= X= MA(d) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31	P-I plf plf plf lbs lbs ft ft	Deflections: (DL= DL+LL=	P v <> inches)	145.53 ^A < Overhang -0.017 -0.100 RAd=	B^ L> Midspan 0.078 0.454	lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(I) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103	P-I plf plf plf lbs lbs ft ft ft-lbs ft-lbs	Deflections: (DL= DL+LL=	P v <> inches)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl=	B^ L> Midspan 0.078 0.454 311 1293	lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69	P-I plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs	Deflections: (DL= DL+LL= (+downward,	P v <> inches)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAI= RAW=	B^ L> Midspan 0.078 0.454	lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl=	B^ L> Midspan 0.078 0.454 311 1293	lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAI= RAW=	B^ L Midspan 0.078 0.454 311 1293 -864	lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl= RAw= RA(d+I)=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604	lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl= RAw= RA(d+I)=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604	lbs lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAI= RAw= RA(d+I)= RA(d+W)=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604 -553	lbs lbs lbs lbs lbs
Wd= WI= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward)	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604 -553 237 1130	lbs lbs lbs lbs lbs lbs
Wd= Wl= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+w) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169 -3	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs lu= ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <> inches) -upward) ft ft	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604 -553 237 1130 -752	lbs lbs lbs lbs lbs lbs
Wd= Wl= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(v) = MA(d+l) = MA(d+l) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169 -3	P-I plf plf plf lbs lbs lbs ft ft ft-lbs ft-lbs ft-lbs ft-lbs ft-lbs lu=	Deflections: (DL= DL+LL= (+downward, 1.33 1.31	P v <x> inches) -upward) ft ft</x>	145.53 ^A < Overhang -0.017 -0.100 RAd= RAI= RAw= RA(d+I)= RA(d+V)= RBd= RBI(Max)= RBW= RB(d+I)=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604 -553 237 1130 -752 1367	lbs lbs lbs lbs lbs lbs lbs
Wd= Wl= Ww= Pd= Pl= Pw= L= X= MA(d) = MA(l) = MA(w) = MA(d+l) = MA(d+w) =	25.53 120.00 -80.21 33.51 0.00 0.00 18.83 1.31 66 103 -69 169 -3	P-I plf plf plf lbs lbs ft ft ft-lbs ft-lbs ft-lbs lu= ft-lbs lu=	Deflections: (DL= DL+LL= (+downward,	P v <x> inches) -upward) ft ft</x>	145.53 ^A < Overhang -0.017 -0.100 RAd= RAl= RAw= RA(d+I)= RA(d+w)= RBd= RBI(Max)= RBw=	B^ L> Midspan 0.078 0.454 311 1293 -864 1604 -553 237 1130 -752	lbs lbs lbs lbs lbs lbs lbs

BEAM DESIGN:

P-k

BEAM DESIGN.		F-III					
Wd=	28.00) plf		P			
WI=	120.00) plf		V	148.00	plf	_
Ww=	-83.77	plf			^A	B^	NI CONTRACTOR OF THE CONTRACTO
Pd=	35.00) lbs		<>	<	L>	
PI=	0.00) lbs		** ************************************		55555	
Pw=	0.00) lbs	Deflections:	(inches)	Overhang	Midspan	
L=	18.83		DL=		-0.019	0.086	=
X=	1.31		DL+LL=		-0.102	0.462	
		1 25	(+downward		0.102	0.102	
MA(d) =	70	ft-lbs	(dominard	, upirala)	RAd=	330	lbs
MA(I) =		ft-lbs			RAI=	1293	
MA(w) =		ft-lbs			RAW=	-903	
MA(d+1) =		ft-lbs lu=	1.33	ft	RA(d+1)=	1632	
MA(d+w) =		ft-lbs lu=					
MA(u+w) -	-2	it-ibs iu-	1.31	IL	RA(d+w)=	-564	IDS
					003	000	nese
					RBd=	260	
					RBI(Max)=	1130	
MADALON		Fred Law L			RBw=	-785	
MAB(d+l)=		ft-lbs lu=	9.42		RB(d+l)=	1390	
MAB(d+w)=	-2472	ft-lbs lu=	1.33	tt	RB(d+w)=	-525	lbs
	USE:	W8X10	Fy =	50	ksi		
					- III 3		
BEAM DESIGN:		P-n		-			
Wd=	25.60	10		P			
WI=	132.50			V	158.10		
Ww=	-83.83	N. C. S. C.			^A	B^	
Pd=	35.03			<>	<	L>	
PI=	0.00	lbs					
Pw=	0.00	lbs	Deflections: (inches)	Overhang	Midspan	
L=	18.83		DL=		-0.017	0.078	13
X=	1.31	ft	DL+LL=		-0.109	0.493	
			(+downward,	-upward)			
MA(d) =	68	ft-lbs	mark consumers whiteheld recognition (The CALCAST HAR STATE OF THE ST	RAd=	313	lbs
MA(I) =		ft-lbs			RAI=	1428	
MA(w) =		ft-lbs			RAw=	-903	
MA(d+l) =		ft-lbs lu=	1.33	ft	RA(d+l)=	1741	
MA(d+w) =		ft-lbs lu=	1.31		RA(d+w)=	-590	
(/ / /	2,5m C .i	THE RESERVE OF THE PARTY OF THE	1.01		1 J ((a · W)-	000	.50
					RBd=	237	lhe
					RBI(Max)=	1248	
					RBw=	-786	
MAB(d+I)=	6076	ft-lbs lu=	9.42	ft.	RB(d+l)=	1485	
		ft-lbs lu=					
MAB(d+w)=	-2000	11-105 IU-	1.33	It	RB(d+w)=	-548	IDS
	LICE.	14/07/40	-	E0.	1.23		
	USE:	W8X10	Fy =	50	KSI		

BEAM DESIGN:

P-m

BEAM DESIG	GN:	P-o					
Wd=	39.98	plf	IP.				
WI=	144.91	plf	V	184.	.90 plf		
Ww=	-101.17	plf		^A	Β'	Ē	
Pd=	42.27	lbs	<	X> <	L>		
PI=	0.00	lbs	03 * .11	2000000			
Pw=	0.00	lbs	Deflections: (inche	es) Overhar	ng Midspan		
L=	18.83	ft	DL=	-0.027	0.123	_	
X=	1.31	ft	DL+LL=	-0.127	0.577		
			(+downward, -upw	vard)			
MA(d) =	90	ft-lbs	98 93 0.23	RA	d= 476	lbs	
MA(I) =	125	ft-lbs		RA	Al= 1561	lbs	
MA(w) =	-87	ft-lbs		RA	w= -1090	lbs	
MA(d+I) =	215	ft-lbs lu=	1.33 ft	RA(d+	1)= 2037	lbs	
MA(d+w) =	3	ft-lbs lu=	1.31 ft	RA(d+v	v)= -614	Ibs	
				RB	d= 372	lbs	
				RBI(Max			
				RB			
MAB(d+I)=	8153	ft-lbs lu=	9.42 ft	RB(d+	I)= 1736	lbs	
MAB(d+w)=	-2714	ft-lbs lu=	1.33 ft	RB(d+w	v)= -576	lbs	
	USE:	W8X10	Fy =	50 ksi			
=							

P1d= P1I=	527 1980	lbs lbs		P1		P2	P3	P ²		P5	
P1w=	-914		A X1	501				1		F	3
P2d=	375	Ibs	11111111111111111111111111111111111111		X2	X3	X4	-	X5	X	6
P21=	1570	lbs									
P2w=	-1049	lbs									
P3d=	409	lbs				X1 =	1.38	ft			
P31=	1570	lbs				X2 =	6.00	ft			
P3w=	-1096	lbs				X3 =	6.00	ft			
P4d=	377	lbs				X4 =	6.00	ft			
P4I=	1733					X5 =	7.25	ft			
P4w=	-1097	lbs				X6 =	1.00	ft			
P5d=	574					L =	27.63	ft			
P5I=	1896										
P5w=	-1323	lbs									
Wd=	58.00	plf									
WI=	0.00	plf									
Ww=	0.00	plf									
	RA(d)=	1921									
	RA(I)=	4428									
97	RA(w)=	-2579			_0						
	RA(d+I)=	6348									
	RA(d+w)=	-658	lbs			-	5				
					-		eflection	74050			
						dl=	0.24				
	DB(d)-	1943	lho			dl+ll=	0.77	in			
	RB(d)= RB(l)=	4320									
	and the same of th	-2901									
	RB(w)= $RB(d+l)=$	6264	Transmitted to the second								
	RB(d+w)=	-957									
	ND(d·W)	-337	IDS								
Ma	span(d+l) =	37979.5	ft lbc	lu-		7.25 ft					
	pan(d+w) =	-5290.7		lu=		7.25 ft					
IVIO	Janta W J	-0200.1	וניוטט	Iu-		1.20 1					
	USE:	W8X58		Fy =		50 ks	i				

P1d= P1l=	642 2532	lbs lbs		P1		P2	P3 ▼	P4 ▼		P5
P1w=	-1123	lbs "	A ///// X1		V0	V2			v.	B _{×6}
P2d=		105	unn X1	-	X2	X3	X4		X5	X6"////////////////////////////////////
P2I= P2w=	2332 -1511									
P3d=		lbs				X1 =	1.3	8 ft		
P3I=	2266					X2 =		0 ft		
P3w=	-1548					X3 =		0 ft		
P4d=	496					X4 =		0 ft		
P4I=	2502					X5 =		5 ft		
P4w= P5d=	-1549 780					X6 = L =	27.6	Oft		
P5I=	2737					L -	21.0	5 11		
P5w=	-1870									
Wd=	67.00	The state of the s								
WV=	0.00	The second secon								
V V VV—	0.00	рп								
	2250200 22									
	RA(d)=	2379								
	RA(I)= RA(w)=	6131 -3504								
_	RA(W)=	8510			_					
	RA(d+w)=	-1125								
							Deflection			
						dl=	0.25			
	RB(d)=	2460	lbc			dl+ll=	0.89) in		
	RB(I)=	6238								
	RB(w)=	-4098								
	RB(d+l)=	8698	lbs		_					
	RB(d+w)=	-1638	lbs							
Msr	oan(d+l) =	52564.0	ft-lbs	lu=		7.25 ft				
	an(d+w) =	-9379.9				7.25 ft				
	oe ##									
	USE:	W8X67		Fy =		50 k	si			

P1d= P1l=	679 2613	lbs lbs		P1		P2	P3	3	P4	Į	P5	5
P1w=	-1185		A X1			270000	1	DEAMER TO	1	555620	1	B X6
P2d=		IDS	7///////////X1	-	X2	X3	-	X4	-	X5	-	X6////////////////////////////////////
P2I=	2395											
P2w=	-1583											
P3d=		lbs				X1 =		1.38				
P3I=	2330					X2 =		6.00				
P3w=	-1623					X3 =		6.00				
P4d=	523					X4 =		6.00				
P4I=	2573					X5 =		7.25				
P4w=	-1624					X6 =		1.00				
P5d=	822					L=		27.63	ft			
P5I=	2814											
P5w=	-1960	IDS										
Wd=	67.00	plf										
WI=	0.00											
Ww=	0.00	75										
	RA(d)=	2460	lbs									
	RA(I)=	6311										
	RA(w)=	-3679										
	RA(d+l)=	8771										
	RA(d+w)=	-1219	lbs									
							Deflec	tion				
						dl=		0.26				
	200 210 72 6140	70 MARIA (1940)	1997			dI+II=		0.91	in			
	RB(d)=	2543										
	RB(I)=	6414										
	RB(w)=	-4295	5.0215.04									
	RB(d+l)=	8957										
	RB(d+w)=	-1752	IDS									
	pan(d+l) =	54091.1	ft-lbs	lu=		7.25	ft					
Msp	an(d+w) =	-10082.3	ft-lbs	lu=		7.25	ft					
	*											
	USE:	W8X67		Fy=		50	ksi					
				')		00	KUI					

P1d= P1I=		6 lbs		P1 ▼		P2	P3	3	P4		P5
P1w=	-753	B lbs	A ////// X1				i				B
P2d=	311	lbs	/////// X1)	K2	X3		X4		X5	B X6
P2 =	1293	3 lbs									
P2w=	-864	Ibs									
P3d=	339	lbs				X1 =		1.38	ft		
P31=	1293	lbs				X2 =		6.00			
P3w=	-903	lbs				X3 =		6.00			
P4d=	313	lbs				X4 =		6.00			
P4I=	1428	lbs				X5 =		7.25			
P4w=	-903	lbs				X6 =		1.00			
P5d=	476	lbs				L =		27.63			
P51=	1561	lbs									
P5w=	-1090	Ibs									
Wd=	48.00	plf									
WI=	0.00										
Ww=	0.00	plf									
	D (/ d) =	1504	lle e								
	RA(d)=										
	RA(I)=										
	RA(w)= RA(d+l)=	-2124 5238									
	RA(d+y)=	-533									
	IVA(u·w)-	-333	105				Deflec	tion			
						dl=	Dellec	0.25	in		
						dl+ll=		0.78			
	RB(d)=	1610	lbs			GI-II		0.70	11.1		
	RB(I)=	3559									
	RB(w)=	-2389									
-	RB(d+I)=	5169									
	RB(d+w)=	-779									
	,	1000									
M	span(d+l) =	31342.8	ft-lbs	lu=		7.25	ft				
Ms	pan(d+w) =	-4297.5	ft-lbs	lu=		7.25	ft				
	LICE	14/02/40		-		1272	AND ADDRESS OF THE PARTY OF THE				
_	USE:	W8X48		Fy =		50	ksi				

Column Des	ign	Col Line A		AISC	15th ed, Use I	First Order An	alysis Criteria
	P DL =	2.46	kips		Clr. Ht.=	10.17	ft
	P LL =	6.31	kips		Fascia Ht.=	1.00	ft
	PWL=	-3.68	kips		Col. Trib=	19.36	ft
E	Base Shear =	0.21	kips		Wind Load=	16.00	psf
Total E	Base Shear =	1.43	kips		# of COL.=	2	
MWL =	w(Fascia Ht•2.5	Col Trib./# of co	ol•L)+ w(Wrap•1/	2 Clr. Ht^2)	Max All. Defl =	1.28	in
M Seis =	Base Shear x L		9.	1	Max Defl Ratio =	L/	100
M Unbal =	Live Load x Col	. Trib.x (Canopy	Width/2)^2/2		Max Defl. =	0.16	in, OK
L=	Clr. Ht. + Fascia	a Ht/2					
Pr =	8.77	kips 1.6Pr<0	.5Py First-Or	der Analysis	Allowed (A-7-1)	
Py =	326.60	kips					
N =	0.00	•Yi (A-7-2)		Use:	TS8X8X1/4		
B2 =		OK, A-8-6		Fy =	46.00	ksi	
MWL =	4.96	kip-ft		K =			
M Seis =	2.25	kip-ft		L, Col =	10.67	ft	
MDL(Nod) =	0.11	kip-ft		A =	7.10	in^2	
M LL(Nod) =		kip-ft		l =	70.70	in^4	
M Unbal DL=	0.00	kip-ft		Cm =	1.00		
M Unbal LL=	0.00	kip-ft		Pe1 =	393.14	kips	
M Unbal WL=	0.00	kip-ft		B1 =		(A-8-3)	
				P,AII =	175.01		
	K			M, All =	44.10	kip-ft	
	Load Combi	nation	Pr, Kips	Mr, Kip-ft	Equation	Result	
	D+L		8.77	0.41		OK	
	D+W		2.46	5.25	A 100 A	OK	
	D+0.7E		2.46	1.75	Secretary and the second	OK	
	D+0.75W+0.7		7.19	4.19	0.12	OK	
	D+0.525E+0.	75L	7.19	1.56	0.06	OK	

Top Connection: Standard Cap Plate Offset Base Plate: MODLBP 8 - 20

From Column							
P dl =	2.46	kips					
P II =	6.31	kips					
P wl =	-3.68	kips					
Soil Density =	110	pcf					
Width =	5.50	ft		Unbalanced Loa	ad to Colur	nn	
Length =	5.50	ft		M dl =	0.00	kip-ft	LENGTH
Depth =	3.00	ft		MII =	0.00	kip-ft	LENGTH/2 LENGTH/2
e =	2.08	ft		M wl =	0.00	kip-ft	6 -
a =	0.00	ft		From Lateral		Lucia sono	J
b =	0.00	ft		M wl =	4.96	kip-ft	PTCIW e
c =	0.00	ft		M el =	2.82	kip-ft	b
k	(ern = L/6 =		0.92	ft			P M
Footing	Weight =		13.61	kips			, t
Soil	Weight =			kips			РТН
Total Loads to S	pread Foo	ting					ĬĬ,
PDL =	16.07	kips		MDL =	5.13	kip-ft	
PLL =	6.31	kips		MLL =	13.15		
PWL =	-3.68	kips		MWL =	-2.71	100 to 10	
				MEL =	2.82	kip-ft	

Load Combination	Pr, Kips	Mr, Kip-ft	ecc, ft	Soil Pressure psf
D+L	22.38	18.27	0.82	1068.92
D+W	12.39	2.42	0.19	166.84
0.6D+W	5.96	0.37	0.06	-119.63
0.6D+0.7E	9.64	5.05	0.52	170.84
D+0.7E	16.07	7.10	0.44	457.31
D+0.75W+0.75L	18.05	12.95	0.72	733.74
D+0.75(0.7E)+0.75L	20.81	16.47	0.79	951.59

q(ALLOW)= 1500.00 psf OK

REINFORCING:

M =17867.31 ft-lbs/ft

Assume: f'c=3000 psi, Fy=40000 psi

d =

32.63 in

As(REQ'D)=

0.38 in^2

As(PROV.)=

0.59 in^2

USE #6's AT 9"O.C. T&B, EACH WAY

OK

Foundation: (Restrained at Grade)

Col Line A

d^2=(4.25*M)/(S3*b)

л(MAX)=	20603	ft-lbs	Pmax=	8.77	kips
S3=	100	PCF X d	Footing Area=	7.07	ft^2
b=	3.000	ft	Bearing=	1240.83	psf
d=	6.633	ft			
Footing=	Round				
USE:	3.00	FT.RND. X	6.75 ft deep footing		

As=12*M/(jd*24000)=

0.2759 in^2

USE:

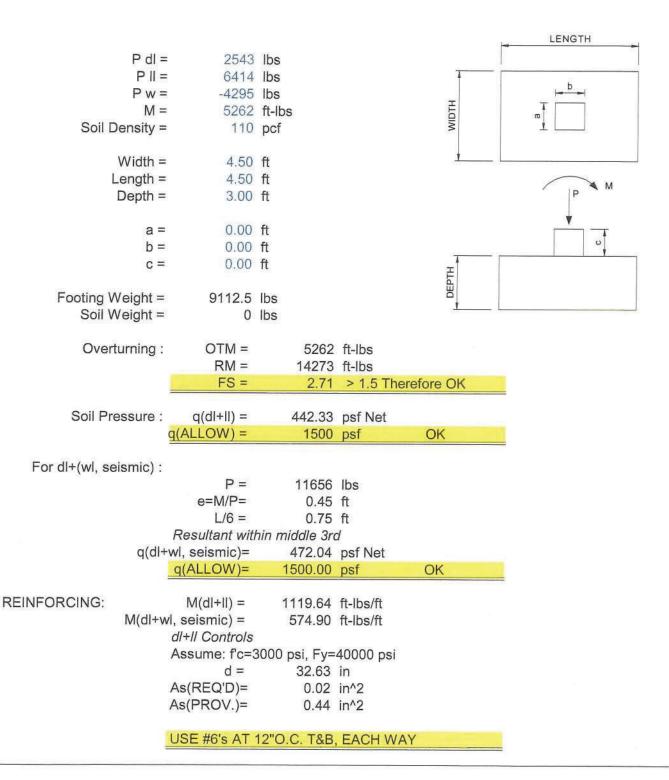
10 #8's (RND. Cage) w/ #4 Ties @ 4" O.C. w/135 degree hooks In The Top

3'-0" of The Footing, #4 Ties @ 12" o.c w/ 135 Degree Hooks In The Balance of Footing

Footing design to allow offset column placement of 1'-9" from centerline of footing.

Column Des	ign	Col Line B		AISC	15th ed, Use I	First Order An	alysis Criteria
	PDL =	2.54	kips		Clr. Ht.=	10.17	ft
	P LL =	6.41	kips		Fascia Ht.=	1.00	ft
	PWL=	-4.29	kips		Col. Trib=	19.36	ft
E	Base Shear =	0.21	kips		Wind Load=	16.00	psf
					# of COL.=	2	
M WL =	w(Fascia Ht•2.5	•Col Trib./# of co	oleL)+ w(Wrape	1/2 Clr. Ht^2)	Max All. Defl =	1.28	in
M Seis =	Base Shear x L			e.	Max Defl Ratio =	L/	100
M Unbal =	Live Load x Col.	Trib.x (Canopy	Width/2)^2/2		Max Defl. =	0.16	in, OK
L=	Clr. Ht. + Fascia		the Committee of the Co				
Pr=	8.96	kips 1.6Pr<0	.5Py First-O	rder Analysis	Allowed (A-7-1	1)	
Py =	326.60		11700			at .	
N =	0.00	•Yi (A-7-2)		Use:	TS8X8X1/4		
B2 =	1.05	OK, A-8-6		Fy =	46.00	ksi	
M WL =	4.96	kip-ft		K =	1.00		
M Seis =	2.25	kip-ft		L, Col =	10.67	ft	
M DL(Nod) =	0.11	kip-ft		A =	7.10	in^2	
M LL(Nod) =	0.29	kip-ft		1 =	70.70	in^4	
M Unbal DL=	0.00	kip-ft		Cm =	1.00		
M Unbal LL=	0.00	kip-ft		Pe1 =	393.14	kips	
M Unbal WL=	0.00	kip-ft		B1 =	1.04	(A-8-3)	
				P,AII =	175.01	kips	
				M, All =	44.10	kip-ft	
-	Load Combi	nation	Pr, Kips	Mr, Kip-ft	Equation	Result	
	D+L		8.96	0.42	0.04	OK	
	D+W		2.54	5.26	0.13	OK	
	D+0.7E		2.54	1.76	0.05	OK	
	D+0.75W+0.7		7.35	0.00		OK	
III	D+0.525E+0.7	75L	7.35	1.57	0.06	OK	

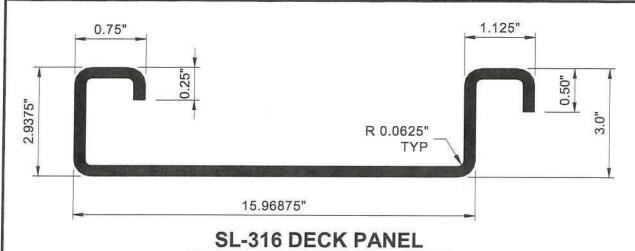
undation:	(Restrained at	Grade)				
	d^2=(4.25*M)/	(S3*b)				
	M(MAX)=	5262	ft-lbs	Pmax=	8.96	kips
	S3=	100	PCF X d	Footing Area=	7.07	ft^2
	b=	3.000	ft	Bearing=	1267.17	psf
	d=	4.209	ft			
	Footing=	Round				
	USE:	3.00	FT.RND. X	5.00 ft deep footing		





LANE SUPPLY, INC.

120 Fairview Arlington, Texas 76010 817-261-9116



	Section Properties										
Gage	Wt, psf	Thickness, in	ASTM 653	+l, in ⁴	-I, in ⁴	+S, in ³	-S, in ³	+M, ft-lbs/ft	-M, ft-lbs/ft		
20	2.20	0.0359	Grade 40	0.9346	0.4680	0.3961	0.3036	592.70	454.44		
	2.20	0.0000	Grade 50	0.9208	0.4522	0.3879	0.2880	725.86	538.92		
18	2.93	0.0478	Grade 40	1.2486	0.6827	0.5329	0.4377	797.77	655.28		
,,,	2.00	0.0470	Grade 50	1.2129	0.6518	0.5141	0.4296	962.09	803.92		

Notes:

- 1 Designed per AISI Cold Formed Steel Manual, 2016 ed.
- 2 Complete calculations are available upon request.
- 3 ± M is allowable bending moment.

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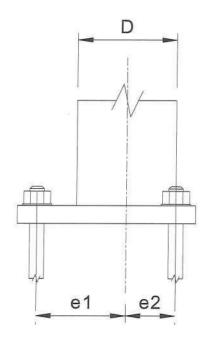
	Moment = Column =	20.00 TS8X8X1/4	kip-ft
	D =	8	in.
	e1 =	8	in.
	e2 =	4	in.
Anch	or Bolts =	1 1/2	in
	t plate =	2.00	in
A36 Steel Plate	Fy =	36	ksi
E70 Electrode	Fw =	0.928	kips / in / 16th
A307 Anchor Bolts	Ft =	20	ksi

Clockwise Moment

Pbolt =	8.57	kips	< 35.3, OK
t(req'd) =	1.04	in	
t(actual) =	2.00	in	
Weld(reg'd) =	3.03	/16th's	
Weld(actual) =	F.P.	/16th's	

Counter-Clokwise Moment

Pbolt = 12.00 kips < 35.3, OK





120 Fairview Arlington, Texas 76010 817-261-9116 FAX 817-275-1660

STANDARD BASE PLATE DESIGN

LBP#			М	P _{BOLT}	Bolt Dia.	t REQ'D	t ACTUAL	Weld Req'd	Weld Actual	Base Plate
_(D	=	M)	(ft-k)	(k)	(in)	(in)	(in)	(1/16 in)	(in)	Mark
8	-	10	10	5.58	1 1/2	0.72	3/4	1.52	1/4	LBP 1
8	-	20	20	10.91	1 1/2	0.99	1	3.03	5/16	LBP 2
8	-55	30	30	16.00	1 1/2	1.17	1 1/4	4.55	5/16	LBP 3
8	1	40	40	20.87	1 1/2	1.32	1 1/2	6.06	F.P.	LBP 4
8	-	50	50	26.09	1 1/2	1.46	1 1/2	7.58	F.P.	LBP 5

TS 8 X 8 COLUMN:

D= 8 in. e= 2 in.

b,d= 8 in.

CONSTANTS:

A36 Steel Plate

E70xx Electrode

A307 Anchor Bolts

Fy = 36 ksi

Fw = 0.928 k/in/16th

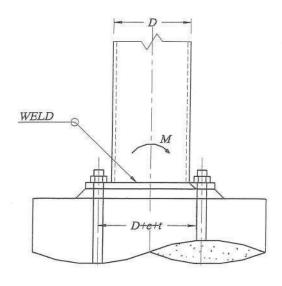
Ft = 20 ksi

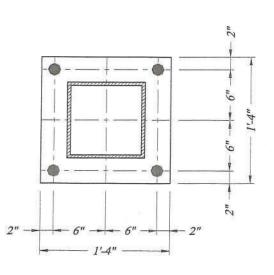
EQUATIONS:

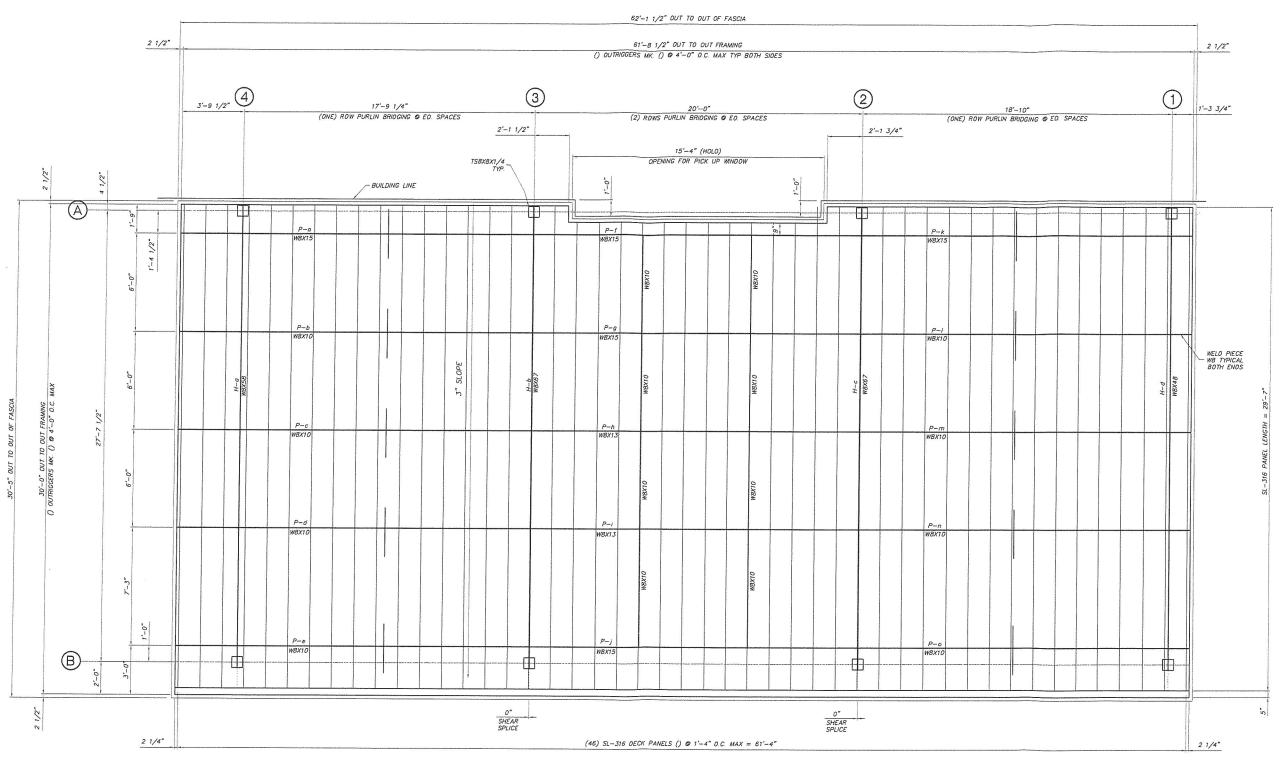
$$P_{BOLT} = \frac{M \times 12 \text{ in/ft}}{2 \text{ bolts (D+e+t)}}$$

$$Weld = \frac{M \times 12 \text{ in/ft}}{S \text{ weld } \times FW} = \frac{M \times 12 \text{ in/ft}}{FW (bd+d\%3)}$$

$$t_{REQD} = \sqrt{\frac{6 \times P \times e \times 2 \text{ bolts}}{0.75 \times Fy \times (D+2t)}}$$







DESIGN LOADS: DEAO LOAD = 3 p.s.f.(DECK + LIGHTS) + WEIGHT OF STRUCTURAL COMPONENTS LIVE LOAD = 20 p.s.f. WIND LOAD = 20 p.s.f. WIND LOAD VILIT = 116 m.p.h. EXP. C WIND VASO = 90 m.p.h. EXP. C BLDG CODE = MISSOURI BUILDING CODE 2018 ADDPTING 2018 INTERNATIONAL BUILDING CODE EQUIVALENT LATERAL FORCE PROCEDURE LATERAL FORCE RESISTING SYSTEM = CANTILLEVERED COLUMN SYSTEM—ORDINARY STEEL MOMENT FRAME PI = 20 p.s.f. Ce = 1.2 Ct = 1.2 LS = 1.0 W = 4.92 Pd = 20.44 SITE CLASS = D SS (0.2) = 0.099 S1 (1.0) = 0.088 SDS = 0.11 SDS = 0.11 FO = 1.60 FV = 2.40 R = 1.25 MADORTANCE FACTOR = 1.0 RISK CATEGORY = 1.0 SEISMIC DESIGN CATEGORY = 0 CONSTRUCTION TYPE = 189 OCCUPANCY CATEGORY = A2 TOTAL SEISMIC BASE SHEAR BOTH ORRECTIONS = 1.43 KIPS