

## **STRUCTURAL CALCULATIONS FOR**

TM Fieldhouse  
1600 SE Hamblen Rd  
Lee's Summit, MO 64063

Project # 22453

5/3/2023



05/03/2023

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## **STRUCTURAL DESIGN CRITERIA (2018 IBC AND ASCE 7-16):**

1. BUILDING OCCUPANCY RISK CATEGORY III.
2. LIVE LOADS [UNIFORM (PSF) / POINT LOADS (KIPS)]:
  - ROOF:.....20 PSF / 300#
  - GROUND LEVEL SLAB .....100 PSF / 2.0 K
  - MEZZANINE & STAIRS .....100 PSF / 300#
3. ROOF SNOW LOAD:
  - GROUND SNOW LOAD (Pg):.....20 PSF
  - FLAT ROOF SNOW LOAD (Pf): .....16.94 PSF W/ DRIFT
  - MIN UNIFORM ROOF SNOW LOAD (Pm):.....22 PSF (NO DRIFT OR RAIN)
  - RAIN ON SNOW SURCHARGE (Prs) .....5.0 PSF
  - SNOW EXPOSURE FACTOR (Ce):.....1.0, EXPOSURE C
  - SNOW LOAD IMPORTANCE FACTOR (Is):.....1.0
  - THERMAL FACTOR (Ct):.....1.1 (just above freezing)
  - SLOPE FACTOR (Cs):.....1.0
4. WIND DESIGN DATA:
  - BASIC WIND SPEED (3 SEC GUST):.....117 MPH
  - ASD WIND SPEED, V(ASD).....90 MPH
  - WIND EXPOSURE:.....C
  - GROUND ELEVATION ABOVE SEA LEVEL.....1,000 FT
  - DIRECTIONALITY FACTOR (Kd) .....0.85
  - INTERNAL PRESSURE COEFF:.....0.18
  - COMPONENTS AND CLADDING WIND (ULTIMATE 1.0\*W) PRESSURES  
(BASED ON TRIB 10 S.F., EXP. C. MAY BE REDUCED FOR COMPONENTS WITH  
LARGER TRIB PER BLDG CODE):
    - WALLS AT CORNERS & EDGES:.....+31 / -41 PSF
    - ALL OTHER MAIN WALL CONDITIONS:.....+31 / -33.3 PSF
    - ROOF CORNERS:.....+14 / -96.3 PSF
    - ROOF EDGES: .....+14 / -71 PSF
    - ALL OTHER MAIN ROOF CONDITIONS:.....+14/ -54 PSF
    - PARAPET EDGES:.....

5. EARTHQUAKE DESIGN DATA:

- SEISMIC IMPORTANCE FACTOR ( $I_e$ ):.....1.25
- MAPPED SPECTRAL RESP ACCEL ( $S_s$  /  $S_1$ ):.....0.100 / 0.068
- SITE CLASS:.....D
- SPECTRAL RESPONSE COEFF ( $S_{ds}$  /  $S_{d1}$ ):.....0.107 / 0.110
- SEISMIC DESIGN CATEGORY:.....B
- SEISMIC FORCE RESISTING SYSTEM:.....R=3, STEEL
- DESIGN BASE SHEAR:.....DETERMINED BY MB MFCR
- SEISMIC RESPONSE COEFF ( $C_s$ ):.....0.044
- ANALYSIS PROCEDURE:.....ELF

6. RAIN LOAD DATA:

- 15-MIN RAIN INTENSITY.....8.28 IN/HR
- 60-MIN RAIN INTENSITY.....3.9 IN/HR

DESIGN ASSUMES APPROPRIATE ROOF SLOPE AND DRAINAGE (INCLUDING OVERFLOWS) ARE PROVIDED. ROOF IS DESIGNED FOR LIVE LOAD INDICATED ABOVE

7. GUARD RAILS:.....50 PLF, AND/OR 200#  
CONCENTRATED LOAD APPLIED IN ANY DIRECTION.

8. ADDITIONAL DELEGATED DESIGN CRITERIA:

A. LOADS

- PEMB COLLATERAL ROOF LOAD:.....5 PSF
- MECHANICAL EQUIPMENT AND LOADS:.....AS INDICATED ON MEP PLANS
- BASKETBALL GOALS, DIVIDING CURTAINS, BASEBALL NETS: AS INDICATED ON ARCH AND MEP PLANS

B. MEMBER DEFLECTION LIMITS (UNDER ROOF LIVE, SNOW, 10 YR WIND, OR SOIL PRESSURE)

- ROOF, SUPPORTING PLASTER CEILING:.....L/360
- ROOF, SUPPORTING OTHER CEILING:.....L/240
- WALL GIRT, BACKING NON-BRITTLE FINISH.....L/180
- WALL GIRT, BACKING BRITTLE FINISH.....L/360

C. BUILDING DRIFT LIMITS (UNDER 10 YR WIND, SEISMIC, OR SOIL PRESSURE):

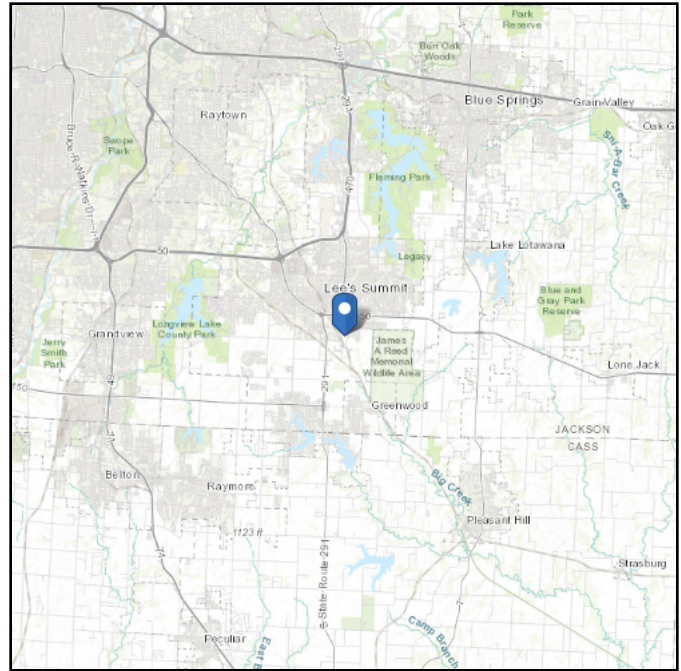
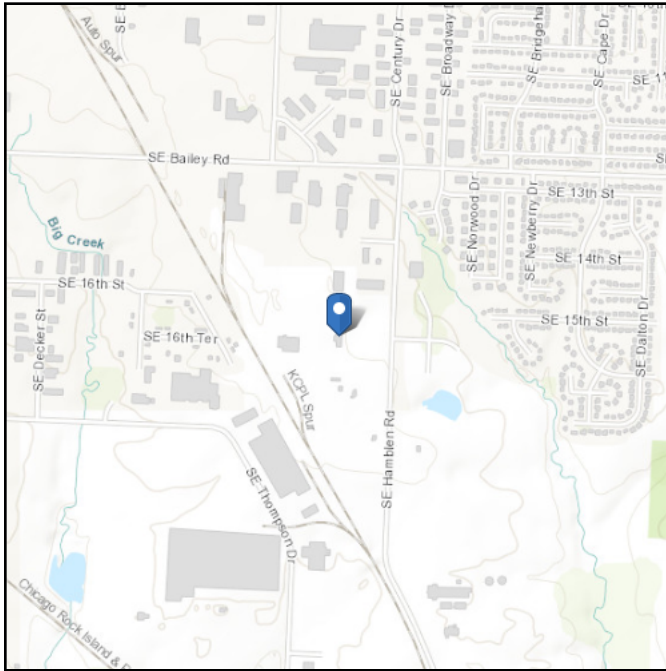
- BRITTLE EXTERIOR FINISH:.....H/240
- METAL WALL PANELS:.....H/100

# ASCE 7 Hazards Report

**Address:**  
1600 SE Hamblen Rd  
Lees Summit, Missouri  
64081

**Standard:** ASCE/SEI 7-16  
**Risk Category:** III  
**Soil Class:** D - Stiff Soil

**Latitude:** 38.89093  
**Longitude:** -94.361076  
**Elevation:** 1024.2 ft (NAVD 88)



## Wind

### Results:

Wind Speed	117 Vmph
10-year MRI	76 Vmph
25-year MRI	83 Vmph
50-year MRI	88 Vmph
100-year MRI	94 Vmph

Data Source: ASCE/SEI 7-16, Fig. 26.5-1C and Figs. CC.2-1–CC.2-4, and Section 26.5.2

Date Accessed: Tue Feb 21 2023

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 3% probability of exceedance in 50 years (annual exceedance probability = 0.000588, MRI = 1,700 years).

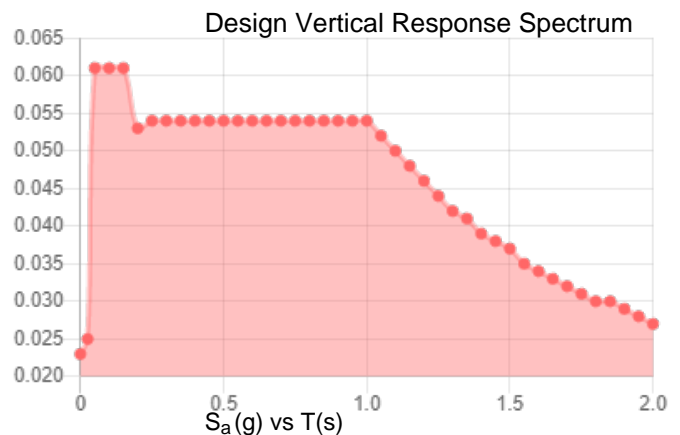
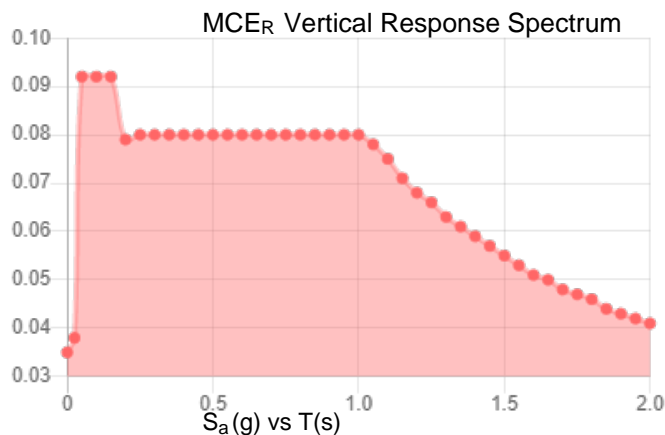
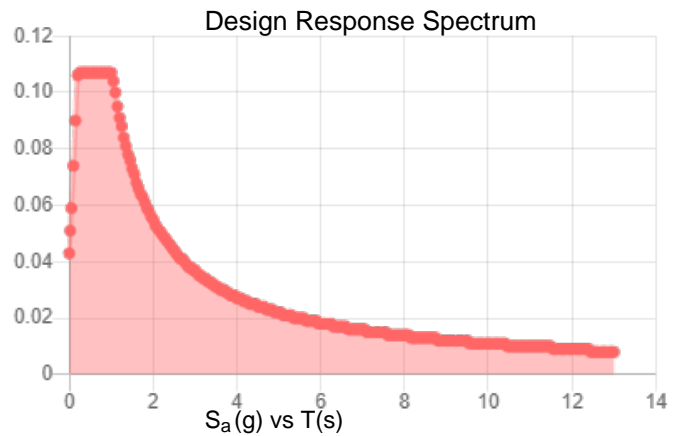
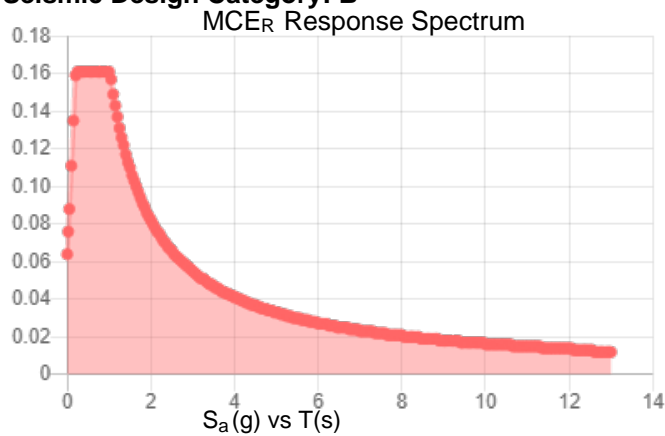
Site is not in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2.

**Site Soil Class:**

**Results:**

$S_S$ :	0.1	$S_{D1}$ :	0.11
$S_1$ :	0.068	$T_L$ :	12
$F_a$ :	1.6	PGA :	0.047
$F_v$ :	2.4	PGA <sub>M</sub> :	0.076
$S_{MS}$ :	0.161	$F_{PGA}$ :	1.6
$S_{M1}$ :	0.164	$I_e$ :	1.25
$S_{DS}$ :	0.107	$C_v$ :	0.7

**Seismic Design Category: B**



**Data Accessed:**

**Tue Feb 21 2023**

**Date Source:**

**USGS Seismic Design Maps based on ASCE/SEI 7-16 and ASCE/SEI 7-16 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-16 Ch. 21 are available from USGS.**

## Ice

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**Results:**

Ice Thickness: 1.50 in.

Concurrent Temperature: 5 F

Gust Speed 40 mph

**Data Source:** Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8

**Date Accessed:** Tue Feb 21 2023

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

## Snow

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**Results:**

Ground Snow Load,  $p_g$ : 20 lb/ft<sup>2</sup>

Elevation: 1024.2 ft

**Data Source:** ASCE/SEI 7-16, Table 7.2-8

**Date Accessed:** Tue Feb 21 2023

Values provided are ground snow loads. In areas designated "case study required," extreme local variations in ground snow loads preclude mapping at this scale. Site-specific case studies are required to establish ground snow loads at elevations not covered.

## Rain

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### Results:

15-minute Precipitation Intensity: 8.28 in./h

60-minute Precipitation Intensity: 3.9 in./h

**Data Source:** NOAA National Weather Service, Precipitation Frequency Data Server, Atlas 14  
(<https://www.nws.noaa.gov/oh/hdsc/>)

**Date Accessed:** Tue Feb 21 2023

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The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 8' retaining wall

### Code Reference:

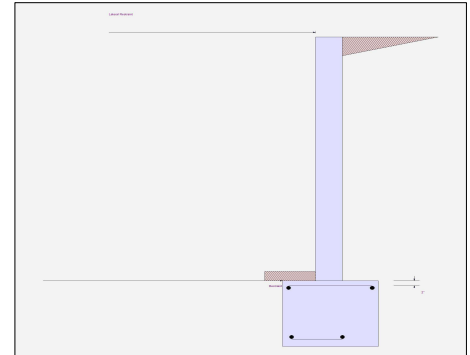
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

#### Criteria

Retained Height	=	8.670 ft
Wall height above soil	=	ft
Total Wall Height	=	8.670 ft
Top Support Height	=	8.670 ft
Slope Behind Wall	=	0
Height of Soil over Toe	=	4.0 in

#### Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method		
At-Rest Heel Pressure	=	60.0 psf/ft
	=	0.0 psf/ft
Passive Pressure	=	250.0 psf/ft
Soil Density	=	110 pcf
Footing  Soil Frictior	=	0.4 psf
Soil height to ignore for passive pressure	=	12 in



#### Surcharge Loads

Surcharge Over Heel	=	psf
>>>Used To Resist Sliding & Overturning		
Surcharge Over Toe	=	psf
Used for Sliding & Overturning		

#### Axial Load Applied to Stem

Axial Dead Load	=	lbs
Axial Live Load	=	lbs
Axial Load Eccentricity	=	in

#### Earth Pressure Seismic Load

#### Uniform Lateral Load Applied to Stem

Lateral Load	=	#/ft
...Height to Top	=	ft
...Height to Bottom	=	ft
Load Type	=	Wind (W) (Strength Level)
Wind on Exposed Stem	=	0.00 psf (Strength Level)
Wind acts left-to-right toward retention side.		
$K_h$ Soil Density Multiplier	=	0.2 g

#### Adjacent Footing Load

Adjacent Footing Load	=	lbs
Footing Width	=	ft
Eccentricity	=	in
Wall to Ftg CL Dist	=	ft
Footing Type		Line Load
Base Above/Below Soil at Back of Wall	=	ft
Poisson's Ratio	=	0.3
Added seismic per unit area	=	0.0 psf

### Design Summary

Total Bearing Load	=	2,791.14 lbs
...resultant ecc.	=	0.0 in
Soil Pressure @ Toe	=	1,046.55 psf OK
Soil Pressure @ Heel	=	1,046.55 psf OK
Allowable	=	psf
Soil Pressure Less Than Allowable		
ACI Factored @ Toe	=	1,255.85 psf
ACI Factored @ Heel	=	1,255.85 psf
Footing Shear @ Toe	=	1.644 psi OK
Footing Shear @ Heel	=	-1.009 psi OK
Allowable	=	94.868 psi
Reaction at Top	=	449.971 lbs
Reaction at Bottom	=	3,181.19 lbs

#### Sliding Calcs

Lateral Sliding Force	=	3,181.19 lbs
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Vertical component of active lateral soil pressure IS NOT considered in the calculation of soil bearing

#### Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.000
Seismic, E	1.000

### Concrete Stem Construction

Thickness	=	8.00 in
Wall Weight	=	100.0 psf
Stem is FIXED to top of footing		

	@ Top Support	Mmax Between Top & Base	@ Base of Wall
	Stem OK	Stem OK	Stem OK
Design Height Above Ftg	= 8.670 ft	0.03482 ft	0.00 ft
Rebar Size	= # 5	# 5	# 5
Rebar Spacing	= 12.00 in	12.00 in	12.00 in
Rebar Placed at	= Center	Center	Center
Rebar Depth 'd'	= 4.0 in	4.0 in	4.0 in
Design Data			
fb/FB + fa/Fa	=	0.793	0.793
Moment.....Actual	= 0.0 ft-#	4,171.06 ft-#	4,171.06 ft-#
Moment.....Allowable	= 5,261.07 ft-#	5,261.07 ft-#	5,261.07 ft-#
Shear Force @ this height	= 721.61 lbs		2,886.50 lbs
Shear.....Actual	= 15.034 psi		60.135 psi
Shear.....Allowable	= 94.868 psi		94.868 psi



Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 8' retaining wall

### Footing Strengths & Dimensions

Toe Width	=	1 ft
Heel Width	=	1.667
Total Footing Width	=	2.667
Footing Thickness	=	28.0 in
Key Width	=	in
Key Depth	=	in
Key Distance from Toe	=	ft
f'c =	4,000.0 psi	Fy = 60000 psi
Footing Concrete Density	=	150 pcf
Min. As %	=	0.0018
Cover @ Top	= 2 in	@ Btm.= 3 in

### Footing Design Results

	Toe	Heel
Factored Pressure	= 1,255.85	1,255.85 psf
Mu' : Upward	= 627.93	ft-#
Mu' : Downward	= 232.0	ft-#
Mu: Design	= 396	154 ft-#
Actual 1-Way Shear	= 1.644	psi
Allow 1-Way Shear	= 94.868	94.868 psi

### Other Acceptable Sizes & Spacings:

Toe: # 5 @ 6.15 in	-or-	#4@ 3.96 in, #5@ 6.15 in, #6@ 8.73 in, #7@ 11.90
Heel: # 5 @ 6.15 in	-or-	#4@ 3.96 in, #5@ 6.15 in, #6@ 8.73 in, #7@ 11.90
Key: # 0 @ 0.00 in	-or-	No key defined
Min footing T&S reinf Area		1.61 in2
Min footing T&S reinf Area per foot		0.60 in2 /ft
If one layer of horizontal bars:		If two layers of horizontal bars:
#4@ 3.97 in		#4@ 7.94 in
#5@ 6.15 in		#5@ 12.30 in
#6@ 8.73 in		#6@ 17.46 in

## Summary of Forces on Footing : Slab RESISTS sliding, stem is FIXED at footing

### Forces acting on footing for soil pressure

>>> Sliding Forces are restrained by the adjacent slab

### Load & Moment Summary For Footing : For Soil Pressure Calcs

Moment @ Top of Footing Applied from Stem	=	-2,606.91 ft-#
Surcharge Over Heel	= 0.0 lbs	0.0 ft
Adjacent Footing Load	= 0.0 lbs	0.0 ft
Axial Dead Load on Stem	= 0.0 lbs	0.0 ft
Soil Over Toe	= 36.667 lbs	0.50 ft
Surcharge Over Toe	= 0.0 lbs	0.0 ft
Stem Weight	= 867.0 lbs	1.333 ft
Soil Over Heel	= 954.02 lbs	2.167 ft
Footing Weight	= 933.45 lbs	1.334 ft
<b>Total Vertical Force</b>	= 2,791.14 lbs	<b>Base Moment = 1,879.38 ft-#</b>

**Stem is specified to be fixed to footing, and top restraint is assumed to react out any tendency for moment at the footing/soil interface, so uniform soil pressure is assumed.**

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Project Title:  
Engineer:  
Project ID:  
Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 8' retaining wall

### Rebar Lap & Embedment Lengths Information

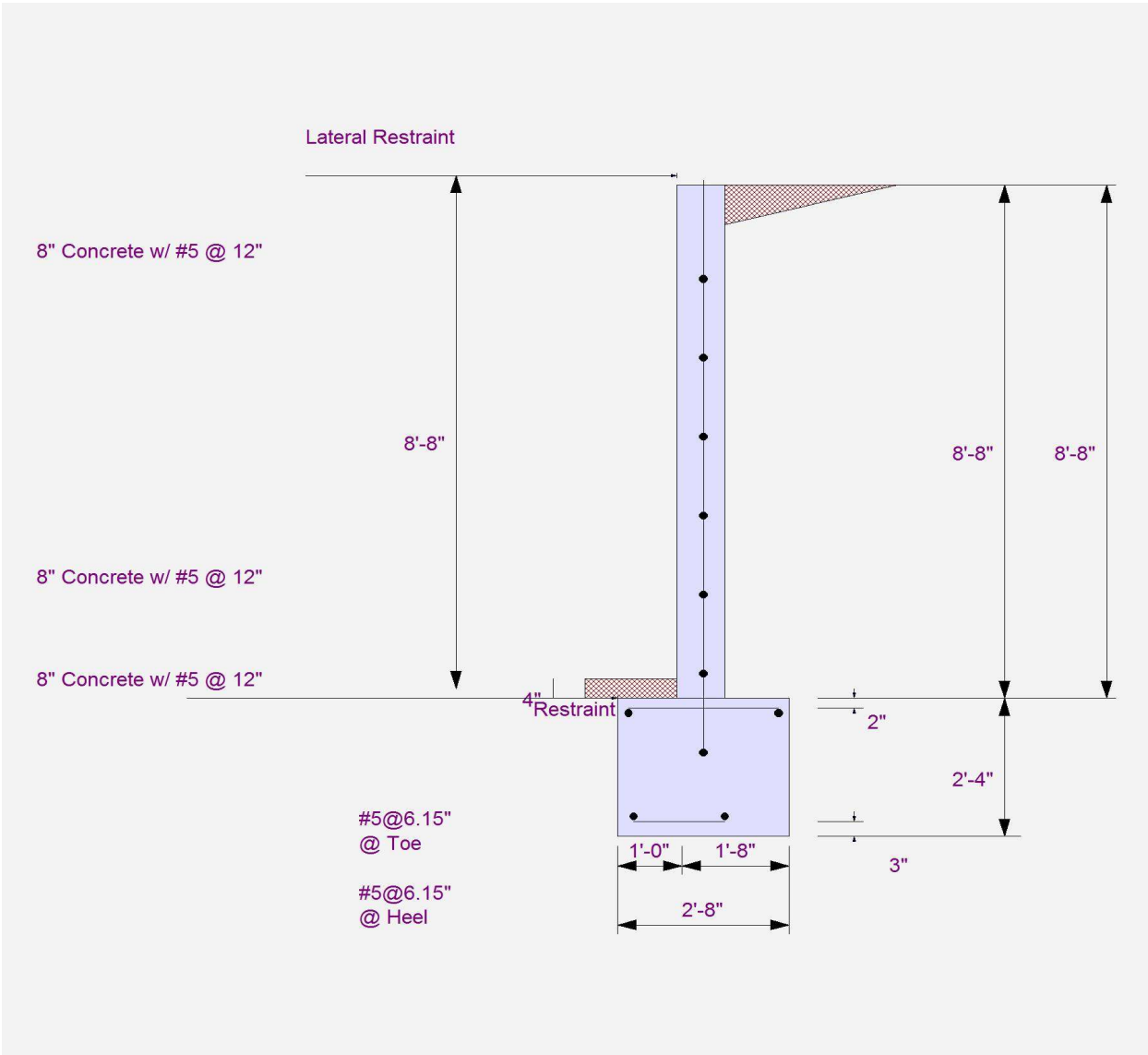
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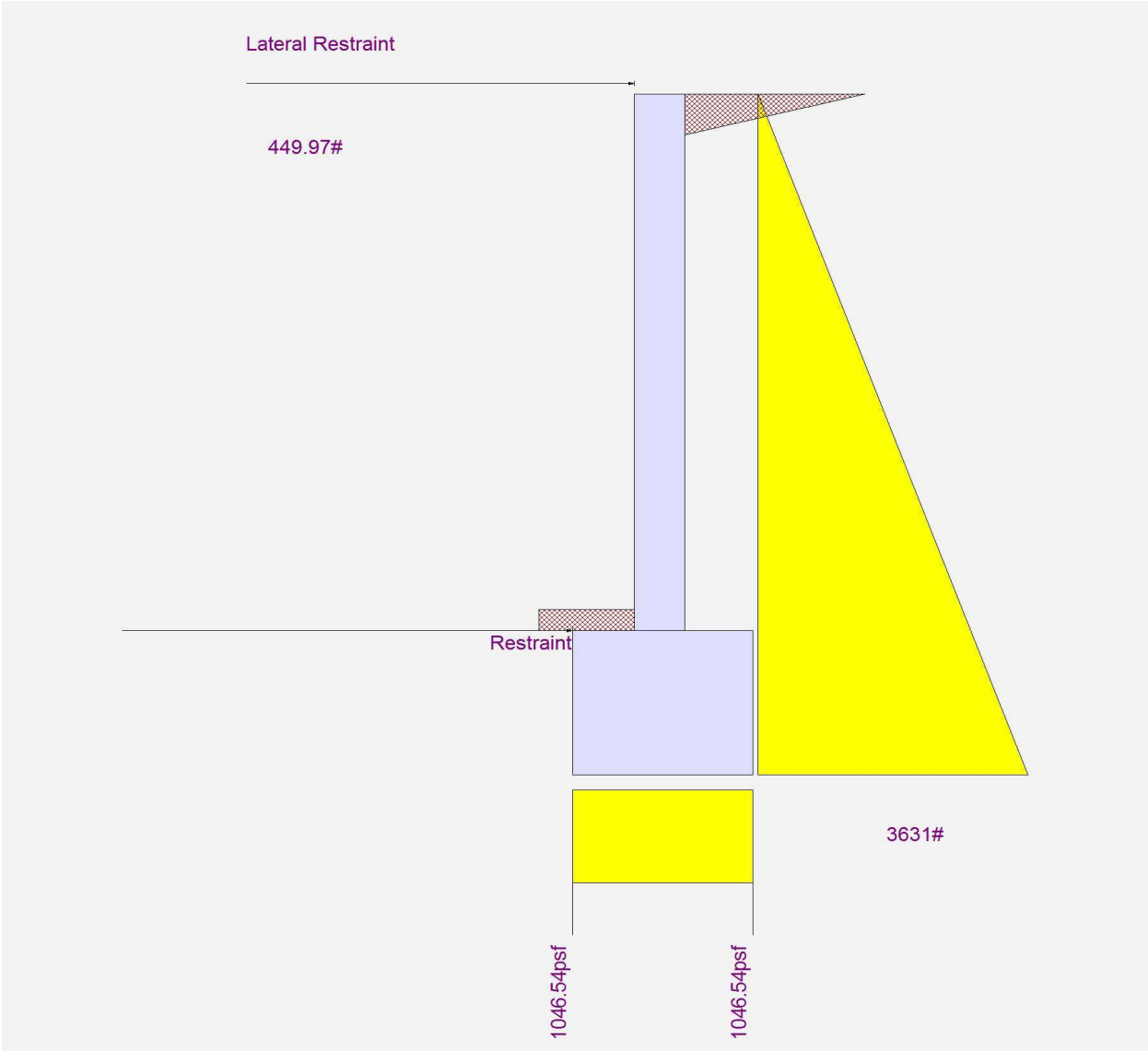
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LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 8' retaining wall



Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 6' retaining wall

### Code Reference:

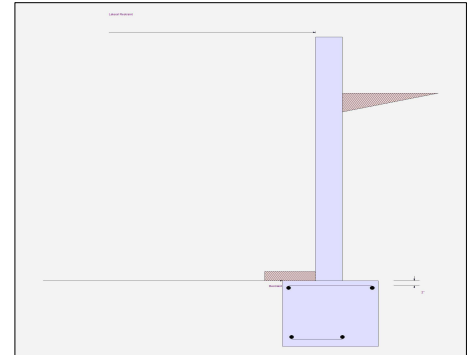
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

#### Criteria

Retained Height	=	6.670 ft
Wall height above soil	=	2.0 ft
Total Wall Height	=	8.670 ft
Top Support Height	=	8.670 ft
Slope Behind Wall	=	0
Height of Soil over Toe	=	4.0 in

#### Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method		
At-Rest Heel Pressure	=	60.0 psf/ft
	=	0.0 psf/ft
Passive Pressure	=	250.0 psf/ft
Soil Density	=	110 pcf
Footing  Soil Frictior	=	0.4 psf
Soil height to ignore for passive pressure	=	12 in



#### Surcharge Loads

Surcharge Over Heel	=	psf
>>>Used To Resist Sliding & Overturning		
Surcharge Over Toe	=	psf
Used for Sliding & Overturning		

#### Axial Load Applied to Stem

Axial Dead Load	=	lbs
Axial Live Load	=	lbs
Axial Load Eccentricity	=	in

#### Earth Pressure Seismic Load

#### Uniform Lateral Load Applied to Stem

Lateral Load	=	#/ft
...Height to Top	=	ft
...Height to Bottom	=	ft
Load Type	=	Wind (W) (Strength Level)
Wind on Exposed Stem	=	0.00 psf (Strength Level)
Wind acts left-to-right toward retention side.		
$K_h$ Soil Density Multiplier	=	0.2 g

#### Adjacent Footing Load

Adjacent Footing Load	=	lbs
Footing Width	=	ft
Eccentricity	=	in
Wall to Ftg CL Dist	=	ft
Footing Type		Line Load
Base Above/Below Soil at Back of Wall	=	ft
Poisson's Ratio	=	0.3
Added seismic per unit area	=	0.0 psf

### Design Summary

Total Bearing Load	=	2,571.06 lbs
...resultant ecc.	=	0.0 in
Soil Pressure @ Toe	=	964.03 psf OK
Soil Pressure @ Heel	=	964.03 psf OK
Allowable	=	psf
Soil Pressure Less Than Allowable		
ACI Factored @ Toe	=	1,156.83 psf
ACI Factored @ Heel	=	1,156.83 psf
Footing Shear @ Toe	=	1.644 psi OK
Footing Shear @ Heel	=	-0.4695 psi OK
Allowable	=	94.868 psi
Reaction at Top	=	166.093 lbs
Reaction at Bottom	=	2,264.71 lbs

<b>Sliding Calcs</b>	
Lateral Sliding Force	= 2,264.71 lbs

Vertical component of active lateral soil pressure IS NOT considered in the calculation of soil bearing

#### Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.000
Seismic, E	1.000

### Concrete Stem Construction

Thickness	=	8.00 in
Wall Weight	=	100.0 psf
Stem is FIXED to top of footing		

	@ Top Support	Mmax Between Top & Base	@ Base of Wall
	Stem OK	Stem OK	Stem OK
Design Height Above Ftg	= 8.670 ft	0.03482 ft	0.00 ft
Rebar Size	= # 5	# 5	# 5
Rebar Spacing	= 12.00 in	12.00 in	12.00 in
Rebar Placed at	= Center	Center	Center
Rebar Depth 'd'	= 4.0 in	4.0 in	4.0 in
Design Data			
fb/FB + fa/Fa	=	0.462	0.462
Moment.....Actual	= 0.0 ft-#	2,429.94 ft-#	2,429.94 ft-#
Moment.....Allowable	= 5,261.07 ft-#	5,261.07 ft-#	5,261.07 ft-#
Shear Force @ this height	= 267.349 lbs		1,868.12 lbs
Shear.....Actual	= 5.570 psi		38.919 psi
Shear.....Allowable	= 94.868 psi		94.868 psi

Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 6' retaining wall

### Footing Strengths & Dimensions

Toe Width	=	1 ft
Heel Width	=	1.667
Total Footing Width	=	2.667
Footing Thickness	=	28.0 in
Key Width	=	in
Key Depth	=	in
Key Distance from Toe	=	ft
$f'_c$ =	4,000.0 psi	$F_y$ = 60000 psi
Footing Concrete Density	=	150 pcf
Min. As %	=	0.0018
Cover @ Top	=	2 in @ Btm.= 3 in

### Footing Design Results

	Toe	Heel
Factored Pressure	= 1,156.83	1,156.83 psf
$\mu_u$ : Upward	= 578.42	ft-#
$\mu_u$ : Downward	= 232.0	ft-#
$\mu_u$ : Design	= 346	72 ft-#
Actual 1-Way Shear	= 1.644	psi
Allow 1-Way Shear	= 94.868	94.868 psi

### Other Acceptable Sizes & Spacings:

Toe: # 5 @ 6.15 in	-or-	#4@ 3.96 in, #5@ 6.15 in, #6@ 8.73 in, #7@ 11.90
Heel: # 5 @ 6.15 in	-or-	#4@ 3.96 in, #5@ 6.15 in, #6@ 8.73 in, #7@ 11.90
Key: # 0 @ 0.00 in	-or-	No key defined
Min footing T&S reinf Area	1.61	in <sup>2</sup>
Min footing T&S reinf Area per foot	0.60	in <sup>2</sup> /ft
If one layer of horizontal bars:	If two layers of horizontal bars:	
#4@ 3.97 in	#4@	7.94 in
#5@ 6.15 in	#5@	12.30 in
#6@ 8.73 in	#6@	17.46 in

### Summary of Forces on Footing : Slab RESISTS sliding, stem is FIXED at footing

#### Forces acting on footing for soil pressure

>>> Sliding Forces are restrained by the adjacent slab

#### Load & Moment Summary For Footing : For Soil Pressure Calcs

Moment @ Top of Footing Applied from Stem	=	-1,518.71 ft-#
Surcharge Over Heel	= 0.0 lbs	0.0 ft
Adjacent Footing Load	= 0.0 lbs	0.0 ft
Axial Dead Load on Stem	= 0.0 lbs	0.0 ft
Soil Over Toe	= 36.667 lbs	0.50 ft
Surcharge Over Toe	= 0.0 lbs	0.0 ft
Stem Weight	= 867.0 lbs	1.333 ft
Soil Over Heel	= 733.94 lbs	2.167 ft
Footing Weight	= 933.45 lbs	1.334 ft
<b>Total Vertical Force</b>	= 2,571.06 lbs	<b>Base Moment</b> = 2,490.71 ft-#

**Stem is specified to be fixed to footing, and top restraint is assumed to react out any tendency for moment at the footing/soil interface, so uniform soil pressure is assumed.**

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Project Title:  
Engineer:  
Project ID:  
Project Descr:

## Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 6' retaining wall

### Rebar Lap & Embedment Lengths Information

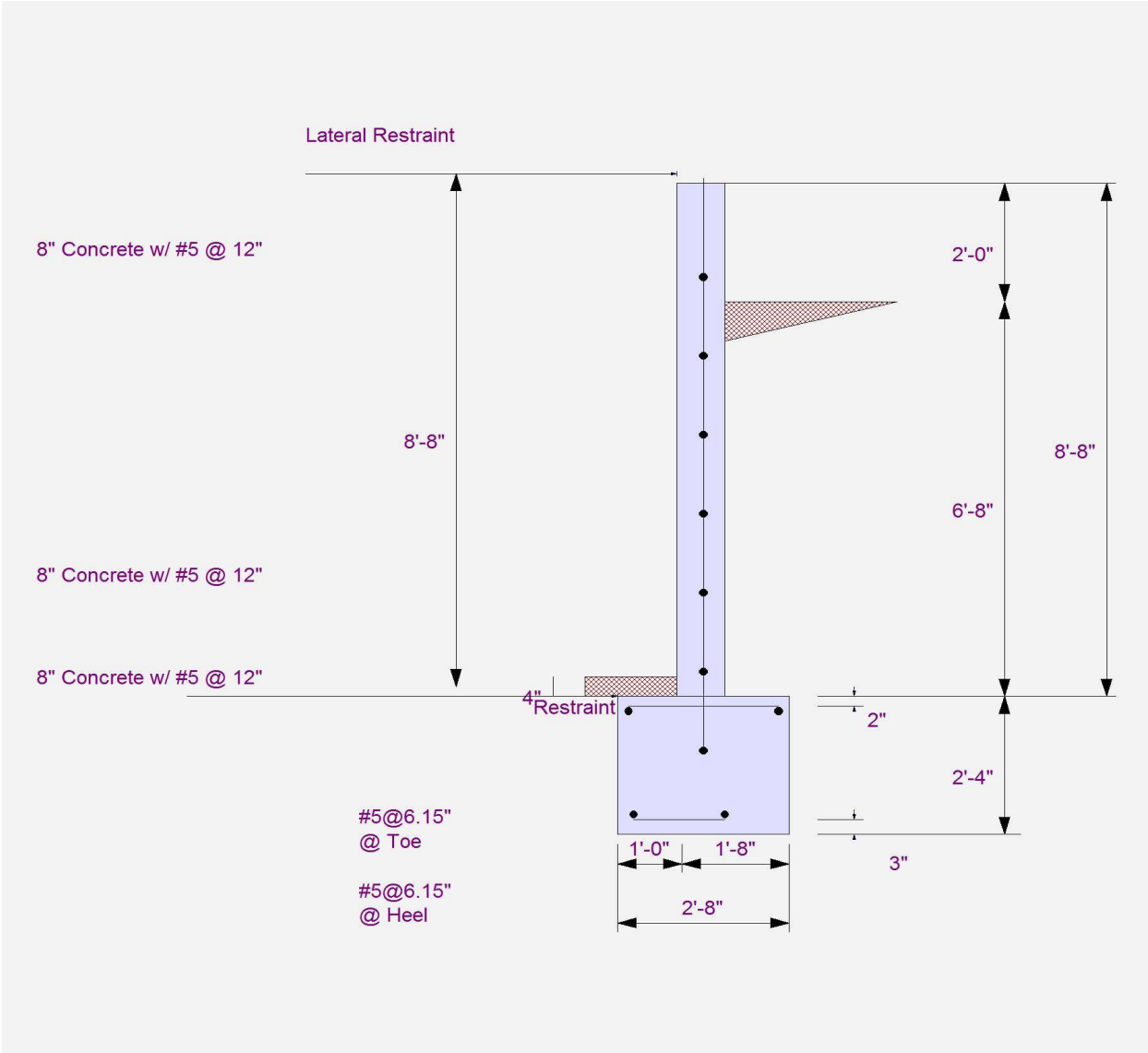
# Restrained Retaining Wall

LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

DESCRIPTION: 6' retaining wall





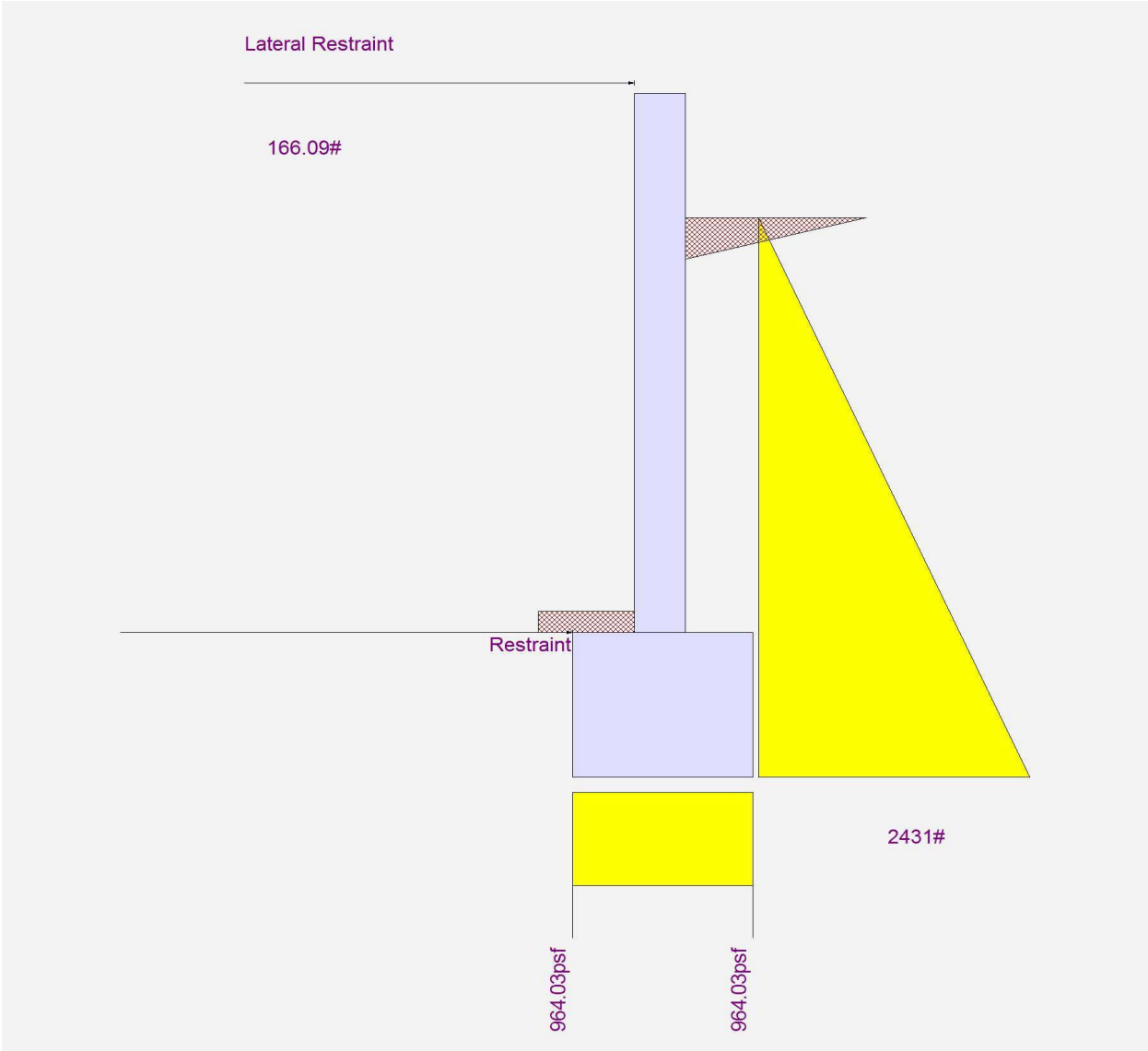
**Restrained Retaining Wall**

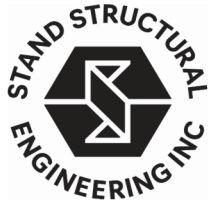
LIC# : KW-06011423, Build:20.22.12.28

Stand Structural Engineering Inc.

(c) ENERCALC INC 1983-2022

**DESCRIPTION:** 6' retaining wall





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Project: TM Fieldhouse  
Project No: 22453

Engineer: BWH  
Date: 05/03/2023

Checked by:  
Date:

## Square Spread Footing Design

$f'_c$ : **3** ksi      W Col BP **8** in  
 $f_y$ : **60** ksi      Rebar Clr: **3** in

$\phi$ -v: **0.75**  
 $\phi$ -f: **0.9**

Footings assume reinforcement in top and bottom, so the min temp and shrinkage reinforcement on one side meets .0009

LRFD Factor: **1.6**

Allowable Bearing,  $q_a$ : **1.5** ksf

Ultimate Bearing,  $q_u$ : **2.4** ksf

### Bar Areas

3	0.11
4	0.2
5	0.31
6	0.44
7	0.6
8	0.79
9	1

v-beam: **82.2** psi      <<Allowable Beam Shear Stress  
v-punch: **164.3** psi      <<Allowable Punching Shear Stress

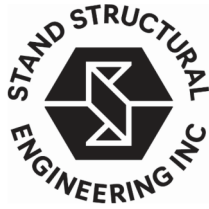
### Rebar Size

Width	Thickness	Depth	Reaction	BEAM SHEAR		PUNCHING SHEAR		LRFD Moment	Beam Min	Temp. & Shrinkage	<b>5</b>	<b>6</b>	Footing Weight
b (ft):	h (in):	d (in):	P-allow:	$\sigma_{act}$	Unity	$\sigma_{act}$	Unity	Mu (kft)	As reqd	As reqd	0.31	0.44	kips
<b>3</b>	<b>30</b>	26	<b>13.50</b>	0.0	<b>0.00</b>	0.7	<b>0.00</b>	4.900	0.056	0.972	4	3	3.38
<b>4</b>	<b>30</b>	26	<b>24.00</b>	0.0	<b>0.00</b>	5.4	<b>0.03</b>	13.333	0.152	1.296	5	3	6.00
<b>5</b>	<b>30</b>	26	<b>37.50</b>	0.0	<b>0.00</b>	11.5	<b>0.07</b>	28.167	0.322	1.620	6	4	9.38
<b>6</b>	<b>30</b>	26	<b>54.00</b>	3.8	<b>0.05</b>	19.0	<b>0.12</b>	51.200	0.585	1.944	7	5	13.50
<b>6.5</b>	<b>30</b>	26	<b>63.38</b>	5.8	<b>0.07</b>	23.2	<b>0.14</b>	66.354	0.759	2.106	7	5	15.84
<b>7</b>	<b>30</b>	26	<b>73.50</b>	7.7	<b>0.09</b>	27.8	<b>0.17</b>	84.233	0.964	2.268	8	6	18.38
<b>7.5</b>	<b>30</b>	26	<b>84.38</b>	9.6	<b>0.12</b>	32.7	<b>0.20</b>	105.063	1.203	2.430	8	6	21.09

Grade Beam Width: **12** in  
Grade Beam Height: **30** in  
Slab Thickness: **4** in

Grade Beam Weight: **0.375** klf  
Wall Weight: **0.25** klf  
Grade Beam Span: **25** ft  
ASD Moment: **49** kip-ft  
(LRFD) 1.4\*Moment: **68** kip-ft  
ASD Shear: **8** kip  
(LRFD) 1.4\*Shear: **11** kip

Uplift Check		Footing Weight	Resisting Slab		Resisting Grade Beam		Bldg Self Weight	Total Weight	Allow. Uplift
Width	Thickness		Area	Weight	Length	Weight			
b (ft):	h (in):	kips	ft^2	kips	ft	kips	kips	kips	kips
<b>3</b>	<b>30</b>	<b>3.4</b>	<b>100</b>	<b>5.0</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	18.75	<b>12.5</b>
<b>4</b>	<b>30</b>	<b>6.0</b>	<b>100</b>	<b>5.0</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	21.38	<b>14.3</b>
<b>5</b>	<b>30</b>	<b>9.4</b>	<b>100</b>	<b>5.0</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	24.75	<b>16.5</b>
<b>6</b>	<b>30</b>	<b>13.5</b>	<b>100</b>	<b>5.0</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	28.88	<b>19.3</b>
<b>6.5</b>	<b>30</b>	<b>15.8</b>	<b>125</b>	<b>6.3</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	32.47	<b>21.6</b>
<b>7</b>	<b>30</b>	<b>18.4</b>	<b>125</b>	<b>6.3</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	35.00	<b>23.3</b>
<b>7.5</b>	<b>30</b>	<b>21.1</b>	<b>125</b>	<b>6.3</b>	<b>25</b>	<b>9.4</b>	<b>1.0</b>	37.72	<b>25.1</b>



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Footing Description	Footing Width (ft)	Footing Thickness (inches)	Max ASD Gravity Reaction (kips)	Gravity Allow. Bearing (kips)	Unity Check	Max ASD Uplift Reaction (kips)	Allow. Uplift (kips)	Unity Check	Hairpin Bar Size #	Max ASD Kickout Force (kips)	Allow. Kickout Force (kips)	Unity Check
120' Footings	7	30	45	73.5	0.61	23.1	23.3	0.99	6	25	14.9	1.67
105' Footings	6.5	30	40	63.4	0.63	20.8	21.65	0.96	6	20	14.93	1.34

Use tie beam. See next page

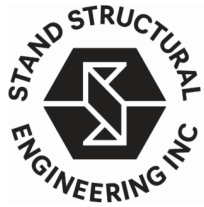
**Reaction Verification**

Dead Load:	5	psf	Total Gravity Load:	30	psf
Collateral Load:	5	psf	Approx. ASD Roof Uplift Load:	17.01	psf
Roof Live/Snow Load:	20	psf	Net ASD Roof Uplift Load:	14.01	psf
Wind Base Pressure:	30	psf	Approx. ASD Wall Load:	19.89	psf
Interior P/S Coeff:	0.18				

**Anchor Rod Design (ASD)**

3/4" CIP Anchors (12" embed)	18 kips uplift	12 kips kickout
1" CIP Anchors (15" embed)	25 kips uplift	15 kips kickout

Footing Description	Bay Spacing	Frame Width	Eave Height	Snow Drift Load	Est. Gravity Reaction	Est. Uplift Reaction	Est. Out Kickout Reaction	Est. In Kickout Reaction
	feet	feet	feet	psf	kips	kips	kips	kips
120' Footings	25	120	32	0	45	23.14	24.44	19.37
105' Footings	25	105	32	0	39.375	20.81	18.52	16.61



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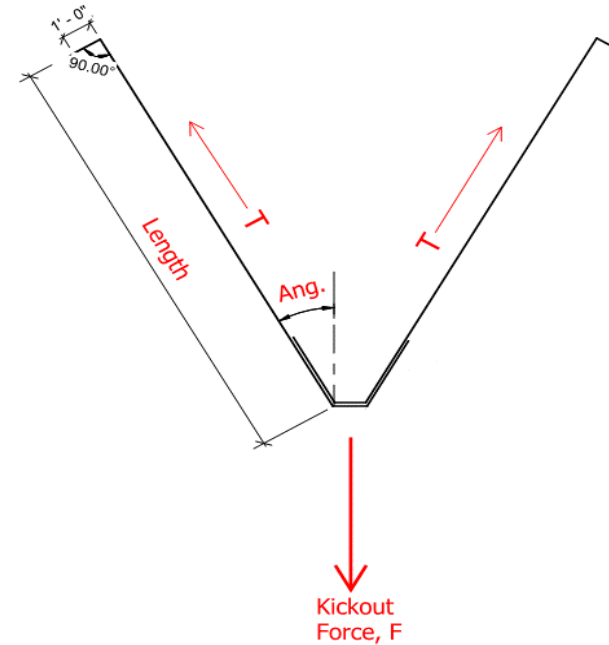
## Hairpin Design

Slab Bar Area: **0.05** in<sup>2</sup>/ft

Hairpin Bar Used		Allowable Tension	Allowable Kickout	Develop. Length	Required Length
Bar #	Area	kips	kips	inches	feet
4	0.2	<b>4.8</b>	<b>6.8</b>	<b>24</b>	<b>7.7</b>
5	0.31	<b>7.4</b>	<b>10.5</b>	<b>30</b>	<b>11.3</b>
6	0.44	<b>10.6</b>	<b>14.9</b>	<b>36</b>	<b>15.4</b>
7	0.6	<b>14.4</b>	<b>20.4</b>	<b>42</b>	<b>20.5</b>

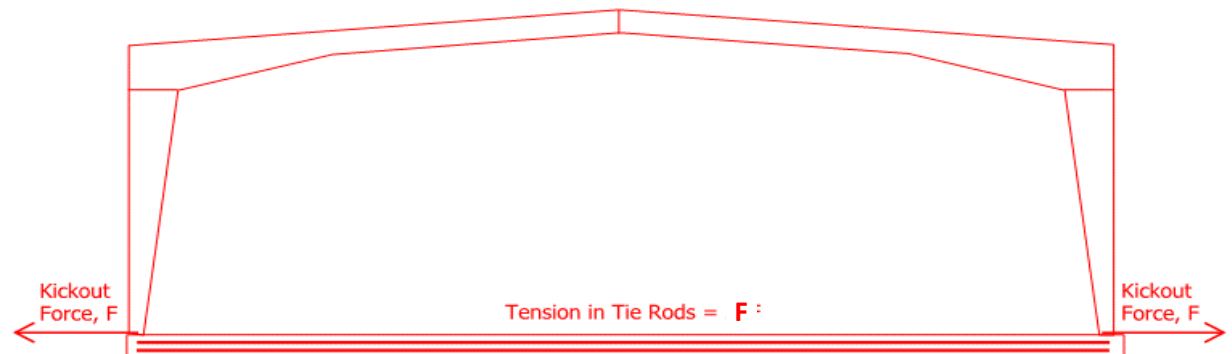
For Kickout forces of 5 kips or less and min. slab reinforcement of #3@18" OC or #4@ 24" OC - Use (4) #4 Slab Dowels (3'x3') @ 24" OC

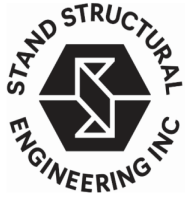
For Kickout forces of greater than 15 kips it is recommended to use tie rods in a grade beam or thickened slab instead of hairpins.



## Tie Rod Design

Tie Rod Length: **120** feet  
 Allow. Elongation: **0.75** inch  
 Kickout Force, F: **25** kips  
 Req'd As (Elongation): **1.66** in<sup>2</sup>  
 Req'd As (Tension): **1.04** in<sup>2</sup>  
 Bar Size Selected: # **5**  
 # of Bars: **6**  
 Actual Area of Steel: **1.9** in<sup>2</sup>  
 Unity Check: **0.89**





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### Floor Loads & Deck Checks

Location	<b>2nd Floor Mezzanine</b>		
Deck Selection	<b>1.0C</b>	<b>26</b> gauge	Width <b>36</b> inches
Total Slab Depth	<b>4</b> inches		Grade <b>50</b> ksi
Concrete Thickness above Deck	<b>3</b> inches		
Concrete Type	<b>Normal Weight</b>		
Fire Rating	<b>0</b> hour	Per IBC / Vulcraft Catalog	
Joist / Beam Spacing	<b>3</b> feet		
Clear Span	<b>2.67</b> feet	(Assumes 4" beam/joist flange)	

### Construction Loads

Construction Live Load	<b>20</b> psf	
Concrete Weight	<b>43</b> psf	
Extra Concrete Weight	<b>6</b> psf	Assume 1/2" extra concrete for ponding. This and the deck self weight should be added in 'Deck Loads' spreadsheet under 'Super DL' in RISA Floor.
Deck Self Weight	<b>1</b> psf	
Construction Dead Load	<b>50</b> psf	
Total Load on Deck	<b>70</b> psf	Construction Dead + Construction Live
Max Const. Clear Span	<b>3.92</b> feet	2 Span Minimum
Total / Allowable Clear Span	<b>0.68</b>	
Allowable Deck Uniform Load	<b>185</b> psf	Deflection = L/240
Total / Allowable Load	<b>0.38</b>	

### Final in-place loads

Live Load	<b>100</b> psf	Offices - 50 psf + 15 psf for partitions.
Partition Loading (if not included in LL)	<b>0</b> psf	Corridors above first floor = 80 psf
Is partition loading based on ASCE 7-16 4.3.2 (movable)?	<b>YES</b> psf	If 'YES', partition loading is included in LL
MEP/finishes	<b>5</b> psf	to included MEP, flooring, ceiling, misc
Superimposed DL	<b>5</b> psf	input in RISA Floor under 'uniform area loads'
Superimposed TL	<b>105</b> psf	LL + partitions + MEP
Allowable Superimposed Load	<b>400</b> psf	Reinforce Slab with 6x6-W2.9xW2.9
Total / Allowable Load	<b>0.26</b>	
Total Final DL	<b>55</b> psf	Load applied to floor beams
Self Weight Beams/Girders/Col	<b>5</b> psf	
Overall Floor DL	<b>60</b> psf	This dead load is total load to columns and footings.
Floor DL for Seismic	<b>70</b> psf	Includes allowance for partitions. If actual partition weight is greater than 10 psf when counted as LL, engineer to manually add the difference.

LOAD TABLES  
ASD - K-SERIES

## ASD

STANDARD LOAD TABLE FOR OPEN WEB STEEL JOISTS, K-SERIES															
Based on a 50 ksi Maximum Yield Strength - Loads Shown In Pounds Per Linear Foot (plf)															
Joist Designation	10K1	12K1	12K3	12K5	14K1	14K3	14K4	14K6	16K2	16K3	16K4	16K5	16K6	16K7	16K9
Depth (in.)	10	12	12	12	14	14	14	14	16	16	16	16	16	16	16
Approx. Wt (lbs./ft.)	5.0	5.0	5.7	7.1	5.2	6.0	6.7	7.7	5.5	6.3	7.0	7.5	8.1	8.6	10.0
Span (ft.)															
10	550														
11	550														
12	550	550	550	550											
13	479	550	550	550											
14	412	500	550	550	550	550	550	550							
15	358	434	543	550	511	550	550	550							
16	313	380	476	550	448	550	550	550	550	550	550	550	550	550	550
17	277	336	420	550	395	495	550	550	512	550	550	550	550	550	550
18	246	299	374	507	352	441	530	550	456	508	550	550	550	550	550
19	221	268	335	454	315	395	475	550	408	455	547	550	550	550	550
20	199	241	302	409	284	356	428	525	368	410	493	550	550	550	550
21	199	241	302	409	284	356	428	525	368	410	493	550	550	550	550
22	199	249	337	434	234	293	353	432	303	337	406	458	498	550	550
23	181	227	308	414	214	268	322	395	277	308	371	418	455	507	550
24	166	208	282	370	196	245	295	362	254	283	340	384	418	465	550
25	154	193	255	334	180	226	272	334	234	260	313	353	384	428	514
26	143	180	233	285	166	209	251	308	216	240	289	326	355	395	474
27	132	166	219	268	154	193	233	285	200	223	268	302	329	366	439
28	121	154	207	255	143	180	216	265	186	207	249	281	306	340	408
29	110	143	190	233	132	166	207	255	175	190	233	265	285	317	380
30	100	132	177	220	121	154	190	233	164	180	216	244	266	296	355
31	97	121	166	207	110	143	180	216	151	168	203	228	249	277	332
32	97	110	143	180	100	132	166	207	142	158	190	214	233	259	311

Live load = 100 psf x 3' = 300 plf < 386 plf OK  
Total load = 160 psf x 3' = 480 plf < 493 plf OK





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Date:

## Simple Span Beam Design

Member Designation: **Storage Mezzanine Beam**

Uniform Load, w:	<b>0.8</b>	klf
Point Load, P:	<b>0</b>	kips
Yield Stress, Fy:	<b>50</b>	ksi
Mod. Of Elasticity, E:	<b>29000</b>	ksi
Beam Length, L:	<b>16.5</b>	ft
Defl. Limit, L/??:	<b>300</b>	
Allowable Deflection:	<b>0.66</b>	inches
End Reactions/Shear:	<b>6.6</b>	kips

\*Point Load Applied At the Center of the Span  
\*Buckling Not Accounted For. Beam Compression Flange Must Be Fully Braced  
\*Self weight is not included. Add it to the uniform load.  
\*Shear Assumed to Not Control

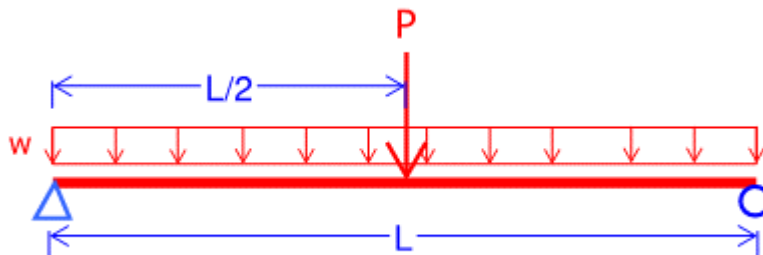
	M (k-ft)	Z or S-reqd (in <sup>3</sup> ):	I-reqd (in <sup>4</sup> ):
Uniform	<b>27.23</b>	<b>10.91</b>	<b>69.71</b>
Point	<b>0.00</b>	<b>0.0000</b>	<b>0.00</b>
Combined	<b>27.23</b>	<b>10.9118</b>	<b>69.71</b>

### Actual Member Selected

Shape:	<b>W8x21</b>	
Beam Loading Direction:	<b>Strong Axis</b>	
Moment of Inertia, I:	<b>75.3</b>	in <sup>4</sup>
Plastic Section Mod., Z:	<b>20.40</b>	in <sup>3</sup>
Elastic Section Mod., S:	<b>18.20</b>	in <sup>3</sup>
Weight, W:	<b>21.0</b>	plf
Area, A:	<b>6.16</b>	in <sup>2</sup>
Depth, d:	<b>8.28</b>	in
Thickness of Web, tw:	<b>0.250</b>	in
Flange Width, bf:	<b>5.27</b>	in
Flange Thickness, tf:	<b>0.400</b>	in

### Unity Check

**0.93**  
**0.53**  
**0.60**





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## Simple Span Beam Design

Member Designation: **Mezzanine Tube**

Uniform Load, w:	<b>0.4</b>	klf
Point Load, P:	<b>0</b>	kips
Yield Stress, Fy:	<b>42</b>	ksi
Mod. Of Elasticity, E:	<b>29000</b>	ksi
Beam Length, L:	<b>10</b>	ft
Defl. Limit, L/??:	<b>240</b>	
Allowable Deflection:	<b>0.50</b>	inches
End Reactions/Shear:	<b>2.0</b>	kips

\*Point Load Applied At the Center of the Span  
\*Buckling Not Accounted For. Beam Compression Flange Must Be Fully Braced  
\*Self weight is not included. Add it to the uniform load.  
\*Shear Assumed to Not Control

	M (k-ft)	Z or S-reqd (in <sup>3</sup> ):	I-reqd (in <sup>4</sup> ):
Uniform	<b>5.00</b>	<b>2.39</b>	<b>6.21</b>
Point	<b>0.00</b>	<b>0.0000</b>	<b>0.00</b>
Combined	<b>5.00</b>	<b>2.3857</b>	<b>6.21</b>

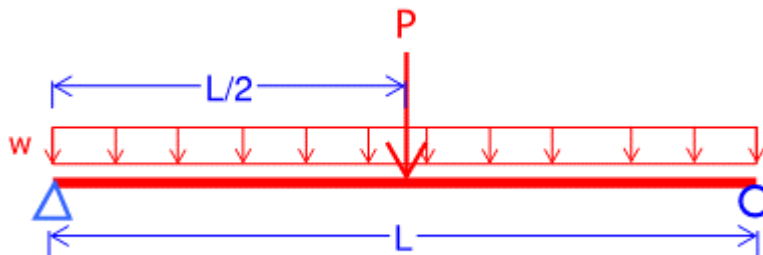
### Actual Member Selected

Shape: **Hss3-1/2x3-1/2x3/8**

Beam Loading Direction: **Strong Axis**

### Unity Check

Moment of Inertia, I:	<b>6.5</b>	in <sup>4</sup>	<b>0.96</b>
Plastic Section Mod., Z:	<b>4.69</b>	in <sup>3</sup>	<b>0.51</b>
Elastic Section Mod., S:	<b>3.71</b>	in <sup>3</sup>	<b>0.64</b>
Weight, W:	<b>14.6</b>	plf	
Area, A:	<b>4.09</b>	in <sup>2</sup>	
Depth, d:	<b>3.50</b>	in	
Thickness of Web, tw:	<b>0.000</b>	in	
Flange Width, bf:	<b>0.00</b>	in	
Flange Thickness, tf:	<b>0.000</b>	in	







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Date:

## Simple Span Beam Design

Member Designation: **Mezzanine Tube @ Stairs**

Uniform Load, w:	<b>1.8</b>	klf
Point Load, P:	<b>0</b>	kips
Yield Stress, Fy:	<b>42</b>	ksi
Mod. Of Elasticity, E:	<b>29000</b>	ksi
Beam Length, L:	<b>5.5</b>	ft
Defl. Limit, L/??:	<b>240</b>	
Allowable Deflection:	<b>0.28</b>	inches
End Reactions/Shear:	<b>5.0</b>	kips

\*Point Load Applied At the Center of the Span  
\*Buckling Not Accounted For. Beam Compression Flange Must Be Fully Braced  
\*Self weight is not included. Add it to the uniform load.  
\*Shear Assumed to Not Control

	M (k-ft)	Z or S-reqd (in <sup>3</sup> ):	I-reqd (in <sup>4</sup> ):
Uniform	<b>6.81</b>	<b>3.25</b>	<b>4.65</b>
Point	<b>0.00</b>	<b>0.0000</b>	<b>0.00</b>
Combined	<b>6.81</b>	<b>3.2476</b>	<b>4.65</b>

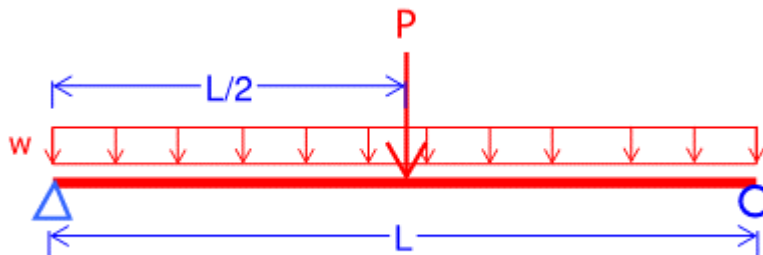
### Actual Member Selected

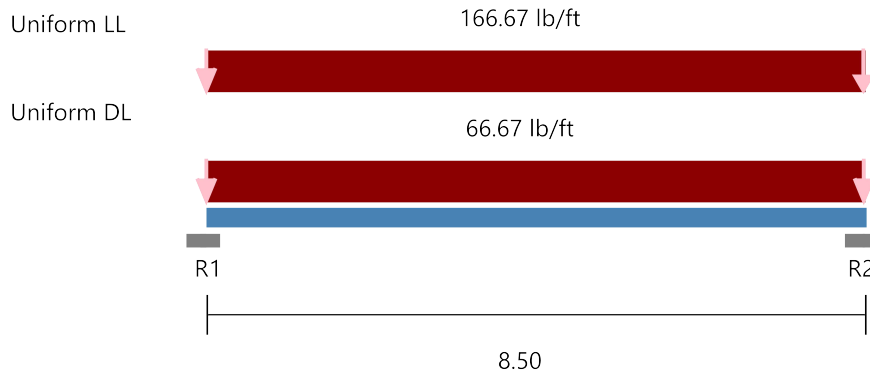
Shape: **HSS3-1/2x3-1/2x3/8**

Beam Loading Direction: **Strong Axis**

### Unity Check

Moment of Inertia, I:	<b>6.5</b>	in <sup>4</sup>	<b>0.72</b>
Plastic Section Mod., Z:	<b>4.69</b>	in <sup>3</sup>	<b>0.69</b>
Elastic Section Mod., S:	<b>3.71</b>	in <sup>3</sup>	<b>0.88</b>
Weight, W:	<b>14.6</b>	plf	
Area, A:	<b>4.09</b>	in <sup>2</sup>	
Depth, d:	<b>3.50</b>	in	
Thickness of Web, tw:	<b>0.000</b>	in	
Flange Width, bf:	<b>0.00</b>	in	
Flange Thickness, tf:	<b>0.000</b>	in	





**Section :** 600S200-54 (50 ksi) @ 16 in" o.c. Single C Stud (punched)

**Maxo =** 2532.9 ft-lb **Va =** 2822.9 lb **I =** 3.319 in<sup>4</sup>

**Deflection Limits:** Total Load - 240 Live Load - 360

**Load Comb:**

1. DL + LL All spans	4. LL All spans
2. DL + LL Even spans	5. LL Even spans
3. DL + LL Odd spans	6. LL Odd spans

#### Joist Flexural and Deflection

	Mmax (ft-lb)	K-phi (lb-in/in)	Lm (in)	Ma-dist (ft-lb)	Mmax/ Ma min	Load Comb.	TL Defl	Load Comb.	LL Defl	Load Comb.
Span	2107	0.0	102.0	2281.9	0.923	1	L/364	1	L/510	4

#### Joist Bending and Web Crippling

Support	Load (lb)	Load Comb.	Bearing (in)	Pa (lb)	Pn (lb)	Max Intr.	Load Comb.	Stiffeners Required
R1	991.7	1	1.00	598.9	1048.1	0.86	1	YES
R2	991.7	1	1.00	598.9	1048.1	0.86	1	YES

#### Joist Bending and Shear

Support	Vmax (lb)	Load Comb.	Va Factor	V/Va	M/Ma	Intr. Unstiffened	Load Comb.	Intr. Stiffened	Load Comb.
R1	991.7	1	1.000	0.35	0.00	0.35	1	N/A	N/A
R2	991.7	1	1.000	0.35	0.00	0.35	1	N/A	N/A

#### Joist Reaction and Connections

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie Connector	Connector Interaction	Anchor Interaction
R1	0.0	991.7	SSC4.25 (4#10) & (3) #10 to A36 steel (Joist Bearing on Support)	0.00 %	0.00 %
R2	0.0	991.7	SSC4.25 (4#10) & (3) #10 to A36 steel (Joist Bearing on Support)	0.00 %	0.00 %

\* Reference catalog for connector and anchor requirement notes as well as screw placement requirements