

CKR ENGINEERS

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STRUCTURAL CALCULATIONS

Mo'Bettahs - Lee's Summit
NW Chipman Rd & NW Ward Rd
Lee's Summit, MO

Project: 23150

April 10, 2023



Scope of Work

- Gravity analysis
- Lateral analysis
- Structural design to resist gravity and lateral forces
- Calculations are valid only at the above address
- Sign drawings attached for reference only
- Design of sign cabinets not included

Design Summary

Project: Mo'Bettahs - Lee's Summit
Job #: 23150
Date: 4/10/2023

Sign Pole

A standard **6** in Schedule 40 pipe is adequate for strength and deflection.

Sign Foundation

A **3** ft diameter x **5** ft deep unreinforced concrete footing under the sign is adequate.

Design Criteria:

2018 International Building Code

Project: Mo'Bettahs - Lee's Summit
Address: NW Chipman Rd & NW Ward Rd
City, State: Lee's Summit, MO
Job #: 23150
Date: 4/10/2023

Design Loads per ASCE/SEI 7-16

*Minimum Design Loads for Buildings
and Other Structures*

| | | | |
|------------------|------------------|---------------------------------------|--|
| General | (Chapter 1) | Risk Category = II Table 1.5-1 | |
| Dead Load | (Chapter 3) | ASD Level | |
| | Sign Weight | 5 | psf |
| Wind Load | (Chapters 26-31) | Strength Level | |
| | | V = 109 mph | Figure 26.5-1, or value from https://hazards.atcouncil.org |
| | | V _{asd} = 84 mph | IBC Section 1609.3.1 |
| | | Exposure: B | Section 26.7 |

Sign Pole & Foundation Design

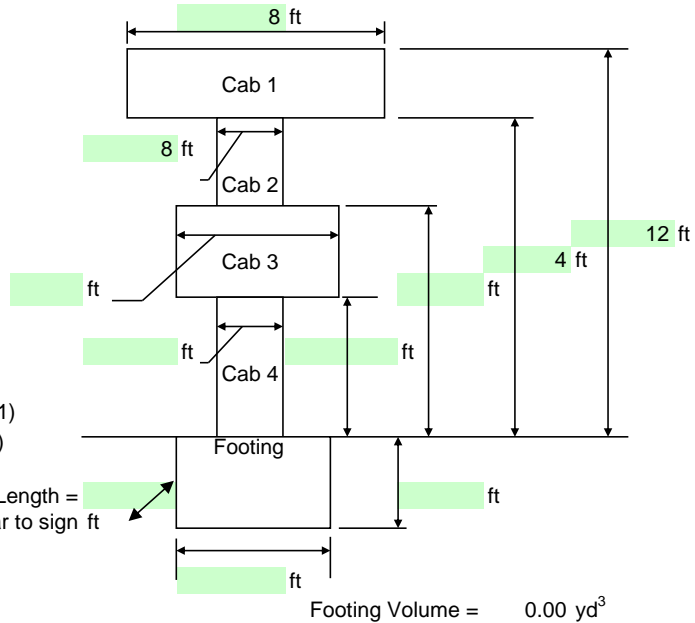
Project: Mo'Bettahs - Lee's Summit
 Location: Lee's Summit, MO
 Job #: 23150

ASCE 7-16 Wind Chapter 26

V = 109 Mph
 Elevation = 1000 (ft)
 $K_d = 0.85$ Table 26.6-1
 Exp. B Section 26.7.3
 Sign Top Height = 12 (ft)
 $K_z = 0.57$ Table 27.3-1
 $K_{zt} = 1$ Figure 26.8-1
 $G = 0.85$ Section 26.9.1
 $K_e = 0.96$ Section 26.10
 $q_z = 14.3$ (psf) - LRFD - Eqn. (26.10-1)
 $q_z = 8.6$ (psf) - ASD - Eqn. (26.10-1)

Soil Passive Pres. = 150 pcf
 Pole $F_y = 35$ ksi
 Pole E = 29000 ksi
 Pole = PIPE6STD
 Only round sections are currently supported

Footing Length =
 Perpendicular to sign ft



Footing Volume = 0.00 yd³

Sign Forces (ASD)

| Cabinet | B (ft) | S (ft) | h (ft) | B/s | s/h | Ybar (ft) | Area (ft ²) | C_f Fig. 29.4-1 | Force (lbf) | Pole Moment (k*ft) | Ftg Moment (k*ft) |
|---------|-----------|-----------|-----------|------|------|--------------|----------------------------|----------------------|----------------|--------------------------|-------------------------|
| 1 | 8 | 8 | 12 | 1.00 | 0.67 | 8 | 64 | 1.65 | 772 | 6.2 | 6.2 |
| 2 | 8 | 4 | 4 | 2.00 | 1.00 | 2.2 | 32 | 1.8 | 421 | 0.9 | 0.9 |
| 3 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | | 0 | 0.0 | 0.0 |
| 4 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | | 0 | 0.0 | 0.0 |
| | | | | | | | | | 1192.7 | 7.1 | 7.1 |

Pole Analysis (ASD)

Assume Pole extends up to bottom of Cab 1

| Cabinet | Cab WT (psf) | Cab WT (lbf) | Pole Section Properties | | | Column Capacity | | |
|---------|-----------------|-----------------|-------------------------|----------------------|--|-------------------------|------------|--|
| 1 | 10.0 | 640 | A = | 5.58 in ² | | KL/r = | 134.40 *** | |
| 2 | 10.0 | 320 | I = | 28.1 in ⁴ | | $F_e =$ | 15.85 ksi | |
| 3 | | 0 | S = | 8.5 in ³ | | Q = | 1 | |
| 4 | | 0 | Z = | 11.3 in ³ | | $F_{cr} =$ | 13.89 ksi | |
| | | 960 | r = | 2.25 in | | $\Omega_b = \Omega_c =$ | 1.67 | |
| | | | D/t = | 23.7 | | $\Omega_c * P_n =$ | 46.40 kips | |
| | | | K = | 2.1 | | $\Omega_b * M_n =$ | 19.74 k*ft | |
| | | | L = | 12 ft | | Unity = | 0.370 | |
| | | | E/ $F_y =$ | 828.57 | | Deflection at Top = | 0.51 in | |
| | | | | | | 0.025 * L = | 3.6 in | |

*** KL/r > 200 is permitted, but not recommended.