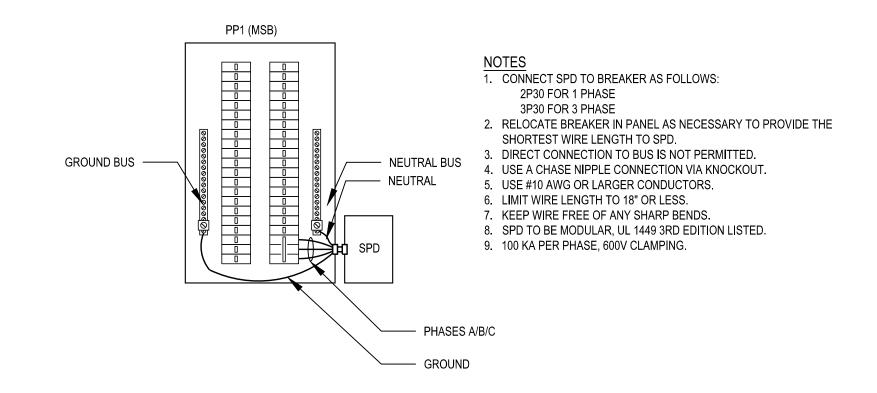
VOLTAGE DROP CALCULATION FROM TRANSFORMER TO MAIN DISCONNECT:	VOLTAGE DROP CALCULATION FROM MAIN DISCONNECT TO PP1:	VOLTAGE DROP CALCULATION TO FARTHEST BRANCH CIRCUIT: PP3-35,37
SOURCE = AC, 3 Φ VOLTAGE = 208.0 COND. MATERIAL = PVC POWER FACTOR = 0.90 COND. TEMP. = 75°C CONDUCTOR METAL = COPPER COND. PER PHASE = 1 WIRE SIZE = 600 MCM LOAD = 86.8 AMPS LENGTH (1-WAY) = 80.0 FEET RESULT: THE VOLTAGE DROP = 0.22%, 0.45V L-L.	SOURCE = AC, 3 Φ VOLTAGE = 208.0 COND. MATERIAL = STEEL POWER FACTOR = 0.90 COND. TEMP. = 75°C CONDUCTOR METAL = COPPER COND. PER PHASE = 1 WIRE SIZE = 600 MCM LOAD = 86.8 AMPS LENGTH (1-WAY) = 25.0 FEET RESULT: THE VOLTAGE DROP = 0.08%, 0.16V L-L.	SOURCE = AC, 1 Φ VOLTAGE = 208.0 COND. MATERIAL = PVC POWER FACTOR = 0.90 COND. TEMP. = 75°C CONDUCTOR METAL = COPPER COND. PER PHASE = 2 WIRE SIZE = #10 LOAD = 0.968 KVA LENGTH (1-WAY) = 160.0 FEET RESULT: THE VOLTAGE DROP = 0.39%, 0.82V.

VOLTAGE DROP CALCULATION TO PP1 = 0.22%+0.08% = 0.30%

VOLTAGE DROP CALCULATION TO FARTHEST BRANCH CIRCUIT: 0.39%

TOTAL PERCENT VOLTAGE DROP = 0.30% + 0.39% = 0.69%

FAULT CURRENT CALCULATION FOR MAIN DISCONNECT AMPS SHORT CIRCUIT FROM ELECTRICAL UTILITIES = 43,237 A RMS WIRE IS: NUMBER OF CONDUCTORS PER PHASE: 1 CONDUCTOR LENGTH 'L': 80' CONDUCTOR C VALUE: 22,965 (#CONDUCTORS PER PHASE x C = 22,965) $f = \frac{1,73 \times L \times I}{C \times E_{L-L}} = \frac{1,73 \times 80 \times 43,237}{22,965 \times 208} = 1.253$ $M = \frac{1}{1+f} = \frac{1}{1+1,253} = 0.444$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTILITY x M} = 43,237 \times 0.444 = 19,197 \text{ A RMS}$ $I_{SCA}^{I} = \text{AVAILABLE FROM UTIL$







I = AVAILABLE SHORT CURRENT IN AMPERES AT BEGINNING OF CIRCUIT

4 ELECTRICAL SERVICE SURGE PROTECTION

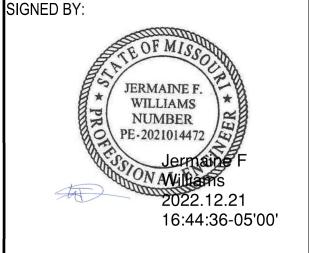
N.T.S.

FUTURE PV SYSTEM EQUIPMENT (SHOWN FOR REFERENCE ONLY FOR SPACE PLANNING AND STRUCTURAL DESIGN) TRANS- AC --INVERTER---FUTURE PV SYSTEM RIGID CONDUIT (TYP) ----FUTURE PV SYSTEM DISCONNECT SWITCH IF REQUIRED — ROOF FUTURE PV SYSTEM PERFORMANCE METER -FUTURE PV SYSTEM "SOLAR-READY" (1)4" C. W/ FUSED DISCONNECT ----(4)///0000 00 LABEL AT EACH PANEL ----- 1 SET 2" C 4 #1/0 CU _____ 1 #6 CU GRD BUILDING MANAGEMENT SYSTEM (BMS) CONTROLS METER SOCKET PP1 PP2 PAD MOUNTED UTILITY TRANSFORMER SPD 208/120V, 3PH, 4W GRADE ELECTRICAL PANEL AREA DATA ROOM \ (4) #600 CU, (1) #3 CU GND FUTURE PV SYSTEM RIGID CONDUIT (TYP) — 400A FUSED MAIN (1)4" C. W/ DISCONNECT SWITCH (4)#600 CU CLASS J 22,000 AIC 43,237 SCA PRIMARY CONDUCTORS BUILDING STELL AND TERMINATION AT TRANSFORMER BY UTILITY COMPANY -- SYSTEMS GROUND BAR CONCRETE-ENCASED ELECTRODE 20' OR GREATER, ELECTRODE SHALL BE ENCASED BY AT LEAST 2 INCHES OF CONCRETE AND SHALL BE LOCATED HORIZONTALLY WITHIN THAT PORTION OF A CONCRETE FOUNDATION OR FOOTING THAT IS IN DIRECT CONTACT WITH THE EARTH OR WITHIN VERTICAL FOUNDATIONS OR STRUCTURAL COMPONENTS OR MEMBERS THAT ARE IN DIRECT CONTACT WITH **EXOTHERMIC** THE EARTH. CONNECTION (TYP.) -LINE TYPE LEGEND FUTURE -----GROUND RODS (2) 3/4" X 10' COPPER CLAD 5' OUTSIDE BUILDING 10' CENTER TO

1 ELECTRICAL RISER DIAGRAM
E-6 N.T.S.

BI Consulting
ENVIRO BUSINESS, INC.
21 B Street | Burlington, MA 01803
Fel: (781) 273-2500 | www.ebiconsulting.com

ш



R ROAD MO 64081

908 NW PRYOR LEE'S SUMMIT, N

PRYOR ROAD & OWENSTEIN DRIVE

	EBI JOB #4121000090		
	ISSUE	DATE	DESCRIPTION
	0	03/02/2022	PERMIT
	1	04/11/2022	PERMIT REVISIONS
	2	8/18/2022	ASI #1 - CONSTRUCTION SET
	3	10/10/2022	PARAPET RFI #12
	4	12/21/2022	STORM SWITCH REMOVAL



PRYOR & LOWENSTEIN
PROTOTYPE VERSION 20.4

CONTENTS

ONE-LINE DIAGRAM & ELECTRICAL SYSTEM DETAILS

02/04/2022 SHEET

F-7