

STRUCTURAL DESIGN CALCULATIONS

Shake Shack, **Sign DTC.1 Qty. 2**

2051 NW Lowenstein Drive

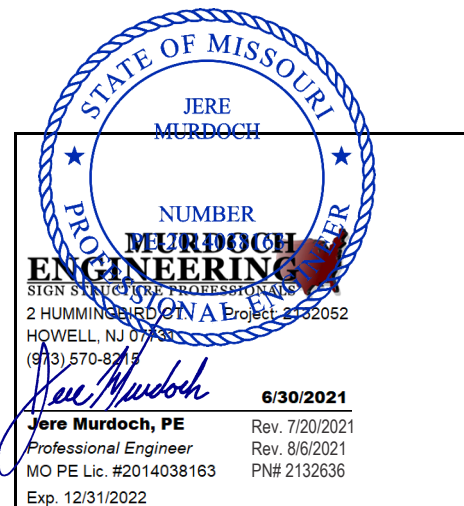
Lee's Summit, MO 64081

DESIGN SPECIFICATIONS			
IBC	2018	with	MO amendments
ASCE	7-16	Minimum Design Loads for Buildings & Other Structures	
ACI	318-14	Building Code Requirements for Structural Concrete	
ANSI/AISC	360-16	Specification for Structural Steel Buildings	
DESIGN LOADS			
Wind	V =	115	mph
Exposure	C		
Risk Cat.	II		
Grnd. Snow	Pg =	20	psf

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WIND LOADING & STEEL CALCULATIONS

Ultimate Wind Speed=	115	IBC-2018
Normal Wind Speed=	89.08	IBC-2018 Nominal
Exposure=	C	open terrain, scattered buildings <30Ft.
Cf=	1.70	ASCE 7-10 Force Coefficient
G=	0.85	Gust Factor
Kh=	0.85	Velocity pressure Coefficient @ height
Kzt=	1	Topographic factor
I=	1	Importance factor
Kd=	0.85	Wind directionality factor

STEEL COLUMN DESIGN

Areas Subject to Wind Forces

Description	(cF)	Height (ft)	Width (ft)	Area (sqft)	Centroid (ft)	Wind (psf)
Roof 21psf*1.2 = 25.2> (20psf sL)	1.70	6.00	9.00	54.00	10.0	25.2
Pole Cladding	1.67	11.00	1.76	19.36	5.5	21

Calculation of Design Forces at Critical Heights

y (ft)	M (#)	V (#)		y (ft)	M (#)	V (#)	M (#) Per/Column	V (#) Per/Column
@ grade	15,844	1,767		17.67			15,844	1,767
9.00	1,361	1,361		17.67			1,021	1,021
17.67				17.67				

Column Support Design Table

# of Cols	Column Type (P, TS)	Column Size	Length (ft)	Start Elev (ft)	End Elev (ft)	Sleeve Depth (in)	S act (in^3)	fb (ksi)
1	TS	5XX.25	9.00		9.00	N/A	6.41	29.7
2	TS	2XX.125	9.00	8.67	17.67	4.0	0.49	16.8

TS = Steel Tube 6x6x3/8" > 5"x5"x1/4" Min. = OK

TS = Steel Tube (Canopy Roof) = Proposed 3.5"x3.5" x 3/16" > 2"x2" x 1/8" Min. = OK

FOOTING CALCULATIONS

# Footings=	1		Moment/Per/Footing, M=	15844.08	lb-ft
Pass lat soil res, q=	150	psf	Composite Centroid, h=	8.81	ft
			Equiv Concentrated Load, P= M/h=	1,798	lb

Rectangular Pier

Width, W=	4.0	ft, parallel to sign face
Length, L=	6.0	ft, perpendicular to sign face
Depth, D= (A/2)(1+ SQR(1 + (4.36h)/A))=	4.4	ft
	3.87	Yards Conc
S1= (2)(q)(D/3)=	429	psf
b= Sqrt(W^2 + L^2)=	7.2	ft
A= (2.34)(P) / (S1)(b)=	1.4	

Calc Depth

Augured (round footing)

Diameter, b=	3.00	ft, round augured hole
Depth, D= (A/2)(1+ SQR(1 + (4.36h)/A))=	6.01	ft
	1.57	Yard Conc
S1= (q)(2)(D/3)=	607	psf
A= (2.34 P) / (S1)(b)=	2.31	

Calc Depth

Foundation Bearing Check

Allowable Soil Bearing Pressure=	1,500	psf, IBC 2018
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Square			Round		
Sign Wt=	1,166	lb	Sign Wt=	1,166	lb
Base Wt=	15,693	lb	Base Wt=	6,368	lb
Area=	24.0	sq ft	Area=	7.1	sq ft
q max=	702	psf, soil	q max=	1,066	psf, soil
OK, with depth increase			OK, with depth increase		

BASEPLATE CALCULATIONS

Plate Design

# of Base Plates=	1	
Maximum Column Dimension, OD=	6.00	in, perpendicular to sign face
Number of Bolts, n=	2	per line front and back
Compressive Strength of Concrete, f_c =	3,000	psi at 28 days
Moment / per/Base Plate, M=	15,844	lb-ft
Bolt Line Spacing, L=	9.04	in, from front to back
Base Plate Dimensions:	N= 12.50	in B= 12.50 in
Tension per Bolt Line, T=	21,032	lb, = M/L (simple moment couple)
Maximum Moment on the Plate, Mpl=	31,969	lb-in, = (T)((L-OD)/2)
Plate Thickness w/o Gussets, t=	0.94	in, = $\sqrt{(6M)/(0.75F_y(4/3) B_{eff})}$
Plate Thickness w/ Gussets, t=	0.75	in, = $\sqrt{(6M)/(0.75F_y(4/3) B_{eff}) * 0.8}$
Alum. PL Thickness w/o Gussets, t=	1.10	in, = $\sqrt{(6M)/(0.52F_y(4/3) B_{eff})}$
Alum. PL Thickness w/ Gussets, t=	0.88	

Anchor Bolt Design

(using A36 threaded rod with embedded end nut)

Tension per Anchor, Ta=	10,516	lb, = T/n
Req. Gross Area of Anchor Bolts, Ag=	0.41	sq in, = $Ta/0.33F_u$ (1/3 inc)
Min. Diameter of Anchor Bolts, D=	0.73	in
Actual Bolt Diameter to be Used=	1.375	in
Req Proj Concrete Surface Area, Ap=	83	sq in, = $Ta/(2 \sqrt{f_c})$ (1/3 inc)
Req Embedded Bolt Length, L=	27.50	in, = $\sqrt{Ap/3.14}$, min 20D
Min. Spacing to Edge of Concrete=	27.50	in
Min. Spacing Between Bolts in a Line, s=	13.75	in, = 2L
Actual Spacing Between Bolts in a Line, s=	9.04	in
# of Overlaps=	1	
Revised Ap Based on Overlap=	1380.60	in ²
Actual Shear Capacity of Concrete Cone=	201,145	lb. (1/3 inc)

Shear Engineering OK

Shear stress per bolt, f_v =	298	psi, = V_a/A_b
Allowed Tension Stress with Shear, F_t =	25,456	psi, = $0.43F_u - 1.8f_v$, max $0.33F_u$ (1/3 inc)
Actual Tension Stress per Bolt, f_t =	7,082	psi, = T_a/A_b

Tension Engineering OK

Weld Design

(check connection of base column to plate, pipe and square tube only)

Shape of Column=	TS	(P=round, TS=square)
1/32" Less TS or P Thk. Fillet Weld Leg Size, a=	0.344	in, Max.
Section Modulus of Weld, S_w =	16.59	in ³ , = $1.34(b^2)(a)$
Actual Weld Stress, f_w =	11,457	psi, = M/S_w

Weld Engineering OK, <0.3Ft of E7018