



**KAW
VALLEY**
ENGINEERING

**MASTER DRAINAGE PLAN
LEE'S SUMMIT HIGH SCHOOL
ADDITIONS & RENOVATIONS & ATHLETICS
400 SE BLUE PARKWAY
LEE'S SUMMIT, MISSOURI 64063
SECTION 8, TOWNSHIP 47 N, RANGE 31 W**

Prepared for:

LEE SUMMIT SCHOOL DISTRICT
502 SE Transport Drive
Lee's Summit, Missouri 64081

Prepared by:

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October 9, 2020

Kaw Valley Engineering Project No. **C20D0496**

MASTER DRAINAGE PLAN

LEE’S SUMMIT HIGH SCHOOL ADDITIONS & RENOVATIONS

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Project No. C20D0496

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EXHIBITS

Exhibit A – FEMA Firmette, Existing Conditions & Soils Map

Exhibit B – Proposed Grading Plan

Exhibit C – Drainage Area Map & Calculations, Storm Sewer Plan and Profiles,
BMP Plan, EDDB Calculations

Exhibit D – PondPack Analysis

REVISIONS

Revision 0 – October 9, 2020

Initial Issue

INTRODUCTION

The Lee's Summit School District is proposing extensive building additions and ancillary improvements to Lee's Summit High School (LSHS) at 400 SE Blue Parkway in Lee's Summit, Missouri. With authorization from the Lee Summit School District, Inc., Kaw Valley Engineering, Inc. has completed a study of the existing and proposed storm drainage conditions associated with the project.

PURPOSE OF STUDY

The purpose of this study is to analyze the changes in storm water drainage conditions and flows associated with the proposed project. Furthermore, the study will show that the proposed drainage system for this project will comply with the adopted City of Lee's Summit, Missouri storm water guidelines.

CITY STORMWATER MANAGEMENT REQUIREMENTS

Based upon the Storm Water Management Guidelines as described in the KC Metropolitan Chapter of APWA as adopted by the City of Lee's Summit, the redevelopment on this property would be subject to the following requirements:

- The post development storm water peak release rates and volumes shall be equal to or less than the existing storm water peak release rates as defined under Comprehensive Protection strategy outlined in APWA Section 5601.5 A4.a as modified in the City of Lee's Summit Design and Construction Manual.
- Volumetric and/or extended detention control of the 90% mean annual event (Water Quality Event or 1.37") shall be provided as well.

EXISTING CONDITIONS

The project site is located on the north side of the Blue Parkway, west of Missouri Highway 291. The address is 400 SE Blue Parkway as located on the general vicinity map.



The Lee's Summit High School property consists of approximately 45.53 acres. However, a project area of 16.31 acres has been defined since part of the site will remain undisturbed and is not part of the scope of this project. The project site currently consists of a school building, concrete hardscape, parking areas and driveways, athletics spaces, and green space. Table 1 details the existing land cover of the project area. Storm water runoff from the existing project area generally drains by overland flow and storm sewer to the northwest corner of the property and enters an open channel that discharges into an unnamed tributary upstream of Prairie Lee Lake. This site is in Zone "X" on the revised flood insurance rate map for Lee's Summit (community panel No. 29095C0436G & 29095C0438G) dated January 20, 2017. A copy of the Flood Panel (Firmette) is included in Exhibit A for reference. The existing site topography (demolition plan) is also included in Exhibit A.

Table 1 - Existing Land Cover in the Project Area							
Description	Area (Sq. Ft)	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
Existing	710,300	16.31	522,850	12.00	74%	0.74	92

A soils map has been provided for the site. The soils were identified according to the soil survey maps in the *NRCS Web Soil Survey*. The map indicates that the following soils exist on the site and included the following engineering characteristics and soil and water features information.

- **10082- Arisburg-Urban Land Complex, 1 to 5 percent slopes.** The surface water runoff class is medium. The water table is at a depth of about 18 to 36 inches. This somewhat poorly drained soil is not hydric and is classed in Hydrologic Group C. No seasonal water table is present.

- **10180- Udarents-Urban Land – Sampsel Complex, 2 to 5 percent slopes.** The surface water runoff class is very high. The water table is at a depth is more than 80 inches. This somewhat poorly drained soil is not hydric and is classed in Hydrologic Group C and C/D.

DESCRIPTION OF PROPOSED IMPROVEMENTS

As stated above, the proposed improvements at Lee’s Summit High School will include a building addition, improvements to pedestrian access and flow and stadium, reconstruction of the building services area and, extension of the emergency access drive and expansion of the existing parking lots to offset the loss in existing parking spaces. The proposed improvements will encompass 16.31 acres of land which includes the disturbance and development within the Prairie Lee Lake watershed. To mitigate the increase in runoff, an extended dry/detention basin will be constructed in the northwest corner of the site to collect and treat runoff from portions of the largest parking expansion area. The proposed improvements will preserve the general drainage patterns on the Campus. Storm Sewers will be extended and resized to address onsite capacity issues. Table 2 details the proposed land cover of the property within the project area. See Exhibit B Proposed Grading Plan.

Table 2 - Proposed Land Cover in the Project Area							
Description	Area (Sq. Ft)	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
Proposed Undetained	676,500	15.53	504,850	11.59	75%	0.75	92
Proposed Detained (STF)	33,800	0.78	30,250	0.69	89%	0.84	95
Proposed	710,300	16.31	535,100	12.28	75%	0.75	92

DRAINAGE ANALYSIS

The storm runoff for the project site was analyzed for the WQv, 2-year, 10-year, and 100-year events for the existing and proposed conditions.

The Curve Number (CN) for the drainage areas to be used in the calculations are identified in Tables 1 and 2. This number was based upon the percentage of impervious and pervious surfaces as specified in section 5600 of APWA. It was assumed that pervious surfaces CN value of 74 and impervious surfaces have a CN value of 98.

Time of concentration (Tc) for the proposed conditions was calculated using methods outlined in APWA 5600. The time of concentration (Tc) was calculated for each project area for the existing and proposed conditions using the Urban Hydrology for Small Watersheds TR-55 manual.

Runoff for storm sewer design was calculated using the Rational Method as described in The KC Metropolitan Chapter of APWA Section 5600. Runoff for detention and routing was calculated using the SCS method as described in TR-55.

STORM SEWER ANALYSIS

The existing private storm sewer system will be modified, and new structures and pipes will be installed as part of this project. During review of the existing infrastructure, it was noted that contributions from the Lee's Summit High School exceeded the capacity of the existing public storm sewer on Browning Street for a 10-year event. As part of this project, a substantial portion of the south half of the Lee's Summit High School Campus will be redirected via a new storm extension between the existing school and tennis courts. The proposed storm sewer system was designed using the Rational Method described in the KC Metropolitan Chapter of APWA Section 5600. Refer to Exhibit C for the drainage area map, storm sewer calculations and storm sewer plan and profiles.

RELEASE RATE REQUIREMENTS

The Kansas City Metropolitan Chapter of APWA stipulates that the post development release rate of runoff shall be less than the existing condition. As indicated in Tables 1 and 2 of the report, the amount of impervious surfaces within the project limits will increase. Table 3 shows the comparison of the existing and proposed release rates without mitigation. The proposed condition was subdivided to document the unmitigated release rates in both the detained (proposed as part of this project) and undetained drainage areas.

Table 3 - Comparative Analysis of Project Area								
Description	Area (ac)	Curve Number	Tc (min)	WQv Year Storm		2 Year Storm	10 Year Storm	100 Year Storm
				Q (cfs)	Volume (ac-ft)	Q (cfs)	Q (cfs)	Q (cfs)
Existing	16.31	91.7	10.10	15.4	0.939	55.9	93.9	133.2
<i>Proposed Undetained</i>	<i>15.53</i>	<i>91.9</i>	<i>10.10</i>	<i>1.1</i>	<i>0.058</i>	<i>3.3</i>	<i>5.3</i>	<i>7.5</i>
<i>Proposed Detained (STF)</i>	<i>0.78</i>	<i>95.5</i>	<i>5.00</i>	<i>14.7</i>	<i>0.894</i>	<i>53.3</i>	<i>89.4</i>	<i>126.8</i>
Proposed	16.31	92.1		15.8	1.0	56.6	94.7	134.3
Difference				0.4	0.013	0.7	0.8	1.1

To account for this increase of storm water runoff associated with the proposed project, Kaw Valley Engineering recommends that the Lee Summit School District constructs an on-site extended dry detention basin to reduce the peak discharge outflow from the site for all storm events analyzed and reduce volumetric increases for the WQv event.

DETENTION BASIN & ANALYSIS RESULTS

The extended dry detention basin (STF) will be located in the northwest corner of the site and is designed in accordance with APWA 5600 standards. The detention basin will treat runoff from an adjacent parking lot. The detention basin will consist of an above ground detention pond and underground chamber system. The surface pond will have a bottom elevation of 1010.0, top

elevation of 1012.0, and maximum side slopes of 3:1 for ease of maintenance. The basin floor will be constructed with a highly permeable Loamy Sand and rip rap floor that will infiltrate surface water into an underground gravel bed and chamber system. The chamber system will be equipped with inspection ports, an overflow drain and capped underdrain routed to the primary outlet structure. The underdrain will be equipped with a secured cleanout cap and 1" orifice. The cap can be removed for underdrain maintenance and inspection. Table 4 provides the drainage area and impervious coverage of the runoff entering the detention basin (STF).

Table 4 – Extended Dry Detention Basin (STF)						
Description	Area (ac)	Impervious Area (SF)	Impervious Area (ac)	% Impervious	Rational 'C'	CN
EEDB (STF)	0.78	30,250	0.69	89%	0.83	95

The detention basin will receive stormwater from overland flow via a flume from the adjacent parking to the south. The outflow will be regulated by an 8" drain tied to the chamber system beneath the basin floor. This 8" drain is designed to limit the discharge from the WQv (1-year event) storm through the basin underdrain system. The gravel bed and chamber system allow for the storage of runoff for extended periods of time. Both the underdrain and 8" chamber connector drain will connect to a 4' by 4' yard inlet with a 6" x 4' opening on the west face of the box. This outlet is designed to detain the 2-year, 10-year and 100-year events. The structure will be located on the east side of the basin and will also serve as the emergency outlet structure. The flow from the outlet structure will be conveyed through a 15-inch HDPE storm pipe and discharge to the east into an existing drainage channel. If consecutive 100-year storm events are realized, the detention basin berm will be overtopped on the north and east sides of pond and runoff will drain by overland flow into the existing channel on the north side of the Lee's Summit High School property. Rip rap will be installed at the discharge point of the 15" HDPE storm line. The rip rap apron is to be at least 20' long and consist of 12" to 15" (D50) stone based on the pipe size and discharge velocity. The Drainage Area Map, BMP Plan, and EEDB Calculations are included in Exhibit C of the report.

As documented in Table 5 below, the proposed extended dry detention basin will effectively limit the post construction runoff to the less than the existing rates for the WQv, 2-year, 10-year and 100-year storm events. The requisite increase in volume associated with the WQv is also addressed. The Pondpack Analysis for the existing and proposed conditions is included in Exhibit D of the report.

Table 5 - Proposed Condition with Infiltration Basin Routing Summary

1-year (WQv) Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow from Project Area
Inflow (cfs)	1.1	14.7	Proposed Inflow (cfs)	1.1
Outflow (cfs)	0.04	14.7	Proposed Outflow (cfs)*	14.7
Storage (ac-ft)	0.031		Existing Flow (cfs)	15.8
Max WS Elev.	1077.88		Difference in Flow (cfs)	-1.1
Calculated Volume Reduction				0.020
Prescribed Volume Reduction				0.013
2-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow from Project Area
Inflow (cfs)	3.3	53.3	Proposed Inflow (cfs)	56.6
Outflow (cfs)	2.7	53.3	Proposed Outflow (cfs)*	55.9
Storage (ac-ft)	0.047		Existing Flow (cfs)	55.9
Max WS Elev.	1011.03		Difference in Flow (cfs)	0.0
10-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow from Project Area
Inflow (cfs)	5.3	89.4	Proposed Inflow (cfs)	94.7
Outflow (cfs)	3.5	89.4	Proposed Outflow (cfs)*	92.9
Storage (ac-ft)	0.07		Existing Flow (cfs)	93.9
Max WS Elev.	1011.62		Difference in Flow (cfs)	-1.0
100-year Design Storm	Proposed Detained STF	Proposed Undetained	Comparative Analysis	Peak Outflow From Project Area
Inflow (cfs)	7.5	126.8	Proposed Inflow (cfs)	134.3
Outflow (cfs)	6.4	126.8	Proposed Outflow (cfs)*	133.2
Storage (ac-ft)	0.082		Existing Flow (cfs)	133.2
Max WS Elev.	1011.91		Difference in Flow (cfs)	0.0

*Note: Summation of Hydrographs vary from Peak Outflow due to offsetting peaks.

Based on these findings, it is the opinion of Kaw Valley Engineering, Inc. that the City of Lee's Summit, Missouri design requirements are satisfied for the planned improvements associated with the LSHS Additions and Renovations and LSHS Athletics projects.

Respectfully submitted,
Kaw Valley Engineering, Inc.

David D. Wood, P.E.
 Project Manager



Exhibit A
FEMA Firmette
Existing Conditions Plan
Soils Map

National Flood Hazard Layer FIRMMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone X
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped



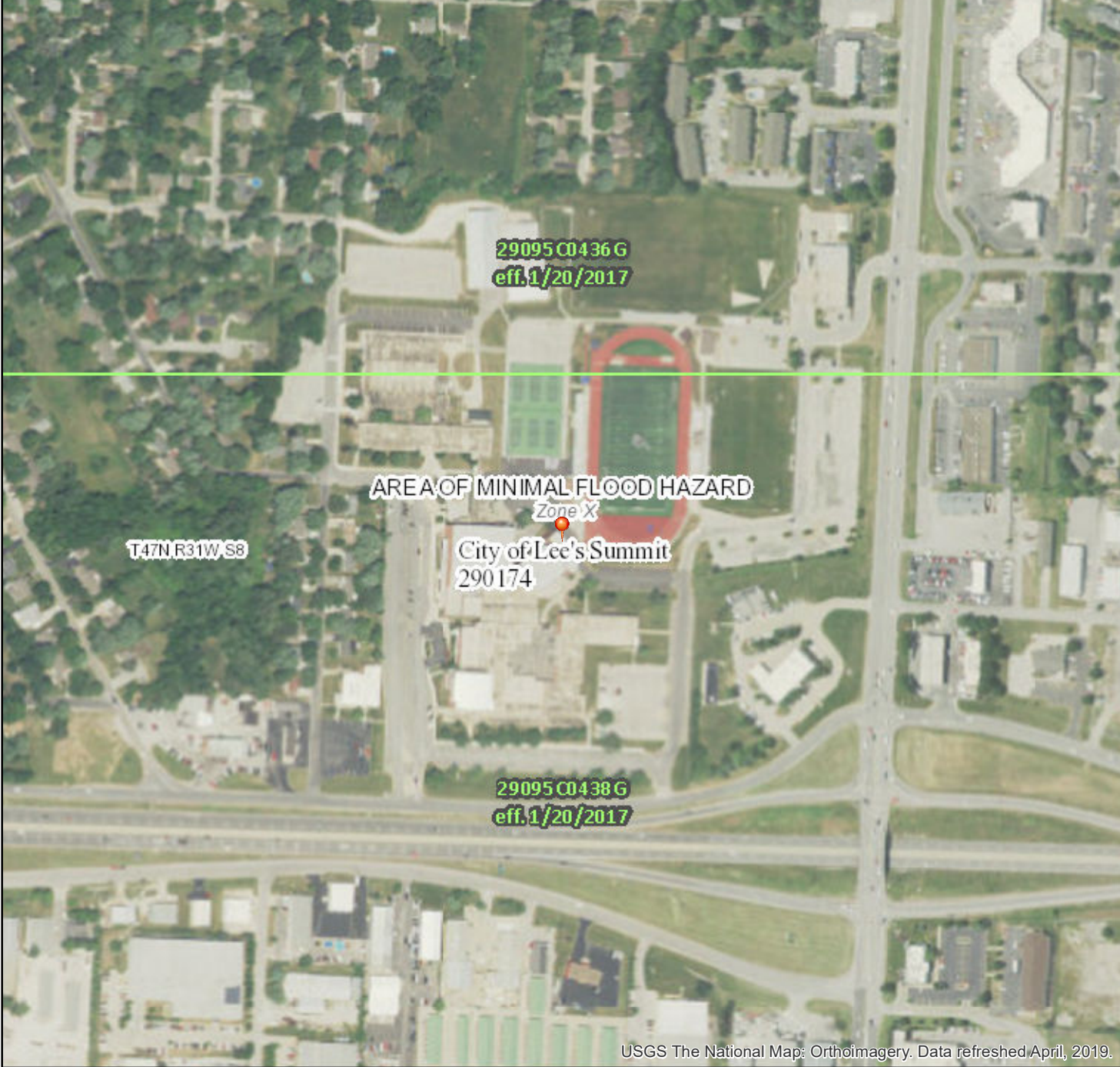
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/28/2020 at 2:17:12 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

38°54'32.47"N

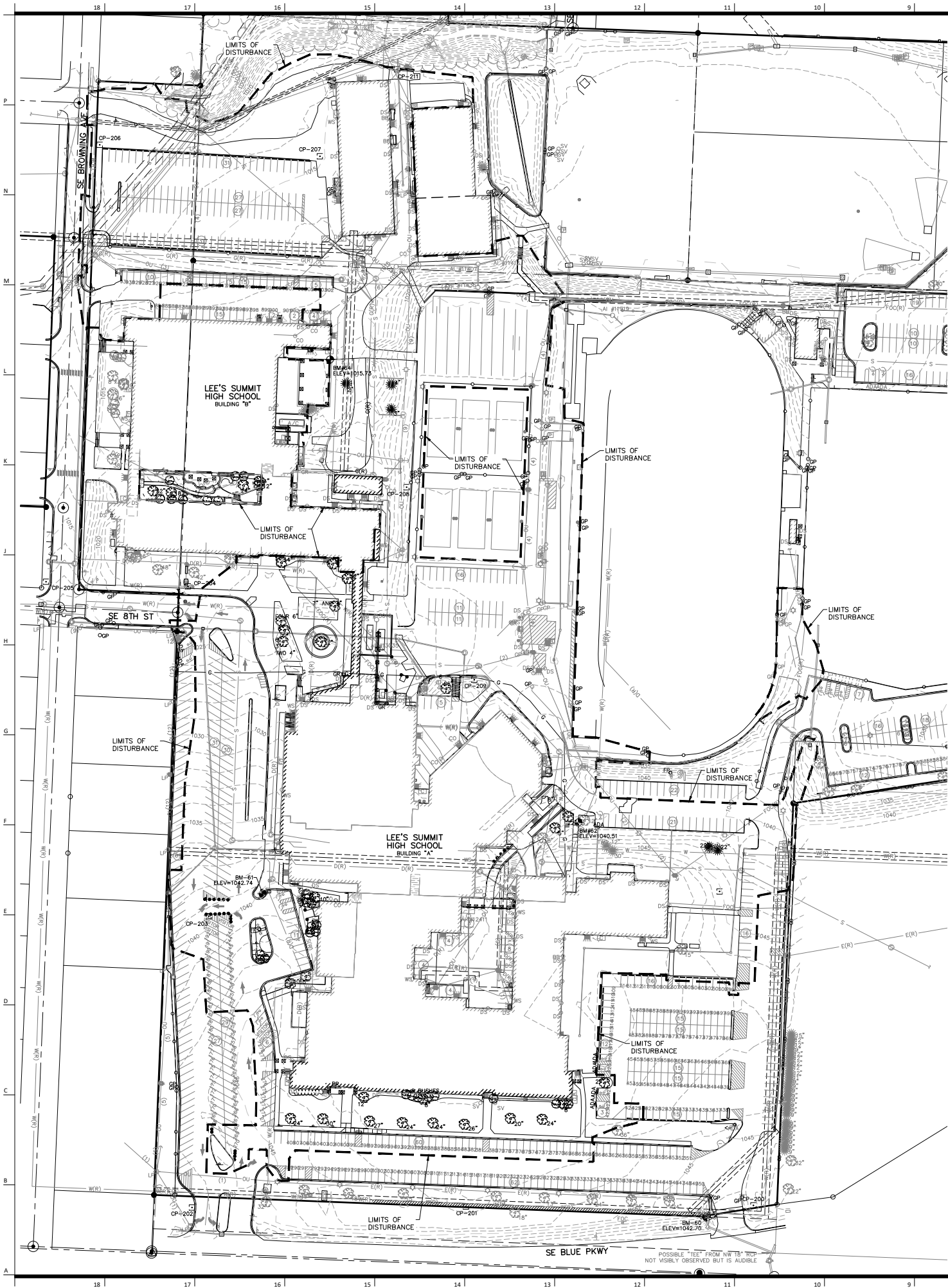


USGS The National Map: Orthoimagery. Data refreshed April, 2019.

94°21'38.73"W

0 250 500 1,000 1,500 2,000 Feet 1:6,000

38°54'4.47"N



DESCRIPTIONS: (PER TITLE COMMITMENT)

TRACT 1: (MISSOURI WARRANTY DEED, BOOK 823, AT PAGE 733)(DEED 1A)
ALL OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, EXCEPT THAT PART CONVEYED TO THE STATE OF MISSOURI BY WARRANTY DEED RECORDED IN BOOK 656 AT PAGE 111 (DEED 1B), AND ALSO EXCEPT THAT PART THEREOF CONVEYED TO THE STATE OF MISSOURI BY WARRANTY DEED RECORDED IN BOOK 661 AT PAGE 166 (DEED 1C).

ALSO EXCEPT THAT PART THEREOF CONVEYED TO ARTHUR B. MCLENNAN AND PAULINE P. MCLENNAN, HUSBAND AND WIFE BY WARRANTY DEED RECORDED IN BOOK 883 AT PAGE 51 (DEED 1D), AND ALSO EXCEPT A TRACT OF LAND IN SAID SOUTHWEST QUARTER OF THE NORTHWEST QUARTER, SECTION 8, TOWNSHIP 47, RANGE 31 DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT 651.69 FEET NORTH OF THE SOUTHEAST CORNER OF THE SAID QUARTER QUARTER SECTION, THENCE WEST 491.69 FEET; THENCE NORTH 63 FEET; THENCE EAST 491.69 FEET TO THE QUARTER SECTION LINE; THENCE SOUTH 63 FEET TO POINT OF BEGINNING.

TRACT 2: (MISSOURI WARRANTY DEED, BOOK 1243, AT PAGE 716)(DEED 2)
ALL OF THE WEST 327 FEET OF THE NORTH 2 ACRES OF THE SOUTH 5 ACRES OF THE SOUTHEAST QUARTER OF THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT 198 FEET NORTH OF THE SOUTHWEST CORNER OF THE SOUTHEAST QUARTER OF THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN JACKSON COUNTY, MISSOURI, AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 132 FEET; THENCE SOUTH 327 FEET; THENCE SOUTH 132 FEET TO POINT OF BEGINNING.

TRACT 3: (MISSOURI WARRANTY DEED, BOOK 1277, AT PAGE 325)(DEED 3)
THE SOUTH 5 ACRES OF THE WEST HALF OF THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

TRACT 4: (REPORT OF COMMISSIONERS, BOOK 1484, AT PAGE 306)(DEED 4)
ALL OF THE WEST 327 FEET OF THE SOUTH 3 ACRES OF THAT PART OF THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 8 TOWNSHIP 47, RANGE 31 IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI DESCRIBED AS FOLLOWS:

BEGINNING AT THE SOUTHWEST CORNER OF THE SOUTHEAST QUARTER OF THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 198 FEET; THENCE SOUTH 198 FEET TO THE POINT OF BEGINNING.

TRACT 5: (MISSOURI WARRANTY DEED, BOOK 1491, AT PAGE 140)(DEED 5)
ALL THAT PART OF THE EAST HALF OF THE NORTHWEST QUARTER OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI DESCRIBED AS FOLLOWS:

BEGINNING AT THE NORTHEAST CORNER OF THE INTERSECTION OF 7TH STREET AND BROWNING AVENUE; THENCE SOUTH ALONG THE EAST LINE OF BROWNING AVENUE A DISTANCE OF 678.52 FEET TO THE NORTH LINE OF 8TH STREET; THENCE EAST ALONG THE NORTH LINE OF 8TH STREET A DISTANCE OF 133 FEET TO THE EAST LINE OF SAID QUARTER SECTION; THENCE NORTH ALONG THE EAST LINE OF SAID QUARTER SECTION A DISTANCE OF 678.52 FEET TO THE NORTH LINE OF 7TH STREET EXTENDED; THENCE WEST ALONG THE NORTH LINE OF 7TH STREET EXTENDED A DISTANCE OF 135.77 FEET TO THE POINT OF BEGINNING.

TRACT 6: (MISSOURI WARRANTY DEED, BOOK 1536, AT PAGE 205)(DEED 6)
ALL THAT PART OF THE SOUTHWEST 1/4 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47 RANGE 31, DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT 556.69 FEET NORTH OF THE SOUTHEAST CORNER OF 1/4 OF 1/4 SECTION; THENCE WEST 491.68 FEET; THENCE NORTH 158 FEET; THENCE EAST 491.68 FEET; THENCE SOUTH 158 FEET TO THE POINT OF BEGINNING. ALL IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

EXCEPT THAT PART CONTAINED IN THE REPORT OF COMMISSIONERS RECORDED AS DOCUMENT NO 131081 IN BOOK 189 AT PAGE 465, DESCRIBED AS FOLLOWS:

ALL THAT PART OF THE SW 1/4 OF THE NE 1/4 OF SECTION 8, 14TH, R31W, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI DESCRIBED AS FOLLOWS: BEGINNING AT A POINT 714.6 FEET NORTH AND 57 FEET WEST OF THE SOUTHEAST CORNER OF THE SW 1/4 OF THE NE 1/4 OF SAID SECTION 8, SAID POINT BEING TO FEET WESTERLY OF THE CENTERLINE OF STATE HIGHWAY DESIGNATED ROUTE 00 (71 BY-PASS), AS MEASURED AT RIGHT ANGLES THERETO; THENCE SOUTH 3 DEGREES 14 MINUTES 23 SECONDS WEST PARALLELING SAID HIGHWAY CENTERLINE, 158 FEET; THENCE WEST PARALLELING THE SOUTH LINE OF SAID 1/4 1/4 SECTION, A DISTANCE OF 432 FEET; THENCE NORTH PARALLELING THE EAST LINE OF SAID 1/4 1/4 SECTION, A DISTANCE OF 75 FEET; THENCE NORTHEASTERLY ALONG A STRAIGHT LINE TO THE POINT OF BEGINNING.

TRACT 7: (MISSOURI WARRANTY DEED, BOOK 1869, AT PAGE 312)(DEED 7)
BEGINNING AT A POINT 1320.0 FEET NORTH OF THE EAST-WEST CENTER LINE OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, AND ON THE EAST LINE OF THE EAST 1/2 OF THE NORTHWEST 1/4 OF SAID SECTION; THENCE WEST 186.3 FEET; THENCE NORTH 100 FEET; THENCE EAST 186.3 FEET TO A POINT ON THE EAST LINE; THENCE SOUTH ON SAID EAST LINE 100.0 FEET TO THE POINT OF BEGINNING, EXCEPTING THEREFROM THAT PART SITUATED IN US HIGHWAY 71 BY-PASS.

TRACT 8: (MISSOURI WARRANTY DEED, BOOK 1869, AT PAGE 313)(DEED 8)
ALL OF THE SOUTH 3 ACRES OF THE EAST 1/2 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31, IN LEE'S SUMMIT JACKSON COUNTY, MISSOURI, EXCEPT THE WEST 327 FEET THEREOF AND ALSO EXCEPT THE SOUTH 100 FEET OF THE EAST 186.3 FEET THEREOF.

TRACT 9: (MISSOURI WARRANTY DEED, BOOK 1-79, AT PAGE 635)(DEED 9)
THE EAST 88.5 FEET OF THAT PART OF LOT 1, MUCKEY ADDITION, A SUBDIVISION IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI, LYING SOUTH OF THE SOUTH LINE OF 6TH STREET, AS SAID DEED IS RECORDED IN BOOK 1039 AT PAGE 122, EXCEPT THE NORTH 155 FEET OF SAID EAST 88.5 FEET.

TRACT 10: (MISSOURI WARRANTY DEED, BOOK 551, AT PAGE 135)(DEED 10)
ALL OF THE NORTH 2 ACRES OF THE SOUTH 5 ACRES OF THE SOUTHWEST CORNER OF THE SW 1/4 OF THE NE 1/4 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31, EXCEPT ALL THE WEST 327 FEET THEREOF MORE PARTICULARLY DESCRIBED AS FOLLOWS: BEGINNING AT A POINT 198 FEET NORTH OF THE SOUTHWEST CORNER OF THE SOUTHEAST 1/4 OF THE NORTHWEST 1/4 OF SECTION 8, TOWNSHIP 47, RANGE 31 AND RUNNING THENCE EAST 327 FEET; THENCE NORTH 132 FEET; THENCE WEST 327 FEET; THENCE SOUTH 132 FEET TO POINT OF BEGINNING, ALL IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

TRACT 11: (MISSOURI WARRANTY DEED, BOOK 623, AT PAGE 833)(DEED 11)
THE SOUTH 220 FEET OF THE WEST 88.5 FEET OF LOT 1, MUCKEY ADDITION, A SUBDIVISION IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI.

DESCRIPTION: (PER TITLE COMMITMENT)

TRACT 1: (MISSOURI WARRANTY DEED, Bk. 1-80, Pg. 1904)
ALL THAT PART OF LOT 3, MUCKEY ADDITION, A SUBDIVISION OF LAND IN LEE'S SUMMIT, JACKSON COUNTY, MISSOURI ACCORDING TO THE RECORDED PLAT THEREOF, LYING SOUTH OF THE SOUTH LINE OF 6TH STREET IN LEE'S SUMMIT, AS SAID STREET IS DESCRIBED IN THE DEED RECORDED IN BOOK 1039 AT PAGE 122.

HORIZONTAL AND VERTICAL DATUM:
UNLESS OTHERWISE NOTED THE COORDINATES SHOWN HEREON ARE GROUND COORDINATES BASED ON THE MISSOURI STATE PLANE (1983) WEST ZONE (NAD 1983) (NAD 1983).
CAF: 0.9998978
1 METER GROUND COORDINATES X COMBINED ADJUSTMENT FACTOR (CAF) = GRID COORDINATES SCALED AROUND 0.0
NORTHING: 303,646.030 (GRID/METERS) 996,313.829 (GROUND/FEET)
EASTING: 860,950.475 (GRID/METERS) 2,824,923.692 (GROUND/FEET)
ELEVATION: 321.8 (METERS) 1055.77 (FEET)

SITE BENCHMARKS:
BM-55 FOUND CUT SQUARE AT THE WEST NORTHWEST CONCRETE HEADWALL ON THE WEST SIDE OF THE EAST ENTRY DRIVE TO LEE'S SUMMIT HIGH SCHOOL. ELEVATION= 1042.70
BM-61 SET CUT SQUARE WITH PUNCH IN THE SOUTHWEST EDGE ON A CONCRETE LIGHT BASE ON THE NORTH SIDE OF THE DRIVE LANE AT THE HIGH SCHOOL ADMINISTRATION CENTER ENTRY. ELEVATION= 1042.74
BM-62 SET CUT SQUARE AT THE NORTH CORNER OF THE FIRST STEP UP OF A CONCRETE WALK ON THE NORTH SIDE OF THE EAST MAIN WING. ELEVATION= 1040.51
BM-63 SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF A CONCRETE PATIO WITH COVERED TABLES ON THE EAST SIDE OF BUILDING "B". ELEVATION= 1015.74
BM-64 SET CUT SQUARE AT THE TOP NORTHEAST CORNER OF STEPS TO THE NORTH ENTRY TO BUILDING "B" ON THE WEST SIDE. ELEVATION= 1015.34

PROJECT CONTROL:
CP-200 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996572.06 (GROUND)
EASTING: 2827438.76 (GROUND)
ELEV = 1049.49
CP-201 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996570.39 (GROUND)
EASTING: 2827055.45 (GROUND)
ELEV = 1045.24
CP-202 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996569.25 (GROUND)
EASTING: 2826689.97 (GROUND)
ELEV = 1042.52
CP-203 MAG NAIL
NORTHING: 996957.62 (GROUND)
EASTING: 2826712.48 (GROUND)
ELEV = 1039.43
CP-204 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997397.36 (GROUND)
EASTING: 2826684.55 (GROUND)
ELEV = 1023.04
CP-205 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997403.51 (GROUND)
EASTING: 2826495.31 (GROUND)
ELEV = 1018.15
CP-206 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997885.93 (GROUND)
EASTING: 2826567.03 (GROUND)
ELEV = 1012.56
CP-207 1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997970.64 (GROUND)
EASTING: 2826680.58 (GROUND)
ELEV = 1014.79

LEGEND:
CONTROL POINT
BENCHMARK
STREET/TRAFFIC SIGN
PAINTED DIRECTIONAL ARROW
TURN LANE DIRECTION
HANDICAP SYMBOL
PARKING STALL COUNT
WHEEL STOP
UNDERGROUND FIBER OPTIC CABLE
UNDERGROUND FIBER OPTIC (FROM RECORDS)
TELEPHONE PEDESTAL
SANITARY SEWER MANHOLE
STORM SEWER MANHOLE
AREA INLET
CURB INLET
SANITARY SEWER CLEAN OUT
FLOOR DRAIN
FLARED END SECTION
SANITARY SEWER LINE
STORM SEWER LINE
CORRUGATED METAL PIPE
REINFORCED CONCRETE PIPE
VITRIFIED CLAY PIPE
DUCTILE IRON PIPE
HIGH DENSITY POLYETHYLENE
WALL MOUNTED LIGHT
WALL MOUNTED CAMERA
UNDERGROUND ELECTRIC
OVERHEAD UTILITY LINE (# OF LINES)
PULL BOX
LIGHT POLE
UTILITY POLE
UTILITY POLE W/ LIGHT
UTILITY POLE W/ TRANSFORMER
GUY ANCHOR
WATER LINE PER RECORD
UNDERGROUND ELECTRIC PER RECORD
WALL MOUNTED ELECTRICAL OUTLET
BACK TO BACK OF CURB MEASUREMENT
UNDERGROUND ELECTRIC PEDESTAL
UNDERGROUND GAS PER RECORD
SANITARY SEWER LINE PER RECORD
STORM SEWER LINE PER RECORD
AIR CONDITIONER
UNDERGROUND GAS
GAS METER
GAS VALVE
GAS RISER
GAS LINE SIGN
EXISTING SPOT ELEVATION
EXISTING GRADE 5' CONTOUR
EXISTING GRADE 1' CONTOUR
DOOR ELEVATION
AT THRESHOLD
FF FINISH FLOOR ELEVATION
BHE BUILDING HEIGHT/ELEVATION
EDGE TO EDGE OF ASPHALT
WATER SPIGOT
WATER LINE
WATER METER
WATER LINE GATE VALVE
FIRE HYDRANT
SPRINKLER CONTROL BOX
WATER MANHOLE
SPRINKLER VALVE
SEAMLESS FINE CONNECTOR
CANOPY SUPPORT
MAIL BOX
CONCRETE JOINT/CUT LINE
BUSH
DECIDUOUS TREE
CONIFEROUS TREE
TREE LINE
FLAG POLE
TRASH ENCLOSURE
LANDSCAPING AREA
CONC CONCRETE
LW LOWEST WIRE HEIGHT
ELECTRIC METER
SPEAKER BOX
BREAKER BOX
HANDICAP SIGN
HANDICAP RAMP
GATE POST
CHAIN LINK FENCE
WOOD FENCE
BOLLARD

UNLESS A PROFESSIONAL SEAL WITH SIGNATURE AND DATE IS AFFIXED, THIS DOCUMENT IS PRELIMINARY AND IS NOT INTENDED FOR CONSTRUCTION, RECORDING PURPOSES OR MAP INFORMATION.

NOT FOR CONSTRUCTION

Architectural Corporation
Missouri License No. 2018022991
Jame Doe
Date: MM/DD/YYYY
License No. A-0000000

REVISIONS
Number DESCRIPTION DATE

PROJECT NO: 0119-0100
DATE: October 13, 2020

EXISTING CONDITIONS
C400
50% Construction Documents

PROJ. NO. C20_0496 DSN: DOW ENGINEER
CIN: 0458E/COR/DWG DWN: JLN MO # 2011037427
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
PH. (913) 894-5150 | FAX (913) 894-5977
www.kvweng.com | www.kvweng.com
KAW VALLEY ENGINEERING, INC. IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000042. EXPIRES 12/31/21



VICINITY MAP
SEC 8 TWP 47N RNG 31W
NOT TO SCALE

Lee's Summit
High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4200 Pennsylvania Avenue
Kansas City, MO 64111
816.933.6653 voice
www.goulddevans.com
structural engineer:
Bob D. Campbell & Company, Inc.
4338 Bellview
Kansas City, MO 64111
816.533.4144

civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
816.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700

Custom Soil Resource Report Soil Map

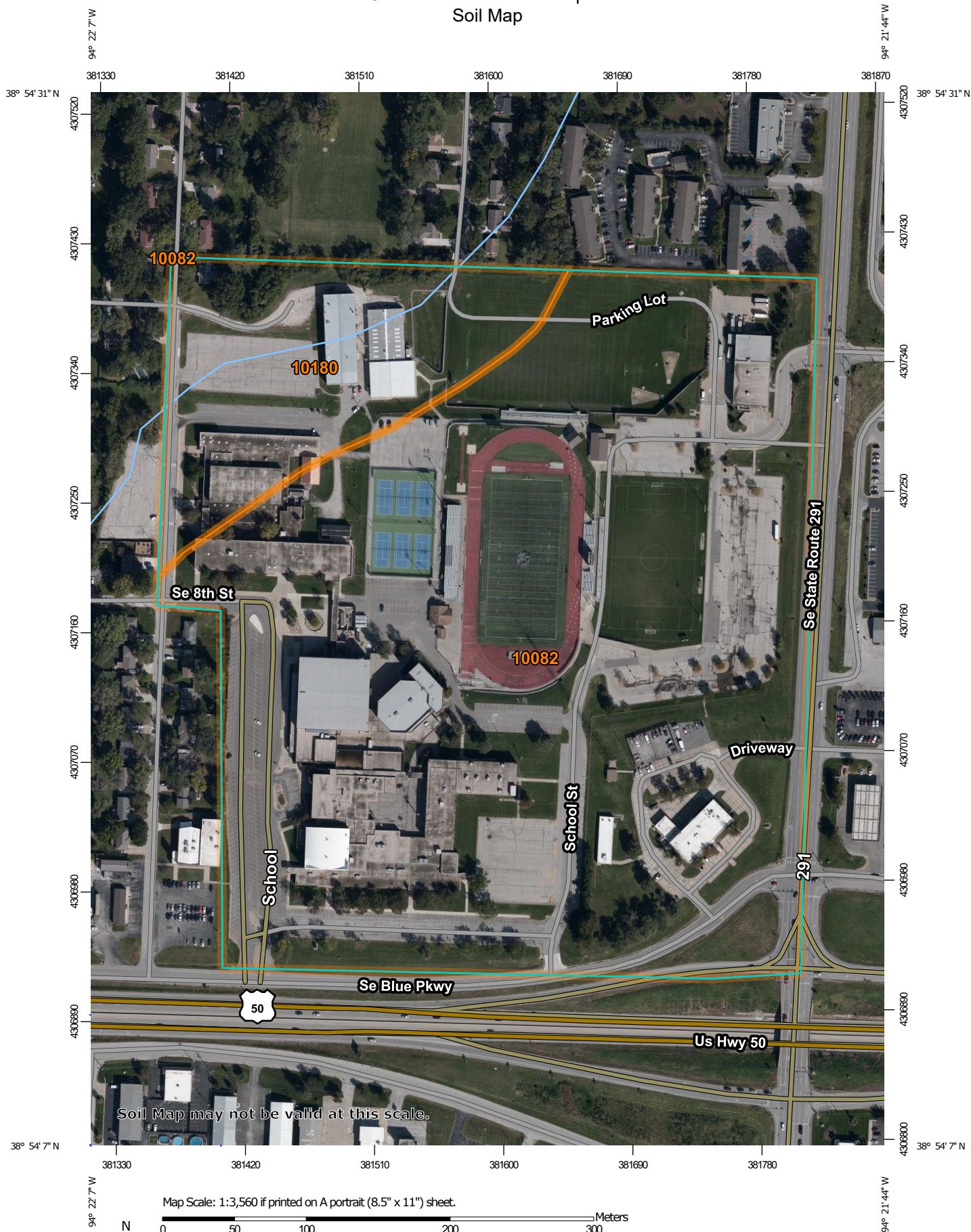


Exhibit B

Proposed Grading Plan

Lee's Summit High School

400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4300 Pennsylvania Avenue
Kansas City, MO 64111
816.931.6655
www.goulddevans.com

structural engineer:
Bolt & Campbell & Company, Inc.
4338 Bellview
Kansas City, MO 64111
816.533.4144

civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
913.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700

**NOT FOR
CONSTRUCTION**

Architectural Corporation
Missouri License No. 2018022991
June Doe Date: MM/DD/YYYY
Architect License No. A-00000000

REVISIONS

Number	Description	Date

PROJECT NO: 0119-0100
DATE: October 13, 2020

OVERALL GRADING PLAN

C300

50% Construction Documents



Know what's below.
Call before you dig.

PROJ. NO. C20_0496
CIN: 0456GP.DWG

DAVID D. WOOD
ENGINEER
MO # 2011037427

14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
PH. (913) 894-5150 | FAX (913) 894-5977
www.kveng.com | www.kveng.com

KAW VALLEY ENGINEERING, INC., IS AUTHORIZED TO OFFER ENGINEERING SERVICES BY MISSOURI STATE CERTIFICATE OF AUTHORITY # 000842. EXPIRES 12/31/21

HORIZONTAL AND VERTICAL DATUM:
UNLESS OTHERWISE NOTED THE COORDINATES SHOWN HEREON ARE GROUND COORDINATES BASED ON THE MISSOURI STATE PLANE (1983) WEST ZONE (NAD 1983) (NAD 1983)
CAP: 0.0000078
SCALED AROUND 0.0

JA-25 (PID: 095025)
NORTHING: 303646.030 (GRID/METERS) 996313.829 (GROUND/FEET)
EASTING: 860950.475 (GRID/METERS) 2824923.692 (GROUND/FEET)
ELEVATION: 321.8 (METERS) 1055.77 (FEET)

SITE BENCHMARKS:

BM-61
FOUND CUT SQUARE AT THE WEST NORTHWEST CONCRETE HEADWALL ON THE WEST SIDE OF THE EAST ENTRY DRIVE TO LEE'S SUMMIT HIGH SCHOOL
ELEVATION= 1042.70

BM-61
SET OUT SQUARE WITH PUNCH IN THE SOUTHWEST EDGE OF DRIVE LANE AT THE HIGH SCHOOL ADMINISTRATION CENTER ENTRY
ELEVATION= 1042.74

BM-62
SET OUT SQUARE AT THE NORTHEAST CORNER OF THE FIRST STEP UP OF A CONCRETE WALK ON THE NORTH SIDE OF THE EAST MAIN WING
ELEVATION= 1040.51

BM-63
SET OUT SQUARE AT THE TOP NORTHEAST CORNER OF A CONCRETE PATIO WITH COVERED TABLES ON THE EAST SIDE OF BUILDING "B"
ELEVATION= 1015.74

BM-64
SET OUT SQUARE AT THE TOP NORTHEAST CORNER OF STEPS TO THE NORTH ENTRY TO BUILDING "B" ON THE WEST SIDE
ELEVATION= 1015.34

PROJECT CONTROL:

CP-#201
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996572.06 (GROUND)
EASTING: 282749.83 (GROUND)
ELEV = 1048.49

CP-#201
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996570.39 (GROUND)
EASTING: 2827055.45 (GROUND)
ELEV = 1048.24

CP-#202
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 996569.25 (GROUND)
EASTING: 2826889.97 (GROUND)
ELEV = 1042.52

CP-#203
NAG NAIL
NORTHING: 996957.62 (GROUND)
EASTING: 2826712.48 (GROUND)
ELEV = 1039.43

CP-#204
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997397.36 (GROUND)
EASTING: 2826884.55 (GROUND)
ELEV = 1023.04

CP-#205
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997403.51 (GROUND)
EASTING: 2826468.31 (GROUND)
ELEV = 1018.15

CP-#206
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997585.83 (GROUND)
EASTING: 282567.03 (GROUND)
ELEV = 1012.56

CP-#207
1/2" REBAR W/ ORANGE KVE CAP
NORTHING: 997970.64 (GROUND)
EASTING: 2826860.58 (GROUND)
ELEV = 1014.79

NOTE:

- CONTRACTOR SHALL REFER TO ARCHITECTURAL PLANS FOR EXACT LOCATIONS AND DIMENSIONS OF ENTRANCE, SLOPED PAVING, EXIT PORCHES, RAMPS, TRUCK DOCKS, PRECISE BUILDING DIMENSIONS AND EXACT BUILDING UTILITY ENTRANCE LOCATIONS.
- THESE PLANS HAVE NOT BEEN VERIFIED WITH FINAL ARCHITECTURAL CONTRACT DRAWINGS. CONTRACTOR SHALL VERIFY AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES. CONTRACTOR IS FULLY RESPONSIBLE FOR REVIEW AND COORDINATION OF ALL DRAWINGS AND CONTRACTOR DOCUMENTS.
- ALL DIMENSIONS ARE TO BACK OF CURB UNLESS NOTED OTHERWISE.
- ALL DIMENSIONS ARE PERPENDICULAR TO PROPERTY LINE.

WARRANTY / DISCLAIMER

THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN OR DO WARRANTY THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTINUOUS BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR

THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS. THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

SAFETY NOTICE TO CONTRACTOR

IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

GRADING NOTES:

- THE CONSTRUCTION AREA SHALL BE CLEARED, GRUBBED, AND STRIPPED OF TOPSOIL AND ORGANIC MATTER FROM ALL AREAS TO BE OCCUPIED BY BUILDING AND PAVING. TOPSOIL FOR REPLACEMENT ON SLOPES MAY BE STOCKPILED ON SITE. EXCESS TOPSOIL MAY BE WASTED IN FILL SLOPES PROVIDED THAT NO TOPSOIL WILL BE WASTED WITHIN 10 FEET OF THE EDGE OF THE BUILDING OR PARKING AREA. BURNING OF TIMBER WILL NOT BE PERMITTED UNLESS APPROVAL IS OBTAINED FROM GOVERNING OFFICIALS. STRIPPING EXISTING TOPSOIL AND ORGANIC MATTER SHALL BE TO A MINIMUM DEPTH OF 6 INCHES. CONSTRUCTION MANAGER SHALL DESIGNATE LOCATION OF STOCKPILE AREAS DURING CONSTRUCTION. ANY UNAUTHORIZED STOCKPILE SHALL BE REMOVE/RELOCATED AT THE CONTRACTORS EXPENSE.
- AREAS TO RECEIVE FILL SHALL BE SCARIFIED AND THE TOP 12-INCH DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698 WITH A MOISTURE CONTENT OF +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT OF LESS THAN 40 AND 0 TO +4% FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40. ANY UNSUITABLE AREAS SHALL BE UNDERCUT AND REPLACED WITH SUITABLE MATERIAL BEFORE ANY FILL MATERIAL CAN BE APPLIED.
- OFF-SITE SOIL MATERIAL FOR USE UNDER BUILDING AND PAVED AREAS SHALL HAVE A PLASTICITY INDEX OF 25 OR LESS, A LIQUID LIMIT OF 45 OR LESS AND CONTAIN NO ROCK LARGER THAN THREE INCHES. OFF-SITE FILL MATERIAL SHALL BE APPROVED BY THE OWNER'S TESTING AGENCY PRIOR TO BRINGING ON SITE.
- EARTHWORK UNDER THE BUILDING, PAVING AND LIGHTLY LOADED STRUCTURAL FEATURES SHALL COMPLY WITH THE CONTRACT DOCUMENTS AND PROJECT GEOTECHNICAL REPORT. THE BUILDING PAD SHALL BE EXCAVATED AS REQUIRED TO ALLOW THE PLACEMENT OF LOW VOLUME CHANGE MATERIAL. REFER TO GEOTECHNICAL REPORT FOR PREPARING BUILDING PAD AND LOW VOLUME CHANGE THICKNESS REQUIREMENTS. OTHER FILL MATERIAL SHALL BE MADE IN LIFTS NOT TO EXCEED EIGHT INCHES DEPTH COMPACTED TO 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D 698. LVC SOILS SHALL BE COMPACTED AT A MOISTURE CONTENT OF 0 TO +4% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT GREATER THAN 40 AND +/- 3% OF OPTIMUM FOR SOILS WITH A LIQUID LIMIT LESS THAN 40. NO ROCK LARGER THAN THREE INCHES IN ANY DIMENSION NOR ANY SHALE SHALL BE PLACED IN THE TOP 24 INCHES OF EMBANKMENT.
- ON-SITE HIGH PLASTICITY CLAYS MAY BE TREATED WITH 5% TYPE 1/2 PORTLAND CEMENT BY WEIGHT. REFER TO PROJECT GEOTECHNICAL REPORT FOR REQUIREMENTS.
- AREAS THAT ARE TO BE CUT TO SUBGRADE LEVELS SHALL BE PROOF ROLLED WITH A LOADED DUMP TRUCK OR SIMILAR APPROVED CONSTRUCTION EQUIPMENT TO DETECT UNSUITABLE SOIL CONDITIONS.
- IN ALL AREAS OF EXCAVATION, IF UNSUITABLE SOIL CONDITIONS ARE ENCOUNTERED, THE OWNER'S ENGINEER SHALL RECOMMEND TO THE OWNER THE METHODS OF UNDERCUTTING AND REPLACEMENT OF PROPERLY COMPACTED, APPROVED FILL MATERIAL. ALL PROOFROLLING AND UNDERCUTTING SHOULD BE PERFORMED DURING A PERIOD OF DRY WEATHER.
- ALL EXCAVATIONS SHALL BE CONSIDERED AS UNCLASSIFIED. REFER TO PROJECT GEOTECHNICAL REPORT.
- ALL DISTURBED SLOPES ARE TO BE 3:1 OR FLATTER.
- DETENTION BASIN AND ALL SLOPES DISTURBED EXCEEDING 4:1 SHALL BE HYDROSEED, SODDED OR PROTECTED BY EROSION CONTROL BLANKETS THAT WILL PREVENT EROSION AND PLACED SUCH THAT THE SURFACE IS FLUSH WITH SURROUNDING GROUND AND SHAPED TO CHANNEL WATER IN DIRECTIONS INDICATED. SEE GENERAL NOTES ON THIS SHEET.
- ALL SLOPES AND AREAS DISTURBED BY CONSTRUCTION SHALL BE GRADED SMOOTH AND A MINIMUM OF FOUR INCHES OF TOPSOIL APPLIED. IF ADEQUATE TOPSOIL IS NOT AVAILABLE ON-SITE, THE CONTRACTOR SHALL PROVIDE TOPSOIL, APPROVED BY THE OWNER, AS NEEDED. THE AREA SHALL THEN BE SODDED OR SEEDED, FERTILIZED, MULCHED, WATERED AND MAINTAINED UNTIL HARDY GRASS GROWTH IS ESTABLISHED IN ALL AREAS. ANY AREAS DISTURBED FOR ANY REASON SHALL BE CORRECTED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER PRIOR TO FINAL ACCEPTANCE OF THE PROJECT. REFER TO THE NOTES ON THIS SHEET FOR TEMPORARY SEEDING SPECIFICATIONS. REFER TO PROJECT SITE PLAN FOR FINAL STABILIZATION TREATMENTS.
- CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS.
- THE CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO AVOID PROPERTY DAMAGE TO ADJACENT PROPERTIES DURING THE CONSTRUCTION PHASES OF THIS PROJECT. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR ANY DAMAGES TO THE ADJACENT PROPERTIES OCCURRING DURING THE CONSTRUCTION PHASES OF THIS PROJECT.
- IT IS NOT THE DUTY OF THE ENGINEER OR THE OWNER TO REVIEW THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES, IN, ON OR NEAR THE CONSTRUCTION SITE AT ANY TIME DURING CONSTRUCTION.
- IF ANY OF THESE NOTES CONFLICT WITH THE PROJECT GEOTECHNICAL REPORT (CFS PROJECT 20-1075) AND ALL ADDENDUMS PREPARED BY CFS ENGINEERS DATED JUNE 12, 2020, RECOMMENDATIONS IN GEOTECHNICAL REPORT SHALL GOVERN.

0 30 60 120
SCALE: 1" = 60'

PROPOSED BUILDING ADDITION
FF=1024.3±
(MATCH EXISTING)

PROPOSED BUILDING ADDITION
FF=1026.5±
(MATCH EXISTING)

PROPOSED BUILDING ADDITION
FF=1024.3± NORTH
FF=1038.0± CENTRAL NORTH
FF=1041.7± CENTRAL SOUTH
FF=1049.0± SOUTH

PROPOSED BUILDING ADDITION
FF=1049.2±
(MATCH EXISTING)

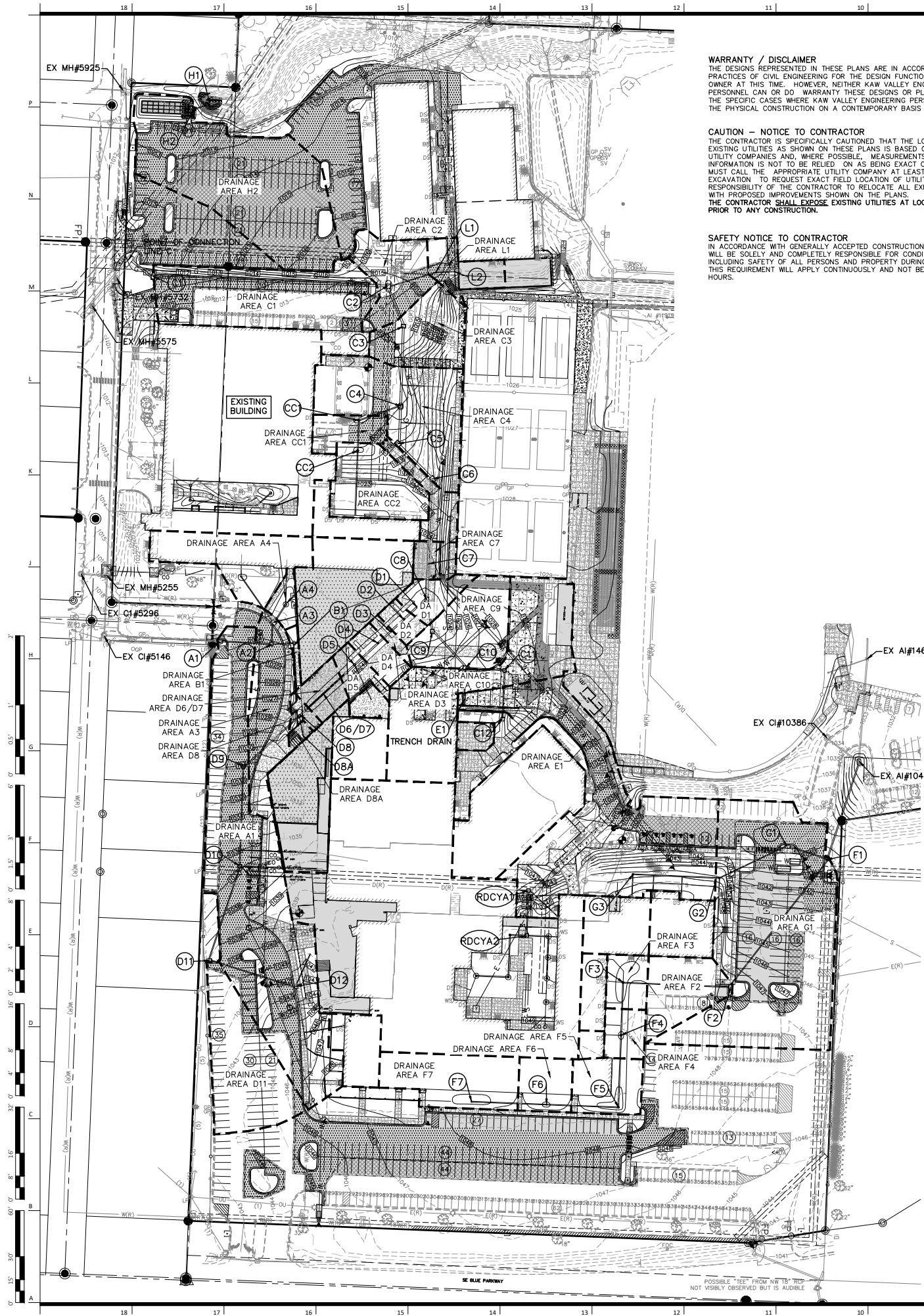
PROPOSED BUILDING ADDITION AREA
FF=1049.2±
(MATCH EXISTING)

GREENHOUSE (BY OTHERS)
CONCRETE PAD IN CONTRACT

EXISTING BUILDING

POSSIBLE "TEE" FROM NW TO "RCP"
NOT VISIBLY OBSERVED BUT IS AUDIBLE

Exhibit C
Drainage Area Map & Calculations
Storm Sewer Plan and Profiles
BMP Plan
EDDB Calculations



WARRANTY / DISCLAIMER
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Tc Calculations 10-09-2020
Lee's Summit School District - Lee's Summit High School Addition and Renovation
KVE Project # C20D0496

Structure	Pipe	Design Storm (years)	Time of Concentration										Notes
			Tributary Area, A (ac)	Impervious Area	Runoff Coefficient, C	Total Distance	D1	Slope	Inlet Time (min)	D2	Travel Time (min)	Time of Concentration (min)	
A4	A4 - A3	10-year	0.04	0.01	0.45	30	30	2.5	4.7	0	0.0	4.7	5 Min Minimum
A3	A3 - A2	10-year	0.26	0.22	0.81	195	100	5.0	3.1	95	0.2	3.2	5 Min Minimum
A2	A2 - A1	10-year											
A1	A1 - CI#5146	10-year	1.12	0.89	0.78	625	100	5.0	3.4	525	0.9	4.3	5 Min Minimum
B1	B1 - A1	10-year											
C12	C12 - C11	10-year											
C11	C11 - C10	10-year											
C10	C10 - C9	10-year	0.80	0.60	0.90	180	100	2.0	2.9	80	0.1	3.0	5 Min Minimum
C9	C9 - C8	10-year	0.26	0.05	0.42	90	90	8.0	5.8	0	0.0	5.8	
C8	C8 - C7	10-year											
C7	C7 - C6	10-year	0.06	0.06	0.90	50	50	1.0	2.5	0	0.0	2.5	5 Min Minimum
C6	C6 - C5	10-year											
C5	C5 - C4	10-year											
C4	C4 - C3	10-year	0.46	0.15	0.50	120	100	15.0	4.4	20	0.0	4.4	5 Min Minimum
C3	C3 - C2	10-year	0.22	0.08	0.52	80	80	15.0	3.8	0	0.0	3.8	5 Min Minimum
C2	C2 - C1	10-year	0.20	0.11	0.63	80	80	6.0	2.0	0	0.0	2.0	5 Min Minimum
C1	C1 - INSERTA TEE 60" RCP	10-year	0.55	0.45	0.79	270	100	1.5	4.9	170	0.3	5.1	
CC2	CC2 - CC1	10-year											
CC1	CC1 - C4	10-year											
D12	D12 - D11	10-year											
D11	D11 - D10	10-year	0.37	0.37	0.90	220	100	6.0	3.0	120	0.2	3.2	5 Min Minimum
D10	D10 - D9	10-year											
D9	D9 - D8	10-year											
D8	D8 - D7/D6	10-year	0.03	0.02	0.70	50	50	6.0	2.8	0	0.0	2.8	5 Min Minimum
D7/D6	D7/D6 - D5	10-year	0.07	0.07	0.90	50	50	6.0	1.4	0	0.0	1.4	5 Min Minimum
D5	D5 - D4	10-year	0.06	0.05	0.80	50	50	6.0	2.1	0	0.0	2.1	5 Min Minimum
D4	D4 - D3	10-year	0.06	0.03	0.80	50	50	6.0	3.5	0	0.0	3.5	5 Min Minimum
D3	D3 - D2	10-year	0.05	0.02	0.54	50	50	6.0	3.9	0	0.0	3.9	5 Min Minimum
D2	D2 - D1	10-year	0.04	0.03	0.75	50	50	6.0	2.5	0	0.0	2.5	5 Min Minimum
D1	D1 - C9	10-year	0.07	0.03	0.56	50	50	6.0	3.8	0	0.0	3.8	5 Min Minimum
E1 (Dock Trench Drain)	E1 (Dock Trench Drain) - C11	10-year	1.15	0.69	0.66	460	100	5.0	4.6	360	0.6	5.2	
F7	F7 - F6	10-year	0.26	0.20	0.76	60	60	2.0	3.7	0	0.0	3.7	5 Min Minimum
F6	F6 - F5	10-year	0.11	0.08	0.74	30	30	2.0	2.8	0	0.0	2.8	5 Min Minimum
F5	F5 - F4	10-year	0.15	0.06	0.54	60	60	2.0	6.2	0	0.0	6.2	
F4	F4 - F3	10-year	0.08	0.00	0.30	30	30	2.0	6.3	0	0.0	6.3	
F3	F3 - F2	10-year	0.09	0.00	0.30	30	30	2.0	6.3	0	0.0	6.3	
F2	F2 - F1	10-year	0.19	0.09	0.58	100	100	2.0	7.4	0	0.0	7.4	
F1	F1 - AI #10447	10-year											
G3	G3 - G2	10-year											
G2	G2 - G1	10-year											
G1	G1 - F1	10-year	1.14	1.00	0.83	340	100	4.0	3.1	240	0.4	3.5	5 Min Minimum
H2	H2 - H1	10-year	0.78	0.69	0.83	340	100	2.0	3.8	100	0.2	4.0	5 Min Minimum

811 Know what's below. Call before you dig.

PROJ. NO. C20_0496
CTN: 0496DAM.DWG
DAVID D. WOOD
ENGINEER
MO # 2011037427
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
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Lee's Summit High School
400 SE Blue Pkwy
Lee's Summit, MO 64063

owner:
Lee's Summit R-7 School District
301 NE Tudor Road
Lee's Summit, MO 64086

architect:
Gould Evans
4200 Pennsylvania Avenue
Kansas City, MO 64111
816.933.6655 voice
www.goulddevans.com

structural engineer:
Bob D. Campbell & Company, Inc.
4338 Bellview
Kansas City, MO 64111
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civil engineer:
Kaw Valley Engineering
14700 West 114th Terrace
Lenexa, KS 66215
913.485.0318

mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700

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Architectural Corporation
Missouri License No.: 2018022991
Jame Doe
Date: MM/DD/YYYY
License No. A-00000000

REVISIONS

Number	DESCRIPTION	DATE
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PROJECT NO: 0119-0100
DATE: October 13, 2020

DRAINAGE AREA MAP
C600
50% Construction Documents

STORM SEWER CONSTRUCTION NOTES:

- ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH SECTION 2600 STORM SEWER OF THE KANSAS CITY METRO CHAPTER OF APWA SPECIFICATIONS AS ADOPTED AND AMENDED BY THE CITY OF LEE'S SUMMIT, MISSOURI STANDARD SPECIFICATIONS, REFERENCE APWA SPECIFICATION SECTION 2102.4 FOR EXCAVATION, TRENCHING AND BACKFILLING FOR PIPE AND STORM STRUCTURES.
- A MINIMUM OF 18" COVER SHALL BE PROVIDED PRIOR TO AND MAINTAINED AFTER INSTALLATION OF STORM SEWER.
- ALL COORDINATES FOR CURB INLETS ARE TO THE MIDDLE OF THE INSIDE FRONT FACE. ALL COORDINATES FOR PVC STRUCTURES AND CONCRETE YARD INLETS ARE TO THE CENTER OF THE STRUCTURE.
- ALL JUNCTION BOXES/AREA INLETS HAVE ONE COORDINATE PROVIDED AT THE CENTER OF STRUCTURE. SEE PLAN FOR CLARIFICATION. ORIENT STRUCTURES PARALLEL TO ADJACENT CURB, BUILDING OR WALL FACE, UNLESS NOTED OTHERWISE.
- RIM ELEVATION IS PROVIDED AT COORDINATE, UNLESS NOTED OTHERWISE. CONTRACTOR TO ADJUST ELEVATION OF RIM AS REQUIRED TO MATCH SLOPE OF ADJACENT CURB LINE. REFER TO GRADING PLAN (C300 SERIES SHEETS).
- ALL EXISTING UTILITIES INDICATED ON THE DRAWING ARE ACCORDING TO THE BEST INFORMATION AVAILABLE TO THE ENGINEER; HOWEVER, ALL UTILITIES ACTUALLY EXISTING MAY NOT BE SHOWN. UTILITIES DAMAGED THROUGH THE NEGLIGENCE OF THE CONTRACTOR TO OBTAIN THE LOCATION OF SAME SHALL BE REPAIRED OR REPLACED BY THE CONTRACTOR AT THEIR EXPENSE.
- ALL BACKFILL SHALL BE COMPACTED TO 95 PERCENT STANDARD DENSITY AT OPTIMUM MOISTURE.
- ALL EXCAVATION BENEATH THE STREETS AND PARKING LOTS FOR DRAINAGE PIPE LESS THAN 4'-0" IN DIAMETER SHALL BE BACKFILLED WITH AGGREGATE TO FOUR FEET (4') PAST BACK OF CURB IN ACCORDANCE WITH APWA SPECIFICATIONS SECTION 2102.4.J.
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- ALL HDPE PIPE JOINTS SHALL BE WATER TIGHT.

SAFETY NOTICE TO CONTRACTOR

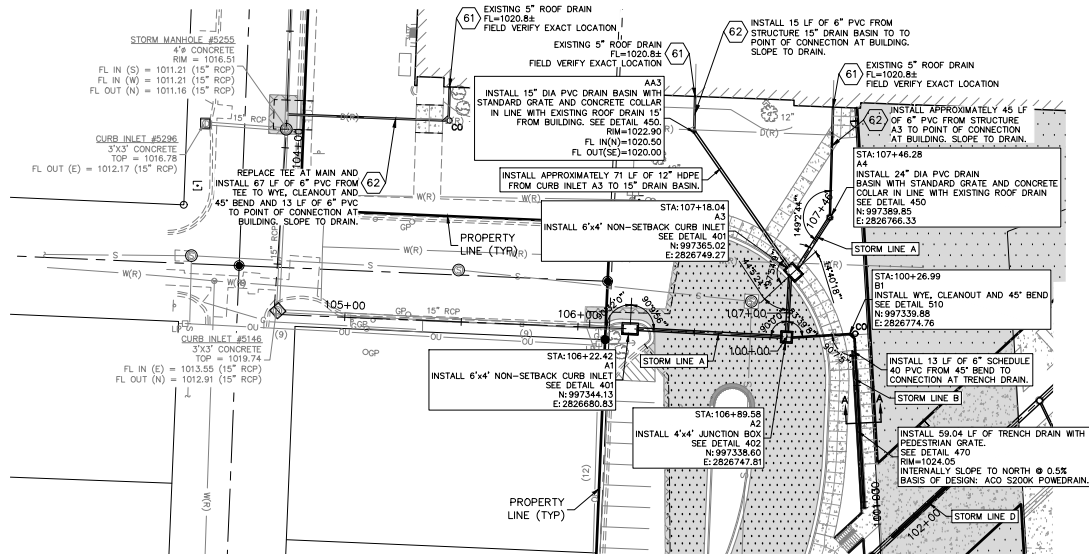
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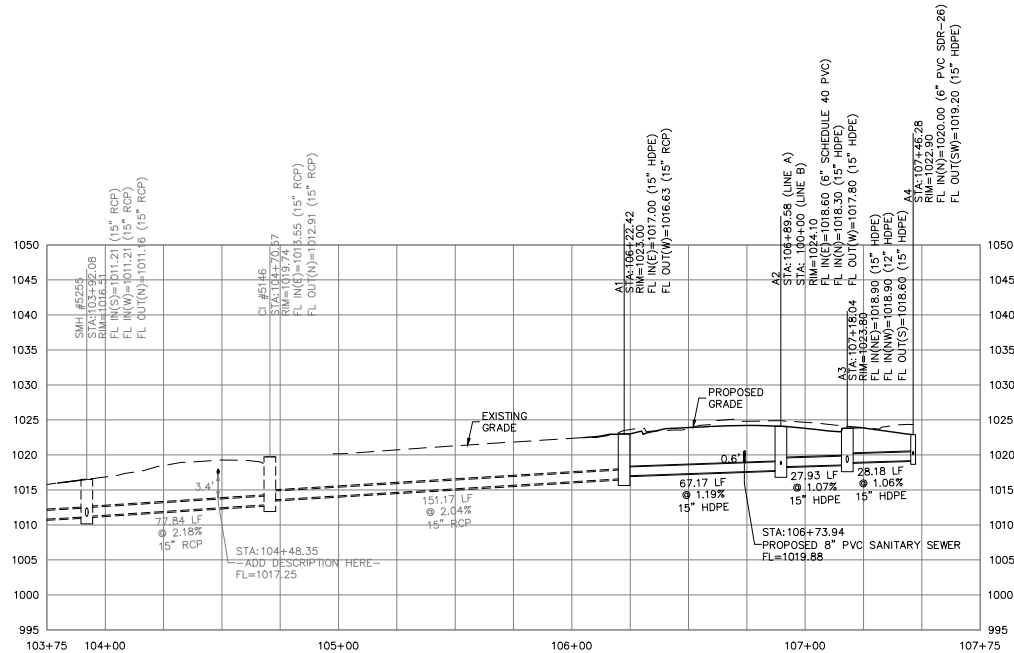
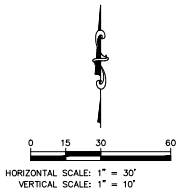
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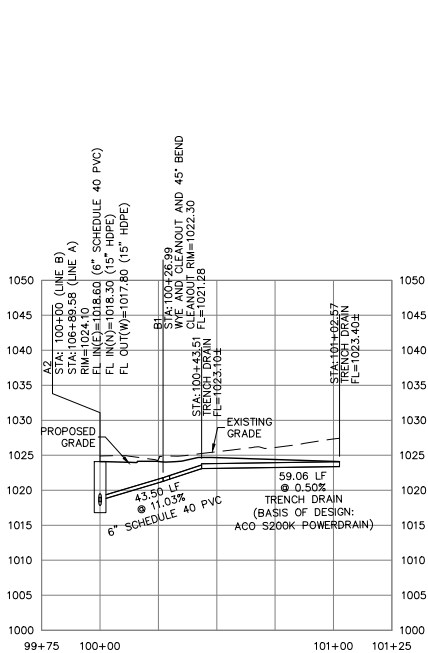
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PRIVATE STORM SEWER LINES A AND B PLAN



PRIVATE STORM SEWER LINE A PROFILE

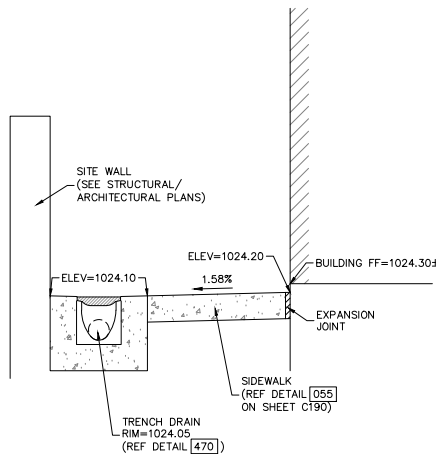


PRIVATE STORM SEWER LINE B PROFILE

- DETAILS SEE SHEET C690 AND C691
- 401 NON-SETBACK CURB INLET
 - 402 JUNCTION BOX
 - 406 CONCRETE FLARED END SECTION WITH TOE WALL AND RIP RAP
 - 433 DOWNSPOUT COLLECTOR
 - 450 PVC DRAIN BASIN - CONTRACTOR TO ORDER INLETS ONE FOOT TALLER THAN PLAN ELEVATION SO INLET CAN BE FIELD ADJUSTED
 - 460 INLINE DRAIN
 - 470 TRENCH DRAIN
 - 510 CLEANOUT

NOTES

- 61 STORM SEWER POINT OF CONNECTION AT BUILDING REFER TO MEP PLANS
- 62 PVC SDR-26 ROOF DRAIN, IF DRAIN IS LESS THAN 2' USE SCHEDULE 40 PVC FOR THE ENTIRE RUN. SLOPE TO DRAIN (1% MINIMUM FOR 6" AND LARGER ROOF DRAINS, 2% MINIMUM FOR 4" ROOF DRAINS)
- 63 PVC STORM LINE AND TEE FOR FOUNDATION DRAIN. COORDINATE WITH ARCHITECTURAL PLANS FOR SIZE.



SECTION A-A

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PROJECT NO: 0119-0100
DATE: October 13, 2020

PRIVATE STORM SEWER
PLAN AND PROFILE

C610

50% Construction
Documents



Know what's below.
Call before you dig.

PROJ. NO. C20-0496
CITY: OASD/PP/DWG
DSN: DOW
DWN: NUN
DAVID D. WOOD
ENGINEER
MO # 2011037427
14700 WEST 114TH TERRACE
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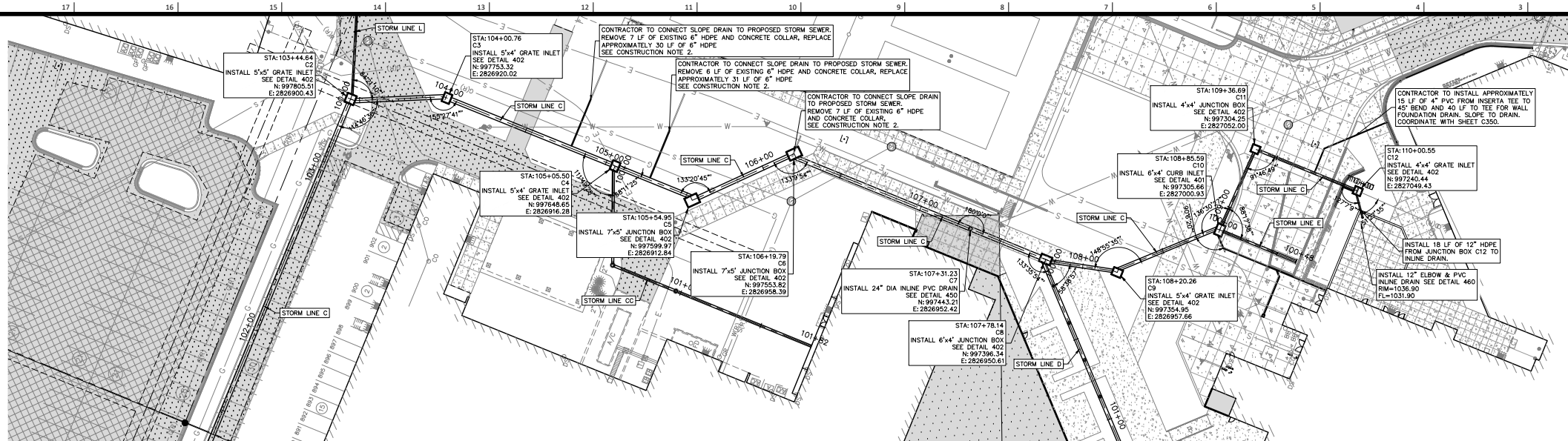
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Henderson Engineers
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816.663.8700



PRIVATE STORM SEWER LINES C PLAN

HORIZONTAL SCALE: 1" = 30'
VERTICAL SCALE: 1" = 10'

DETAILS SEE SHEET C690 AND C691

- 401 NON-SETBACK CURB INLET
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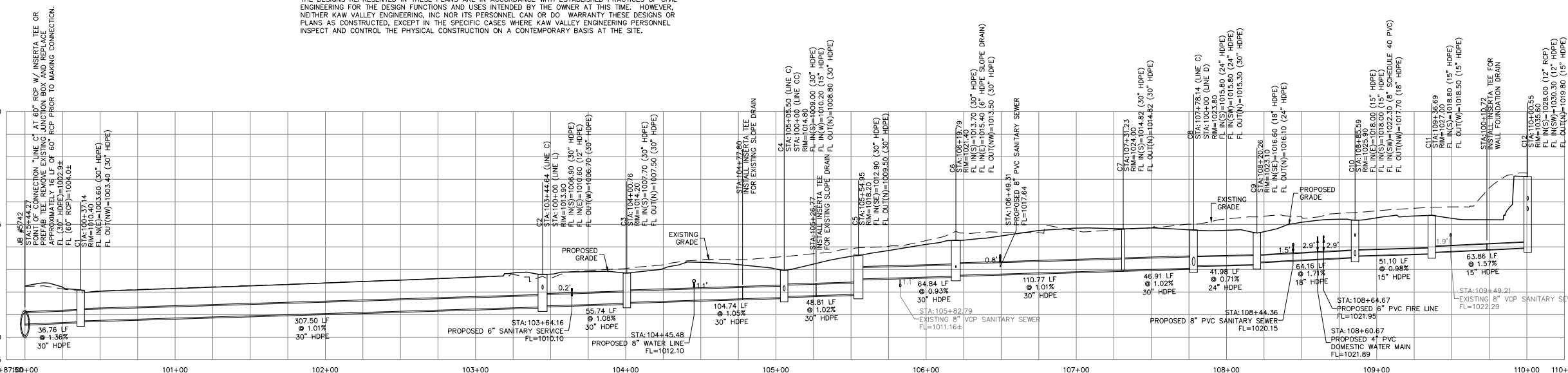
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PRIVATE STORM SEWER LINE C PROFILE



PROJ. NO. C20-0496
CITY: OASERPP.DWG
DSN: DOW
DWN: NUN
ENGINEER
MO # 2011037427
14700 WEST 114TH TERRACE
LENEXA, KANSAS 66215
PH. (913) 894-5150 | FAX (913) 894-5977
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Architectural Corporation
Missouri License No. 2018022991
June Doe
Architect
Date: MM/DD/YYYY
License No. A-00000000

REVISIONS	DESCRIPTION	DATE
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PROJECT NO: 0119-0100
DATE: October 13, 2020

PRIVATE STORM SEWER PLAN AND PROFILE

C620

50% Construction Documents

Lee's Summit High School

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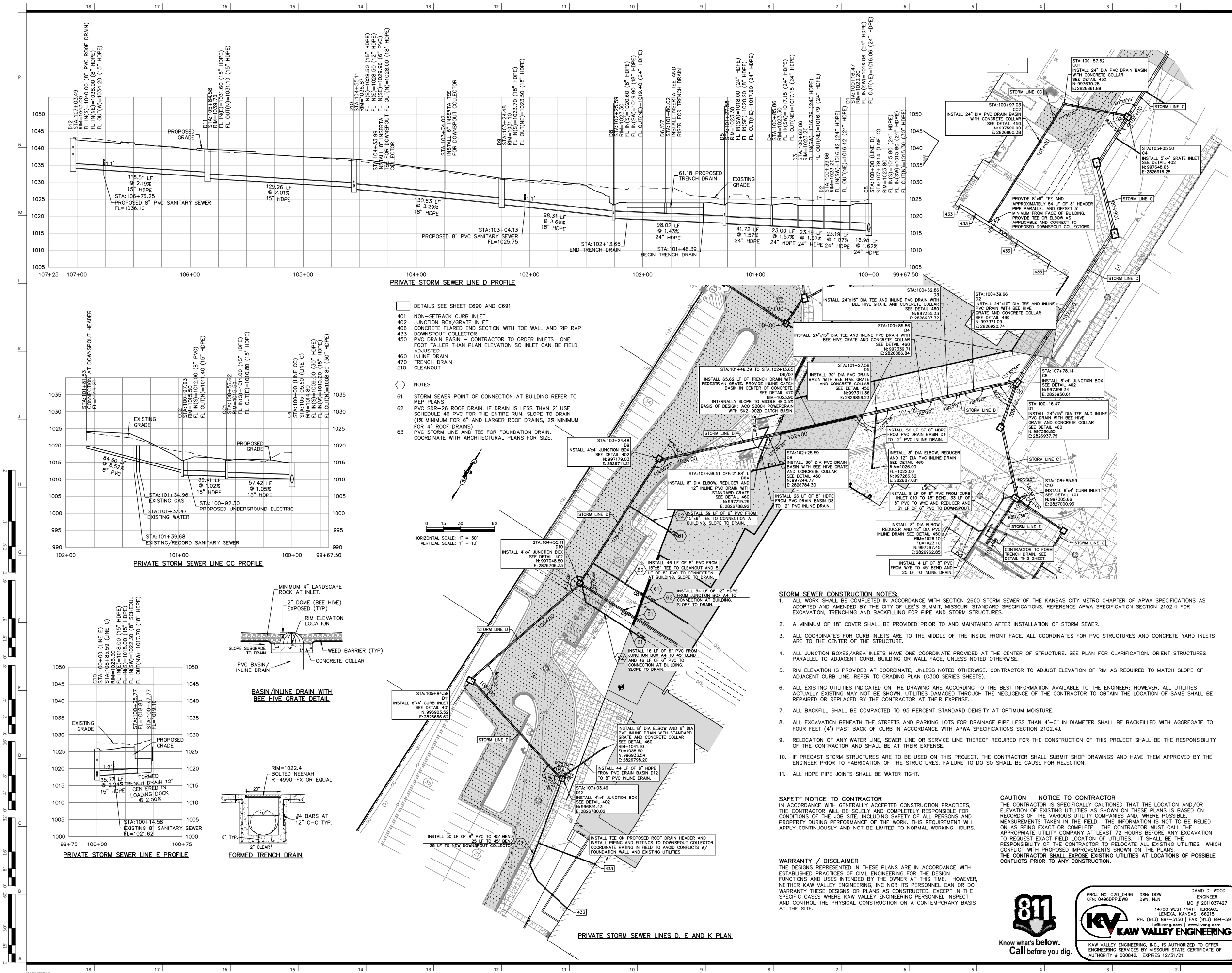
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PROJECT NO: 0119-0100
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**PRIVATE STORM SEWER
PLAN AND PROFILE**

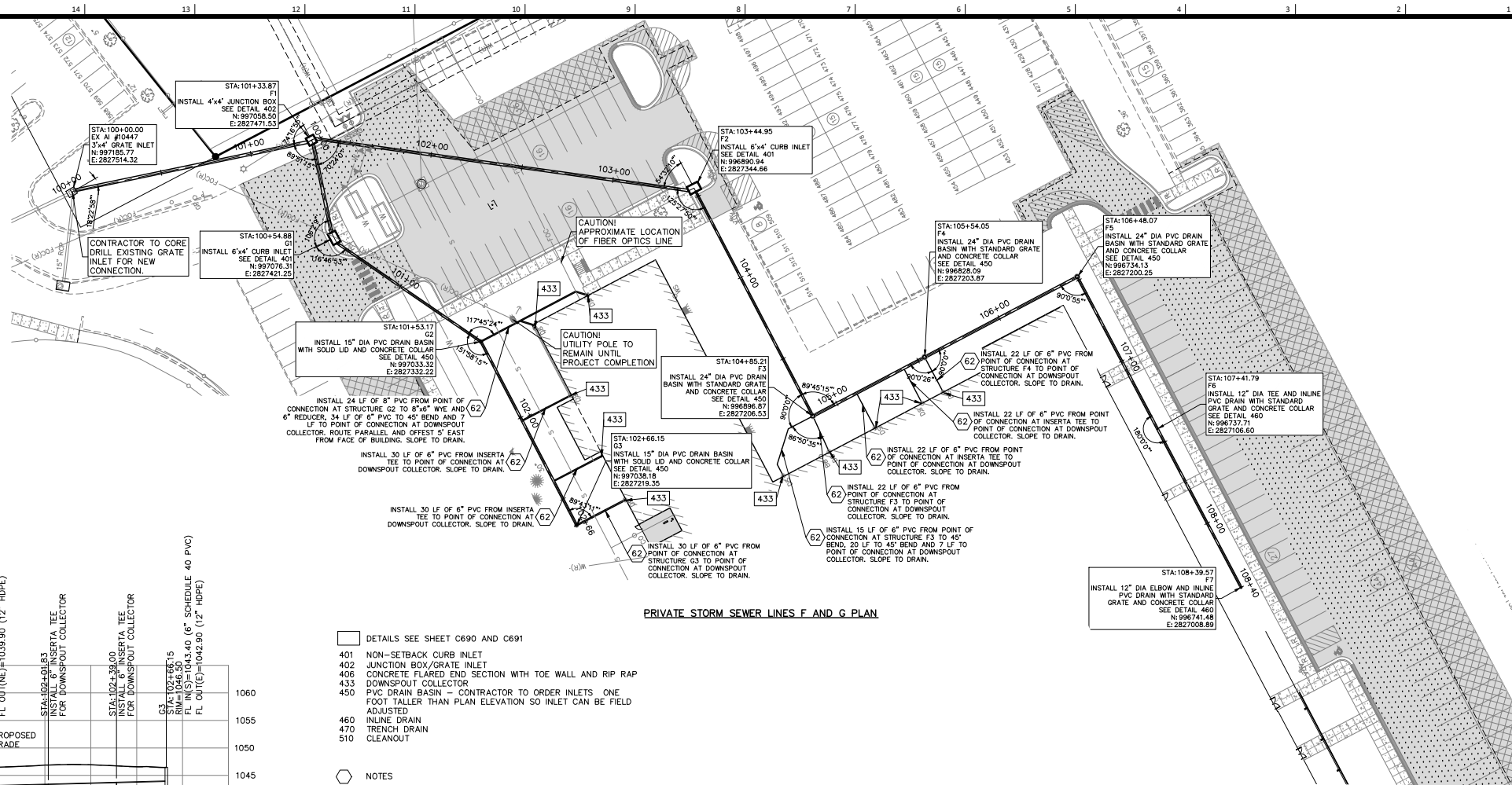
C630

50% Construction
Documents



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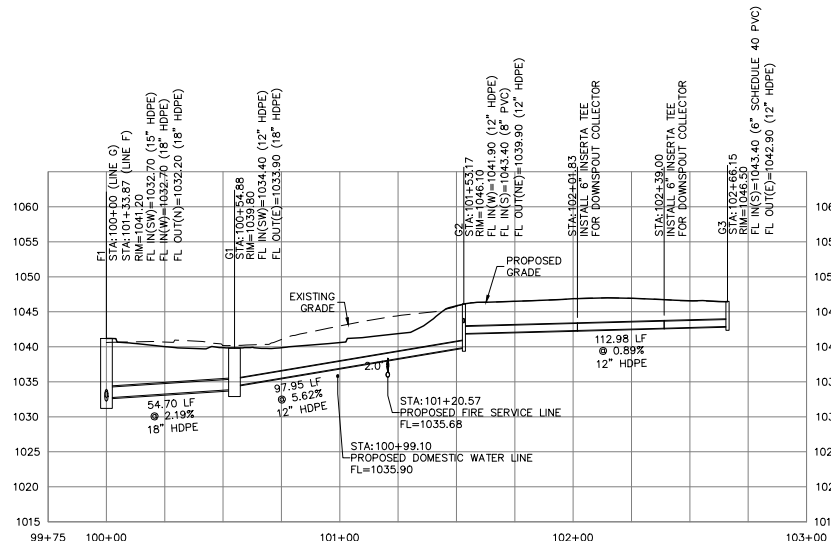


PRIVATE STORM SEWER LINES F AND G PLAN

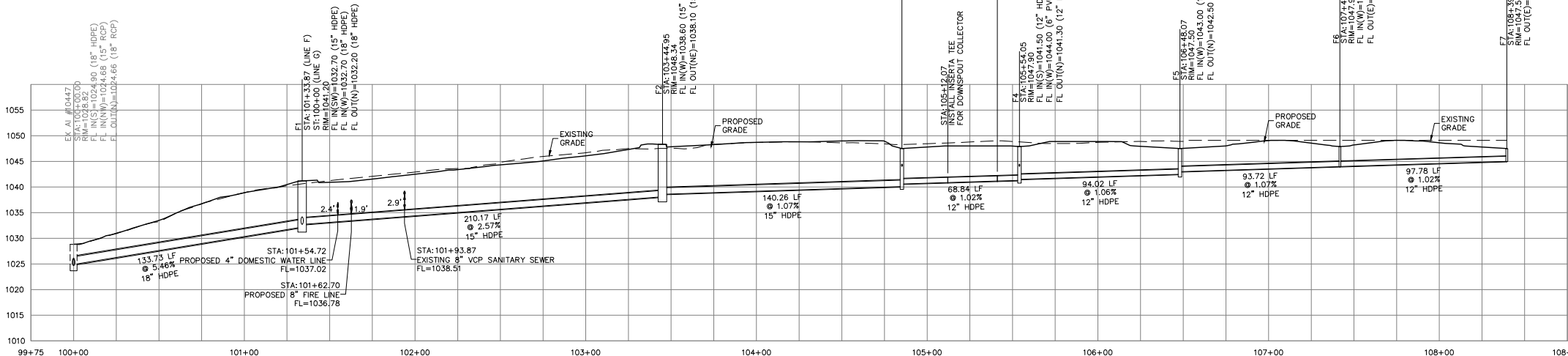
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PRIVATE STORM SEWER LINE G PROFILE



PRIVATE STORM SEWER LINE F PROFILE

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CITY: OASERPP.DWG

DAVID D. WOOD
ENGINEER
MO # 2011037427

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REVISIONS

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PROJECT NO: 0119-0100
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PRIVATE STORM SEWER PLAN AND PROFILE

C640

50% Construction Documents

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PROJECT NO: 0119-0100
DATE: October 13, 2020

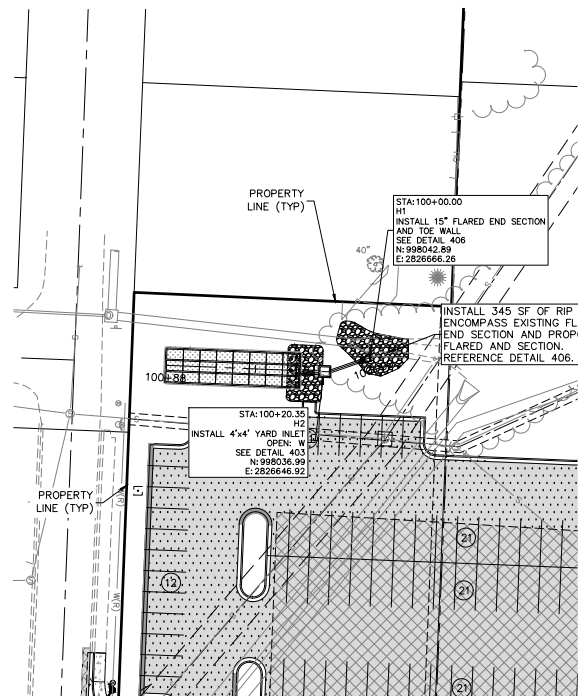
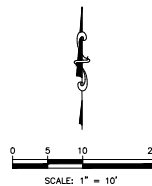
BMP PLAN

C660

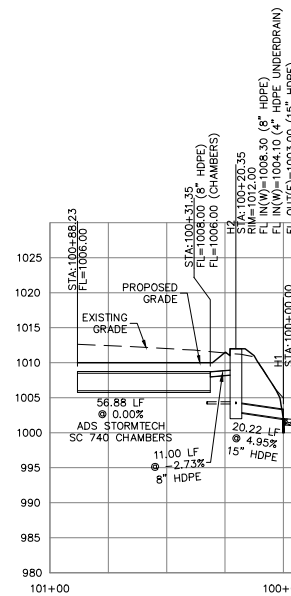
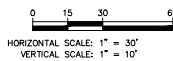
50% Construction Documents

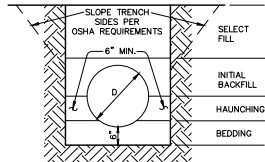
LEGEND:

- MONUMENT FOUND
ORIGIN UNKNOWN UNLESS
OTHERWISE NOTED
- 1/2"x24" REBAR
WAS 24" CAP SET
(UNLESS NOTED OTHERWISE)
- ⊕ BENCHMARK
- ⊙ CONTROL POINT
- ⊕ BUSH
- ⊕ CABLE TV PEDESTAL
- ⊕ DOWN SPOUT
- ⊕ DECIDUOUS TREE
- ⊕ ELECTRICAL TRANSFORMER
- ⊕ ELECTRIC METER
- FF FINISH FLOOR ELEVATION
- WOOD FENCE
- FIRE SPRINKLER VALVE
- UNDERGROUND GAS
- GATE POST
- GAS LINE RISER
- HDPE HIGH DENSITY POLYETHYLENE
- ⊕ LIGHT POLE
- ⊕ SPRINKLER CONTROL BOX
- ⊕ STORM SEWER MANHOLE
- STREET/TRAFFIC SIGN
- UNDERGROUND ELECTRIC
- UNDERGROUND TELEVISION
- ⊕ WALL MOUNTED LIGHT
- ⊕ WALL MOUNTED SIAMSE FIRE CONNECTOR
- EXISTING GRADE 1' CONTOUR
- EXISTING GRADE 5' CONTOUR
- PROPOSED ASPHALT PAVEMENT
- PROPOSED CONCRETE PAVEMENT
- SWALE



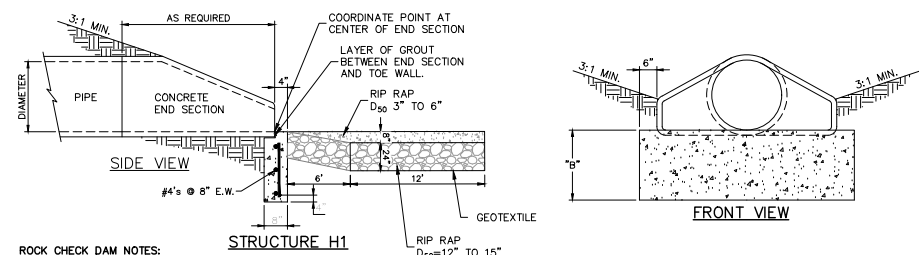
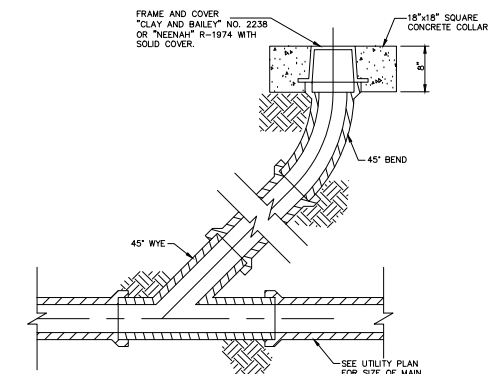
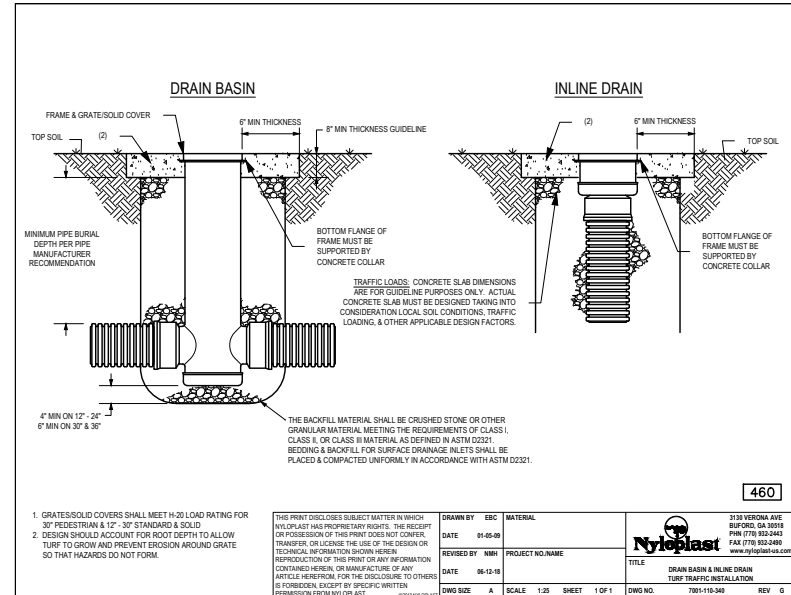
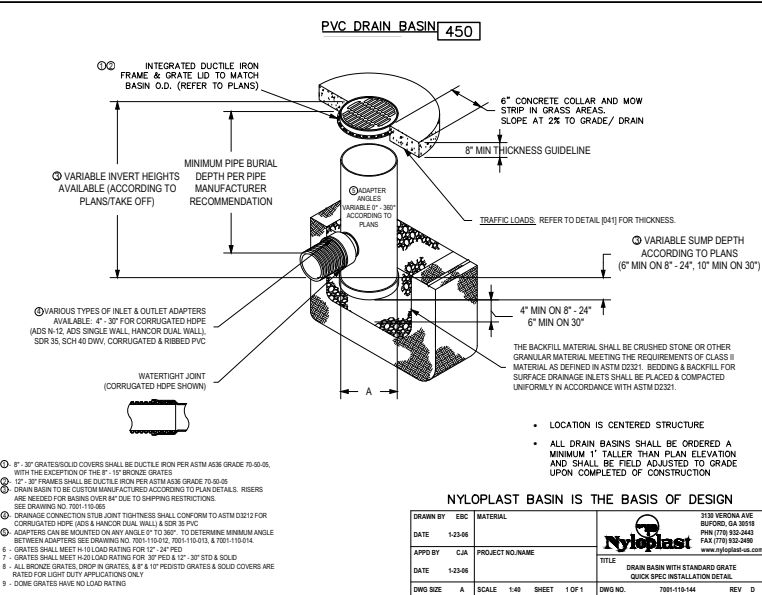
PRIVATE STORM SEWER LINE H PLAN





- FLEXIBLE PIPE: INCLUDES CORRUGATED METAL PIPE, CORRUGATED POLYETHYLENE PIPE AND/OR POLYVINYL CHLORIDE PIPE.
- BEDDING SHALL BE COMPACTED CRUSHED STONE AND SHALL BE SHARPED TO THE BOTTOM OF THE PIPE.
 - HAUNCHING AND INITIAL BACKFILL MATERIAL SHALL BE CLASS I OR II (REF. ASTM D2321) GRANULAR MATERIAL AND SHALL BE COMPACTED TO 95% STANDARD PROCTOR.

TRENCH AND BEDDING DETAILS
REFER TO KANSAS CITY METROPOLITAN
CHAPTER OF APWA SPECIFICATIONS SECTION
2102.4

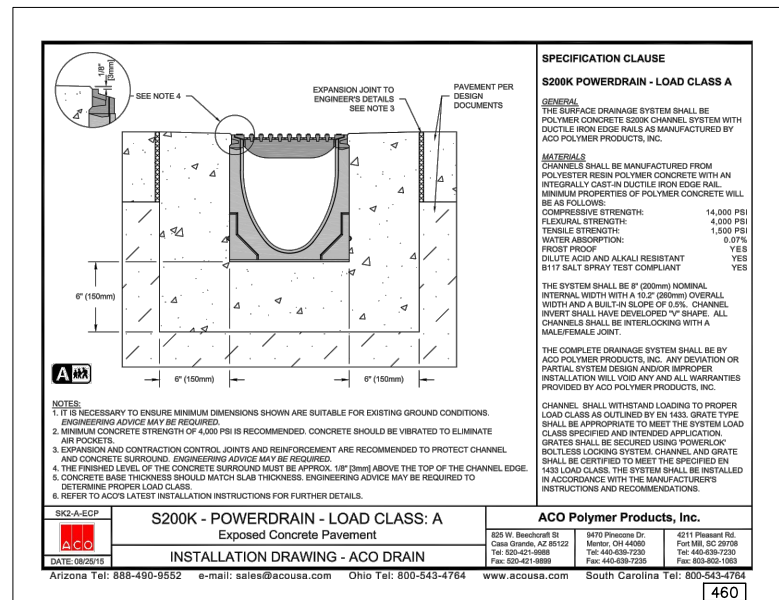


- ROCK CHECK DAM NOTES:**
- CONSTRUCTION SPECIFICATIONS & INSTALLATION:
 - THE MAXIMUM HEIGHT OF THE DAM SHALL BE 1 FEET. THE CENTER OF THE CHECK DAM IS AT THE SAME ELEVATION OF THE OUTER EDGES.
 - FOR ADDED STABILITY, THE BASE OF THE CHECK DAM SHALL BE KEYED INTO THE SOIL APPROXIMATELY 6 INCHES.
 - STONE SHOULD BE PLACED ACCORDING TO THE CONFIGURATION ABOVE. HAND OR MECHANICAL PLACEMENT WILL BE NECESSARY TO ACHIEVE COMPLETE COVERAGE OF THE DITCH OR SWALE AND TO INSURE THAT THE CENTER OF THE DAM IS LOWER THEN THE EDGES.
 - GEOTEXTILE MAY BE USED UNDER THE STONE TO PROVIDE A STABLE FOUNDATION AND TO FACILITATE REMOVAL OF THE STONE.
 - INSPECTION AND MAINTENANCE:
 - CHECK DAMS SHOULD BE CHECKED FOR SEDIMENT ACCUMULATION AFTER EACH STORM EVENT OF 1/2" OR GREATER. SEDIMENT SHOULD BE REMOVED WHEN IT REACHES 1/2 OF THE ORIGINAL HEIGHT OF THE DAM.
 - REGULAR INSPECTIONS SHOULD BE MADE TO ENSURE THAT THE CENTER OF THE DAM IS LOWER THEN THE EDGES. EROSION CAUSED BY HIGH FLOWS AROUND EDGES OF THE DAM SHOULD BE CORRECTED.

- NOTES:**
- THE DEPTH OF THE TOE WALL SHALL BE PER TABLE. IF BEDROCK IS ENCOUNTERED A MINIMUM OF 12" INTO BEDROCK IS REQUIRED.
 - ALL CONCRETE SHALL MEET APWA 2600 SPECIFICATIONS.

CONCRETE FLARED END SECTION
W/ TOE WALL AND RIP RAP STILLING BASIN

TABLE	
TOE WALL DEPTH	"b"
PIPE DIAMETER	"b"
12" - 21"	24"
24" - 48"	30"
54" - 66"	36"



PROJ. NO. C20-0496
CIN: 04560ET.DWG

DSN: DOW
DWN: HUN

DAVID D. WOOD
ENGINEER
MO # 2011037427

14700 WEST 114TH TERRACE
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KAW VALLEY ENGINEERING

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Lee's Summit High School

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Lee's Summit, MO 64063

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301 NE Tudor Road
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NOT FOR CONSTRUCTION

Architectural Corporation
Missouri License No.: 2018022991
June Doe Date: MM/DD/YYYY
License No. A-00000000

REVISIONS

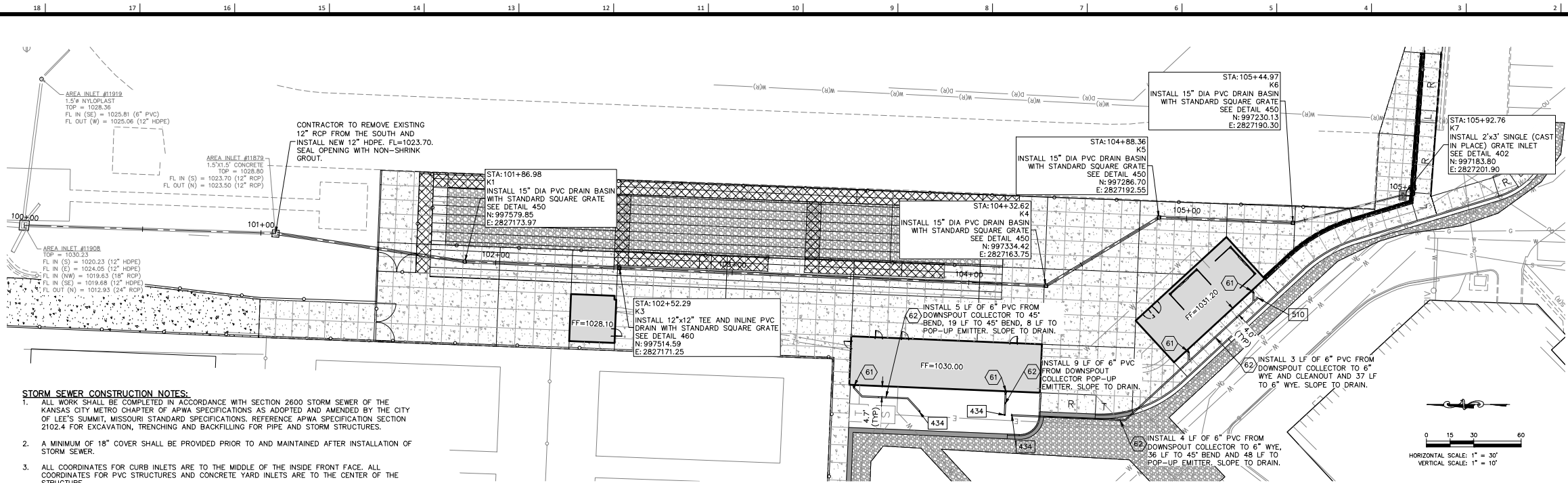
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PROJECT NO: 0119-0100
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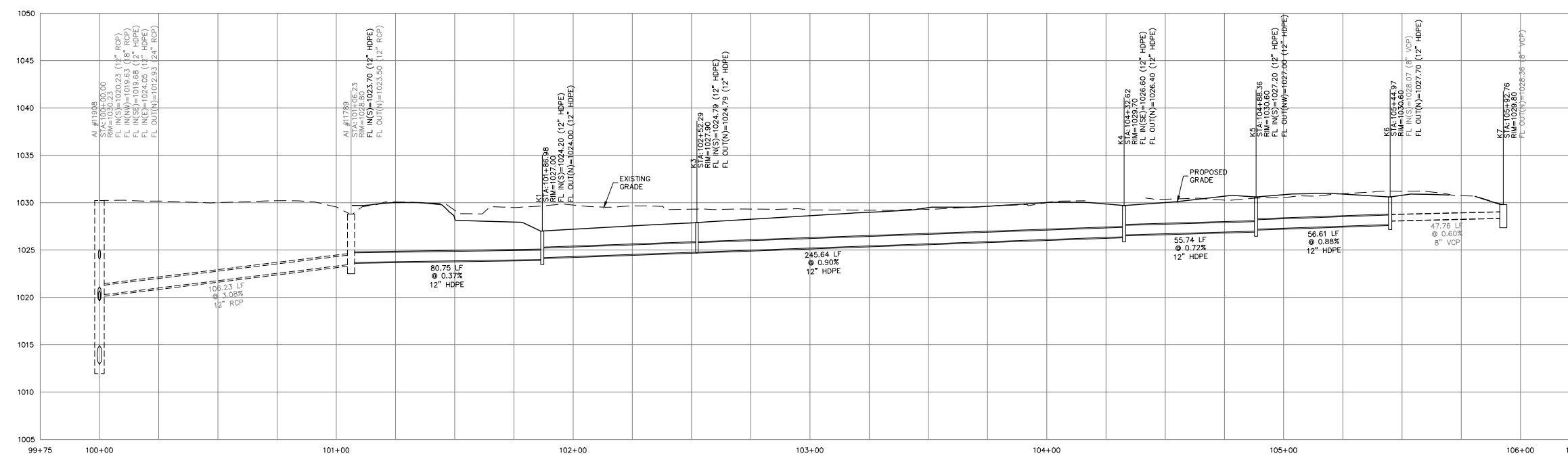
STORM SEWER DETAILS

C691

50% Construction Documents



- STORM SEWER CONSTRUCTION NOTES:**
- ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH SECTION 2600 STORM SEWER OF THE KANSAS CITY METRO CHAPTER OF APWA SPECIFICATIONS AS ADOPTED AND AMENDED BY THE CITY OF LEE'S SUMMIT, MISSOURI STANDARD SPECIFICATIONS, REFERENCE APWA SPECIFICATION SECTION 2102.4 FOR EXCAVATION, TRENCHING AND BACKFILLING FOR PIPE AND STORM STRUCTURES.
 - A MINIMUM OF 18" COVER SHALL BE PROVIDED PRIOR TO AND MAINTAINED AFTER INSTALLATION OF STORM SEWER.
 - ALL COORDINATES FOR CURB INLETS ARE TO THE MIDDLE OF THE INSIDE FRONT FACE. ALL COORDINATES FOR PVC STRUCTURES AND CONCRETE YARD INLETS ARE TO THE CENTER OF THE STRUCTURE.
 - ALL JUNCTION BOXES/AREA INLETS HAVE ONE COORDINATE PROVIDED AT THE CENTER OF STRUCTURE. SEE PLAN FOR CLARIFICATION. ORIENT STRUCTURES PARALLEL TO ADJACENT CURB, BUILDING OR WALL FACE, UNLESS NOTED OTHERWISE.
 - RIM ELEVATION IS PROVIDED AT COORDINATE, UNLESS NOTED OTHERWISE. CONTRACTOR TO ADJUST ELEVATION OF RIM AS REQUIRED TO MATCH SLOPE OF ADJACENT CURB LINE. REFER TO GRADING PLAN (C300 SERIES SHEETS).
 - ALL EXISTING UTILITIES INDICATED ON THE DRAWING ARE ACCORDING TO THE BEST INFORMATION AVAILABLE TO THE ENGINEER; HOWEVER, ALL UTILITIES ACTUALLY EXISTING MAY NOT BE SHOWN. UTILITIES DAMAGED THROUGH THE NEGLIGENCE OF THE CONTRACTOR TO OBTAIN THE LOCATION OF SAME SHALL BE REPAIRED OR REPLACED BY THE CONTRACTOR AT THEIR EXPENSE.
 - ALL BACKFILL SHALL BE COMPACTED TO 95 PERCENT STANDARD DENSITY AT OPTIMUM MOISTURE.
 - ALL EXCAVATION BENEATH THE STREETS AND PARKING LOTS FOR DRAINAGE PIPE LESS THAN 4'-0" IN DIAMETER SHALL BE BACKFILLED WITH AGGREGATE TO FOUR FEET (4') PAST BACK OF CURB IN ACCORDANCE WITH APWA SPECIFICATIONS SECTION 2102.4J.
 - RELOCATION OF ANY WATER LINE, SEWER LINE OR SERVICE LINE THEREOF REQUIRED FOR THE CONSTRUCTION OF THIS PROJECT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR AND SHALL BE AT THEIR EXPENSE.
 - IF PRECAST STORM STRUCTURES ARE TO BE USED ON THIS PROJECT, THE CONTRACTOR SHALL SUBMIT SHOP DRAWINGS AND HAVE THEM APPROVED BY THE ENGINEER PRIOR TO FABRICATION OF THE STRUCTURES. FAILURE TO DO SO SHALL BE CAUSE FOR REJECTION.
 - ALL HDPE PIPE JOINTS SHALL BE WATER TIGHT.



SAFETY NOTICE TO CONTRACTOR

IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.

WARRANTY / DISCLAIMER

THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER KAW VALLEY ENGINEERING, INC NOR ITS PERSONNEL CAN OR DO WARRANTY THESE DESIGNS OR PLANS AS CONSTRUCTED, EXCEPT IN THE SPECIFIC CASES WHERE KAW VALLEY ENGINEERING PERSONNEL INSPECT AND CONTROL THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

CAUTION - NOTICE TO CONTRACTOR

THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 72 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLANS. THE CONTRACTOR SHALL EXPOSE EXISTING UTILITIES AT LOCATIONS OF POSSIBLE CONFLICTS PRIOR TO ANY CONSTRUCTION.

811

Know what's below.
Call before you dig.

PROJ. NO. C20_0496
CITY: OASDPR.DWG
DSN: DOW
DWN: NUN
ENGINEER
MO # 2011037427
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mechanical/electrical engineer:
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816.663.8700

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DAVID D. WOOD
NUMBER
PE-2011037427
PROFESSIONAL ENGINEER

Kaw Valley Engineering, Inc.
Missouri Certificate of Authority: 000842
David Wood
Engineer
Date: 09/28/2020
License No. PE-2011037427

REVISIONS		
Number	DESCRIPTION	DATE

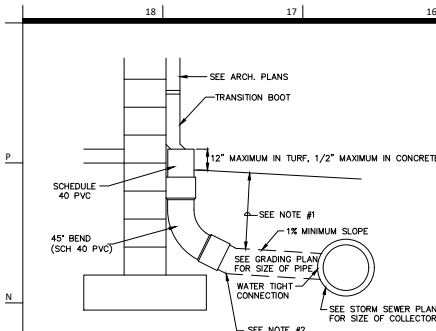
PROJECT NO: 0119-0100
DATE: SEPTEMBER 28, 2020

**STORM SEWER
PLAN AND PROFILE**

H-C600

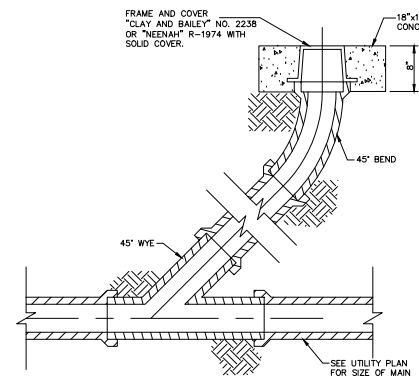
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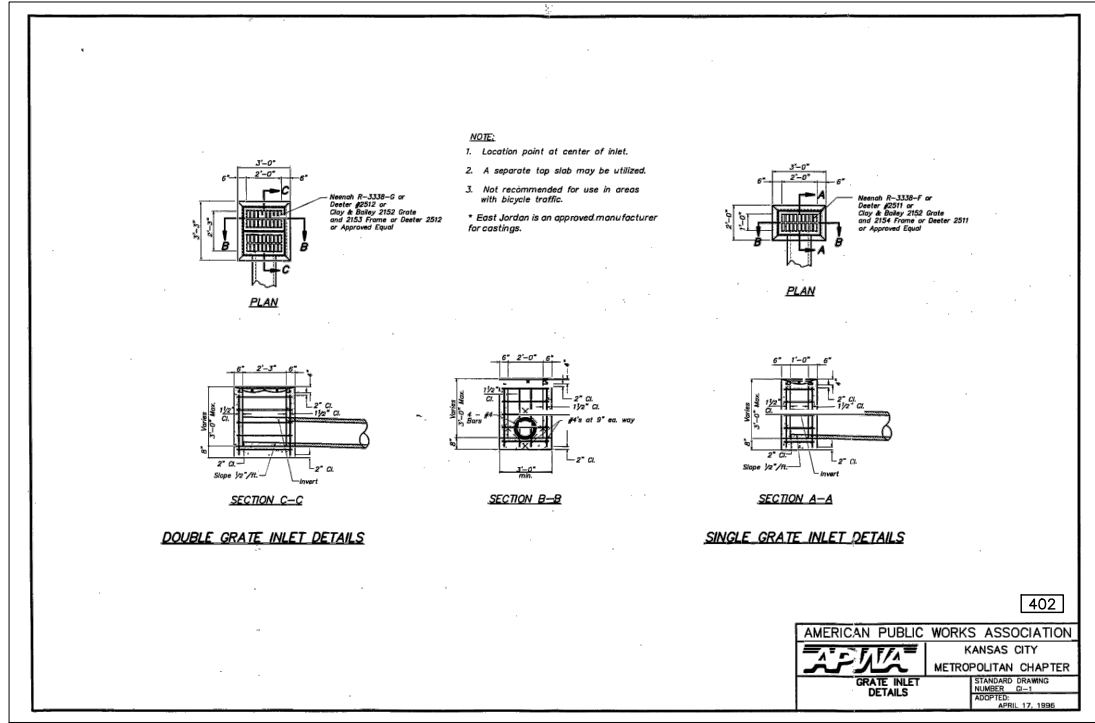
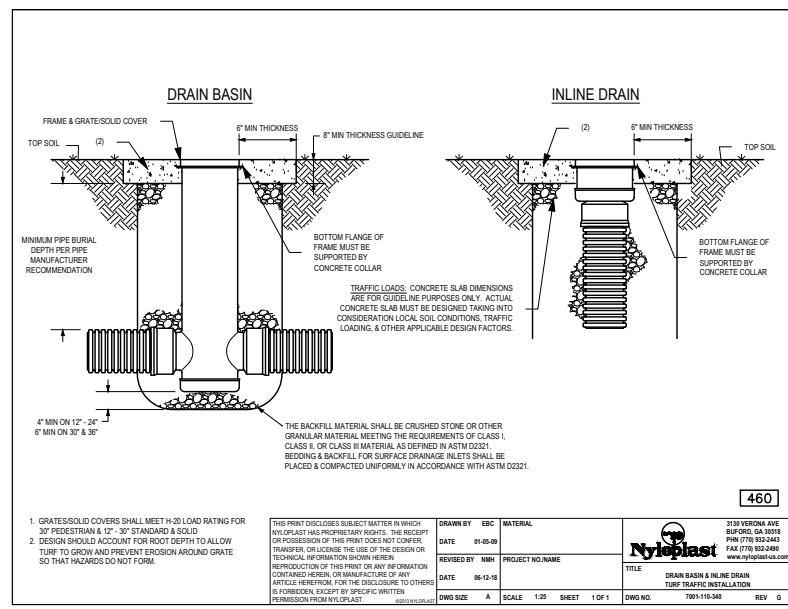
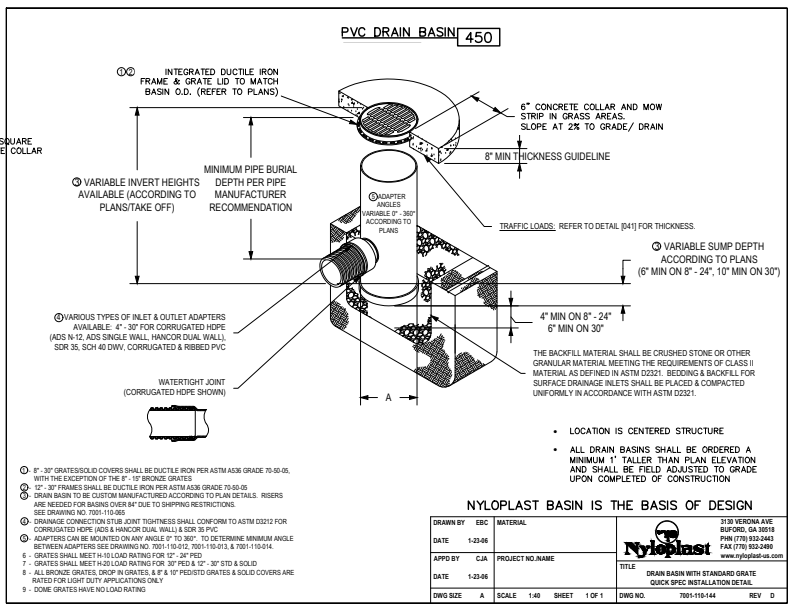


NOTES:
1) FOR ALL DEPTHS OF COVER LESS THAN TWO (2) FEET, PIPE MUST BE SCHEDULE 40 PVC. FOR DEPTHS OF COVER GREATER THAN TWO (2) FEET, FLEXIBLE PIPE MAY BE USED. REFER TO SPECIFICATIONS FOR ALLOWABLE PIPE TYPES.
2) A WATERTIGHT CONNECTION SHALL BE MAINTAINED WITH ANY TRANSITION FROM SCHEDULE 40 PVC PIPE TO ANY OTHER PIPE TYPE.
3) THE DOWNSPOUT COLLECTOR DRAIN SHALL BE INSTALLED BEFORE THE DOWNSPOUTS ARE INSTALLED ON THE BUILDING. SITEWORK CONTRACTOR SHALL BE RESPONSIBLE FOR ALL WORK TO AND INCLUDING THE RODENT SCREEN. BUILDING CONTRACTOR SHALL BE RESPONSIBLE FOR THE CONNECTION AT THE POINT OF THE RODENT SCREEN.

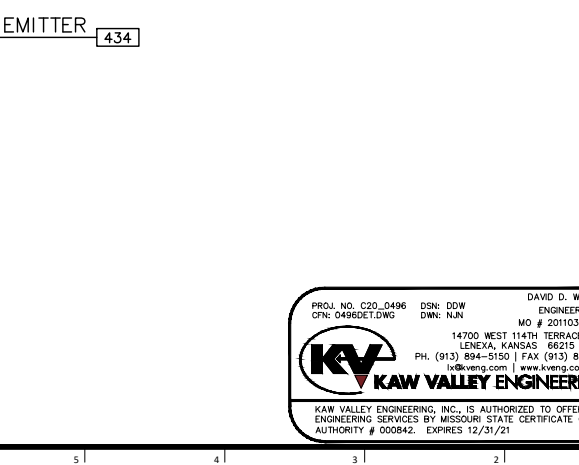
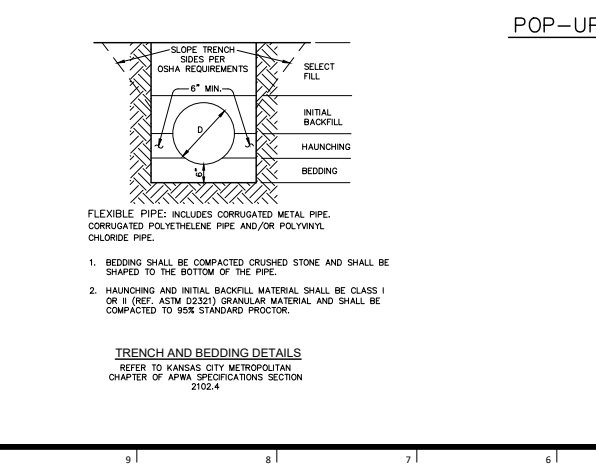
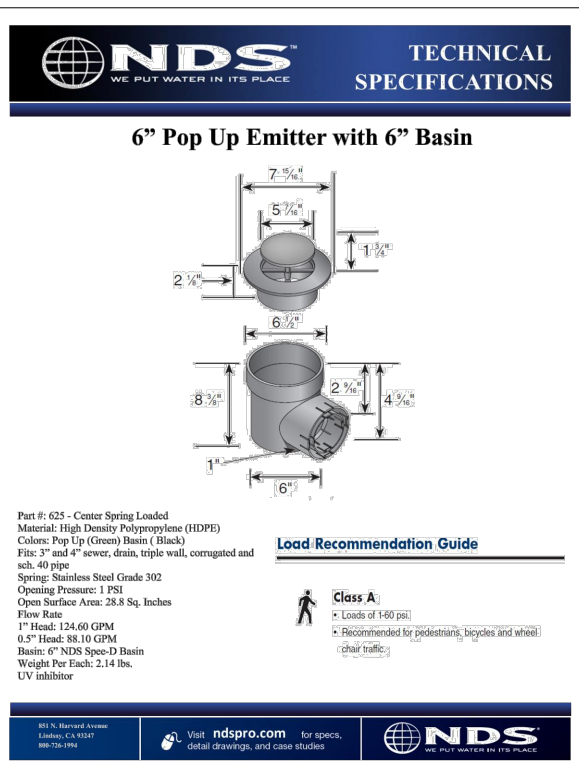
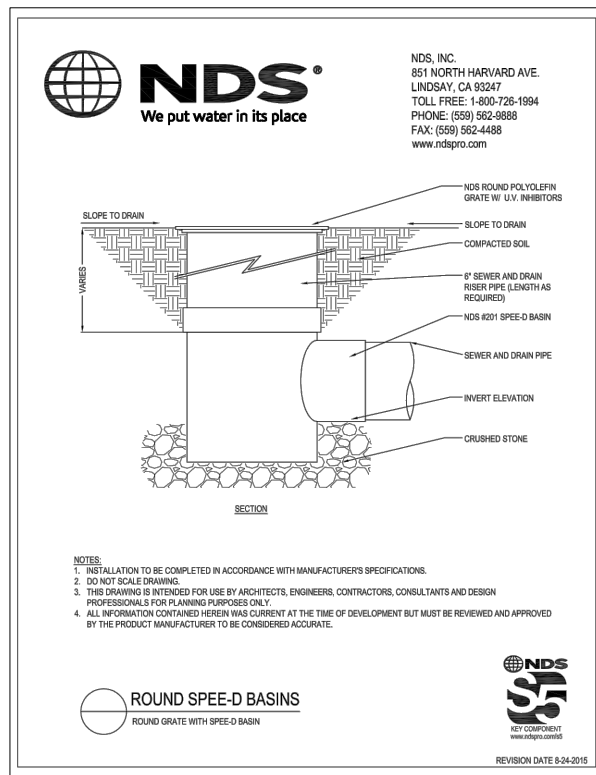
DOWNSPOUT COLLECTOR 433



CLEAN-OUT 510



INLET NOTES
GENERAL
1. ALL STORM SEWER STRUCTURES SHALL BE POURED IN PLACE.
2. DO NOT SCALE THESE DRAWINGS FOR DIMENSIONS OR CLEARANCES. ANY QUESTIONS REGARDING DIMENSIONS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO CONSTRUCTION.
3. THE FIRST DIMENSION LISTED IN THE CONSTRUCTION NOTES IS THE "L" DIMENSION, THE SECOND DIMENSION IS THE "W" DIMENSION, THE CONCRETE THICKNESS AND REINFORCEMENT SHOWN IS FOR BOXES WITH ("L"x"W") AND ("W"x"H") LESS THEN OR EQUAL TO 20, A SPECIAL DESIGN IS REQUIRED. PRECASTER SHALL PROVIDE DESIGN CALCULATIONS FOR DEEP STRUCTURES TO ENGINEER PRIOR TO CONSTRUCTING BOX.
CONCRETE
4. CONCRETE USED IN THIS WORK SHALL BE CLASS "A" CONCRETE (AE) THROUGHOUT, AND SHALL MEET THE REQUIREMENTS OF THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.
5. CONCRETE CONSTRUCTION SHALL MEET THE APPLICABLE REQUIREMENTS OF STANDARD SPECIFICATIONS FOR MOBS, LATEST EDITION, EXCEPT AS MODIFIED IN THE APWA TECHNICAL SPECIFICATIONS.
6. INLET FLOORS SHALL BE SHAPED WITH NON-REINFORCED CONCRETE INVERTS TO PROVIDE SMOOTH FLOW.
7. BEVEL ALL EXPOSED EDGES WITH 3/4" TRIANGULAR MOLDING.
8. 6" SOLID CONCRETE BLOCK OR BRICK MAY BE USED IN WALLS IN LIEU OF POURED CONCRETE WHERE NEITHER "H"x"L" NOR "H"x"W" (IN FEET) EXCEED FOURTEEN. BLOCK OR BRICK MAY BE USED IN ANY BOX WHERE "H" IS 9' OR LESS.
9. ALL CRUSHED STONE USED AS AGGREGATE FOR CONCRETE CONSTRUCTION SHALL BE OBTAINED FROM QUARRIES AND BEDS DESIGNATED BY THE MISSOURI DEPARTMENT OF TRANSPORTATION AS MEETING DURABILITY REQUIREMENTS OF KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.
REINFORCING STEEL
10. REINFORCING STEEL SHALL BE NEW BILLET, MINIMUM GRADE 60 AS PER ASTM A615, AND SHALL BE BENT COLD.
11. ALL DIMENSIONS RELATIVE TO REINFORCING STEEL ARE TO CENTERLINE OF BARS. 2" CLEARANCE SHALL BE PROVIDED THROUGHOUT UNLESS NOTED OTHERWISE. TOLERANCE OF +/- 3/8" SHALL BE PERMITTED.
12. ALL LAP SPLICES NOT SHOWN SHALL BE A MINIMUM OF 40 BAR DIAMETERS IN LENGTH.
13. ALL REINFORCING STEEL SHALL BE SUPPORTED ON FABRICATED STEEL BAR SUPPORTS @ 3'-0" MAXIMUM SPACING.
14. ALL DOWELS SHALL BE ACCURATELY PLACED AND SECURELY TIED IN PLACE PRIOR TO PLACEMENT OF BOTTOM SLAB CONCRETE. STICKING OF DOWELS INTO FRESH OR PARTIALLY HARDENED CONCRETE WILL NOT BE ACCEPTABLE.
CONSTRUCTION
15. THE BOTTOM SLAB SHALL BE AT LEAST 24 HOURS OLD BEFORE PLACING SIDEWALL CONCRETE. ALL SIDEWALL FORMS SHALL REMAIN IN PLACE A MINIMUM OF 24 HOURS AFTER SIDEWALLS ARE POURED BEFORE REMOVAL, AND AFTER REMOVAL, SHALL BE IMMEDIATELY TREATED WITH MEMBRANE CURING COMPOUND.
16. MATERIAL SELECTION AND COMPACTION REQUIREMENTS FOR BACKFILL AROUND STRUCTURES SHALL BE AS SPECIFIED IN THE KANSAS CITY METROPOLITAN CHAPTER OF THE APWA TECHNICAL SPECIFICATIONS.



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Athletics Facilities**

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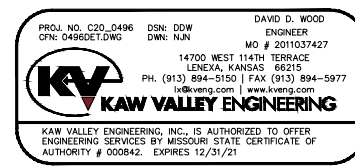
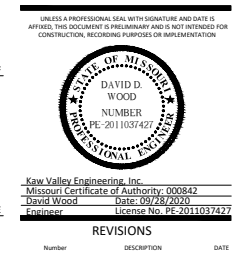
mechanical/electrical engineer:
Henderson Engineers
1801 Main St
Kansas City, MO 64108
816.663.8700

PROJECT NO: 0119-0100
DATE: SEPTEMBER 28, 2020

STORM DETAILS

H-C690

BID SET



Extended Dry Detention Basin Design			
Tributary Area	0.78 AC		0.78 Acres
Impervious Area	0.69 AC	88%	84 CN
Pervious Area	0.09 AC	12%	
Treatment Volume (from PondPack)	3180 ft ³		
WQv Storage Elevation	1008		
Basin Bottom Elevation Above Sediment Deposition	N/A		
Water Quality Outlet, Perforated Riser Pipe/Underlain (24-hour draw down)			
Depth of WQV at outlet:	3.9 ft		
Average Head of WQV over invert of orifice:	1.95 ft		
Average WQV outflow rate:	0.0367 cfs		
Utilize 1" Orifice in Screw in Cap			

I. Basin Water Quality Storage Volume			
Step 1) Tributary Area to EDOB, A _t (ac)	A _t (ac)=	0.78	
Step 2) Calculate WQv, using methodology in Section 6	WQ _v (ac-ft)=	0.0730	3,179.88 CF
Step 3) Add 20 percent to account for silt and sediment deposition	V _{storage} (ac-ft)=	0.0876	3,815.86 CF

III. Flood Control			
Refer to APWA Specifications Section 5608			
Notes:			
IV. Trash Racks			
Step 1) Total outlet area, A _{out} (in ²)	A _{out} (in ²)=	N/A	
Step 2) Required trash rack open area, A _r (in ²)	A _r (in ²)=	N/A	
--not applicable for perforated riser--			

V. Basin Shape			
Step 1) Length to width ratio should be at least 3:1 (L:W) wherever practicable	(L:W)=	3:1	
Step 2) Low flow channel side lining (Concrete, Soil/Riprap, None, or Specify)	Lining Type=	Soil/Riprap	
Step 3) Top stage floor drainage slope (toward low flow channel), S _u (%)	S _u (%)=	2	
Top stage depth, D _u (ft)	D _u (ft)=	4.5	
Step 4) Bottom stage volume, V _{bs} (ac-ft)	V _{bs} (% of WQ _v)=	-	
VI. Forebay (Optional)			
Step 1) Volume should be greater than 10% of WQ _v	Min V _{fb} (ac-ft)=	0.0073	
Step 2) Forebay depth, Z _{fb} (ft)	Z _{fb} (ft)=	0.5	
Step 3) Forebay surface area, A _{fb} (ac)	Min A _{fb} (ac)=	0.0146	
Step 4) Paved/hard bottom and sides?	Yes or No	No	

VII. Basin Side Slopes			
Step 1) Basin side slopes should be at least 4:1 (H:V)	Basin SS (H:V)=	3:1	Max

VIII. Dam Embankment Side Slopes			
Step 1) Dam embankment slopes should be at least 3:1 (H:V)	Dam Emb. SS (H:V)=	3:1	

IX. Vegetation			
Step 1) Native Grass, Irrigated Turf Grass, Specify	Vegetation Type=	Native	

X. Inlet Protection			
Step 1) Indicate method of inlet protection/energy dissipation at EDOB inlet	Inlet Protection=	Riprap	

XI. Access			
Step 1) Indicate that access has been provided for maintenance vehicles	Is Access Provided=	Yes	

WQv release rate		# of holes	# of holes req'd	# holes	Total discharge	Time to
orifice size	discharge cfs	duration hr	req'd (d/s)	used	(cfs)	empty (hrs)
1/32	0.0000	24664.33	1027.68	616.63	0.0000	#DIV/0!
1/16	0.0001	6166.08	256.92	154.15	0.0000	#DIV/0!
3/32	0.0003	2740.48	114.19	68.51	0.0000	#DIV/0!
1/8	0.0006	1541.52	64.23	38.54	0.0000	#DIV/0!
5/32	0.0009	986.57	42.11	24.66	0.0000	#DIV/0!
3/16	0.0013	686.12	28.55	17.13	0.0000	#DIV/0!
7/32	0.0018	503.35	20.97	12.58	0.0000	#DIV/0!
1/4	0.0023	385.38	16.06	9.63	0.0000	#DIV/0!
9/32	0.0029	304.50	12.69	7.61	0.0000	#DIV/0!
5/16	0.0036	246.64	10.28	6.17	0.0000	#DIV/0!
11/32	0.0043	203.84	8.49	5.10	0.0000	#DIV/0!
3/8	0.0052	171.28	7.14	4.38	0.0000	#DIV/0!
13/32	0.0061	145.94	6.08	3.65	0.0000	#DIV/0!
7/16	0.0070	125.84	5.24	3.15	0.0000	#DIV/0!
15/32	0.0081	106.62	4.57	2.74	0.0000	#DIV/0!
1/2	0.0092	96.35	4.03	2.41	0.0000	#DIV/0!
17/32	0.0103	85.34	3.56	2.13	0.0000	#DIV/0!
9/16	0.0116	76.12	3.17	1.90	0.0000	#DIV/0!
19/32	0.0129	68.32	2.85	1.71	0.0000	#DIV/0!
5/8	0.0143	61.66	2.57	1.54	0.0000	#DIV/0!
21/32	0.0158	55.93	2.33	1.40	0.0000	#DIV/0!
11/16	0.0173	50.96	2.12	1.27	0.0000	#DIV/0!
23/32	0.0189	46.62	1.94	1.17	0.0000	#DIV/0!
3/4	0.0206	42.82	1.78	1.07	0.0206	42.82
25/32	0.0224	39.46	1.64	0.99	0.0000	#DIV/0!
13/16	0.0242	36.49	1.52	0.91	0.0000	#DIV/0!
27/32	0.0261	33.83	1.41	0.85	0.0000	#DIV/0!
7/8	0.0281	31.46	1.31	0.79	0.0000	#DIV/0!
29/32	0.0301	29.33	1.22	0.73	0.0000	#DIV/0!
15/16	0.0322	27.40	1.14	0.69	0.0000	#DIV/0!
31/32	0.0344	25.67	1.07	0.64	0.0000	#DIV/0!
1	0.0367	24.09	1.00	0.60	1	0.0367 24.09
1 1/32	0.0390	22.65	0.94	0.57	0.0000	#DIV/0!
1 1/16	0.0414	21.34	0.89	0.53	0.0000	#DIV/0!
1 3/32	0.0439	20.13	0.84	0.50	0.0000	#DIV/0!
1 1/8	0.0464	19.03	0.79	0.48	0.0000	#DIV/0!
1 5/32	0.0490	18.02	0.75	0.45	0.0000	#DIV/0!
1 3/16	0.0517	17.08	0.71	0.43	0.0000	#DIV/0!
1 7/32	0.0545	16.22	0.68	0.41	0.0000	#DIV/0!
1 1/4	0.0573	15.42	0.64	0.39	0.0000	#DIV/0!
1 9/32	0.0602	14.67	0.61	0.37	0.0000	#DIV/0!
1 5/16	0.0632	13.98	0.58	0.35	0.0000	#DIV/0!
1 11/32	0.0662	13.34	0.56	0.33	0.0000	#DIV/0!
1 3/8	0.0693	12.74	0.53	0.32	0.0000	#DIV/0!
1 13/32	0.0725	12.18	0.51	0.30	0.0000	#DIV/0!
1 7/16	0.0758	11.66	0.49	0.29	0.0000	#DIV/0!
1 15/32	0.0791	11.17	0.47	0.28	0.0000	#DIV/0!
1 1/2	0.0825	10.71	0.45	0.27	0.0000	#DIV/0!
1 17/32	0.0860	10.27	0.43	0.26	0.0000	#DIV/0!
1 9/16	0.0895	9.87	0.41	0.25	0.0000	#DIV/0!
1 19/32	0.0931	9.48	0.40	0.24	0.0000	#DIV/0!
1 5/8	0.0968	9.12	0.38	0.23	0.0000	#DIV/0!
1 21/32	0.1006	8.78	0.37	0.22	0.0000	#DIV/0!
1 11/16	0.1044	8.46	0.35	0.21	0.0000	#DIV/0!
1 23/32	0.1083	8.15	0.34	0.20	0.0000	#DIV/0!
1 3/4	0.1123	7.86	0.33	0.20	0.0000	#DIV/0!
1 25/32	0.1164	7.59	0.32	0.19	0.0000	#DIV/0!
1 13/16	0.1206	7.33	0.31	0.18	0.0000	#DIV/0!
1 27/32	0.1247	7.09	0.30	0.18	0.0000	#DIV/0!
1 7/8	0.1289	6.85	0.29	0.17	0.0000	#DIV/0!
1 29/32	0.1333	6.63	0.28	0.17	0.0000	#DIV/0!
1 15/16	0.1377	6.42	0.27	0.16	0.0000	#DIV/0!
1 31/32	0.1421	6.21	0.26	0.16	0.0000	#DIV/0!
2	0.1467	6.02	0.25	0.15	0.0000	#DIV/0!

Orifice Flow - Circular		Q=C _d A(2gh) ^{1/2}				Hw/D	
Orifice size	Q (cfs)	A (ft ²)	h (in.)	C	h (ft)	Q (cfs)	Hw/D
1/32	0.0313	0.000	0.0008	0.6	1.95	0.000	748.80
1/16	0.0625	0.000	0.0031	0.6	1.95	0.000	374.40
3/32	0.0938	0.000	0.0069	0.6	1.95	0.000	248.60
1/8	0.1250	0.000	0.0123	0.6	1.95	0.001	187.20
5/32	0.1563	0.000	0.0192	0.6	1.95	0.001	148.76
3/16	0.1875	0.000	0.0276	0.6	1.95	0.001	124.80
7/32	0.2188	0.000	0.0376	0.6	1.95	0.002	106.97
1/4	0.2500	0.000	0.0491	0.6	1.95	0.002	93.60
9/32	0.2813	0.000	0.0621	0.6	1.95	0.003	83.60
5/16	0.3125	0.001	0.0767	0.6	1.95	0.004	74.88
11/32	0.3438	0.001	0.0928	0.6	1.95	0.004	68.07
3/8	0.3750	0.001	0.1104	0.6	1.95	0.005	62.40
13/32	0.4063	0.001	0.1296	0.6	1.95	0.006	57.60
7/16	0.4375	0.001	0.1503	0.6	1.95	0.007	53.49
15/32	0.4688	0.001	0.1726	0.6	1.95	0.008	49.92
1/2	0.5000	0.001	0.1963	0.6	1.95	0.009	46.80
17/32	0.5313	0.002	0.2217	0.6	1.95	0.010	44.05
9/16	0.5625	0.002	0.2485	0.6	1.95	0.012	41.60
19/32	0.5938	0.002	0.2769	0.6	1.95	0.013	39.41
5/8	0.6250	0.002	0.3068	0.6	1.95	0.014	37.44
21/32	0.6563	0.002	0.3382	0.6	1.95	0.016	35.66
11/16	0.6875	0.003	0.3712	0.6	1.95	0.017	34.04
23/32	0.7188	0.003	0.4057	0.6	1.95	0.019	32.56
3/4	0.7500	0.003	0.4418	0.6	1.95	0.021	31.20
25/32	0.7813	0.003	0.4794	0.6	1.95	0.022	29.95
13/16	0.8125	0.004	0.5185	0.6	1.95	0.024	28.80
27/32	0.8438	0.004	0.5591	0.6	1.95	0.026	27.73
7/8	0.8750	0.004	0.6013	0.6	1.95	0.028	26.74
29/32	0.9063	0.004	0.6450	0.6	1.95	0.030	25.82
15/16	0.9375	0.005	0.6903	0.6	1.95	0.032	24.95
31/32	0.9688	0.005	0.7371	0.6	1.95	0.034	24.15
1	1.0000	0.005	0.7854	0.6	1.95	0.037	23.40
1 1/32	1.0313	0.006	0.8353	0.6	1.95	0.039	22.69
1 1/16	1.0625	0.006	0.8866	0.6	1.95	0.041	22.02
1 3/32	1.0938	0.007	0.9396	0.6	1.95	0.044	21.39
1 1/8	1.1250	0.007	0.9940	0.6	1.95	0.046	20.80
1 5/32	1.1563	0.007	1.0500	0.6	1.95	0.049	20.24
1 3/16	1.1875	0.008	1.1075	0.6	1.95	0.052	19.71
1 7/32	1.2188	0.008	1.1666	0.6	1.95	0.054	19.20
1 1/4	1.2500	0.009	1.2272	0.6	1.95	0.057	18.72
1 9/32	1.2813	0.009	1.2893	0.6	1.95	0.060	18.26
1 5/16	1.3125	0.009	1.3530	0.6	1.95	0.063	17.83
1 11/32	1.3438	0.010	1.4182	0.6	1.95	0.066	17.41
1 3/8	1.3750	0.010	1.4849	0.6	1.95	0.069	17.02
1 13/32	1.4063	0.011	1.5532	0.6	1.95	0.073	16.64
1 7/16	1.4375	0.011	1.6230	0.6	1.95	0.076	16.28
1 15/32	1.4688	0.012	1.6943	0.6	1.95	0.079	15.93
1 1/2	1.5000	0.012	1.7671	0.6	1.95	0.083	15.60
1 17/32	1.5313	0.013	1.8415	0.6	1.95	0.086	15.28
1 9/16	1.5625	0.013	1.9175	0.6	1.95	0.090	14.98
1 19/32	1.5938	0.014	1.9949	0.6	1.95	0.093	14.68
1 5/8	1.6250	0.014	2.0739	0.6	1.95	0.097	14.40
1 21/32	1.6563	0.015	2.1545	0.6	1.95	0.101	14.13
1 23/32	1.6875	0.015	2.2369	0.6	1.95	0.104	13.87
1 1/2	1.7188	0.016	2.3201	0.6	1.95	0.108	13.61
1 3/4	1.7500	0.017	2.4053	0.6	1.95	0.112	13.37
1 25/32	1.7813	0.017	2.4924	0.6	1.95	0.116	13.14
1 11/16	1.8125	0.018	2.5802	0.6	1.95	0.120	12.91
1 27/32	1.8438	0.019	2.6699	0.6	1.95	0.125	12.69
1 13/16	1.8750	0.019	2.7610	0.6	1.95	0.129	12.48
1 29/32	1.9063	0.020	2.8540	0.6	1.95	0.133	12.28
1 15/16	1.9375	0.020	2.9483	0.6	1.95	0.138	12.08
1 31/32	1.9688	0.021	3.0442	0.6	1.95	0.142	11.89
2	2.0000	0.022	3.1416	0.6	1.95	0.147	11.70

Exhibit D

PondPack Analysis

Lee's Summit High School - Network Layout

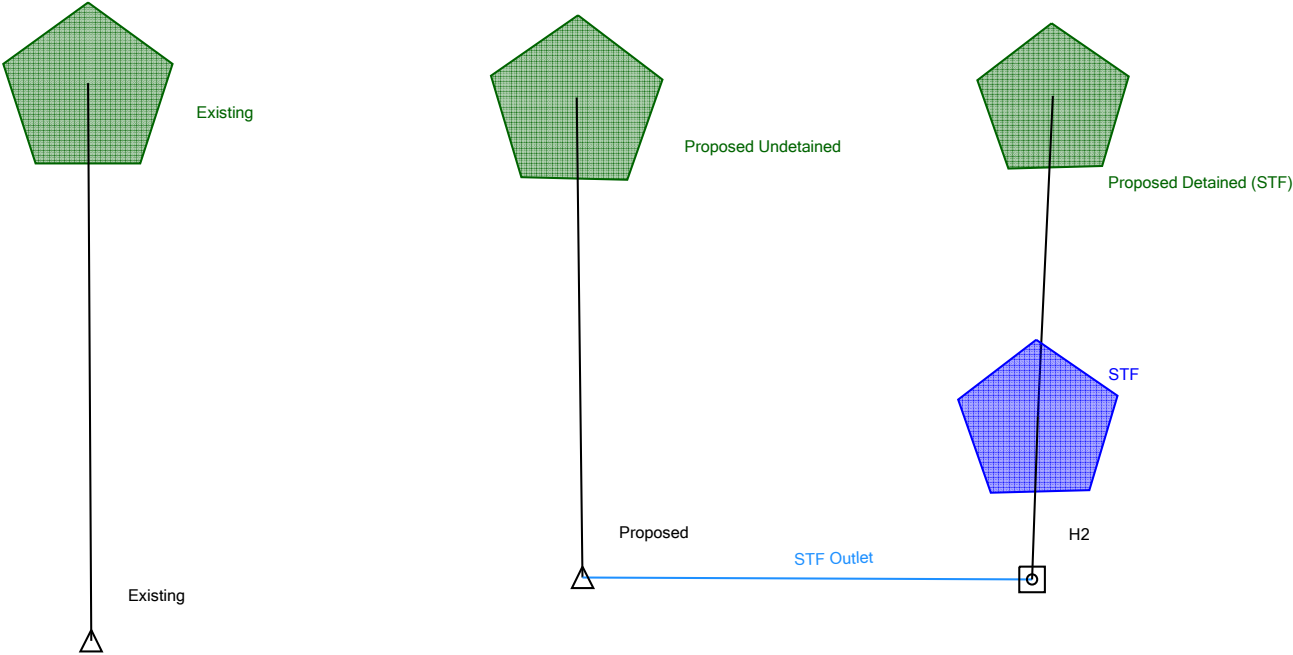


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Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Proposed Detained (STF)	WQv	1	0.058	11.900	1.05
Proposed Detained (STF)	2-year	2	0.190	11.900	3.28
Proposed Detained (STF)	10-YEAR	10	0.318	11.900	5.33
Proposed Detained (STF)	100-YEAR	100	0.452	11.900	7.47
Existing	WQv	1	0.939	12.000	15.40
Existing	2-year	2	3.576	12.000	55.92
Existing	10-YEAR	10	6.210	12.000	93.86
Existing	100-YEAR	100	9.018	12.000	133.16
Proposed Undetained	WQv	1	0.894	12.000	14.67
Proposed Undetained	2-year	2	3.406	12.000	53.26
Proposed Undetained	10-YEAR	10	5.915	12.000	89.40
Proposed Undetained	100-YEAR	100	8.589	12.000	126.83

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)
Existing	WQv	1	0.939	12.000	15.40
Existing	2-year	2	3.576	12.000	55.92
Existing	10-YEAR	10	6.210	12.000	93.86
Existing	100-YEAR	100	9.018	12.000	133.16
Proposed	WQv	1	0.932	12.000	14.70
Proposed	2-year	2	3.557	12.000	55.96
Proposed	10-YEAR	10	6.187	12.000	92.85
Proposed	100-YEAR	100	8.995	12.000	133.19

Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (hours)	Peak Flow (ft ³ /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
STF (IN)	WQv	1	0.058	11.900	1.05	(N/A)	(N/A)
STF (OUT)	WQv	1	0.038	13.500	0.04	1,007.88	0.031
STF (IN)	2-year	2	0.190	11.900	3.28	(N/A)	(N/A)
STF (OUT)	2-year	2	0.151	12.000	2.70	1,011.03	0.047
STF (IN)	10-YEAR	10	0.318	11.900	5.33	(N/A)	(N/A)
STF (OUT)	10-YEAR	10	0.272	12.050	3.51	1,011.62	0.070
STF (IN)	100-YEAR	100	0.452	11.900	7.47	(N/A)	(N/A)
STF (OUT)	100-YEAR	100	0.406	12.000	6.37	1,011.91	0.082

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

Time-Depth Curve: 100-yr	
Label	100-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	100 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.1	0.1	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.2
2.000	0.2	0.2	0.2	0.2	0.2
2.500	0.2	0.2	0.2	0.2	0.3
3.000	0.3	0.3	0.3	0.3	0.3
3.500	0.3	0.3	0.3	0.3	0.4
4.000	0.4	0.4	0.4	0.4	0.4
4.500	0.4	0.4	0.4	0.5	0.5
5.000	0.5	0.5	0.5	0.5	0.5
5.500	0.5	0.6	0.6	0.6	0.6
6.000	0.6	0.6	0.6	0.6	0.7
6.500	0.7	0.7	0.7	0.7	0.7
7.000	0.8	0.8	0.8	0.8	0.8
7.500	0.8	0.8	0.9	0.9	0.9
8.000	0.9	0.9	0.9	1.0	1.0
8.500	1.0	1.0	1.0	1.1	1.1
9.000	1.1	1.1	1.2	1.2	1.2
9.500	1.2	1.3	1.3	1.3	1.3
10.000	1.4	1.4	1.4	1.5	1.5
10.500	1.6	1.6	1.6	1.7	1.7
11.000	1.8	1.8	1.9	2.0	2.1
11.500	2.2	2.3	2.7	3.3	4.3
12.000	5.0	5.2	5.3	5.4	5.5
12.500	5.6	5.7	5.7	5.8	5.8
13.000	5.9	5.9	6.0	6.0	6.0
13.500	6.1	6.1	6.1	6.2	6.2
14.000	6.2	6.3	6.3	6.3	6.3
14.500	6.4	6.4	6.4	6.4	6.5
15.000	6.5	6.5	6.5	6.6	6.6
15.500	6.6	6.6	6.6	6.7	6.7
16.000	6.7	6.7	6.7	6.7	6.8
16.500	6.8	6.8	6.8	6.8	6.8
17.000	6.9	6.9	6.9	6.9	6.9

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 100-YEAR

Return Event: 100 years
 Storm Event: 100-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
17.500	6.9	6.9	7.0	7.0	7.0
18.000	7.0	7.0	7.0	7.0	7.1
18.500	7.1	7.1	7.1	7.1	7.1
19.000	7.1	7.1	7.2	7.2	7.2
19.500	7.2	7.2	7.2	7.2	7.2
20.000	7.2	7.2	7.3	7.3	7.3
20.500	7.3	7.3	7.3	7.3	7.3
21.000	7.3	7.3	7.4	7.4	7.4
21.500	7.4	7.4	7.4	7.4	7.4
22.000	7.4	7.4	7.4	7.5	7.5
22.500	7.5	7.5	7.5	7.5	7.5
23.000	7.5	7.5	7.5	7.5	7.5
23.500	7.6	7.6	7.6	7.6	7.6
24.000	7.6	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Time-Depth Curve: 10-yr	
Label	10-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	10 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.2	0.2	0.2	0.2	0.2
3.000	0.2	0.2	0.2	0.2	0.2
3.500	0.2	0.2	0.2	0.2	0.3
4.000	0.3	0.3	0.3	0.3	0.3
4.500	0.3	0.3	0.3	0.3	0.3
5.000	0.3	0.4	0.4	0.4	0.4
5.500	0.4	0.4	0.4	0.4	0.4
6.000	0.4	0.4	0.5	0.5	0.5
6.500	0.5	0.5	0.5	0.5	0.5
7.000	0.5	0.6	0.6	0.6	0.6
7.500	0.6	0.6	0.6	0.6	0.6
8.000	0.7	0.7	0.7	0.7	0.7
8.500	0.7	0.7	0.8	0.8	0.8
9.000	0.8	0.8	0.8	0.9	0.9
9.500	0.9	0.9	0.9	1.0	1.0
10.000	1.0	1.0	1.0	1.1	1.1
10.500	1.1	1.2	1.2	1.2	1.3
11.000	1.3	1.3	1.4	1.4	1.5
11.500	1.6	1.7	1.9	2.4	3.1
12.000	3.6	3.8	3.8	3.9	4.0
12.500	4.0	4.1	4.1	4.2	4.2
13.000	4.2	4.3	4.3	4.3	4.4
13.500	4.4	4.4	4.4	4.5	4.5
14.000	4.5	4.5	4.5	4.6	4.6
14.500	4.6	4.6	4.6	4.7	4.7
15.000	4.7	4.7	4.7	4.7	4.8
15.500	4.8	4.8	4.8	4.8	4.8
16.000	4.8	4.9	4.9	4.9	4.9
16.500	4.9	4.9	4.9	4.9	4.9
17.000	5.0	5.0	5.0	5.0	5.0

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
17.500	5.0	5.0	5.0	5.0	5.1
18.000	5.1	5.1	5.1	5.1	5.1
18.500	5.1	5.1	5.1	5.1	5.1
19.000	5.2	5.2	5.2	5.2	5.2
19.500	5.2	5.2	5.2	5.2	5.2
20.000	5.2	5.2	5.3	5.3	5.3
20.500	5.3	5.3	5.3	5.3	5.3
21.000	5.3	5.3	5.3	5.3	5.3
21.500	5.3	5.3	5.4	5.4	5.4
22.000	5.4	5.4	5.4	5.4	5.4
22.500	5.4	5.4	5.4	5.4	5.4
23.000	5.4	5.4	5.5	5.5	5.5
23.500	5.5	5.5	5.5	5.5	5.5
24.000	5.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

Time-Depth Curve: 2-yr	
Label	2-yr
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	2 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.1
1.500	0.1	0.1	0.1	0.1	0.1
2.000	0.1	0.1	0.1	0.1	0.1
2.500	0.1	0.1	0.1	0.1	0.1
3.000	0.1	0.1	0.1	0.1	0.1
3.500	0.1	0.1	0.2	0.2	0.2
4.000	0.2	0.2	0.2	0.2	0.2
4.500	0.2	0.2	0.2	0.2	0.2
5.000	0.2	0.2	0.2	0.2	0.2
5.500	0.2	0.3	0.3	0.3	0.3
6.000	0.3	0.3	0.3	0.3	0.3
6.500	0.3	0.3	0.3	0.3	0.3
7.000	0.3	0.4	0.4	0.4	0.4
7.500	0.4	0.4	0.4	0.4	0.4
8.000	0.4	0.4	0.4	0.4	0.5
8.500	0.5	0.5	0.5	0.5	0.5
9.000	0.5	0.5	0.5	0.5	0.6
9.500	0.6	0.6	0.6	0.6	0.6
10.000	0.6	0.6	0.7	0.7	0.7
10.500	0.7	0.7	0.8	0.8	0.8
11.000	0.8	0.8	0.9	0.9	1.0
11.500	1.0	1.1	1.2	1.5	2.0
12.000	2.3	2.4	2.4	2.5	2.5
12.500	2.6	2.6	2.6	2.7	2.7
13.000	2.7	2.7	2.7	2.8	2.8
13.500	2.8	2.8	2.8	2.8	2.9
14.000	2.9	2.9	2.9	2.9	2.9
14.500	2.9	2.9	3.0	3.0	3.0
15.000	3.0	3.0	3.0	3.0	3.0
15.500	3.0	3.0	3.1	3.1	3.1
16.000	3.1	3.1	3.1	3.1	3.1
16.500	3.1	3.1	3.1	3.1	3.1
17.000	3.2	3.2	3.2	3.2	3.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: 2-year

Return Event: 2 years
 Storm Event: 2-yr

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
17.500	3.2	3.2	3.2	3.2	3.2
18.000	3.2	3.2	3.2	3.2	3.2
18.500	3.3	3.3	3.3	3.3	3.3
19.000	3.3	3.3	3.3	3.3	3.3
19.500	3.3	3.3	3.3	3.3	3.3
20.000	3.3	3.3	3.3	3.3	3.4
20.500	3.4	3.4	3.4	3.4	3.4
21.000	3.4	3.4	3.4	3.4	3.4
21.500	3.4	3.4	3.4	3.4	3.4
22.000	3.4	3.4	3.4	3.4	3.4
22.500	3.4	3.4	3.4	3.5	3.5
23.000	3.5	3.5	3.5	3.5	3.5
23.500	3.5	3.5	3.5	3.5	3.5
24.000	3.5	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

Time-Depth Curve: WQ	
Label	WQ
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	1 years

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.0	0.0	0.0	0.0
1.000	0.0	0.0	0.0	0.0	0.0
1.500	0.0	0.0	0.0	0.0	0.0
2.000	0.0	0.0	0.0	0.0	0.0
2.500	0.0	0.0	0.0	0.0	0.0
3.000	0.0	0.0	0.1	0.1	0.1
3.500	0.1	0.1	0.1	0.1	0.1
4.000	0.1	0.1	0.1	0.1	0.1
4.500	0.1	0.1	0.1	0.1	0.1
5.000	0.1	0.1	0.1	0.1	0.1
5.500	0.1	0.1	0.1	0.1	0.1
6.000	0.1	0.1	0.1	0.1	0.1
6.500	0.1	0.1	0.1	0.1	0.1
7.000	0.1	0.1	0.1	0.1	0.1
7.500	0.1	0.2	0.2	0.2	0.2
8.000	0.2	0.2	0.2	0.2	0.2
8.500	0.2	0.2	0.2	0.2	0.2
9.000	0.2	0.2	0.2	0.2	0.2
9.500	0.2	0.2	0.2	0.2	0.2
10.000	0.2	0.3	0.3	0.3	0.3
10.500	0.3	0.3	0.3	0.3	0.3
11.000	0.3	0.3	0.3	0.4	0.4
11.500	0.4	0.4	0.5	0.6	0.8
12.000	0.9	0.9	1.0	1.0	1.0
12.500	1.0	1.0	1.0	1.0	1.0
13.000	1.1	1.1	1.1	1.1	1.1
13.500	1.1	1.1	1.1	1.1	1.1
14.000	1.1	1.1	1.1	1.1	1.1
14.500	1.1	1.2	1.2	1.2	1.2
15.000	1.2	1.2	1.2	1.2	1.2
15.500	1.2	1.2	1.2	1.2	1.2
16.000	1.2	1.2	1.2	1.2	1.2
16.500	1.2	1.2	1.2	1.2	1.2
17.000	1.2	1.2	1.2	1.2	1.2

Subsection: Time-Depth Curve
 Label: SCS Type II
 Scenario: WQv

Return Event: 1 years
 Storm Event: WQ

CUMULATIVE RAINFALL (in)
Output Time Increment = 0.100 hours
Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
17.500	1.2	1.3	1.3	1.3	1.3
18.000	1.3	1.3	1.3	1.3	1.3
18.500	1.3	1.3	1.3	1.3	1.3
19.000	1.3	1.3	1.3	1.3	1.3
19.500	1.3	1.3	1.3	1.3	1.3
20.000	1.3	1.3	1.3	1.3	1.3
20.500	1.3	1.3	1.3	1.3	1.3
21.000	1.3	1.3	1.3	1.3	1.3
21.500	1.3	1.3	1.3	1.3	1.3
22.000	1.3	1.3	1.3	1.3	1.3
22.500	1.3	1.3	1.3	1.4	1.4
23.000	1.4	1.4	1.4	1.4	1.4
23.500	1.4	1.4	1.4	1.4	1.4
24.000	1.4	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Elevation-Volume-Flow Table (Pond)
Label: STF
Scenario: WQv

Return Event: 1 years
Storm Event: WQ

Infiltration	
Infiltration Method (Computed)	Constant
Infiltration Rate (Constant)	0.01 ft ³ /s
Initial Conditions	
Elevation (Water Surface, Initial)	1,005.50 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft ³ /s
Flow (Initial Infiltration)	0.00 ft ³ /s
Flow (Initial, Total)	0.00 ft ³ /s
Time Increment	0.050 hours

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,005.50	0.00	0.000	0.000	0.00	0.00	0.00
1,005.60	0.01	0.001	0.000	0.01	0.01	0.30
1,005.70	0.01	0.001	0.000	0.01	0.02	0.60
1,005.80	0.01	0.002	0.000	0.01	0.02	0.89
1,005.90	0.02	0.002	0.000	0.01	0.02	1.18
1,006.00	0.02	0.003	0.000	0.01	0.02	1.48
1,006.10	0.02	0.005	0.000	0.01	0.03	2.25
1,006.20	0.02	0.006	0.000	0.01	0.03	3.03
1,006.30	0.02	0.008	0.000	0.01	0.03	3.80
1,006.40	0.02	0.009	0.000	0.01	0.03	4.58
1,006.50	0.03	0.011	0.000	0.01	0.03	5.36
1,006.60	0.03	0.013	0.000	0.01	0.03	6.13
1,006.70	0.03	0.014	0.000	0.01	0.03	6.91
1,006.80	0.03	0.016	0.000	0.01	0.04	7.68
1,006.90	0.03	0.017	0.000	0.01	0.04	8.46
1,007.00	0.03	0.019	0.000	0.01	0.04	9.23
1,007.10	0.03	0.020	0.000	0.01	0.04	9.91
1,007.20	0.03	0.022	0.000	0.01	0.04	10.59
1,007.30	0.03	0.023	0.000	0.01	0.04	11.27
1,007.40	0.04	0.025	0.000	0.01	0.04	11.95
1,007.50	0.04	0.026	0.000	0.01	0.04	12.63
1,007.60	0.04	0.027	0.000	0.01	0.04	13.31
1,007.70	0.04	0.029	0.000	0.01	0.04	13.98
1,007.80	0.04	0.030	0.000	0.01	0.05	14.66
1,007.90	0.04	0.032	0.000	0.01	0.05	15.34
1,008.00	0.04	0.033	0.000	0.01	0.05	16.02
1,008.10	0.04	0.034	0.000	0.01	0.05	16.36
1,008.20	0.04	0.034	0.000	0.01	0.05	16.70
1,008.30	0.04	0.035	0.000	0.01	0.05	17.04

Subsection: Elevation-Volume-Flow Table (Pond)
Label: STF
Scenario: WQv

Return Event: 1 years
Storm Event: WQ

Elevation (ft)	Outflow (ft ³ /s)	Storage (ac-ft)	Area (ft ²)	Infiltration (ft ³ /s)	Flow (Total) (ft ³ /s)	2S/t + O (ft ³ /s)
1,008.40	0.07	0.036	0.000	0.01	0.08	17.40
1,008.50	0.15	0.037	0.000	0.01	0.16	17.82
1,008.60	0.27	0.037	0.000	0.01	0.28	18.28
1,008.70	0.44	0.038	0.000	0.01	0.44	18.79
1,008.80	0.63	0.039	0.000	0.01	0.63	19.31
1,008.90	0.84	0.039	0.000	0.01	0.84	19.86
1,009.00	1.08	0.040	0.000	0.01	1.09	20.45
1,009.10	1.22	0.040	0.000	0.01	1.22	20.58
1,009.20	1.34	0.040	0.000	0.01	1.34	20.70
1,009.30	1.45	0.040	0.000	0.01	1.45	20.81
1,009.40	1.55	0.040	0.000	0.01	1.55	20.91
1,009.50	1.64	0.040	0.000	0.01	1.65	21.01
1,009.60	1.73	0.040	0.000	0.01	1.74	21.10
1,009.70	1.82	0.040	0.000	0.01	1.82	21.18
1,009.80	1.90	0.040	0.000	0.01	1.91	21.27
1,009.90	1.98	0.040	0.000	0.01	1.98	21.34
1,010.00	2.05	0.040	0.000	0.01	2.06	21.42
1,010.10	2.12	0.041	0.000	0.01	2.13	21.78
1,010.20	2.19	0.041	0.000	0.01	2.20	22.14
1,010.30	2.26	0.042	0.000	0.01	2.27	22.50
1,010.40	2.33	0.042	0.000	0.01	2.33	22.86
1,010.50	2.39	0.043	0.000	0.01	2.40	23.21
1,010.60	2.45	0.044	0.000	0.01	2.46	23.56
1,010.70	2.52	0.044	0.000	0.01	2.52	23.91
1,010.80	2.57	0.045	0.000	0.01	2.58	24.26
1,010.90	2.63	0.045	0.000	0.01	2.64	24.61
1,011.00	2.69	0.046	0.000	0.01	2.70	24.96
1,011.10	2.74	0.050	0.000	0.01	2.75	26.90
1,011.20	2.80	0.054	0.000	0.01	2.80	28.84
1,011.30	2.85	0.058	0.000	0.01	2.86	30.79
1,011.40	2.90	0.062	0.000	0.01	2.91	32.73
1,011.50	2.96	0.066	0.000	0.01	2.96	34.66
1,011.60	3.39	0.069	0.000	0.01	3.39	36.98
1,011.70	4.13	0.073	0.000	0.01	4.13	39.61
1,011.80	5.08	0.077	0.000	0.01	5.08	42.45
1,011.90	6.19	0.081	0.000	0.01	6.19	45.45
1,012.00	7.44	0.085	0.000	0.01	7.45	48.59

Subsection: Level Pool Pond Routing Summary
Label: STF (IN)
Scenario: WQv

Return Event: 1 years
Storm Event: WQ

Infiltration				
Infiltration Method (Computed)		Constant		
Infiltration Rate (Constant)		0.01 ft³/s		
Initial Conditions				
Elevation (Water Surface, Initial)		1,005.50 ft		
Volume (Initial)		0.000 ac-ft		
Flow (Initial Outlet)		0.00 ft³/s		
Flow (Initial Infiltration)		0.00 ft³/s		
Flow (Initial, Total)		0.00 ft³/s		
Time Increment		0.050 hours		
Inflow/Outflow Hydrograph Summary				
Flow (Peak In)		1.05 ft³/s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)		0.01 ft³/s	Time to Peak (Infiltration)	10.150 hours
Flow (Peak Outlet)		0.04 ft³/s	Time to Peak (Flow, Outlet)	13.500 hours
Elevation (Water Surface, Peak)		1,007.88 ft		
Volume (Peak)		0.031 ac-ft		
Mass Balance (ac-ft)				
Volume (Initial)		0.000 ac-ft		
Volume (Total Inflow)		0.058 ac-ft		
Volume (Total Infiltration)		0.008 ac-ft		
Volume (Total Outlet Outflow)		0.038 ac-ft		
Volume (Retained)		0.012 ac-ft		
Volume (Unrouted)		0.000 ac-ft		
Error (Mass Balance)		0.2 %		

Subsection: Level Pool Pond Routing Summary
Label: STF (IN)
Scenario: 2-year

Return Event: 2 years
Storm Event: 2-yr

Infiltration			
Infiltration Method (Computed)		Constant	
Infiltration Rate (Constant)		0.01 ft³/s	
Initial Conditions			
Elevation (Water Surface, Initial)		1,005.50 ft	
Volume (Initial)		0.000 ac-ft	
Flow (Initial Outlet)		0.00 ft³/s	
Flow (Initial Infiltration)		0.00 ft³/s	
Flow (Initial, Total)		0.00 ft³/s	
Time Increment		0.050 hours	
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)		3.28 ft³/s	Time to Peak (Flow, In)
Infiltration (Peak)		0.01 ft³/s	Time to Peak (Infiltration)
Flow (Peak Outlet)		2.70 ft³/s	Time to Peak (Flow, Outlet)
			11.900 hours
			5.350 hours
			12.000 hours
Peak Conditions			
Elevation (Water Surface, Peak)		1,011.03 ft	
Volume (Peak)		0.047 ac-ft	
Mass Balance (ac-ft)			
Volume (Initial)		0.000 ac-ft	
Volume (Total Inflow)		0.190 ac-ft	
Volume (Total Infiltration)		0.010 ac-ft	
Volume (Total Outlet Outflow)		0.151 ac-ft	
Volume (Retained)		0.029 ac-ft	
Volume (Unrouted)		0.000 ac-ft	
Error (Mass Balance)		0.1 %	

Subsection: Level Pool Pond Routing Summary
 Label: STF (IN)
 Scenario: 10-YEAR

Return Event: 10 years
 Storm Event: 10-yr

Infiltration				
Infiltration Method (Computed)		Constant		
Infiltration Rate (Constant)		0.01 ft³/s		
Initial Conditions				
Elevation (Water Surface, Initial)		1,005.50 ft		
Volume (Initial)		0.000 ac-ft		
Flow (Initial Outlet)		0.00 ft³/s		
Flow (Initial Infiltration)		0.00 ft³/s		
Flow (Initial, Total)		0.00 ft³/s		
Time Increment		0.050 hours		
Inflow/Outflow Hydrograph Summary				
Flow (Peak In)		5.33 ft³/s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)		0.01 ft³/s	Time to Peak (Infiltration)	3.450 hours
Flow (Peak Outlet)		3.51 ft³/s	Time to Peak (Flow, Outlet)	12.050 hours
Elevation (Water Surface, Peak)		1,011.62 ft		
Volume (Peak)		0.070 ac-ft		
Mass Balance (ac-ft)				
Volume (Initial)		0.000 ac-ft		
Volume (Total Inflow)		0.318 ac-ft		
Volume (Total Infiltration)		0.011 ac-ft		
Volume (Total Outlet Outflow)		0.272 ac-ft		
Volume (Retained)		0.035 ac-ft		
Volume (Unrouted)		0.000 ac-ft		
Error (Mass Balance)		0.1 %		

Subsection: Level Pool Pond Routing Summary
Label: STF (IN)
Scenario: 100-YEAR

Return Event: 100 years
Storm Event: 100-yr

Infiltration				
Infiltration Method (Computed)		Constant		
Infiltration Rate (Constant)		0.01 ft³/s		
Initial Conditions				
Elevation (Water Surface, Initial)		1,005.50 ft		
Volume (Initial)		0.000 ac-ft		
Flow (Initial Outlet)		0.00 ft³/s		
Flow (Initial Infiltration)		0.00 ft³/s		
Flow (Initial, Total)		0.00 ft³/s		
Time Increment		0.050 hours		
Inflow/Outflow Hydrograph Summary				
Flow (Peak In)		7.47 ft³/s	Time to Peak (Flow, In)	11.900 hours
Infiltration (Peak)		0.01 ft³/s	Time to Peak (Infiltration)	2.500 hours
Flow (Peak Outlet)		6.37 ft³/s	Time to Peak (Flow, Outlet)	12.000 hours
Elevation (Water Surface, Peak)		1,011.91 ft		
Volume (Peak)		0.082 ac-ft		
Mass Balance (ac-ft)				
Volume (Initial)		0.000 ac-ft		
Volume (Total Inflow)		0.452 ac-ft		
Volume (Total Infiltration)		0.011 ac-ft		
Volume (Total Outlet Outflow)		0.406 ac-ft		
Volume (Retained)		0.035 ac-ft		
Volume (Unrouted)		0.000 ac-ft		
Error (Mass Balance)		0.1 %		

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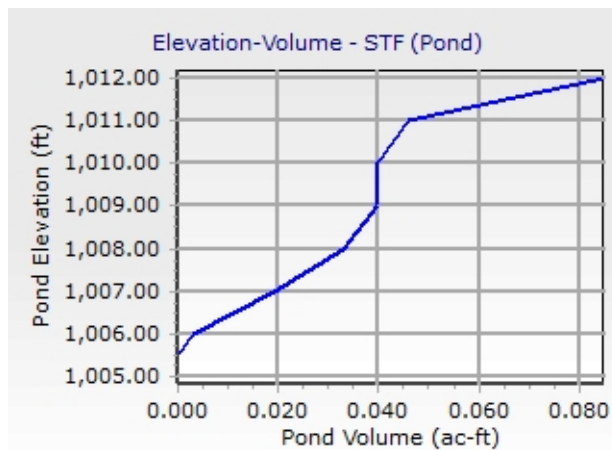
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Elevation-Volume - STF (Pond)

Pond Elevation (ft)	Pond Volume (ac-ft)
1,005.50	0.000
1,006.00	0.003
1,007.00	0.019
1,008.00	0.033
1,009.00	0.040
1,010.00	0.040
1,011.00	0.046
1,012.00	0.085

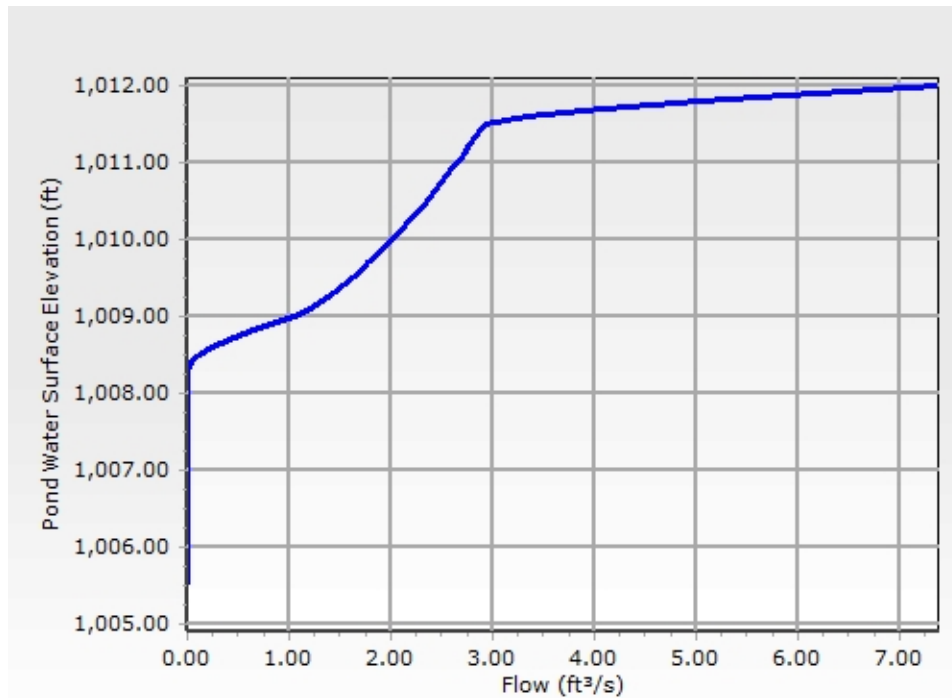


Composite Outlet Structure Detailed Report: STF Outlet

Element Details			
Label	STF Outlet	Notes	
Headwater Range			
Headwater Type	Use Pond for Headwater Range	Maximum (Headwater)	1,012.00 ft
Pond Minimum (Headwater)	STF 1,005.50 ft	Increment (Headwater)	0.10 ft
SpotElevation (ft)			
Tailwater Setup			
Tailwater Type	Free Outfall		
Tailwater Tolerances			
Maximum Iterations	30	Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft	Flow Tolerance (Minimum)	0.001 ft³/s
Headwater Tolerance (Maximum)	0.50 ft	Flow Tolerance (Maximum)	10.000 ft³/s
Tailwater Tolerance (Minimum)	0.01 ft		
Outlet Structure			
Outlet Structure Type	Culvert	Culvert Type	Circular
Outlet Structure (IDs and Direction)			
Outlet ID	Line A	Downstream ID	Tailwater
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Culvert Data			
Number of Barrels	1	Downstream Invert	1,002.00 ft
Length	18.00 ft	Diameter	15.0 in
Upstream Invert	1,003.00 ft		
Unsubmerged->Submerged			
Specify Transitions	False	Compute Inlet Control Only	False
Culvert Coefficients			

Composite Outlet Structure Detailed Report: STF Outlet

Culvert Coefficients			
Inlet Description	Concrete - Groove end w/headwall	C	0.0292
Chart	Chart 1	Y	0.7400
Nomograph	Nomograph 2	Manning's n	0.013
Equation Form	Form 1	Ke	0.200
K	0.0018	Kr	0.000
M	2.0000	Slope Correction Factor	-0.500
Culvert (Advanced)			
Convergence Tolerance	0.00 ft	Specify Number of Backwater Sections	False



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.50	0.00	0.00	0.00	Free Outfall
1,005.60	0.00	0.00	0.00	Free Outfall

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.70	0.00	0.00	0.00	Free Outfall
1,005.80	0.00	0.00	0.00	Free Outfall
1,005.90	0.00	0.00	0.00	Free Outfall
1,006.00	0.00	0.00	0.00	Free Outfall
1,006.10	0.00	0.00	0.00	Free Outfall
1,006.20	0.00	0.00	0.00	Free Outfall
1,006.30	0.00	0.00	0.00	Free Outfall
1,006.40	0.00	0.00	0.00	Free Outfall
1,006.50	0.00	0.00	0.00	Free Outfall
1,006.60	0.00	0.00	0.00	Free Outfall
1,006.70	0.00	0.00	0.00	Free Outfall
1,006.80	0.00	0.00	0.00	Free Outfall
1,006.90	0.00	0.00	0.00	Free Outfall
1,007.00	0.00	0.00	0.00	Free Outfall
1,007.10	0.00	0.00	0.00	Free Outfall
1,007.20	0.00	0.00	0.00	Free Outfall
1,007.30	0.00	0.00	0.00	Free Outfall
1,007.40	0.00	0.00	0.00	Free Outfall
1,007.50	0.00	0.00	0.00	Free Outfall
1,007.60	0.00	0.00	0.00	Free Outfall
1,007.70	0.00	0.00	0.00	Free Outfall
1,007.80	0.00	0.00	0.00	Free Outfall
1,007.90	0.00	0.00	0.00	Free Outfall
1,008.00	0.00	0.00	0.00	Free Outfall
1,008.10	0.00	0.00	0.00	Free Outfall
1,008.20	0.00	0.00	0.00	Free Outfall
1,008.30	0.00	0.00	0.00	Free Outfall
1,008.40	0.03	1,003.09	Free Outfall	Free Outfall
1,008.50	0.11	1,003.18	Free Outfall	Free Outfall
1,008.60	0.24	1,003.27	Free Outfall	Free Outfall
1,008.70	0.41	1,003.35	Free Outfall	Free Outfall
1,008.80	0.60	1,003.43	Free Outfall	Free Outfall
1,008.90	0.82	1,003.51	Free Outfall	Free Outfall
1,009.00	1.07	1,003.58	Free Outfall	Free Outfall
1,009.10	1.20	1,003.62	Free Outfall	Free Outfall
1,009.20	1.32	1,003.66	Free Outfall	Free Outfall
1,009.30	1.43	1,003.68	Free Outfall	Free Outfall
1,009.40	1.54	1,003.71	Free Outfall	Free Outfall
1,009.50	1.63	1,003.73	Free Outfall	Free Outfall
1,009.60	1.72	1,003.76	Free Outfall	Free Outfall

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,009.70	1.78	1,003.77	Free Outfall	Free Outfall
1,009.80	1.87	1,003.79	Free Outfall	Free Outfall
1,009.90	1.95	1,003.81	Free Outfall	Free Outfall
1,010.00	2.02	1,003.83	Free Outfall	Free Outfall
1,010.10	2.09	1,003.84	Free Outfall	Free Outfall
1,010.20	2.16	1,003.86	Free Outfall	Free Outfall
1,010.30	2.23	1,003.87	Free Outfall	Free Outfall
1,010.40	2.29	1,003.89	Free Outfall	Free Outfall
1,010.50	2.36	1,003.90	Free Outfall	Free Outfall
1,010.60	2.42	1,003.92	Free Outfall	Free Outfall
1,010.70	2.48	1,003.93	Free Outfall	Free Outfall
1,010.80	2.54	1,003.94	Free Outfall	Free Outfall
1,010.90	2.59	1,003.95	Free Outfall	Free Outfall
1,011.00	2.66	1,003.97	Free Outfall	Free Outfall
1,011.10	2.71	1,003.98	Free Outfall	Free Outfall
1,011.20	2.76	1,003.99	Free Outfall	Free Outfall
1,011.30	2.82	1,004.00	Free Outfall	Free Outfall
1,011.40	2.87	1,004.01	Free Outfall	Free Outfall
1,011.50	2.92	1,004.02	Free Outfall	Free Outfall
1,011.60	3.35	1,004.11	Free Outfall	Free Outfall
1,011.70	4.09	1,004.25	Free Outfall	Free Outfall
1,011.80	5.04	1,004.43	Free Outfall	Free Outfall
1,011.90	6.17	1,004.64	Free Outfall	Free Outfall
1,012.00	7.40	1,004.95	Free Outfall	Free Outfall
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

Downstream ID = Tailwater (Pond Outfall)

Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

Downstream ID = Tailwater (Pond Outfall)

Message
WS below an invert; no flow.
WS below an invert; no flow.
WS below an invert; no flow.
WS below an invert; no flow.
CRIT.DEPTH CONTROL Vh= .023ft
Dcr= .067ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .044ft
Dcr= .129ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .066ft
Dcr= .191ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .087ft
Dcr= .249ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .107ft
Dcr= .303ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .127ft
Dcr= .355ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .148ft
Dcr= .406ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .159ft
Dcr= .433ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .168ft
Dcr= .454ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .175ft
Dcr= .473ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .183ft
Dcr= .491ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .190ft
Dcr= .506ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .197ft
Dcr= .521ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .201ft
Dcr= .531ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .207ft
Dcr= .544ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .212ft
Dcr= .556ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .217ft
Dcr= .566ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .222ft
Dcr= .576ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .227ft
Dcr= .587ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .232ft
Dcr= .597ft CRIT.DEPTH Hev= .00ft

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Line A (Culvert-Circular)

Mannings open channel maximum capacity: 16.38 ft³/s

Upstream ID = Area Inlet Opening, Underdrain

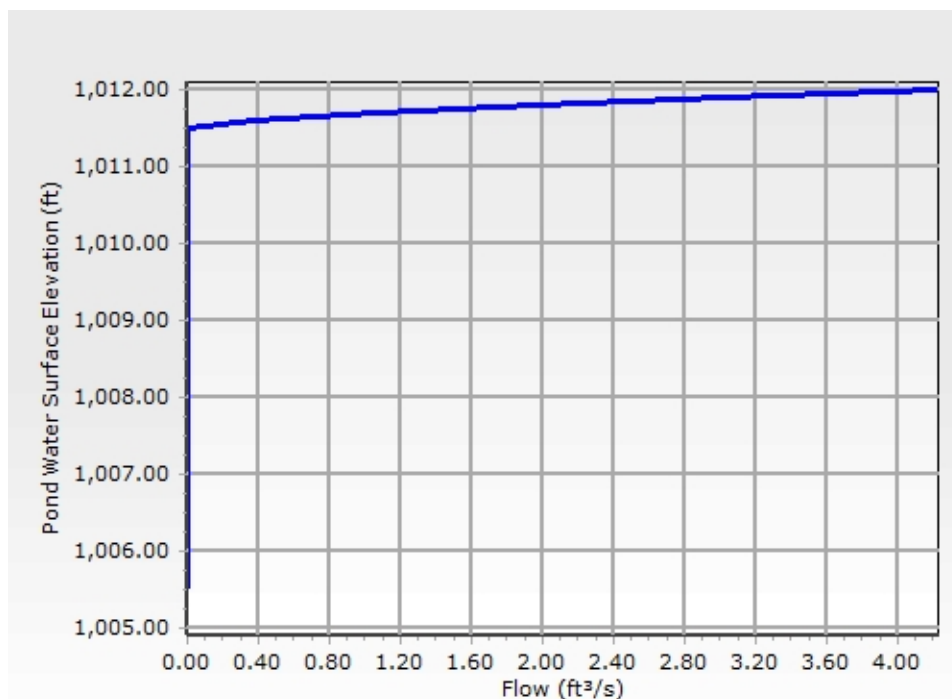
Downstream ID = Tailwater (Pond Outfall)

Message
CRIT.DEPTH CONTROL Vh= .236ft
Dcr= .605ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .240ft
Dcr= .614ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .244ft
Dcr= .622ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .248ft
Dcr= .631ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .252ft
Dcr= .638ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .256ft
Dcr= .646ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .260ft
Dcr= .654ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .264ft
Dcr= .661ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .267ft
Dcr= .667ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .271ft
Dcr= .674ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .274ft
Dcr= .681ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .278ft
Dcr= .687ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .306ft
Dcr= .738ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .359ft
Dcr= .819ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .430ft
Dcr= .910ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .531ft
Dcr= 1.004ft CRIT.DEPTH Hev= .00ft
INLET CONTROL... Submerged: HW
=1.95

Outlet Structure			
Outlet Structure Type		Orifice	
Outlet Structure (IDs and Direction)			
Outlet ID	Area Inlet Opening	Downstream ID	Line A
Flow Direction	Forward Flow Only	Notes	

Composite Outlet Structure Detailed Report: STF Outlet

Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Area Orifice	Orifice Orientation	Perpendicular Orifice
Number of Openings	1	Datum Elevation	1,011.00 ft
Orifice Coefficient	0.600	Top Elevation	1,011.50 ft
Orifice Area	2.0 ft ²		
Outlet Structure (Common)			
Elevation	1,010.90 ft		



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Area Inlet Opening (Orifice-Area)

Upstream ID = Weir West Opening (Rectangular Weir)

Downstream ID = Line A (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft³/s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.50	0.00	0.00	0.00	0.00
1,005.60	0.00	0.00	0.00	0.00
1,005.70	0.00	0.00	0.00	0.00

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Area Inlet Opening (Orifice-Area)

Upstream ID = Weir West Opening (Rectangular Weir)

Downstream ID = Line A (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.80	0.00	0.00	0.00	0.00
1,005.90	0.00	0.00	0.00	0.00
1,006.00	0.00	0.00	0.00	0.00
1,006.10	0.00	0.00	0.00	0.00
1,006.20	0.00	0.00	0.00	0.00
1,006.30	0.00	0.00	0.00	0.00
1,006.40	0.00	0.00	0.00	0.00
1,006.50	0.00	0.00	0.00	0.00
1,006.60	0.00	0.00	0.00	0.00
1,006.70	0.00	0.00	0.00	0.00
1,006.80	0.00	0.00	0.00	0.00
1,006.90	0.00	0.00	0.00	0.00
1,007.00	0.00	0.00	0.00	0.00
1,007.10	0.00	0.00	0.00	0.00
1,007.20	0.00	0.00	0.00	0.00
1,007.30	0.00	0.00	0.00	0.00
1,007.40	0.00	0.00	0.00	0.00
1,007.50	0.00	0.00	0.00	0.00
1,007.60	0.00	0.00	0.00	0.00
1,007.70	0.00	0.00	0.00	0.00
1,007.80	0.00	0.00	0.00	0.00
1,007.90	0.00	0.00	0.00	0.00
1,008.00	0.00	0.00	0.00	0.00
1,008.10	0.00	0.00	0.00	0.00
1,008.20	0.00	0.00	0.00	0.00
1,008.30	0.00	0.00	0.00	0.00
1,008.40	0.00	0.00	0.00	1,003.09
1,008.50	0.00	0.00	0.00	1,003.18
1,008.60	0.00	0.00	0.00	1,003.27
1,008.70	0.00	0.00	0.00	1,003.35
1,008.80	0.00	0.00	0.00	1,003.43
1,008.90	0.00	0.00	0.00	1,003.51
1,009.00	0.00	0.00	0.00	1,003.58
1,009.10	0.00	0.00	0.00	1,003.62
1,009.20	0.00	0.00	0.00	1,003.66
1,009.30	0.00	0.00	0.00	1,003.68
1,009.40	0.00	0.00	0.00	1,003.71
1,009.50	0.00	0.00	0.00	1,003.73
1,009.60	0.00	0.00	0.00	1,003.76
1,009.70	0.00	0.00	0.00	1,003.77
1,009.80	0.00	0.00	0.00	1,003.79

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Area Inlet Opening (Orifice-Area)

Upstream ID = Weir West Opening (Rectangular Weir)

Downstream ID = Line A (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,009.90	0.00	0.00	0.00	1,003.81
1,010.00	0.00	0.00	0.00	1,003.83
1,010.10	0.00	0.00	0.00	1,003.84
1,010.20	0.00	0.00	0.00	1,003.86
1,010.30	0.00	0.00	0.00	1,003.87
1,010.40	0.00	0.00	0.00	1,003.89
1,010.50	0.00	0.00	0.00	1,003.90
1,010.60	0.00	0.00	0.00	1,003.92
1,010.70	0.00	0.00	0.00	1,003.93
1,010.80	0.00	0.00	0.00	1,003.94
1,010.90	0.00	0.00	0.00	1,003.95
1,011.00	0.00	0.00	0.00	1,003.97
1,011.10	0.00	0.00	0.00	1,003.98
1,011.20	0.00	0.00	0.00	1,003.99
1,011.30	0.00	0.00	0.00	1,004.00
1,011.40	0.00	0.00	0.00	1,004.01
1,011.50	0.00	0.00	0.00	1,004.02
1,011.60	0.38	1,010.93	Free Outfall	1,004.11
1,011.70	1.07	1,010.99	Free Outfall	1,004.25
1,011.80	1.97	1,011.07	Free Outfall	1,004.43
1,011.90	3.04	1,011.17	Free Outfall	1,004.64
1,012.00	4.24	1,011.27	Free Outfall	1,004.95
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Area Inlet Opening (Orifice-Area)

Upstream ID = Weir West Opening (Rectangular Weir)

Downstream ID = Line A (Culvert-Circular)

Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Area Inlet Opening (Orifice-Area)

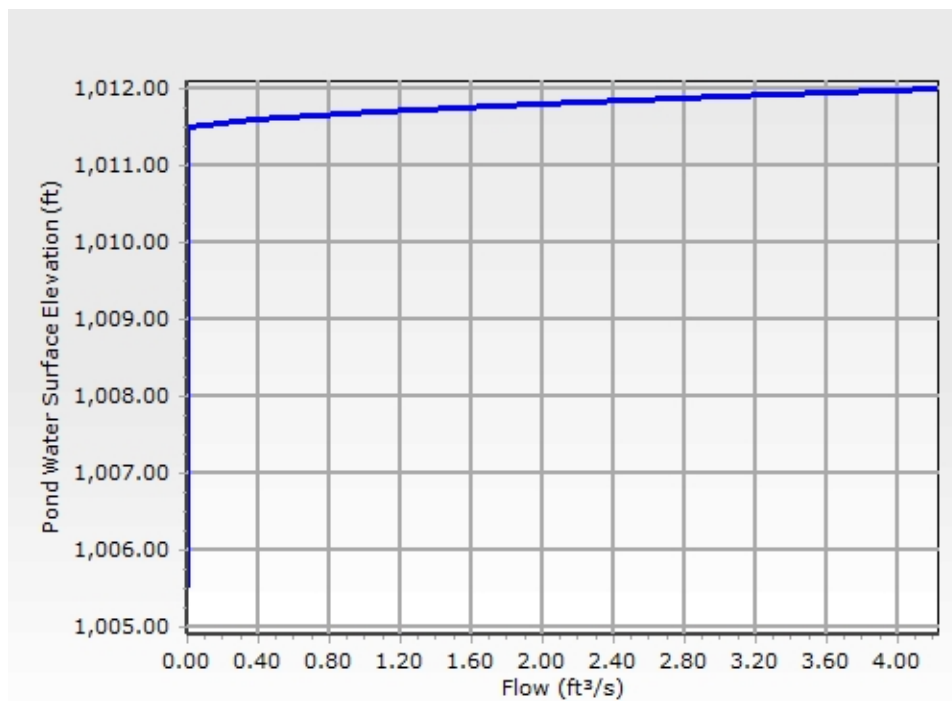
Upstream ID = Weir West Opening (Rectangular Weir)

Downstream ID = Line A (Culvert-Circular)

Message	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
WS below an invert; no flow.	
Hi=.03; Ht=.50; Qt=6.81	
Hi=.09; Ht=.50; Qt=6.81	
Hi=.17; Ht=.50; Qt=6.81	
Hi=.27; Ht=.50; Qt=6.81	
Hi=.37; Ht=.50; Qt=6.81	
Outlet Structure	
Outlet Structure Type	
Weir	
Outlet Structure (IDs and Direction)	

Composite Outlet Structure Detailed Report: STF Outlet

Outlet Structure (IDs and Direction)			
Outlet ID	Weir West Opening	Downstream ID	Area Inlet Opening
Flow Direction	Forward Flow Only	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Weir)			
Weir	Rectangular Weir	Rectangular Weir	Suppressed
Vary Coefficient with Depth	False	Weir Length	4.00 ft
Weir Coefficient	3.00 (ft^0.5)/s		
Outlet Structure (Common)			
Elevation	1,011.50 ft		
Outlet Structure (Weir, Advanced)			
User Defined Table	False		



Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir West Opening (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Area Inlet Opening (Orifice-Area)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.50	0.00	0.00	0.00	0.00
1,005.60	0.00	0.00	0.00	0.00
1,005.70	0.00	0.00	0.00	0.00
1,005.80	0.00	0.00	0.00	0.00
1,005.90	0.00	0.00	0.00	0.00
1,006.00	0.00	0.00	0.00	0.00
1,006.10	0.00	0.00	0.00	0.00
1,006.20	0.00	0.00	0.00	0.00
1,006.30	0.00	0.00	0.00	0.00
1,006.40	0.00	0.00	0.00	0.00
1,006.50	0.00	0.00	0.00	0.00
1,006.60	0.00	0.00	0.00	0.00
1,006.70	0.00	0.00	0.00	0.00
1,006.80	0.00	0.00	0.00	0.00
1,006.90	0.00	0.00	0.00	0.00
1,007.00	0.00	0.00	0.00	0.00
1,007.10	0.00	0.00	0.00	0.00
1,007.20	0.00	0.00	0.00	0.00
1,007.30	0.00	0.00	0.00	0.00
1,007.40	0.00	0.00	0.00	0.00
1,007.50	0.00	0.00	0.00	0.00
1,007.60	0.00	0.00	0.00	0.00
1,007.70	0.00	0.00	0.00	0.00
1,007.80	0.00	0.00	0.00	0.00
1,007.90	0.00	0.00	0.00	0.00
1,008.00	0.00	0.00	0.00	0.00
1,008.10	0.00	0.00	0.00	0.00
1,008.20	0.00	0.00	0.00	0.00
1,008.30	0.00	0.00	0.00	0.00
1,008.40	0.00	0.00	0.00	0.00
1,008.50	0.00	0.00	0.00	0.00
1,008.60	0.00	0.00	0.00	0.00
1,008.70	0.00	0.00	0.00	0.00
1,008.80	0.00	0.00	0.00	0.00
1,008.90	0.00	0.00	0.00	0.00
1,009.00	0.00	0.00	0.00	0.00
1,009.10	0.00	0.00	0.00	0.00
1,009.20	0.00	0.00	0.00	0.00
1,009.30	0.00	0.00	0.00	0.00
1,009.40	0.00	0.00	0.00	0.00

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir West Opening (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Area Inlet Opening (Orifice-Area)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,009.50	0.00	0.00	0.00	0.00
1,009.60	0.00	0.00	0.00	0.00
1,009.70	0.00	0.00	0.00	0.00
1,009.80	0.00	0.00	0.00	0.00
1,009.90	0.00	0.00	0.00	0.00
1,010.00	0.00	0.00	0.00	0.00
1,010.10	0.00	0.00	0.00	0.00
1,010.20	0.00	0.00	0.00	0.00
1,010.30	0.00	0.00	0.00	0.00
1,010.40	0.00	0.00	0.00	0.00
1,010.50	0.00	0.00	0.00	0.00
1,010.60	0.00	0.00	0.00	0.00
1,010.70	0.00	0.00	0.00	0.00
1,010.80	0.00	0.00	0.00	0.00
1,010.90	0.00	0.00	0.00	0.00
1,011.00	0.00	0.00	0.00	0.00
1,011.10	0.00	0.00	0.00	0.00
1,011.20	0.00	0.00	0.00	0.00
1,011.30	0.00	0.00	0.00	0.00
1,011.40	0.00	0.00	0.00	0.00
1,011.50	0.00	0.00	0.00	0.00
1,011.60	0.38	1,011.60	Free Outfall	1,010.93
1,011.70	1.07	1,011.70	Free Outfall	1,010.99
1,011.80	1.97	1,011.80	Free Outfall	1,011.07
1,011.90	3.04	1,011.90	Free Outfall	1,011.17
1,012.00	4.24	1,012.00	Free Outfall	1,011.27
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	
0.00	0.00	(N/A)	0.00	

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir West Opening (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Area Inlet Opening (Orifice-Area)

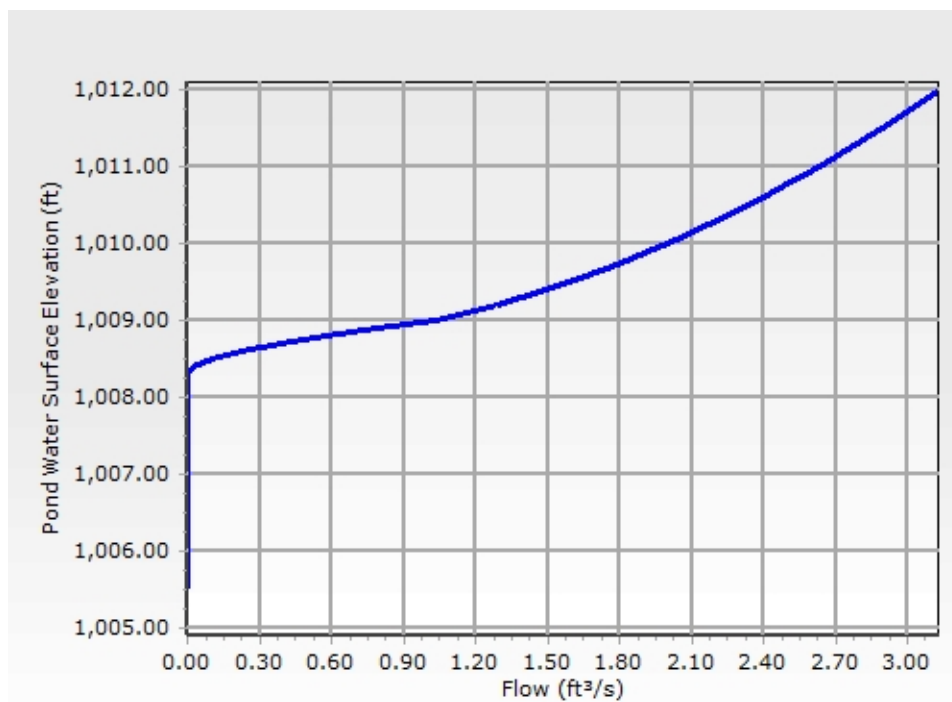
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
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 WS below an invert; no flow.

Composite Outlet Structure Detailed Report: STF Outlet

Outlet Structure			
Outlet Structure (IDs and Direction)			
Outlet ID	Underdrain	Downstream ID	Line A
Flow Direction	Forward and Reverse Flow	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Circular Orifice	Orifice Coefficient	0.610
Number of Openings	1	Orifice Diameter	8.0 in
Outlet Structure (Common)			
Elevation	1,008.30 ft		



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,005.50	0.00	0.00	0.00	0.00
1,005.60	0.00	0.00	0.00	0.00
1,005.70	0.00	0.00	0.00	0.00
1,005.80	0.00	0.00	0.00	0.00
1,005.90	0.00	0.00	0.00	0.00
1,006.00	0.00	0.00	0.00	0.00
1,006.10	0.00	0.00	0.00	0.00
1,006.20	0.00	0.00	0.00	0.00
1,006.30	0.00	0.00	0.00	0.00
1,006.40	0.00	0.00	0.00	0.00
1,006.50	0.00	0.00	0.00	0.00
1,006.60	0.00	0.00	0.00	0.00
1,006.70	0.00	0.00	0.00	0.00
1,006.80	0.00	0.00	0.00	0.00
1,006.90	0.00	0.00	0.00	0.00
1,007.00	0.00	0.00	0.00	0.00
1,007.10	0.00	0.00	0.00	0.00
1,007.20	0.00	0.00	0.00	0.00
1,007.30	0.00	0.00	0.00	0.00
1,007.40	0.00	0.00	0.00	0.00
1,007.50	0.00	0.00	0.00	0.00
1,007.60	0.00	0.00	0.00	0.00
1,007.70	0.00	0.00	0.00	0.00
1,007.80	0.00	0.00	0.00	0.00
1,007.90	0.00	0.00	0.00	0.00
1,008.00	0.00	0.00	0.00	0.00
1,008.10	0.00	0.00	0.00	0.00
1,008.20	0.00	0.00	0.00	0.00
1,008.30	0.00	0.00	0.00	0.00
1,008.40	0.03	1,008.40	Free Outfall	1,003.09
1,008.50	0.11	1,008.50	Free Outfall	1,003.18
1,008.60	0.23	1,008.60	Free Outfall	1,003.27
1,008.70	0.39	1,008.70	Free Outfall	1,003.35
1,008.80	0.58	1,008.80	Free Outfall	1,003.43
1,008.90	0.79	1,008.90	Free Outfall	1,003.51
1,009.00	1.03	1,009.00	Free Outfall	1,003.58
1,009.10	1.17	1,009.10	Free Outfall	1,003.62
1,009.20	1.29	1,009.20	Free Outfall	1,003.66
1,009.30	1.39	1,009.30	Free Outfall	1,003.68
1,009.40	1.50	1,009.40	Free Outfall	1,003.71

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Water Surface Elevation (ft)	Device Flow (ft ³ /s)	(into) Headwater Hydraulic Grade Line (ft)	Converge Downstream Hydraulic Grade Line (ft)	Next Downstream Hydraulic Grade Line (ft)
1,009.50	1.59	1,009.50	Free Outfall	1,003.73
1,009.60	1.68	1,009.60	Free Outfall	1,003.76
1,009.70	1.76	1,009.70	Free Outfall	1,003.77
1,009.80	1.84	1,009.80	Free Outfall	1,003.79
1,009.90	1.92	1,009.90	Free Outfall	1,003.81
1,010.00	2.00	1,010.00	Free Outfall	1,003.83
1,010.10	2.07	1,010.10	Free Outfall	1,003.84
1,010.20	2.14	1,010.20	Free Outfall	1,003.86
1,010.30	2.21	1,010.30	Free Outfall	1,003.87
1,010.40	2.27	1,010.40	Free Outfall	1,003.89
1,010.50	2.33	1,010.50	Free Outfall	1,003.90
1,010.60	2.40	1,010.60	Free Outfall	1,003.92
1,010.70	2.46	1,010.70	Free Outfall	1,003.93
1,010.80	2.51	1,010.80	Free Outfall	1,003.94
1,010.90	2.57	1,010.90	Free Outfall	1,003.95
1,011.00	2.63	1,011.00	Free Outfall	1,003.97
1,011.10	2.68	1,011.10	Free Outfall	1,003.98
1,011.20	2.74	1,011.20	Free Outfall	1,003.99
1,011.30	2.79	1,011.30	Free Outfall	1,004.00
1,011.40	2.84	1,011.40	Free Outfall	1,004.01
1,011.50	2.89	1,011.50	Free Outfall	1,004.02
1,011.60	2.94	1,011.60	Free Outfall	1,004.11
1,011.70	2.99	1,011.70	Free Outfall	1,004.25
1,011.80	3.04	1,011.80	Free Outfall	1,004.43
1,011.90	3.09	1,011.90	Free Outfall	1,004.64
1,012.00	3.13	1,012.00	Free Outfall	1,004.95
Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)	
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00
0.00	0.00	(N/A)	0.00	0.00

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Downstream Hydraulic Grade Line Error (ft)	Convergence Error (ft ³ /s)	Downstream Channel Tailwater (ft)	Tailwater Error (ft)
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00
0.00	0.00	(N/A)	0.00

Message

WS below an invert; no flow.
 WS below an invert; no flow.
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 WS below an invert; no flow.
 WS below an invert; no flow.

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Message
WS below an invert; no flow.
WS below an invert; no flow.
WS below an invert; no flow.
CRIT.DEPTH CONTROL Vh= .026ft
Dcr= .073ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .052ft
Dcr= .148ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .080ft
Dcr= .220ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .111ft
Dcr= .290ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .143ft
Dcr= .357ft CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL Vh= .180ft
Dcr= .420ft CRIT.DEPTH Hev= .00ft
H =.37
H =.47
H =.57
H =.67
H =.77
H =.87
H =.97
H =1.07
H =1.17
H =1.27
H =1.37
H =1.47
H =1.57
H =1.67
H =1.77
H =1.87
H =1.97
H =2.07
H =2.17
H =2.27
H =2.37
H =2.47
H =2.57
H =2.67
H =2.77
H =2.87
H =2.97
H =3.07

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

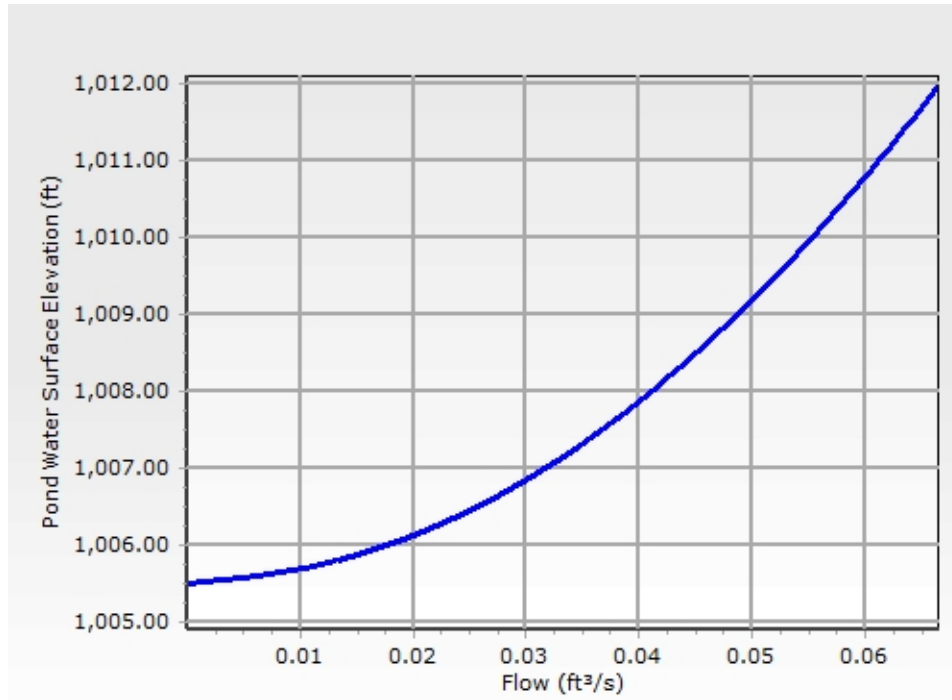
Structure ID = Underdrain (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Line A (Culvert-Circular)

Message			
H =3.17			
H =3.27			
H =3.37			
Outlet Structure			
Outlet Structure Type		Orifice	
Outlet Structure (IDs and Direction)			
Outlet ID	Drawdown	Downstream ID	Tailwater
Flow Direction	Forward and Reverse Flow	Notes	
Outlet Structure (Advanced)			
Elevation (On)	0.00 ft	Elevation (Off)	0.00 ft
Outlet Structure (Orifice)			
Orifice	Circular Orifice	Orifice Coefficient	0.600
Number of Openings	1	Orifice Diameter	1.0 in
Outlet Structure (Common)			
Elevation	1,005.50 ft		

Composite Outlet Structure Detailed Report: STF Outlet



RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Drawdown (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft³/s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,005.50	0.00	(N/A)	0.00
1,005.60	0.01	(N/A)	0.00
1,005.70	0.01	(N/A)	0.00
1,005.80	0.01	(N/A)	0.00
1,005.90	0.02	(N/A)	0.00
1,006.00	0.02	(N/A)	0.00
1,006.10	0.02	(N/A)	0.00
1,006.20	0.02	(N/A)	0.00
1,006.30	0.02	(N/A)	0.00
1,006.40	0.02	(N/A)	0.00
1,006.50	0.03	(N/A)	0.00
1,006.60	0.03	(N/A)	0.00
1,006.70	0.03	(N/A)	0.00
1,006.80	0.03	(N/A)	0.00
1,006.90	0.03	(N/A)	0.00
1,007.00	0.03	(N/A)	0.00
1,007.10	0.03	(N/A)	0.00

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Drawdown (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,007.20	0.03	(N/A)	0.00
1,007.30	0.03	(N/A)	0.00
1,007.40	0.04	(N/A)	0.00
1,007.50	0.04	(N/A)	0.00
1,007.60	0.04	(N/A)	0.00
1,007.70	0.04	(N/A)	0.00
1,007.80	0.04	(N/A)	0.00
1,007.90	0.04	(N/A)	0.00
1,008.00	0.04	(N/A)	0.00
1,008.10	0.04	(N/A)	0.00
1,008.20	0.04	(N/A)	0.00
1,008.30	0.04	(N/A)	0.00
1,008.40	0.04	(N/A)	0.00
1,008.50	0.05	(N/A)	0.00
1,008.60	0.05	(N/A)	0.00
1,008.70	0.05	(N/A)	0.00
1,008.80	0.05	(N/A)	0.00
1,008.90	0.05	(N/A)	0.00
1,009.00	0.05	(N/A)	0.00
1,009.10	0.05	(N/A)	0.00
1,009.20	0.05	(N/A)	0.00
1,009.30	0.05	(N/A)	0.00
1,009.40	0.05	(N/A)	0.00
1,009.50	0.05	(N/A)	0.00
1,009.60	0.05	(N/A)	0.00
1,009.70	0.05	(N/A)	0.00
1,009.80	0.05	(N/A)	0.00
1,009.90	0.05	(N/A)	0.00
1,010.00	0.06	(N/A)	0.00
1,010.10	0.06	(N/A)	0.00
1,010.20	0.06	(N/A)	0.00
1,010.30	0.06	(N/A)	0.00
1,010.40	0.06	(N/A)	0.00
1,010.50	0.06	(N/A)	0.00
1,010.60	0.06	(N/A)	0.00
1,010.70	0.06	(N/A)	0.00
1,010.80	0.06	(N/A)	0.00
1,010.90	0.06	(N/A)	0.00
1,011.00	0.06	(N/A)	0.00
1,011.10	0.06	(N/A)	0.00
1,011.20	0.06	(N/A)	0.00

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Drawdown (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,011.30	0.06	(N/A)	0.00
1,011.40	0.06	(N/A)	0.00
1,011.50	0.06	(N/A)	0.00
1,011.60	0.06	(N/A)	0.00
1,011.70	0.07	(N/A)	0.00
1,011.80	0.07	(N/A)	0.00
1,011.90	0.07	(N/A)	0.00
1,012.00	0.07	(N/A)	0.00

Computation Messages

WS below an invert; no flow.

H =.06
H =.16
H =.26
H =.36
H =.46
H =.56
H =.66
H =.76
H =.86
H =.96
H =1.06
H =1.16
H =1.26
H =1.36
H =1.46
H =1.56
H =1.66
H =1.76
H =1.86
H =1.96
H =2.06
H =2.16
H =2.26
H =2.36
H =2.46
H =2.56
H =2.66
H =2.76
H =2.86

Composite Outlet Structure Detailed Report: STF Outlet

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Drawdown (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Computation Messages

H =2.96
H =3.06
H =3.16
H =3.26
H =3.36
H =3.46
H =3.56
H =3.66
H =3.76
H =3.86
H =3.96
H =4.06
H =4.16
H =4.26
H =4.36
H =4.46
H =4.56
H =4.66
H =4.76
H =4.86
H =4.96
H =5.06
H =5.16
H =5.26
H =5.36
H =5.46
H =5.56
H =5.66
H =5.76
H =5.86
H =5.96
H =6.06
H =6.16
H =6.26
H =6.36
H =6.46

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,005.50	0.00	(N/A)	0.00
1,005.60	0.01	(N/A)	0.00
1,005.70	0.01	(N/A)	0.00
1,005.80	0.01	(N/A)	0.00
1,005.90	0.02	(N/A)	0.00
1,006.00	0.02	(N/A)	0.00
1,006.10	0.02	(N/A)	0.00
1,006.20	0.02	(N/A)	0.00
1,006.30	0.02	(N/A)	0.00
1,006.40	0.02	(N/A)	0.00
1,006.50	0.03	(N/A)	0.00
1,006.60	0.03	(N/A)	0.00
1,006.70	0.03	(N/A)	0.00
1,006.80	0.03	(N/A)	0.00
1,006.90	0.03	(N/A)	0.00
1,007.00	0.03	(N/A)	0.00
1,007.10	0.03	(N/A)	0.00
1,007.20	0.03	(N/A)	0.00
1,007.30	0.03	(N/A)	0.00
1,007.40	0.04	(N/A)	0.00
1,007.50	0.04	(N/A)	0.00
1,007.60	0.04	(N/A)	0.00
1,007.70	0.04	(N/A)	0.00
1,007.80	0.04	(N/A)	0.00
1,007.90	0.04	(N/A)	0.00
1,008.00	0.04	(N/A)	0.00
1,008.10	0.04	(N/A)	0.00
1,008.20	0.04	(N/A)	0.00
1,008.30	0.04	(N/A)	0.00
1,008.40	0.07	(N/A)	0.00
1,008.50	0.15	(N/A)	0.00
1,008.60	0.27	(N/A)	0.00
1,008.70	0.44	(N/A)	0.00
1,008.80	0.63	(N/A)	0.00
1,008.90	0.84	(N/A)	0.00
1,009.00	1.08	(N/A)	0.00
1,009.10	1.22	(N/A)	0.00
1,009.20	1.34	(N/A)	0.00
1,009.30	1.45	(N/A)	0.00
1,009.40	1.55	(N/A)	0.00
1,009.50	1.64	(N/A)	0.00
1,009.60	1.73	(N/A)	0.00
1,009.70	1.82	(N/A)	0.00
1,009.80	1.90	(N/A)	0.00
1,009.90	1.98	(N/A)	0.00

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
1,010.00	2.05	(N/A)	0.00
1,010.10	2.12	(N/A)	0.00
1,010.20	2.19	(N/A)	0.00
1,010.30	2.26	(N/A)	0.00
1,010.40	2.33	(N/A)	0.00
1,010.50	2.39	(N/A)	0.00
1,010.60	2.45	(N/A)	0.00
1,010.70	2.52	(N/A)	0.00
1,010.80	2.57	(N/A)	0.00
1,010.90	2.63	(N/A)	0.00
1,011.00	2.69	(N/A)	0.00
1,011.10	2.74	(N/A)	0.00
1,011.20	2.80	(N/A)	0.00
1,011.30	2.85	(N/A)	0.00
1,011.40	2.90	(N/A)	0.00
1,011.50	2.96	(N/A)	0.00
1,011.60	3.39	(N/A)	0.00
1,011.70	4.13	(N/A)	0.00
1,011.80	5.08	(N/A)	0.00
1,011.90	6.19	(N/A)	0.00
1,012.00	7.44	(N/A)	0.00

Contributing Structures

(no Q: Weir West
Opening,Area Inlet
Opening,Underdrain,Line
A,Drawdown)
Drawdown (no Q: Weir
West Opening,Area Inlet
Opening,Underdrain,Line
A)
Drawdown (no Q: Weir
West Opening,Area Inlet
Opening,Underdrain,Line
A)
Drawdown (no Q: Weir
West Opening,Area Inlet
Opening,Underdrain,Line
A)
Drawdown (no Q: Weir
West Opening,Area Inlet
Opening,Underdrain,Line
A)
Drawdown (no Q: Weir
West Opening,Area Inlet
Opening,Underdrain,Line
A)

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Contributing Structures
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Contributing Structures
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Drawdown (no Q: Weir West Opening,Area Inlet Opening,Underdrain,Line A)
Underdrain,Line A,Drawdown (no Q: Weir West Opening,Area Inlet Opening)
Underdrain,Line A,Drawdown (no Q: Weir West Opening,Area Inlet Opening)
Underdrain,Line A,Drawdown (no Q: Weir West Opening,Area Inlet Opening)

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Contributing Structures
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)

Composite Outlet Structure Detailed Report: STF Outlet

Composite Rating Table

Tailwater Elevation = Free Outfall (STF Outlet)

Contributing Structures
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Underdrain,Line
A,Drawdown (no Q: Weir
West Opening,Area Inlet
Opening)
Weir West Opening,Area
Inlet
Opening,Underdrain,Line
A,Drawdown
Weir West Opening,Area
Inlet
Opening,Underdrain,Line
A,Drawdown
Weir West Opening,Area
Inlet
Opening,Underdrain,Line
A,Drawdown
Weir West Opening,Area
Inlet
Opening,Underdrain,Line
A,Drawdown
Weir West Opening,Area
Inlet
Opening,Underdrain,Line
A,Drawdown

Composite Outlet Structure Detailed Report: STF Outlet

