

August 17, 2020

Walker Custom Homes, LLC Attn: Jason Walker

Re: 1805 River Run Drive

Vista Structural Engineering, LLC, was asked to address the following item called out during rough-in inspection by the city. Below is the inspection report comment and our response:

• Address wall framing not full plate height per plans at great room and entry; provide engineered letter and correction. At the wall in the great room, there are ceiling joists that prevent the hinge point along the majority of the wall. These ceiling joists should have two 8d toenails through the bottom of the joists and into the top of the plate that they bear on. There are locations where the ceiling joists bear below this plate (see picture on following page). These studs should each have a strap installed, fastened above and below the plate. At the entry, no remediation is needed, as there is a continuous 2x6 plate under the header that extends the full width of the wall, which acts as a beam that resists design out-of-plane (wind) loading, per the attached calculation.

Our firm appreciates the opportunity to serve you. If you have any questions or if you need anything further, please feel free to contact us.

Sincerely,

Vista Structural Engineering, LLC

Dennis Heier, P.E.



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File: WWS022 - field letter.ec6

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Wood Beam Lic. # : KW-06010523

DESCRIPTION: plate at entry wall, under header

CODE REFERENCES

Calculations per NDS 2012, IBC 2012, CBC 2013, ASCE 7-10 Load Combination Set : IBC 2018						
Material Properties						
Analysis Method : Allowable Stress Design	Fb +	900.0 psi	E : Modulus of Elasti	lulus of Elasticity		
Load Combination IBC 2018	Fb -	900.0 psi	Ebend- xx	1,600.0ksi		
	Fc - Prll	1,350.0 psi	Eminbend - xx	580.0 ksi		
Wood Species · Douglas Fir-Larch	Fc - Perp	625.0 psi				
Wood Grade : No.2	Fv .	180.0 psi				
	Ft	575.0 psi	Density	31.210 pcf		
Beam Bracing : Beam is Fully Braced against lateral-torsional l	ouckling		,			



 Applied Loads
 Service loads entered. Load Factors will be applied for calculations.

Uniform Load : W = 0.0140 ksf, Tributary Width = 6.0 ft

DESIGN SUMMARY					Design OK
Maximum Bending Stress Ratio	=	0.482 1 N	Iaximum Shear Stress Ratio	=	0.137 : 1
Section used for this span		2x6	Section used for this span		2x6
	=	902.20psi		=	39.40 psi
	=	1,872.00psi		=	288.00 psi
Load Combination		+0.60W	Load Combination		+0.60W
Location of maximum on span	=	4.750ft	Location of maximum on span	=	9.049 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection Max Downward Transient Deflect Max Upward Transient Deflection Max Downward Total Deflection Max Upward Total Deflection	ction n	0.465 in Ratio : 0.000 in Ratio : 0.279 in Ratio : 0.000 in Ratio :	= 244 >=240 = 0<240 = 408 >=180 = 0<180		

Maximum Forces & Stresses for Load Combinations

oad Combination Max Stress Ratios									Mom	Moment Values			Shear Values			
Segment Length	Span #	М	V	Сd	C _{F/V}	Сi	Cr	Сm	C t	сг	М	fb	F'b	V	fv	F'v
													0.00	0.00	0.00	0.00
Length = 9.50 ft	1			0.90	1.300	1.00	1.00	1.00	1.00	1.00			1053.00	0.00	0.00	162.00
+0.60W					1.300	1.00	1.00	1.00	1.00	1.00			0.00	0.00	0.00	0.00
Length = 9.50 ft	1	0.482	0.137	1.60	1.300	1.00	1.00	1.00	1.00	1.00	0.57	902.20	1872.00	0.22	39.40	288.00
+0.450W					1.300	1.00	1.00	1.00	1.00	1.00			0.00	0.00	0.00	0.00
Length = 9.50 ft	1	0.361	0.103	1.60	1.300	1.00	1.00	1.00	1.00	1.00	0.43	676.65	1872.00	0.16	29.55	288.00
Overall Maximum Deflections																
Load Combination		S	ipan	Max. "-"	Defl	Location	n in Span		Load Co	ombinatio	n		Max. "+"	Defl	Location in	Span
W Only			1	0.4653		4.785							0.0	000	0.	000
Vertical Reac	actions Su				Sup	oport notation : Far left is #1 Values i					Values in K	IPS				
Load Combination					Suppor	t1 Su	pport 2									
Overall MAXimum					0.3	199	0.399									