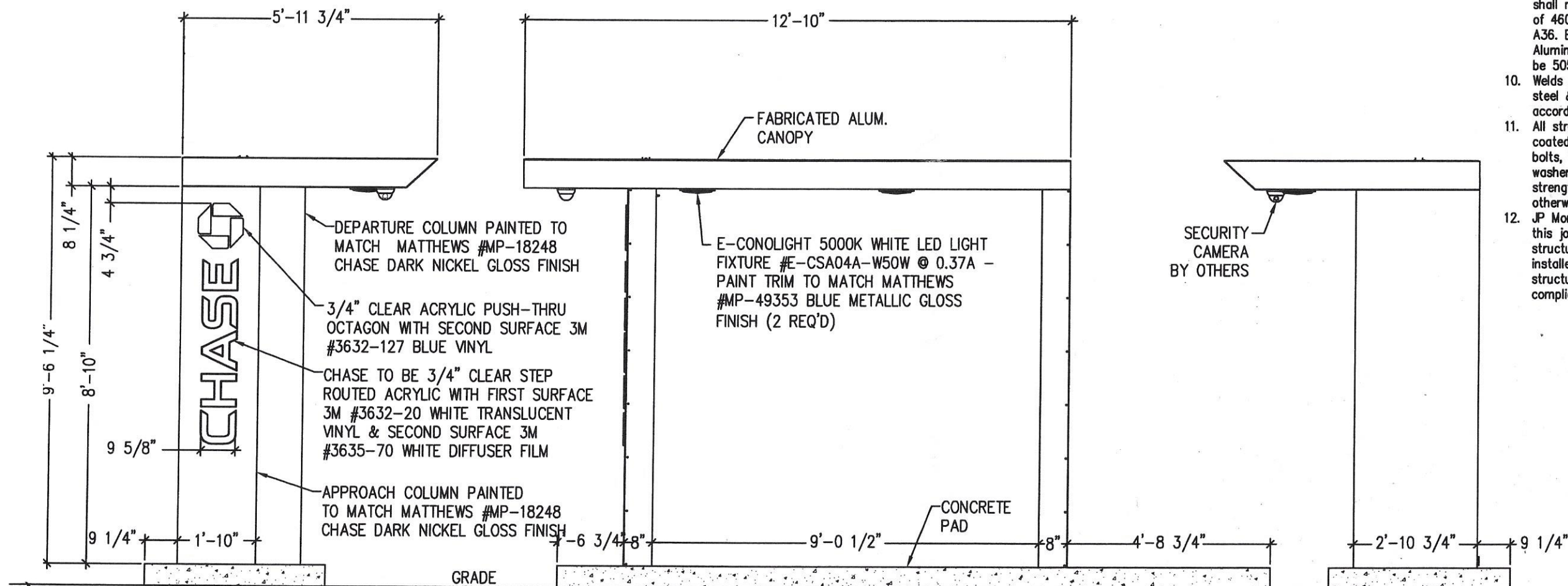
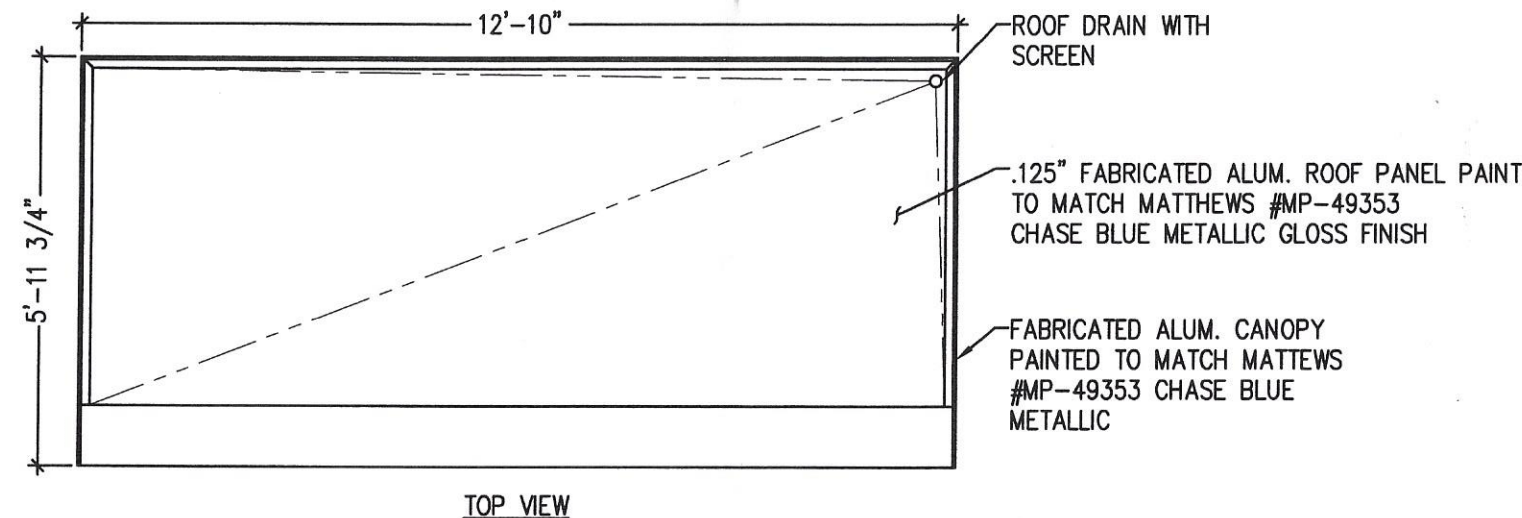


CANOPY ELECTRICAL REQUIREMENTS (NOT INCLUDING ATM MACHINE, SECURITY CAMERA & RELATED APPLIANCES):
LEDS: (41) 7100°K WHITE SLOAN PRISM #701269-7WSJ1-MB
 (43) BLUE SLOAN PRISM #701269-BLSJ1-MB
DOWNLIGHTS: (2) E-CONOLIGHT 5000K WHITE LED LIGHT
 FIXTURE #E-CSA04A-W50W @ 0.37A
LED POWER SUPPLY: (3) SLOAN #701507-60C1 @ 0.70A
TOTAL LOAD: 2.84 AMPS @ 120VAC
CIRCUITS: (1) 20 AMP REQ'D.

ALL EXPOSED PAINTED SURFACES SHALL BE COATED WITH MATTHEWS #282-208SP VOC GLOSS CLEAR, WITH MINIMUM 2 MILS DRY FILM THICKNESS (DFT) PER MATTHEWS APPLICATION SPECIFICATIONS.



General Notes:

- Design is based on a 115 mph, 3 second gust wind design per IBC 2015, Category II, Exposure C. 40psf Ground Snow Load.
- Spread foundation is based on a presumptive safe vertical soil bearing pressure minimum of 1500 psf.
- A soil report was not provided. Foundation analysis assumes Soil Classification 5. Allowable bearing pressure should be verified prior to placement of concrete. In the event that the stated requirements are not met and conditions appear deleterious, cease and secure excavation and immediately contact the project manager.
- Foundation shall not be placed at the top of, or on the side of a slope exceeding 3:1, or adjacent to a fill slope unless re-evaluated by a competent Professional Engineer. Do not place foundation in fill.
- Concrete shall be mixed to attain a minimum 28 day compressive strength of 3000 psi.
- Steel reinforcing bars shall conform to ASTM A615, Grade 60 with deformations in accordance with ASTM A305. Welding of reinforcing bars is prohibited.
- All voids between column base plate and foundation surface shall be completely filled with high-strength, non-shrink grout.
- Anchor bolts shall meet ASTM F1554 Grade 36. Exposed surfaces shall be galvanized or coated to prevent corrosion.
- All support members shall be free from defects. Steel tube shall meet ASTM A500 Grade B with a minimum yield strength of 46000 psi. Steel angle, channel and plate shall meet ASTM A36. Extruded aluminum shapes shall be 6061-T6 alloy. Aluminum sheet shall be 3003-H14 alloy. Aluminum plate shall be 5052-H34 alloy.
- Welds shall be made with E70xx low hydrogen electrodes for steel & with 5356 filler for aluminum by persons qualified in accordance with AWS standards within the past two years.
- All structural bolts shall conform to ASTM A325, and be zinc coated unless noted otherwise. When used with structural bolts, heavy hex nuts shall conform to ASTM A563, and washers shall conform to ASTM F436. Pretension all high strength bolts using the Turn-of-Nut method unless noted otherwise.
- JP Morgan Chase will not be responsible for the safety on this job site before, during or after installation of this structure. It is the responsibility of the contractors and installers to ensure that the installation and erection of this structure is performed using methods that are in full compliance with OSHA regulations.

Jeff L. Griffin
 12255 W. 187th St.
 Mokena, IL 60448



APPROACH ELEVATION

ELEVATION

DEPARTURE ELEVATION

2/18/11	CHANGED COLOR TO ANTI-GRAB DARK NICKEL, REMOVED WHITE OCTAGON ON DEPARTURE COLUMN, CHANGED COLOR OF APPROACH COLUMN TO PINK-SHED, CHANGED COPY TOP PLATE, CHANGED ROOF GROUND TO FACED SIDE, CHANGED APPROACH COLUMN GROUND SIDE TO BLUE PINK SIDE.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO MP-18248 DARK NICKEL FROM MP-49353 METALLIC BLUE	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK
				8/31/11	REMOVED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICEABILITY	TRR	IK	6/20/16	CHANGED PERMLIGHT LEDs TO GE	TRR	IK	10/2/17	UPDATED E-COS SERIES LIGHT FIXTURES TO THE E-CSA04 SERIES LIGHT FIXTURES	JO	IK
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT, CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDs & DOWNLIGHTS	JO	IK
CHASE		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.		SHT. 1 OF 12		BY: TRR DATE: 1/27/09		Project No. 08-1218 Drawing No. B244040		11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.					
										7/30/10	ADDED CLEAR COAT NOTE	TRR	IK						
										6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUD CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK						
										5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK						
										REV.	DATE	DESCRIPTION	BY:	APR:	DESIGNATION: CAN-ATM-SIG-OCT				

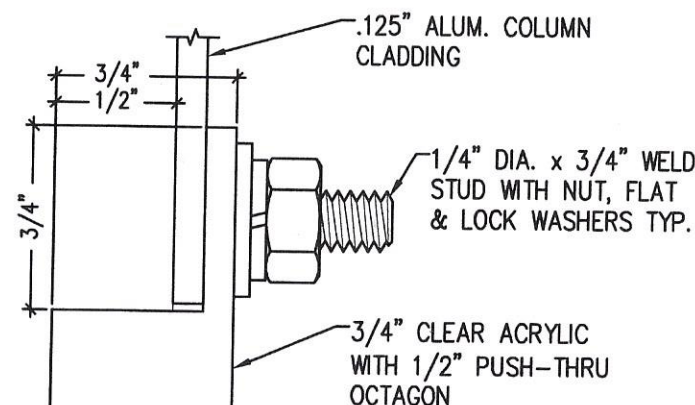
DESIGNATION:

CAN-ATM-SIG-OCT

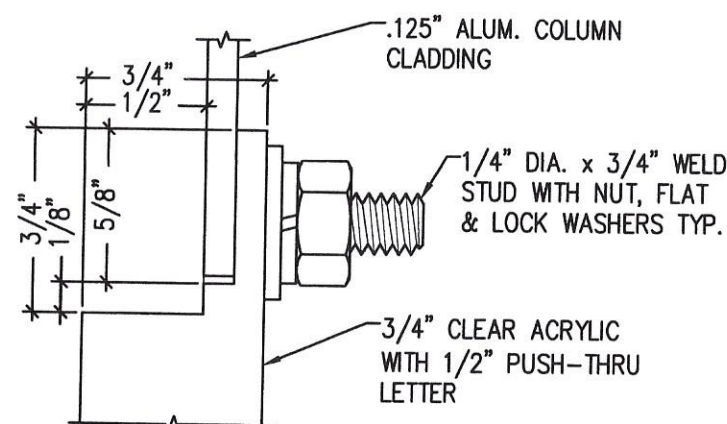
9/11/19

CHANGED ROOF OCTAGON FROM 1/2" TO 1/4" THICK, CHANGED ROOF OCTAGON MOUNTING TUBES TO 1/8" THICK FROM 1/2", CHANGED PLACEMENT OF 4-BOLTS IN APPROACH COLUMN FOR BETTER SERVICE ACCESS, EXTENDED FOUNDATION TO INCLUDE ELEC. PEDESTAL.

TRR IK

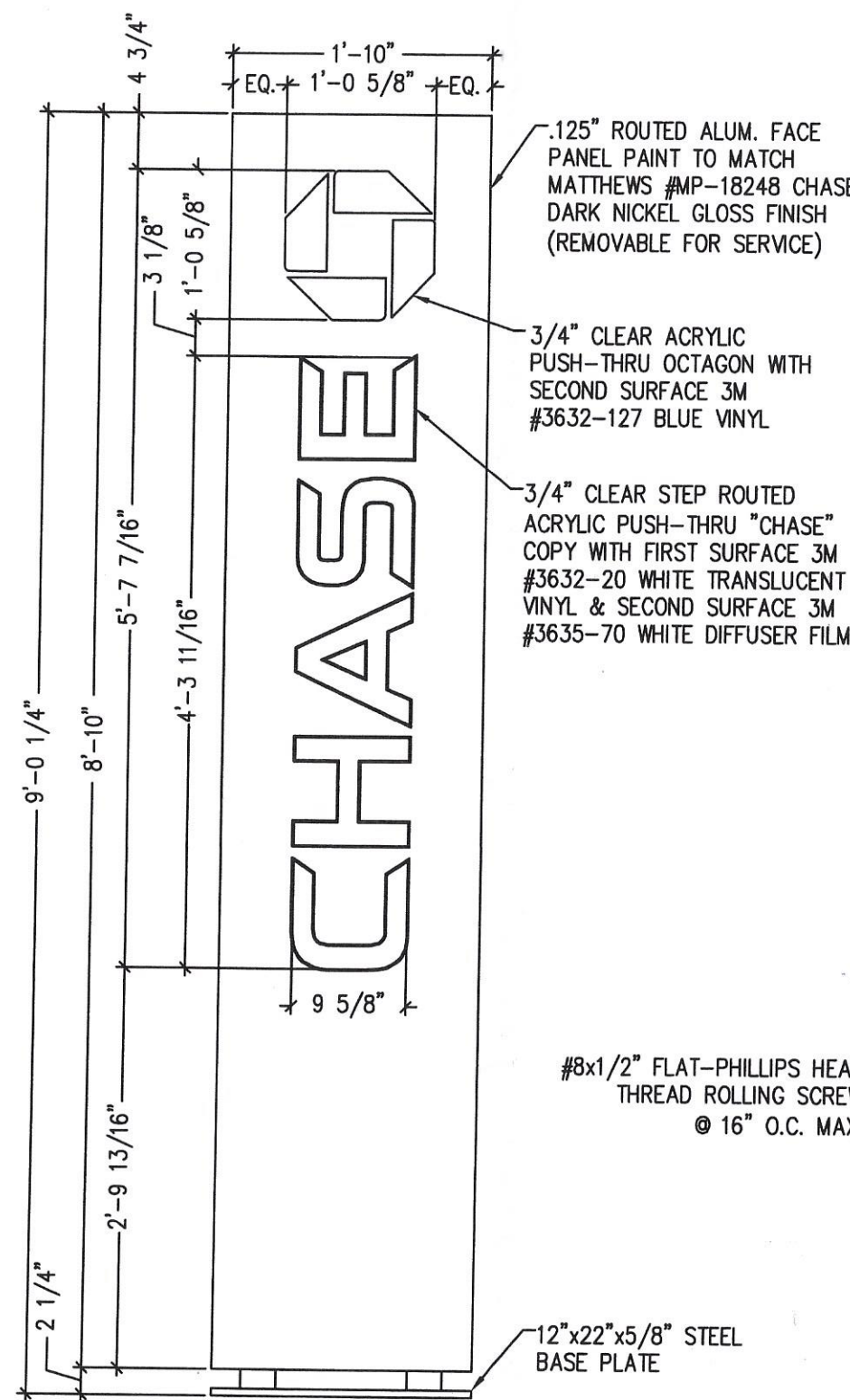


OCTAGON ATTACHMENT DETAIL

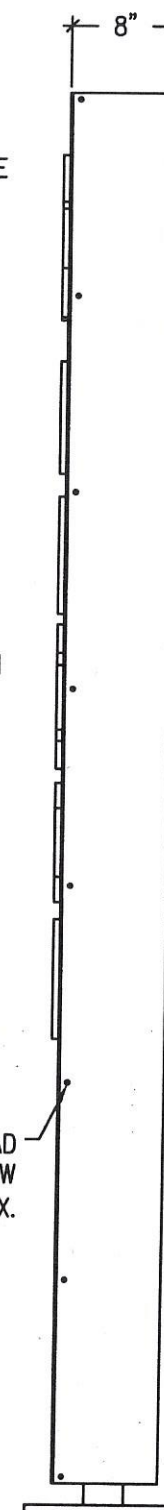


PUSH-THRU LETTER MOUNTING DETAIL

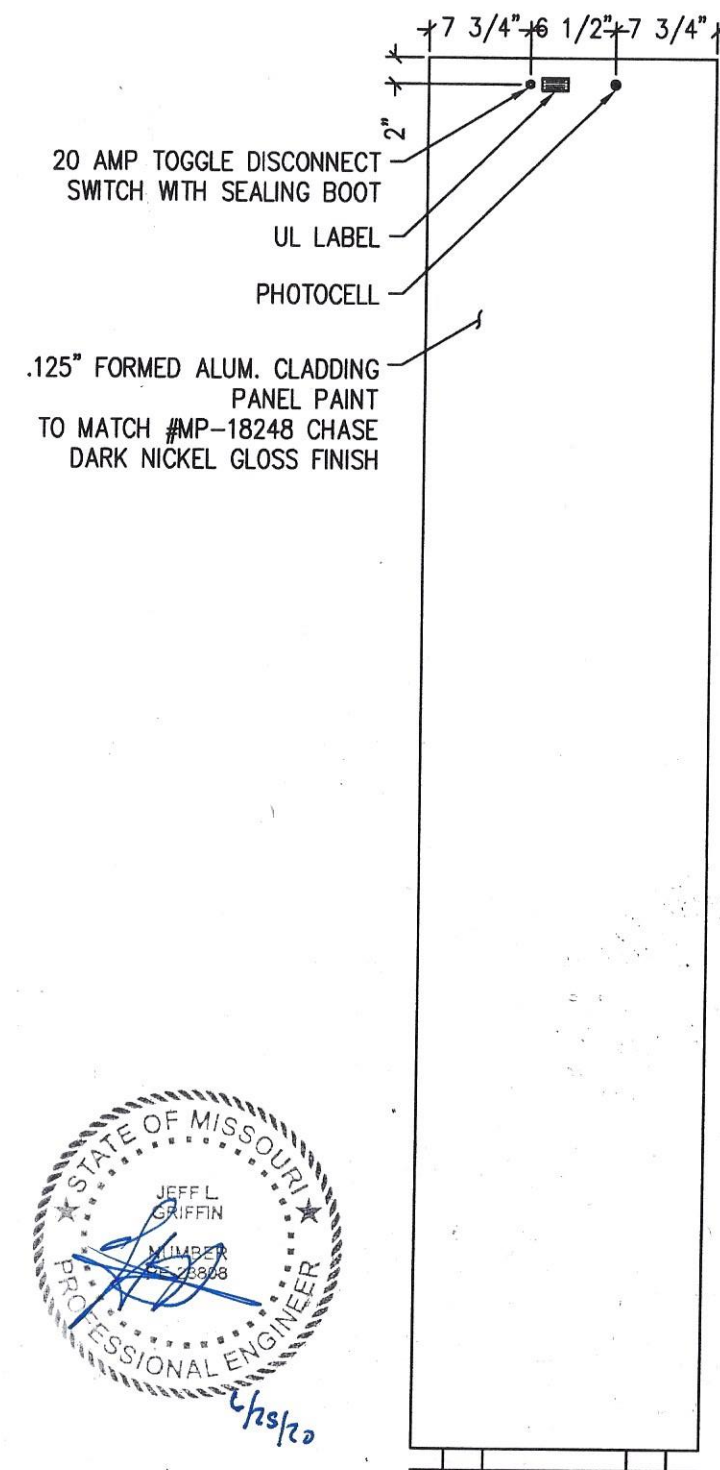
STEP ROUTING OF LETTERS SHALL BE FINISHED WITH A 1/8" DIA. BIT TO PROVIDE SHARP CORNERS



APPROACH COLUMN APPROACH VIEW



APPROACH COLUMN ELEVATION



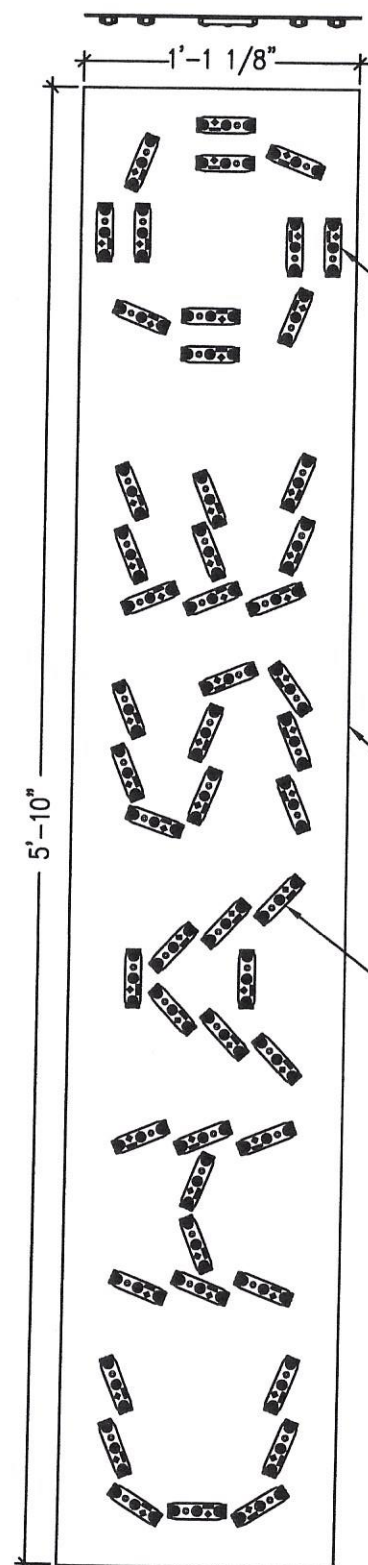
APPROACH COLUMN DEPARTURE VIEW



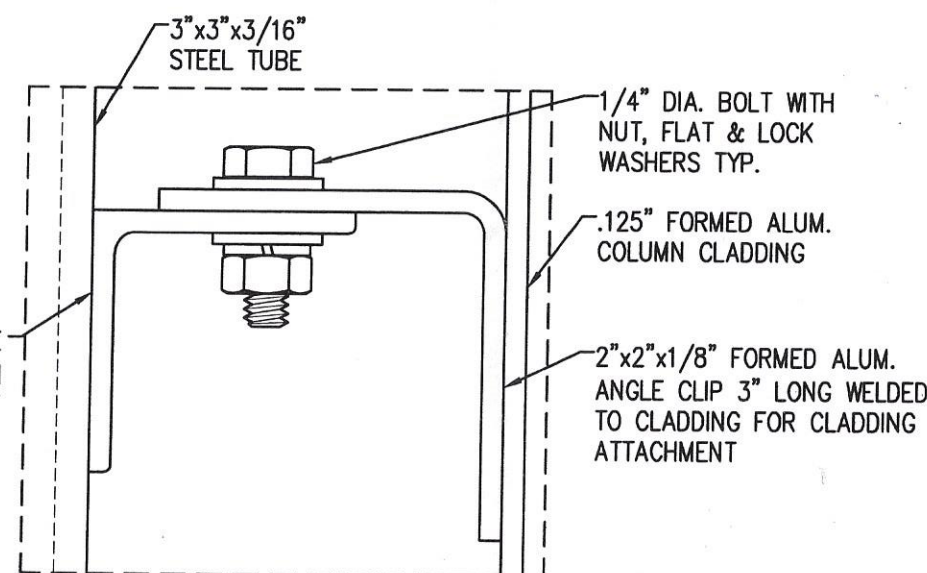
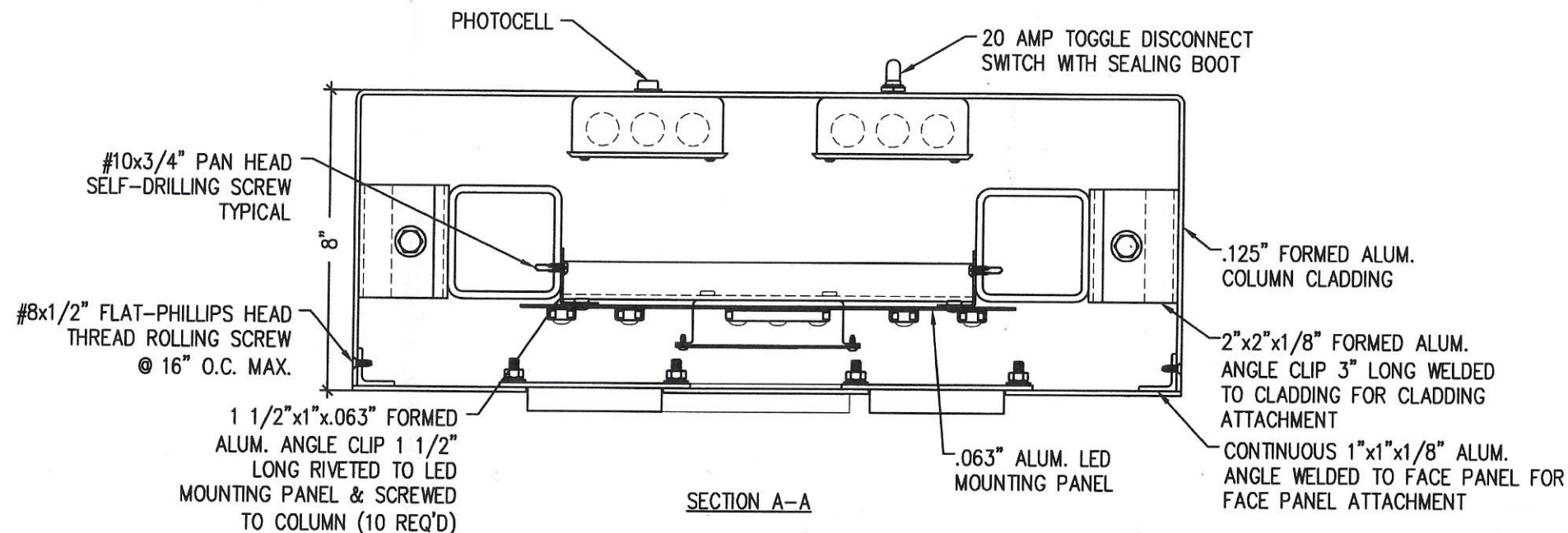
2/18/11	CHANGED COLOR TO 20-1000 DARK NICKEL, REMOVED THE OCTAGON ON DEPARTURE COLUMN, CHANGED OCTAGON ON APPROACH COLUMN TO PUSH-THRU, AND "CHASE" COPY STEP-ROUTED, CHANGED ROOF OCTAGON TO PUSHER, REMOVED APPROACH COLUMN OCTAGON LINE TO BLUE FROM WHITE.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO #MP-18248 DARK NICKEL FROM #MP-40353 METALLIC BLUE	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	8/31/11	REVISED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICABILITY	TRR	IK	6/20/16	CHANGED PERMLIGHT LED TO GE	TRR	IK	10/2/17	UPDATED E-COS SERIES LIGHT FIXTURES TO THE E-COSM4 SERIES LIGHT FIXTURES	JO	IK
				4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT, CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDS & DOWNLIGHTS	JO	IK
CHASE 		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.		SHT. 2		BY: TRR		Project No. 08-1218		11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.					
				OF 12		DATE: 1/27/09		Drawing No. B244040		7/30/10	ADDED CLEAR COAT NOTE	TRR	IK						
										6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUD CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK						
										5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK						
										REV. DATE	DESCRIPTION		BY: APR:						

DESIGNATION: CAN-ATM-SIG-OCT

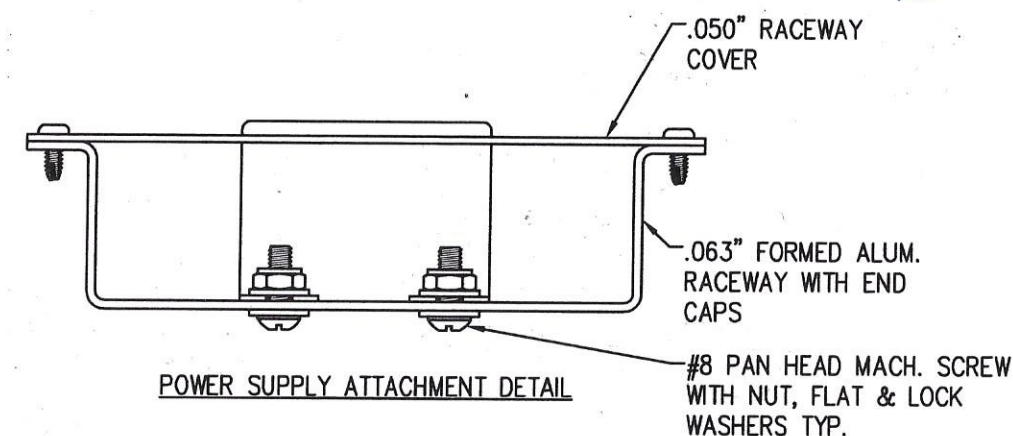
9/11/19	CHANGED ROOF OCTAGON FACES TO CURVED STYLE, CHANGED ROOF OCTAGON MOUNTING TUBES TO .188" THICK FROM .125", CHANGED PLACEMENT OF J-BOLTS IN APPROACH COLUMN FOR BETTER SERVICE ACCESS, EXTENDED FOUNDATION TO INCLUDE ELEC. PESTAL	TRR	IK
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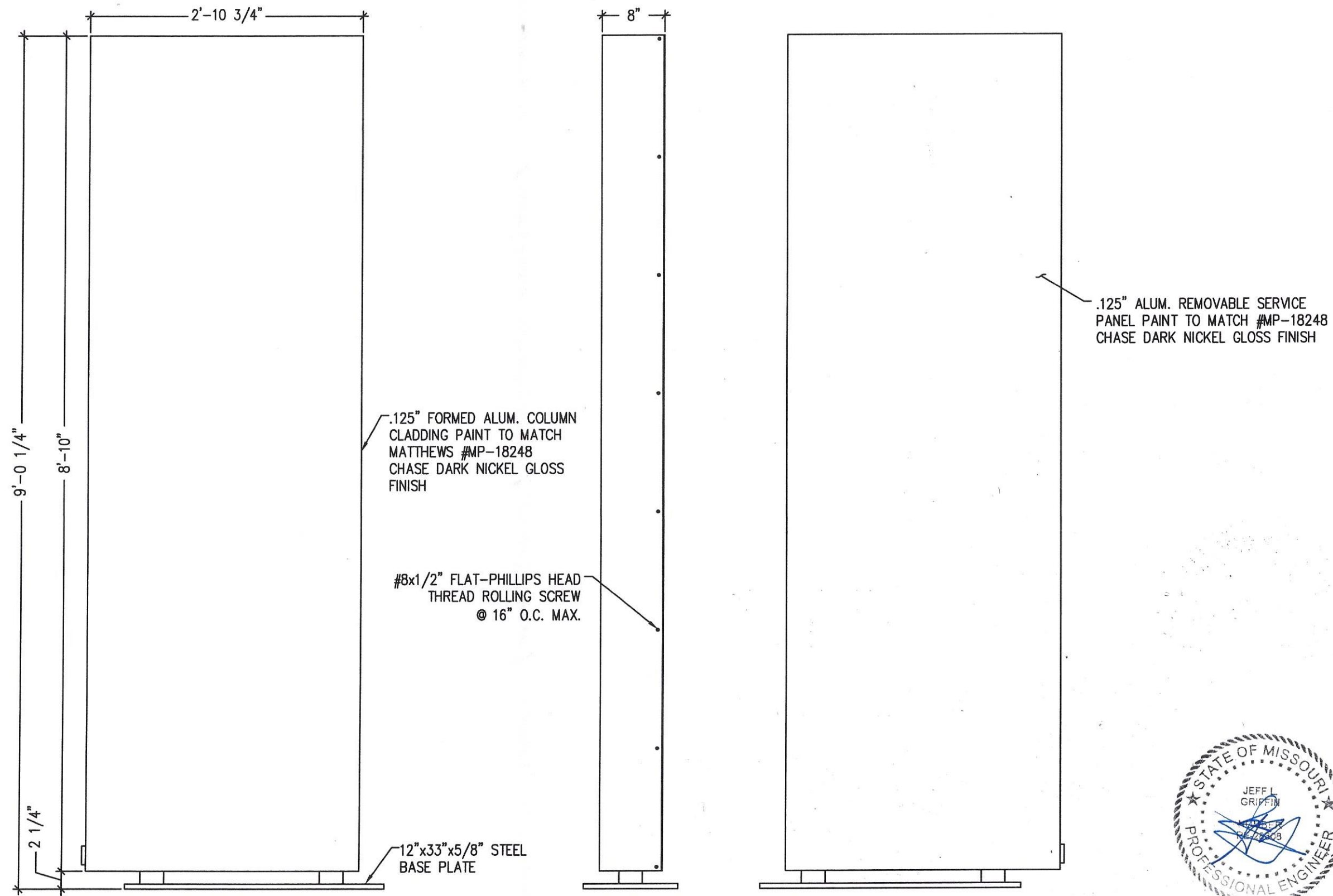
LED MOUNTING PANEL DETAIL



DETAIL A



2/18/11	CHANGED COLOR TO 100% WHITE BASE COLOR. REMOVED WHITE OCTAGON ON ROOF. CHANGED COLOR OF APPROACH COLUMN TO 100% WHITE. CHANGED APPROACH COLUMN COLOR TO 100% WHITE.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO 100% WHITE. CHANGED APPROACH COLUMN COLOR TO 100% WHITE.	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK		
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	8/31/11	REMOVED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICEABILITY	TRR	IK	6/20/16	CHANGED PERMILIGHT LEDS TO GE	TRR	IK	10/2/17	UPDATED E-COS SERIES LIGHT FIXTURES TO THE E-COS4 SERIES LIGHT FIXTURES	JO	IK		
				4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT. CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDS & DOWNLIGHTS	JO	IK		
CHASE		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.		SHT. 4 OF 12		BY: TRR DATE: 1/27/09		Project No. 08-1218 Drawing No. B244040		11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.							
										7/30/10	ADDED CLEAR COAT NOTE	TRR	IK								
										6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUD CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK								
										5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK								
										REV. DATE	DESCRIPTION	BY:	APR:								
																DESIGNATION: CAN-ATM-SIG-OCT		9/11/19	CHANGED ROOF OCTAGON FACES TO CURVED STYLE. CHANGED ROOF OCTAGON MOUNTING TUBES TO 1.88" THICK FROM .125". CHANGED PLACEMENT OF J-BOLTS IN APPROACH COLUMN FOR BETTER SERVICE ACCESS. EXTENDED FOUNDATION TO INCLUDE ELECT. PEDestal.	TRR	IK



.125" ALUM. REMOVABLE SERVICE
PANEL PAINT TO MATCH #MP-18248
CHASE DARK NICKEL GLOSS FINISH

.125" FORMED ALUM. COLUMN
CLADDING PAINT TO MATCH
MATTHEWS #MP-18248
CHASE DARK NICKEL GLOSS
FINISH

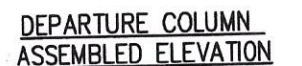
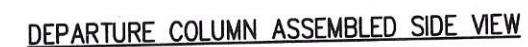
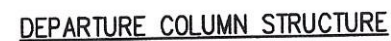
#8x1/2" FLAT-PHILLIPS HEAD
THREAD ROLLING SCREW
@ 16" O.C. MAX.

12"x33"x5/8" STEEL
BASE PLATE



DEPARTURE COLUMN APPROACH VIEW DEPARTURE COLUMN ELEVATION DEPARTURE COLUMN DEPARTURE VIEW

A	2/18/11	CHANGED COLOR TO MP-18248 DARK NICKEL GLOSS. REVISED WHITE OCTAGON ON DEPARTURE COLUMN. CHANGED OCTAGON ON APPROACH COLUMN TO PINK-NICKEL. CHANGED CAP PLATE TO OCTAGON. CHANGED BASE PLATE TO PINK-NICKEL. CHANGED APPROACH COLUMN OCTAGON LINE TO BLUE FROM WHITE.	TRR	IK	A	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO MP-18248 DARK NICKEL FROM MP-18248 METALLIC BLUE.	TRR	IK	A	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	A	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	A	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK	
					A	8/31/11	REVISED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY			TRR	IK	A			7/23/12	REVISED APPROACH COLUMN FOR SERVICABILITY	TRR			IK	A	6/20/16			CHANGED PERMULIGHT LEDs TO GE
A	12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	A	4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT. CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	A	2/22/12	REVISED FOUNDATION	TRR	IK	A	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	A	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDs & DOWNLIGHTS	JO	IK	
CHASE		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.	SHT.		BY:		Project No.		A	11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.				DESIGNATION:		A	9/11/19	CHANGED ROOF OCTAGON FACES TO CURVED STYLE. CHANGED ROOF OCTAGON MOUNTING TUBES TO .188" THICK FROM .125". CHANGED PLACEMENT OF J-SERIES IN APPROACH COLUMN FOR BETTER SERVICE ACCESS. EXTENDED FOUNDATION TO INCLUDE ELECT. PENETRAL.		TRR	IK
			5		TRR		08-1218		A	7/30/10	ADDED CLEAR COAT NOTE	TRR	IK												
			OF		DATE:		Drawing No.		A	6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUB CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK												
									A	5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK												
									REV.	DATE	DESCRIPTION	BY:	APR:												
				12		1/27/09		B244040																	

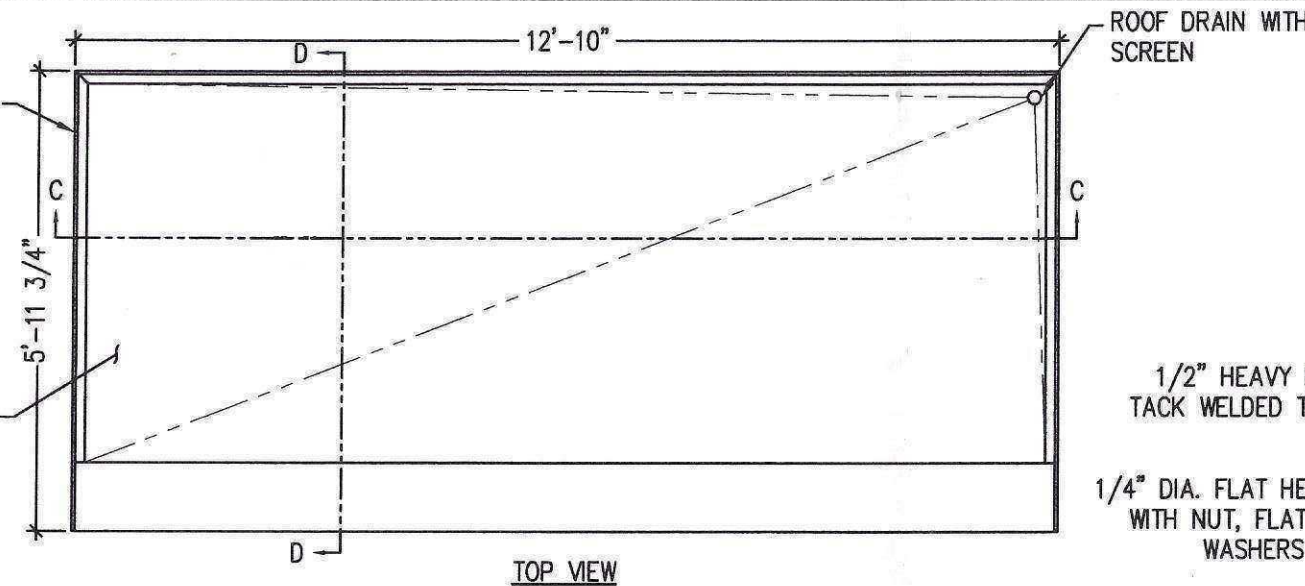


DEPARTURE COLUMN STRUCTURE																								
	2/18/11	CHANGED COLOR TO RDP-7698 DARK BROWN. REVERSED ROOF ORIENTATION OF CANOPY. CHANGED APPROACH COLUMN COLOR FROM BLUE TO RDP-10353 METALLIC BLUE.	TRR	IK		11/22/11	CHANGED DEPARTURE COLUMN COLOR TO RDP-10353 METALLIC BLUE	TRR	IK		10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK		9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK		11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK
	8/31/11	REVERSED LOGO ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK		8/31/11	REVERSED APPROACH COLUMN FOR SERVICEABILITY	TRR	IK		7/23/12	REVISED APPROACH COLUMN FOR SERVICEABILITY	TRR	IK		6/20/16	CHANGED PERMLIGHT LED'S TO GE	TRR	IK		10/2/17	UPDATED E-COS SERIES LIGHT FIXTURES TO THE E-CSA04 SERIES LIGHT FIXTURES	JO	IK
	12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK		4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK		2/22/12	REVISED FOUNDATION	TRR	IK		12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK		6/29/17	REVISED FOUNDATION DETAILS & UPDATED LED'S AND DOWNLIGHTS	JO	IK
		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the consent of the owner is strictly prohibited.	SHT.	6	BY:	TRR	Project No.	08-1218		11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.	DESIGNATION: CAN-ATM-SIG-OCT									
										7/30/10	ADDED CLEAR COAT NOTE	TRR	IK											
										6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUB CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK											
										5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK											
									REV.	DATE	DESCRIPTION		BY:			APR:								

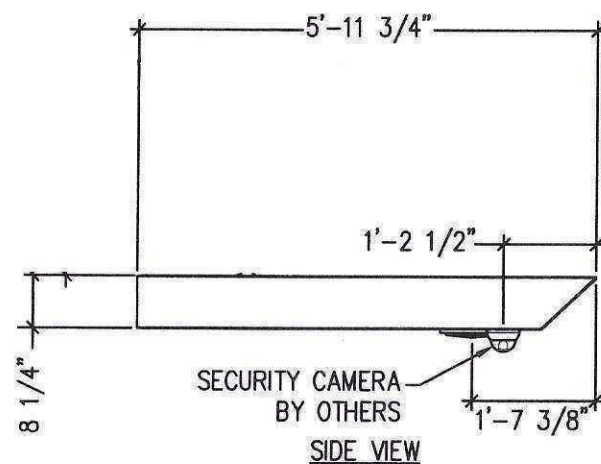


FABRICATED ALUM. CANOPY
PAINTED TO MATCH MATTEWS
#MP-49353 CHASE BLUE
METALLIC

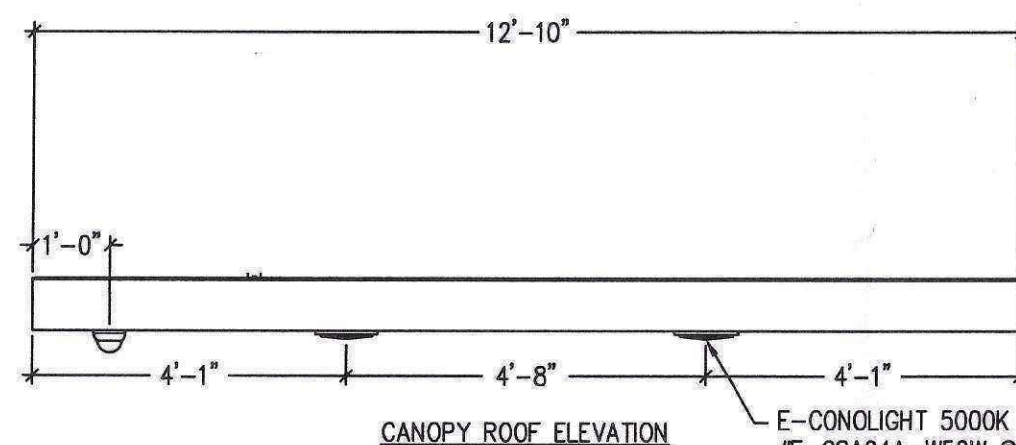
.125" FABRICATED ALUM. ROOF PANEL
PAINT TO MATCH MATTEWS #MP-49353
CHASE BLUE METALLIC GLOSS FINISH



TOP VIEW

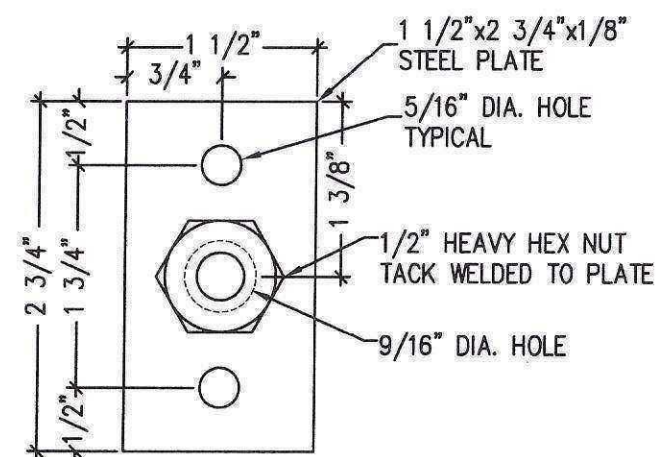


SIDE VIEW



CANOPY ROOF ELEVATION

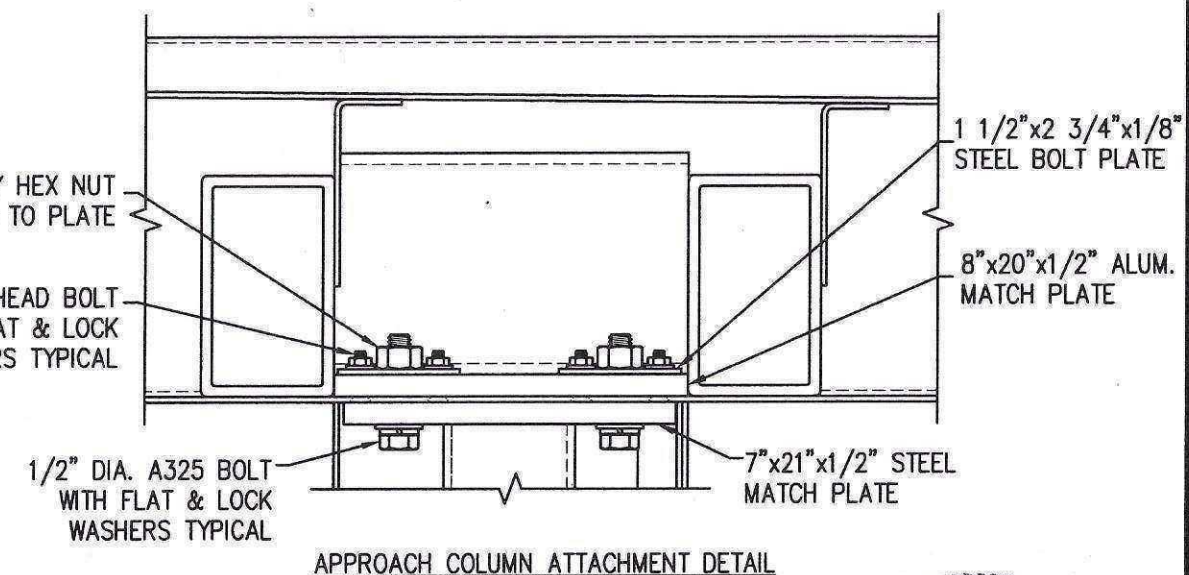
E-CONOLIGHT 5000K WHITE LED LIGHT FIXTURE
#E-CSA04A-W50W @ 0.37A - PAINT TRIM TO
MATCH MATTEWS #MP-49353 BLUE METALLIC
GLOSS FINISH (2 REQ'D)



BOLT PLATE DETAIL

ROOF DRAIN WITH
SCREEN

1/2" HEAVY HEX NUT
TACK WELDED TO PLATE
1/4" DIA. FLAT HEAD BOLT
WITH NUT, FLAT & LOCK
WASHERS TYPICAL

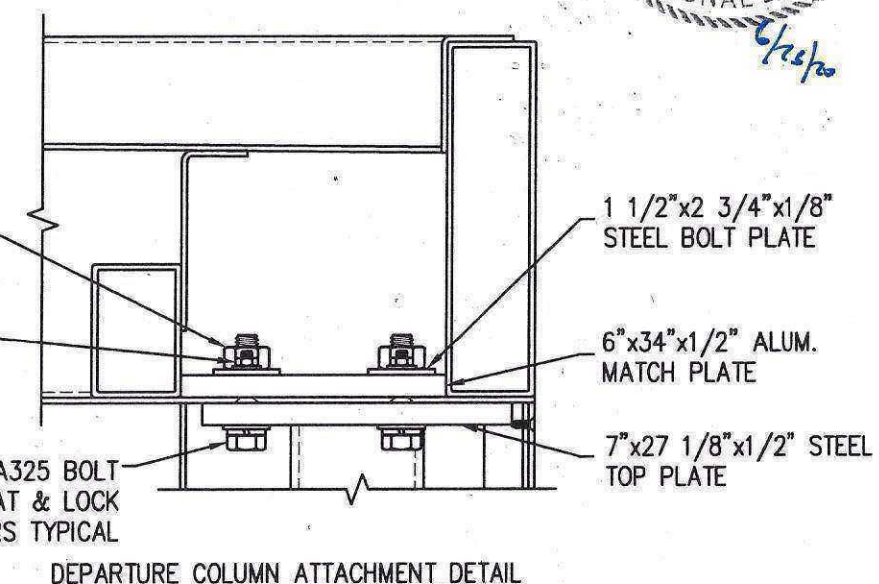


APPROACH COLUMN ATTACHMENT DETAIL



1/2" HEAVY HEX NUT
TACK WELDED TO PLATE
1/4" DIA. FLAT HEAD BOLT
WITH NUT, FLAT & LOCK
WASHERS TYPICAL

1/2" DIA. A325 BOLT
WITH FLAT & LOCK
WASHERS TYPICAL



DEPARTURE COLUMN ATTACHMENT DETAIL

2/18/11	CHANGED COLUMN TO 40-1000 DARK NICKEL. REVISED THREE OCTAGON ON APPROACH COLUMN. CHANGED OCTAGON ON APPROACH COLUMN TO 100-1000. CHANGED APPROACH COLUMN OCTAGON TO 100-1000. CHANGED APPROACH COLUMN OCTAGON TO 100-1000.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO #MP-10249 DARK NICKEL FROM #MP-46353 METALLIC BLUE	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RIJUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	8/31/11	REVISED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICABILITY	TRR	IK	6/20/16	CHANGED PERMLIGHT LEDS TO GE	TRR	IK	10/2/17	UPDATED E-COS SERIES LIGHT FIXTURES TO THE E-CSA04 SERIES LIGHT FIXTURES	JO	IK
				4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT. CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDS & DOWNLIGHTS	JO	IK



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7
OF
12

DATE:
1/27/09

Project No.
08-1218
Drawing No.
B244040

REV.	DATE	DESCRIPTION
11/16/10		ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY
7/30/10		ADDED CLEAR COAT NOTE
6/1/09		ADDED CAP PLATE TO OCTAGON MOUNTING STUD CALLED SECURITY CAMERA TO BE BY OTHERS
5/15/09		CHANGED CANOPY TO PSCO DESIGN

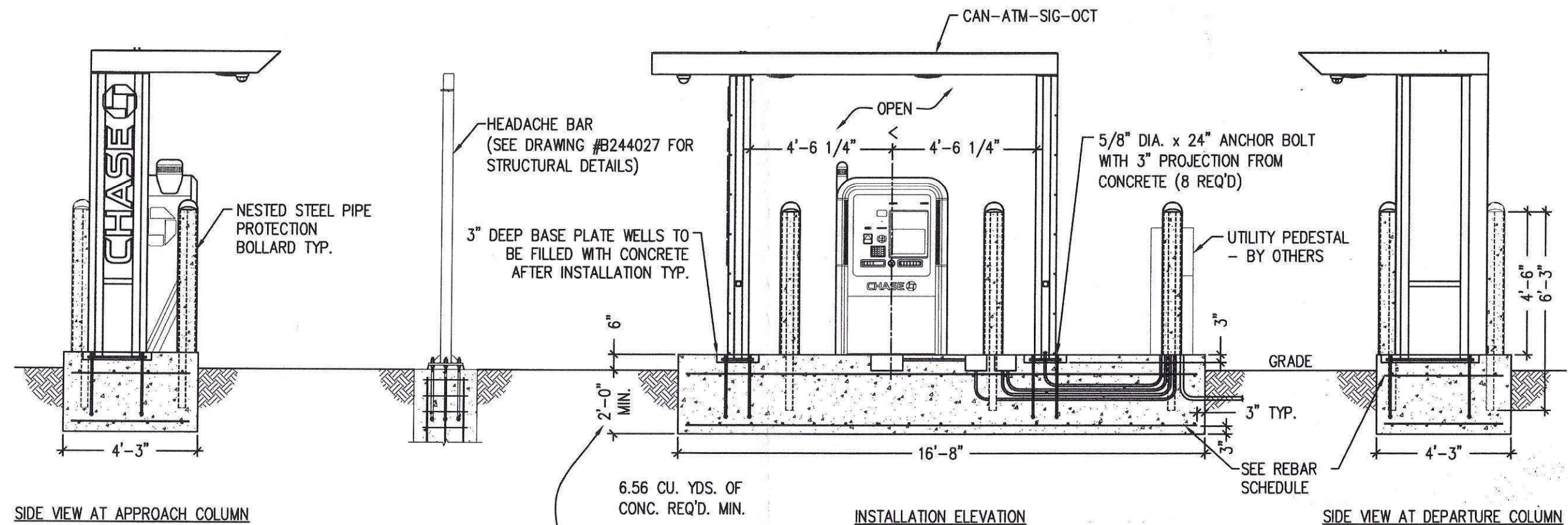
BY:	TRR
APR:	

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DESIGNATION:

CAN-ATM-SIG-OCT

9/11/19	CHANGED ROOF OCTAGON FROM 100-1000 TO 100-1000. CHANGED ROOF OCTAGON MOUNTING STUDS TO 1/2" THICK FROM 1/4". CHANGED PLACEMENT OF J-BOLTS IN APPROACH COLUMN FOR BETTER SERVICE ACCESS. EXTENDED FOUNDATION TO INCLUDE ELECT. PENETRAL	TRR	IK
---------	--	-----	----



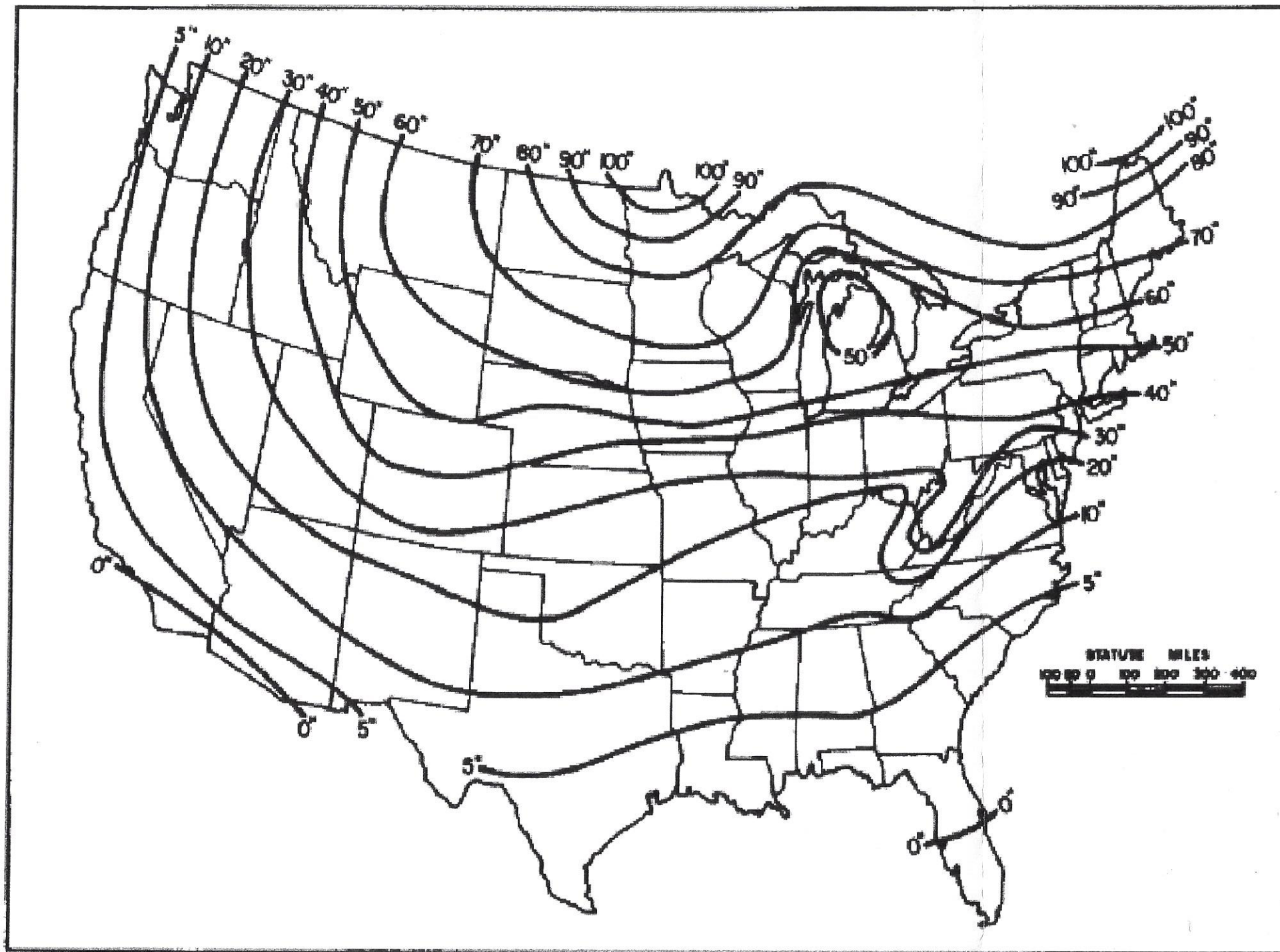
WHERE THE EXTREME FROST PENETRATION DEPTH REQUIREMENT IS GREATER THAN THE SPECIFIED DEPTH OF THE FOUNDATION SHOWN ON THIS SHEET, THE FOUNDATION DESIGN SHOULD BE ALTERED TO MEET THE LOCAL FROST DEPTH REQUIREMENTS. SEE MAP ON SHEET 12 OF 12 FOR GENERAL DEPTH GUIDELINES.

REBAR SCHEDULE		DO NOT WELD REBAR	
SPREAD FOUNDATION			
PLACEMENT	SIZE	SPACING	QUANTITY
OVERTURN BOTTOM STEEL	#5	12"	17
OVERTURN TOP STEEL	#5	12"	17
BOTTOM CROSS STEEL	#5	13"	4
TOP CROSS STEEL	#5	13"	4



2/18/11	CHANGED COLOR TO ANP-SEMI GLOSS WHITE. REVISED WHITE OCTAGON ON DEPARTURE COLUMN. CHANGED OCTAGON ON APPROACH COLUMN TO PINK-WHITE. BASE "CHASE" COPY TYP-REPLACED. CHANGED ROOF COLUMN TO PINK-WHITE. CHANGED APPROACH COLUMN OCTAGON LENS TO BLUE FROM WHITE.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO ANP-18248 DARK NICKEL FROM ANP-10353 METALLIC BLUE.	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK																			
				8/31/11	REVISED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY.	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICABILITY	TRR	IK	6/20/16	CHANGED PERMLIGHT LEDS TO GE	TRR	IK	10/2/17	UPDATED E-OC5 SERIES LIGHT FIXTURES TO THE E-OS404 SERIES LIGHT FIXTURES	JO	IK																			
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT. CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDS & DOWNLIGHTS	JO	IK																			
CHASE These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.				SHT.	BY:	Project No.	11/16/10	ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY	TRR	IK	GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.				DESIGNATION:				CAN-ATM-SIG-OCT				9/11/19				CHANGED ROOF OCTAGON FACES TO CURVED STYLE. CHANGED ROOF OCTAGON MOUNTING TUBES TO .1875" THICK FROM .125". CHANGED PLACEMENT OF J-SERIES IN APPROACH COLUMN FOR BETTER SERVICE ACCESS. EXTENDED FOUNDATION TO INCLUDE ELECT. PEDESTAL.				TRR				IK			
				10	TRR	08-1218	7/30/10	ADDED CLEAR COAT NOTE	TRR	IK																												
				OF	DATE:	Drawing No.	6/1/09	ADDED CAP PLATE TO OCTAGON MOUNTING STUD CALLED SECURITY CAMERA TO BE BY OTHERS	TRR	IK																												
				12	1/27/09	B244040	5/15/09	CHANGED CANOPY TO PSCO DESIGN	TRR	IK																												
											REV. DATE	DESCRIPTION	BY:	APR:																								





WHERE THE EXTREME FROST PENETRATION DEPTH REQUIREMENT IS GREATER THAN THE SPECIFIED DEPTH OF THE FOUNDATION SHOWN ON SHEET 10 OF 12, THE FOUNDATION DESIGN SHOULD BE ALTERED TO MEET THE LOCAL FROST DEPTH REQUIREMENTS. SEE MAP AT LEFT FOR GENERAL GUIDELINES.

FIGURE 7
Extreme Frost Penetration (in inches) Based Upon State Average



2/18/11	CHANGED COLOR TO 100% WHITE. REVISED WIRE COORDINATES OF DEPARTURE COLUMN. CHANGED COLOR OF APPROACH COLUMN TO 100% WHITE. CHANGED APPROACH COLUMN DESIGN FROM 1/2" DIA. TO 1/4" DIA.	TRR	IK	11/22/11	CHANGED DEPARTURE COLUMN COLOR TO 100% WHITE. CHANGED COLOR OF APPROACH COLUMN TO 100% WHITE. CHANGED APPROACH COLUMN DESIGN FROM 1/2" DIA. TO 1/4" DIA.	TRR	IK	10/31/13	ADDED TACK WELD SYMBOL TO A.B. DETAILS	TRR	IK	9/6/16	CHANGED RUUD LIGHT FIXTURE TO CREE	TRR	IK	11/14/17	CHANGED COLUMN TOP PLATES TO 1/2" FROM 1/4"	JO	IK																
				8/31/11	REVISED OCTAGON ON ROOF TO CORRECT ORIENTATION OF LOGO ON DEPARTURE SIDE OF CANOPY	TRR	IK	7/23/12	REVISED APPROACH COLUMN FOR SERVICABILITY	TRR	IK	6/20/16	CHANGED PERMLIGHT LEDS TO GE	TRR	IK	10/2/17	UPDATED E-CSS SERIES LIGHT FIXTURES TO THE E-CSS44 SERIES LIGHT FIXTURES	JO	IK																
12/15/10	ADDED HEADACHE BAR ANCHOR DETAILS	TRR	IK	4/1/11	CHANGED DESIGNATION FROM CAN-ATM TO CAN-ATM-SIG-OCT. CHANGED CANOPY MOUNTING BOLTS FROM 3/8" DIA. TO 1/2" DIA.	TRR	IK	2/22/12	REVISED FOUNDATION	TRR	IK	12/10/14	ADDED HID FIXTURES TO BACK OF CANOPY	TRR	IK	6/29/17	REVISED FOUNDATION DETAILS & UPDATED LEDS & DOWNLIGHTS	JO	IK																
CHASE		These documents represent prototypical design drawings created specifically for use by J.P. Morgan Chase. Use of this unpublished work for any purpose other than the intended application is strongly discouraged. Disclosure or reproduction of any of the information contained within these documents without the written consent of the owner is strictly prohibited.				SHT.		BY:		Project No.		11/16/10		ADDED NOTE TO PAINT LIGHT FIXTURE TRIM TO MATCH CANOPY		TRR		IK		GRAPHICS DEPICTED ARE FOR ILLUSTRATIVE PURPOSES ONLY! USE ONLY APPROVED ARTWORK FOR PRODUCTION.				DESIGNATION:		CAN-ATM-SIG-OCT		9/11/19		CHANGED ROOF OCTAGON FACES TO CURVED STYLE. CHANGED ROOF OCTAGON MOUNTING "TUBES" TO .188" THICK FROM .125". CHANGED PLACEMENT OF J-BOLTS IN APPROACH COLUMN FOR EASIER SERVICE ACCESS. EXTENDED FOUNDATION TO INCLUDE ELECT. PENETRAL.		TRR		IK	
						12		TRR		08-1218		7/30/10		ADDED CLEAR COAT NOTE		TRR		IK																	
						OF		DATE:		Drawing No.		6/1/09		ADDED CAP PLATE TO OCTAGON MOUNTING STUB CALLED SECURITY CAMERA TO BE BY OTHERS		TRR		IK																	
						12		1/27/09		B244040		5/15/09		CHANGED CANOPY TO PSCC DESIGN		TRR		IK																	
								REV. DATE								BY:		APPR:																	

File: IconIdentSolut3389a.mcd

Site: Chase Bank
Location No. 64063
276 South West Blue Parkway
Lees Summit, Missouri 64063

Project: 9'-6 1/4" tall x 12'-10" wide x 5'-11 3/4" deep ATM canopy mounted to 6' above grade spread footing
Drawing No. B244040 sheets 1 thru 12 of 12.

Design loads are based on the 2015 International Building Code (ASCE 7-10) using Exposure C and 115 mph wind speed.

Design Wind Speed: (mph.) $V := 115.0$ Based on Risk Category II

Velocity Pressure Coefficient at a Height of Less Than 15', Exposure C: $K_z := 0.85$ Based on Table 29.3-1

Topographic Factor: $K_{zt} := 1.00$ Based on Table 26.8-1

Wind Directionality Factor: $K_d := 0.85$ Based on Table 26.6-1

Velocity Pressure: (PSF) $q_z := 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2$ $q_z = 24.461$ Based on 29.3-1

Force Coefficient: $C_f := 1.80$ Based on Figure 29.4-1

Gust Effect Factor: $G := 0.85$ Based on 26.9.4 for Other Structures

Load Combination Factor: $LCF := 0.60$ Based on 2.4.1, Case 7

Design Pressure: (PSF) $F := q_z \cdot C_f \cdot G \cdot LCF$ $F = 22.455$ Use: $WL := 22.5$

Design Snow Load: (PSF) $SL := 40.0$ Based on Ground Snow Loads.

Reference: Manual of Steel Construction, AISC 13th Edition.

Tube: ASTM A-500 Gr. B $F_y = 46.0$ ksi.; $F_b = 30.36$ ksi.; $F_v = 18.40$ ksi.

Plate: ASTM A-36 $F_y = 36.0$ ksi.; $F_b = 27.00$ ksi.; $F_v = 14.40$ ksi.

Mounting Bolts: ASTM A-325 $F_u = 133.0$ ksi.; $F_t = 44.00$ ksi.; $F_v = 21.00$ ksi.

Anchor Bolts: ASTM F-1554 Gr. 36 $F_u = 58.0$ ksi.; $F_t = 19.14$ ksi.; $F_v = 14.40$ ksi.

Reference: 2010 Aluminum Design Manual, The Aluminum Association

Tube: 6061-T6 Temper and Alloy $F_y = 35.0$ ksi.; $F_b = 30.72$ ksi.; $F_v = 12.54$ ksi.

Plate: 5052-H34 Temper and Alloy $F_y = 26.0$ ksi.; $F_b = 19.50$ ksi.; $F_v = 10.40$ ksi.

Reference: American Concrete Institute, Code 318.14

Rebar: ASTM A-615 Grade 60 $F_y = 60.0$ ksi.

Concrete: 3,000 psi. compressive strength at 28 days.

Design Loads at EL. 9.02': (Canopy mounting connection.)

Wind Load:

$$\text{Shear: (lbs.)} \quad \text{ShrWL} := \left[\left(\frac{8.25}{12} \right) \cdot 12.83 \cdot WL \right] \quad \text{ShrWL} = 198.464$$

$$\text{Moment: (ft.lbs.)} \quad \text{MtWL} := \text{ShrWL} \cdot \left(\frac{0.69}{2} \right) \quad \text{MtWL} = 68.47$$

Jeff L. Griffin
12255 W. 187th St.
Mokena, IL 60448



Offset Dead Load :

$$\text{Shear : (lbs.)} \quad \text{ShrDL} := (4.15 \cdot 12.83 \cdot 4.5) \quad \text{ShrDL} = 239.6$$

$$\text{Moment : (ft.lbs.)} \quad \text{MtDL} := \text{ShrDL} \cdot \left[\left(\frac{4.15}{2} \right) + 0.92 \right] \quad \text{MtDL} = 717.603$$

Offset Snow Load :

$$\text{Shear : (lbs.)} \quad \text{ShrSL} := (4.15 \cdot 12.83 \cdot \text{SL}) \quad \text{ShrSL} = 2129.78$$

$$\text{Moment : (ft.lbs.)} \quad \text{MtSL} := \text{ShrSL} \cdot \left[\left(\frac{4.15}{2} \right) + 0.92 \right] \quad \text{MtSL} = 6378.691$$

Combined Shear :

$$\text{Summation : (ft.lbs.)} \quad \text{ShrEL9}_{02} := \text{ShrWL} + \text{ShrDL} + \text{ShrSL} \quad \text{ShrEL9}_{02} = 2567.844$$

Design of Canopy Support Tubes at EL. 9.02' : (Based on the smallest tube size member.)

$$\text{Section Modulus of Tube - X Axis : (in.}^3 \text{)} \quad 3" \times 2" \times 1/8" \text{ wall} - \quad \text{TubeSMXAxis} := 0.966$$

$$\text{Moment per Tube - X Axis : (ft.lbs.)} \quad \text{MtTube}_{\text{xaxis}} := \frac{\text{MtDL} + \text{MtSL}}{4} \quad \text{MtTube}_{\text{xaxis}} = 1774.073$$

$$\text{Bending Stress - X Axis : (psi.)} \quad f_{\text{bxaxis}} := \frac{\text{MtTube}_{\text{xaxis}} \cdot 12}{\text{TubeSMXAxis}} \quad f_{\text{bxaxis}} = 22038.18$$

$$\text{Section Modulus of Tube - Y Axis : (in.}^3 \text{)} \quad 3" \times 2" \times 1/8" \text{ wall} - \quad \text{TubeSMYAxis} := 0.783$$

$$\text{Moment per Tube - Y Axis : (ft.lbs.)} \quad \text{MtTube}_{\text{yaxis}} := \frac{\text{MtWL}}{4} \quad \text{MtTube}_{\text{yaxis}} = 17.118$$

$$\text{Bending Stress - Y Axis : (psi.)} \quad f_{\text{byaxis}} := \frac{\text{MtTube}_{\text{yaxis}} \cdot 12}{\text{TubeSMYAxis}} \quad f_{\text{byaxis}} = 262.338$$

$$\text{Area of Tube : (in.}^2 \text{)} \quad 3" \times 2" \times 1/8" \text{ wall} - \quad \text{TubeArea} := 1.201$$

$$\text{Shear per Tube : (lbs.)} \quad \text{ShrTube} := \frac{\text{ShrEL9}_{02}}{4} \quad \text{ShrTube} = 641.961$$

$$\text{Shear Stress : (psi.)} \quad f_v := \frac{\text{ShrTube}}{\text{TubeArea}} \quad f_v = 534.522$$

$$\text{Unity Check :} \quad \text{UCCnpy} := \frac{f_{\text{bxaxis}}}{30720} + \frac{f_{\text{byaxis}}}{30720} + \frac{f_v}{12540} \quad \text{UCCnpy} = 0.769 < 1.00 \quad \text{OK}$$

Canopy Support Tubes

Design of Canopy Mounting Bolts at EL. 9.33' :

$$\text{Mounting Bolt Diameter : (in.)} \quad \text{MntBltDia} := 0.50$$

$$\text{Stress Area : (in.}^2 \text{)} \quad \text{MntBltArea} := \frac{\pi \cdot \text{MntBltDia}^2}{4} \quad \text{MntBltArea} = 0.196$$

(Based on nominal diameter per AISC 4-3)

$$\text{Allowable Tension : (lbs.)} \quad \text{AllwTen} := 44000 \cdot \text{MntBltArea} \quad \text{AllwTen} = 8639$$

$$\text{Allowable Shear : (lbs.)} \quad \text{AllwShr} := 21000 \cdot \text{MntBltArea} \quad \text{AllwShr} = 4123$$

$$\text{Number of Mounting Bolts in Tension :} \quad \text{NoTen} := 4$$

Front to Back Distance Between Mounting Bolts : (in.) $LvrArm := 17.625$

Tension Load per Mounting Bolt : (lbs.) $TenMntBlt := \frac{(MtDL + MtSL) \cdot 12}{NoTen \cdot LvrArm}$ $TenMntBlt = 1207.88$

Number of Mounting Bolts in Shear : $NoShr := 8$

Shear Load per Mounting Bolt : (lbs.) $ShrMntBlt := \frac{ShrEL9_{02}}{NoShr}$ $ShrMntBlt = 320.98$

Unity Check : $UCMntBlt := \frac{TenMntBlt}{AllwTen} + \frac{ShrMntBlt}{AllwShr}$ $UCMntBlt = 0.218 < 1.00$ OK

Mounting Bolts

Use : 1/2" diameter ASTM A-325 bolts and equivalent nuts and washers.

Design of Aluminum Canopy Mounting Plate at EL. 9.33' :

Plate Thickness : (in.) $PltThk := 0.50$ Plate Width : (in.) $PltWdth := 7.0$

Side to Side Distance Between Mounting Bolts : (in.) $Bltsprd := 5.0$

Transfer Distance : (in.) $PLS := \frac{PltWdth - Bltsprd}{2}$ $PLS = 1$

Number of Mounting Bolts in Tension per Plate : $NoTenPlt := 2$

Minimum Thickness Required : (in.) $ReqdThk := \sqrt{\frac{TenMntBlt \cdot NoTenPlt \cdot PLS \cdot 6}{(PltWdth \cdot 19500)}}$ $ReqdThk = 0.326$

Unity Check : $UCCnpyPlt := \frac{ReqdThk}{PltThk}$ $UCCnpyPlt = 0.652 < 1.00$ OK

Canopy Mounting Plate

Design of Steel Column Top Plate at EL. 9.33' :

Plate Thickness : (in.) $PltThk := 0.50$ Plate Width : (in.) $PltWdth := 7.0$

Transfer Distance : (in.) $PLS := 1.375$ (Measured in AutoCAD to furthest distance.)

Minimum Thickness Required : (in.) $ReqdThk := \sqrt{\frac{TenMntBlt \cdot NoTenPlt \cdot PLS \cdot 6}{(PltWdth \cdot 27000)}}$ $ReqdThk = 0.325$

Unity Check : $UCColmnPlt := \frac{ReqdThk}{PltThk}$ $UCColmnPlt = 0.649 < 1.00$ OK

Column Top Plate

Design Loads at Top of Footing :

Wind Load :

Canopy : $Cnpy := \left[\left(\frac{8.25}{12} \right) \cdot 12.83 \cdot WL \right] \cdot \left[\left(\frac{0.69}{2} \right) + 8.83 \right]$ $Cnpy = 1820.908 \text{ ft.lbs.}$

Cladded Poles : $CldPoles := (2 \cdot 8.83 \cdot 2.90 \cdot WL) \cdot \left(\frac{8.83}{2} \right)$ $CldPoles = 5087.471 \text{ ft.lbs.}$
(Based on the widest column.)

Moment : (ft.lbs.) $MtWL := Cnpy + CldPoles$ $MtWL = 6908.378$

$$\text{Shear : (lbs.)} \quad \text{ShrWL} := \left[\left(\frac{8.25}{12} \right) \cdot 12.83 \cdot \text{WL} \right] + (2 \cdot 8.83 \cdot 2.90 \cdot \text{WL}) \quad \text{ShrWL} = 1350.779$$

Offset Dead Load : (Based on 1'-10" deep column.)

$$\text{Shear : (lbs.)} \quad \text{ShrDL} := (4.15 \cdot 12.83 \cdot 6.5) \quad \text{ShrDL} = 346.089$$

$$\text{Summation : (ft.lbs.)} \quad \text{MtDL} := \text{ShrDL} \cdot \left(\frac{4.15}{2} \right) \quad \text{MtDL} = 718.135$$

Offset Snow Load : (Based on 1'-10" deep column.)

$$\text{Shear : (lbs.)} \quad \text{ShrSL} := (4.15 \cdot 12.83 \cdot \text{SL}) \quad \text{ShrSL} = 2129.78$$

$$\text{Moment : (ft.lbs.)} \quad \text{MtSL} := \text{ShrSL} \cdot \left(\frac{4.15}{2} \right) \quad \text{MtSL} = 4419.294$$

Combined Moment :

$$\text{Summation : (ft.lbs.)} \quad \text{MtTOF} := \text{MtWL} + \text{MtDL} + \text{MtSL} \quad \text{MtTOF} = 12045.807$$

Combined Shear :

$$\text{Summation : (ft.lbs.)} \quad \text{ShrTOF} := \text{ShrWL} + \text{ShrDL} + \text{ShrSL} \quad \text{ShrTOF} = 3826.648$$

Design of Pole Structures at Top of Footing :

$$\text{Section Modulus of Tube : (in.}^3 \text{)} \quad \text{HSS 3" x 3" x 3/16" wall} - \quad \text{TubeSM} := 1.64$$

$$\text{Moment per Column : (ft.lbs.)} \quad \text{MtColumn} := \frac{\text{MtTOF}}{2} \quad \text{MtColumn} = 6022.904$$

$$\text{Moment per Tube : (ft.lbs.)} \quad \text{MtTube} := \frac{\text{MtColumn}}{2} \quad \text{MtTube} = 3011.452$$

$$\text{Bending Stress : (psi.)} \quad f_b := \frac{\text{MtTube} \cdot 12}{\text{TubeSM}} \quad f_b = 22035.013$$

$$\text{Area of Tube : (in.}^2 \text{)} \quad \text{HSS 3" x 3" x 3/16" wall} - \quad \text{TubeArea} := 1.89$$

$$\text{Shear per Column : (lbs.)} \quad \text{ShrColumn} := \frac{\text{ShrTOF}}{2} \quad \text{ShrColumn} = 1913.324$$

$$\text{Shear per Tube : (lbs.)} \quad \text{ShrTube} := \frac{\text{ShrColumn}}{2} \quad \text{ShrTube} = 956.662$$

$$\text{Shear Stress : (psi.)} \quad f_v := \frac{\text{ShrTube}}{\text{TubeArea}} \quad f_v = 506.17$$

$$\text{Unity Check - Poles :} \quad \text{UCPoles} := \frac{f_b}{30360} + \frac{f_v}{18400} \quad \text{UCPoles} = 0.753 < 1.00 \quad \text{OK}$$

Design of Anchor Bolts at Top of Footing :

$$\text{Anchor Bolt Diameter : (in.)} \quad \text{AncBltDia} := 0.625$$

$$\text{Stress Area : (in.}^2 \text{)} \quad \text{AncBltArea} := \frac{\pi \cdot \text{AncBltDia}^2}{4} \quad \text{AncBltArea} = 0.307$$

(Based on nominal diameter per AISC 4-3)

Allowable Tension : (lbs.) $AllwTen := 19140 \cdot AncBltArea$ $AllwTen = 5872$

Allowable Shear : (lbs.) $AllwShr := 14400 \cdot AncBltArea$ $AllwShr = 4418$

Number of Anchor Bolts in Tension per Plate : $NoTen := 2$

Front to Back Distance Between Anchor Bolts : (in.) $LvrArm := 19.0$

(Based on approach support - shortest lever arm.)

Tension Load per Anchor Bolt : (lbs.) $TenAncBlt := \frac{MtColumn \cdot 12}{NoTen \cdot LvrArm}$ $TenAncBlt = 1901.97$

Number of Anchor Bolts in Shear : $NoShr := 4$

Shear Load per Anchor Bolt : (lbs.) $ShrAncBlt := \frac{ShrColumn}{NoShr}$ $ShrAncBlt = 478.33$

Unity Check : $UCAncBlts := \frac{TenAncBlt}{AllwTen} + \frac{ShrAncBlt}{AllwShr}$ $UCAncBlts = 0.432 < 1.00$ OK

Anchor Bolts

Allowable Bond Stress : (lbs./in.²) $U := \left(\frac{1}{2} \right) \cdot \left(\frac{4.8 \cdot \sqrt{3000}}{AncBltDia} \right)$ $U = 210.325$

Development Length : (in.) $Ld := \frac{TenAncBlt}{U \cdot \pi \cdot AncBltDia}$ $Ld = 4.606$

Embedment Length : (in.) $AncBltEmb := 24 - 3$ $AncBltEmb = 21$

(24" length minus 3" of thread projection.)

Unity Check : $UCABEmb := \frac{Ld}{AncBltEmb}$ $UCABEmb = 0.219 < 1.00$ OK

Anchor Bolt Embedment

Use : Four (4) 5/8" Dia. x 24" long anchor bolts with 3" top thread and 1-1/2" bottom thread.

Design of Approach Column Base Plate :

Plate Thickness : (in.) $PltThk := 0.625$ Plate Width : (in.) $PltWdth := 12.0$

Transfer Distance : (in.) $PLS := \sqrt{3.0^2 + 1.0^2}$ $PLS = 3.162$

Minimum Thickness Required : (in.) $ReqdThk := \sqrt{\frac{TenAncBlt \cdot NoTen \cdot PLS \cdot 6}{(PltWdth \cdot 27000)}}$ $ReqdThk = 0.472$

Unity Check - Base Plate : $UCBasePlt := \frac{ReqdThk}{PltThk}$ $UCBasePlt = 0.755 < 1.00$ OK

(Approach column.)

Use : 7/8" thick x 12" x 22" base plate with four (4) 3/4" diameter holes on a 9" x 19" bolt pattern.

Design of Departure Column Base Plate :

Plate Thickness : (in.) $PltThk := 0.625$ Plate Width : (in.) $PltWdth := 12.0$

Transfer Distance : (in.) $PLS := \sqrt{3.0^2 + 2.125^2}$ $PLS = 3.676$

$$\text{Minimum Thickness Required : (in.)} \quad \text{ReqdThk} := \sqrt{\frac{\text{TenAncBlk} \cdot \text{NoTen} \cdot \text{PLS} \cdot 6}{(\text{PltWdh} \cdot 27000)}} \quad \text{ReqdThk} = 0.509$$

$$\text{Unity Check - Base Plate :} \quad \text{UCBasePlt} := \frac{\text{ReqdThk}}{\text{PltThk}} \quad \text{UCBasePlt} = 0.814 < 1.00 \quad \text{OK}$$

(Departure column.)

Use : 5/8" thick x 12" x 33" base plate with four (4) 3/4" diameter holes on a 9" x 30" bolt pattern.

Design of Spread Footing :

Loads :

$$\begin{aligned} \text{Moment : (ft.lbs.)} & \quad \text{Ma} := \text{MtTOF} & \quad \text{Ma} = 12045.807 \\ \text{Shear : (lbs.)} & \quad \text{Va} := \text{ShrTOF} & \quad \text{Va} = 3826.648 \end{aligned}$$

Allowables :

$$\begin{aligned} \text{Lateral passive pressure against foundation : (lbs./sq.ft. per foot)} & \quad \text{PP} := 100 \\ \text{Static soil pressure : (lbs./sq.ft.)} & \quad \text{SSP} := 1500 \\ \text{Dynamic soil pressure : (lbs./sq.ft.)} & \quad \text{DSP} := 2000 \end{aligned}$$

Foundation parameters :

$$\begin{aligned} \text{Depth of footing below grade : (ft.)} & \quad \text{DF} := 2.0 \\ \text{Height of footing : (ft.)} & \quad \text{HF} := 2.5 \\ \text{Width of footing : (ft.)} & \quad \text{WF} := 16.67 \\ \text{Length of footing : (ft.)} & \quad \text{LF} := 4.25 \\ \text{(Wind direction)} & \\ \text{Height of footing above grade : (ft.)} & \quad \text{Ht} := \text{HF} - \text{DF} & \quad \text{Ht} = 0.5 \end{aligned}$$

Weight of structure and foundation :

$$\begin{aligned} \text{Design weight of concrete : (lbs./cu.ft.)} & \quad \text{CWT} := 150 \\ \text{Kiosk weight : (lbs.)} & \quad \text{SWT} := 450 \\ \text{ATM weight : (lbs.)} & \quad \text{PWT} := 850 \\ \text{Footing weight : (lbs.)} & \quad \text{FTWT} := \text{HF} \cdot \text{WF} \cdot \text{LF} \cdot \text{CWT} & \quad \text{FTWT} = 26567.813 \\ \text{Net weight : (lbs.)} & \quad \text{NETWT} := \text{SWT} + \text{PWT} + \text{FTWT} & \quad \text{NETWT} = 27867.813 \end{aligned}$$

Check Factor of Safety :

$$\begin{aligned} \text{Overturning moment about heel point of foundation : (ft.lbs.)} & \quad \text{Mo} := \text{Va} \cdot \text{HF} + \text{Ma} & \quad \text{Mo} = 21612.428 \\ \text{Total passive pressure on footing : (lbs./sq.ft.)} & \quad \text{Tpp} := \text{PP} \cdot \text{DF}^2 \cdot \left(\frac{\text{WF}}{2} \right) & \quad \text{Tpp} = 3334 \\ \text{Resisting moment about the heel point : (ft.lbs.)} & \quad \text{Mr} := \text{NETWT} \cdot \left(\frac{\text{LF}}{2} \right) + \text{Tpp} \cdot \left(\frac{\text{DF}}{3} \right) & \quad \text{Mr} = 61441.768 \end{aligned}$$

$$\text{Factor of Safety :} \quad \text{FS} := \frac{\text{Mr}}{\text{Mo}} \quad \text{FS} = 2.843 > 1.5 \quad \text{OK}$$

Check soil bearing pressures :

Static soil pressure : (lbs./sq.ft.) $SBP := \frac{NETWT}{LF \cdot WF}$ $SBP = 393.349 < SSP = 1500$ OK

Dynamic soil pressure : (lbs./sq.ft.)

$$e := \frac{\left[Mo - T_{pp} \cdot \left(\frac{HF}{3} \right) \right]}{NETWT} \quad e = 0.676$$

$$\left(\frac{LF}{2} \right) = 2.125 > e = 0.676 > \left(\frac{LF}{6} \right) = 0.708$$

$$q_a := \frac{2 \cdot NETWT}{3 \cdot WF \cdot \left[\left(\frac{LF}{2} \right) - e \right]} \quad q_a = 769.057 < DSP = 2000 \quad OK$$

Check tensile stress of concrete at pole :

Compressive Strength of Concrete : (psi.) $f_c := 3000$

Overturing moment at pole : (ft.lbs./ft.) $M_p := \left(\frac{LF}{2} \right)^2 \cdot \left(\frac{q_a}{2} \right)$ $M_p = 1736.387$

Section modulus of footing - Per foot of width : (in.³) $S_w := 12 \cdot \frac{(HF \cdot 12)^2}{6}$ $S_w = 1800$

Tensile stress in concrete : (psi.) $f_t := \frac{(M_p \cdot 12)}{S_w}$ $f_t = 11.576$

Allowable stress in concrete : (psi.) $\phi F_t := 0.65 \cdot (5 \cdot \sqrt{f_c})$ $\phi F_t = 178.01 > f_t = 11.576$
REBAR NOT REQUIRED FOR STRESS

Design of temperature and shrinkage steel :

Rebar size : Number := 5

Rebar Area : (in.²) $Area := \frac{\pi \cdot \left(\frac{Number}{8} \right)^2}{4}$ Area = 0.31

For length of footing : $Asl := 0.0016 \cdot HF \cdot WF \cdot 144$ $Asl = 9.602$

Number required : $\frac{Asl}{Area} = 31.297$ Use seventeen (17) #5 Rebar x 3'-9" LG. equally spaced top and bottom using 3" typical clear. (Thirty-four (34) total required.)

For width of footing : $Asw := 0.0016 \cdot HF \cdot LF \cdot 144$ $Asw = 2.448$

Number required : $\frac{Asw}{Area} = 7.979$ Use four (4) #5 Rebar x 13'-0" LG. equally spaced top and bottom using 3" typical clear. (Eight (8) total required.)

Quantity of concrete : (yds.³) $C_y := \frac{(LF \cdot WF \cdot HF)}{27}$ $C_y = 6.56$