

LORAC DESIGN GROUP, LLC
Structural Engineers

June 28, 2017

Mr. Doug Parks
Lee's Summit, Mo. 64064

H A N D D E L I V E R E D

**Re: 1328 NE Brandywine Road, Lee's Summit, Missouri – Structural Review, Porch Structural Slab
Lee's Summit, Permit # PRRES20162554**

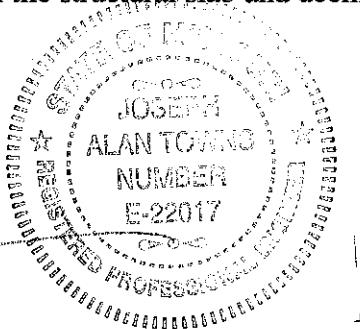
Doug,

This letter is to certify that I have personally inspected and verified through calculation the strength and placement of the front porch structural slab located at the above address.

After careful review, we are comfortable with the structural slab and deem it safe for use.

Photos are available upon request.

For the Firm,
LORAC Design Group, LLC



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Design Calculations

1328 NE Brandywine Road

Lee's Summit, Missouri

Concrete Structural Slab Check at Porch

*	Trib Width (Selected)	1 ft	Per Drawings
*	Max Span	8 ft	Per Drawings
	Slab Thickness	8 inches	OK
	Weight of Concrete	150 pcf	
*	Loading Dead	0.100 kips/ft ²	Per Drawings
	Loading Live	0.100 kips/ft ²	Per Drawings
	Point Load	0.500 kips/ft	Per Drawings
	Trib Area	0.50 feet	By Calculation
	f _c =	4000.00 psi	By Design
	f _y =	60000.00 psi	By Design
	Beam Ldg (Dead)	0.05 kips/lin. ft	
	Beam Ldg (Live)	0.05 kips/lin. ft	
	Moment (Dead)	0.40 kip-feet	By Calculation
	Moment (Live)	0.40 kip-feet	By Calculation
	Moment (Point)	1.00 kip-feet	By Calculation
	Total Moment	1.80 kip-feet	By Calculation
	Factored Moment (Dead)	0.56 kip-feet	By Calculation
	Factored Moment (Live)	0.68 kip-feet	By Calculation
	Factored Moment (Point)	1.40 kip-feet	By Calculation
	Total Factored Mom.	2.64 kip-feet	By Calculation
	Reactions (Dead)	0.20 kips	By Calculation
	Reactions (Live)	0.20 kips	By Calculation
	Total Reaction	0.40 kips/ft	
	b =	12.00 inch	By Design
	d =	6.00 inch	By Calculation
	Omega =	0.0204	
	Omega' =	0.0201	
	rho =	0.0013	

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A_s, R_{qd}	$A_s =$	0.10 in ²
$A_s, min =$	0.23	ACI 10.5.1
Select = Reinforcement #4's @ 12"	0.200 in ² /ft	
	OK	

Beam Check

$T = A_{sfy} =$ 12.00 kips

$a = A_{sfy}/.85f'_{cb} =$ 0.29 inches

Moment Strength = 63.21 in-kips
or 5.27 kip-feet
OK

Check Shear Capacity at Supp. 4.55 kips/ft (Concrete ONLY)
OK S.F. = 11.38

Temp Steel Requirement 0.14 in²/ft²/ft
#3's @12 oc

Deflection Calculations

Sustained Load

$b =$	12.0 inches
$d =$	8.0 inches
$d' =$	1.5 inches
$h =$	8.0 inches
$A_s =$	0.20 in ²
$A'_s =$ Top Steel	0.000 in ²
$f'c =$	4000.0 psi
$f_y =$	60000.0 psi
Weight of Concrete =	150.0 lb/ft ³
span =	8.0 feet
Slab Thickness =	8.0 inches
$M_d =$	0.4 k-ft
$M_I =$	0.7 k-ft
$M_{total} =$	1.1 k-ft
$M_{sus} =$	0.7 k-ft

Minimum Thickness

$h_{min} = l / 18.5 =$ 5.19 inches
OK

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Modulus of Rupture	$fr = (7.5 * f'_c)^{0.5} =$	474 psi	Eq. (9-10)
	$E_c = 33 * (w_c^3 * f'_c)^{0.5} =$	3,834,254 psi	Eq. (8.5.1)
	$n_s = E_s / E_c =$	7.6	

Gross and Cracked Section Moments of Inertia			
	$I_{gross} = bh^3/12 =$	512 in ⁴	
	$B = b/n A_s =$	7.933 in/in	
	$r = ((n-1)*A's)/(n*A_s) =$	0.000	
	$a = (((2dB(1+rd'/d)+(1+r)^2)^{0.5}) - (1+r))/B =$	1.30 inches	
	$I_{cr} = b*a^3/3 + n*A_s*(d-a)^2 + (n-1)*A's*(a-d')^2 =$	77 in ⁴	

Effective Moments of Inertia			
	$M_{cr} = fr * I_g / y_t =$	5.1 ft-k	Eq. (9-8)
	$M_{cr}/M_d =$	12.65	
	$(M_{cr}/M_{sus})^3 =$	319.643	
	$(I_e)_{sus} = (M_{cr}/M_a)^3 * I_g + [1 - (M_{cr}/M_a)^3] * I_{cr} < I_g$	139220 in ⁴	Eq. (9-7)
	$(M_c/M_d + l)^3 =$	102.823	
	$(I_c)d + l =$	44836 in ⁴	

Initial or short-time deflections, using Eq. (4)			
	$(ai)d = (K * (5/48) * M_d l^2) / (E_c * (I_e)d) =$	0.002 inch	9.5.2.2
	$(ai)sus = (K * (5/48) * M_{sus}^2) / (E_c * (I_e)sus) =$	0.000 inch	9.5.2.3
	$(ai)d + l = (K * (5/48) * M_d + l^2) / (E_c * (I_e)d + l) =$	0.000 inch	
	$(ai)l = (ai)d + l - (ai)d =$	0.002 inch	

Long-term deflections at ages 3 mos and 5 yrs (ult. Values)

$\Lambda = (\zeta) / (1 + 50 \rho') =$	1.770	
$a_{cp+sh} = \Lambda * (ai)sus =$	0.000 inch	
$a_{cp+sh} + (ai)l =$	0.002 inch	Ultimate Value

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